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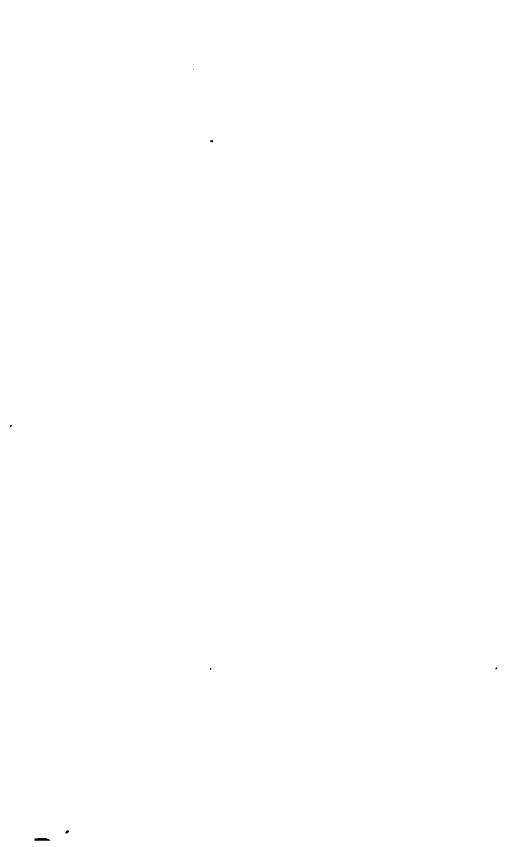
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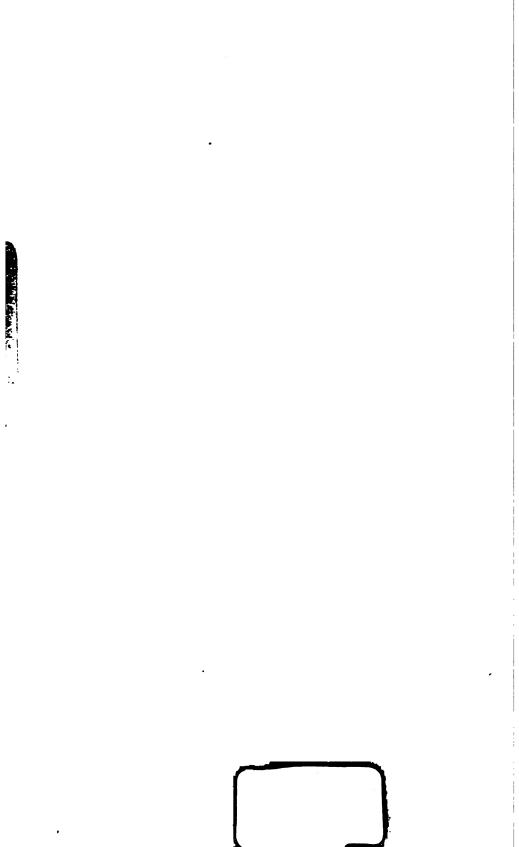
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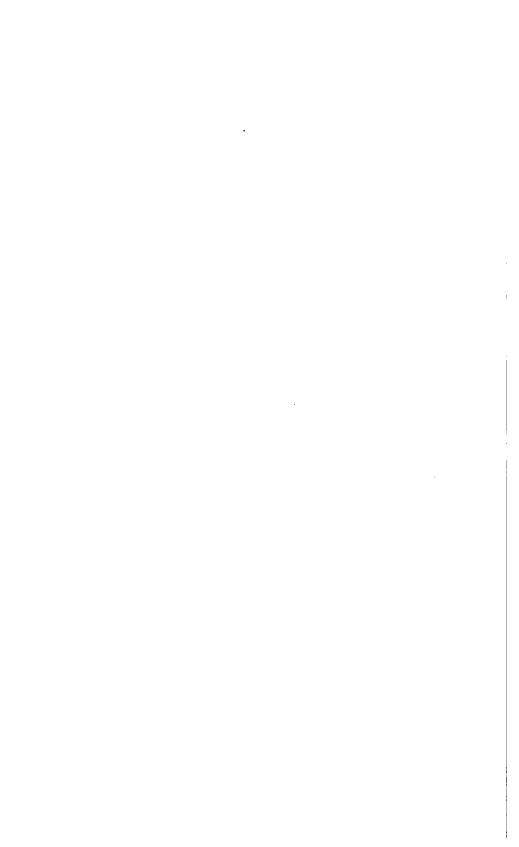
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SMITHSONIAN

MISCELLANEOUS COLLECTIONS.

VOL. I.





"EVERY MAN IS A VALUABLE NEMBER OF SOCIETY WHO BY HIS OBSERVATIONS, RESEARCHES, AND EXPERIMENTS PROGUES KNOWLEDGE FOR MER."—SMITHSON.

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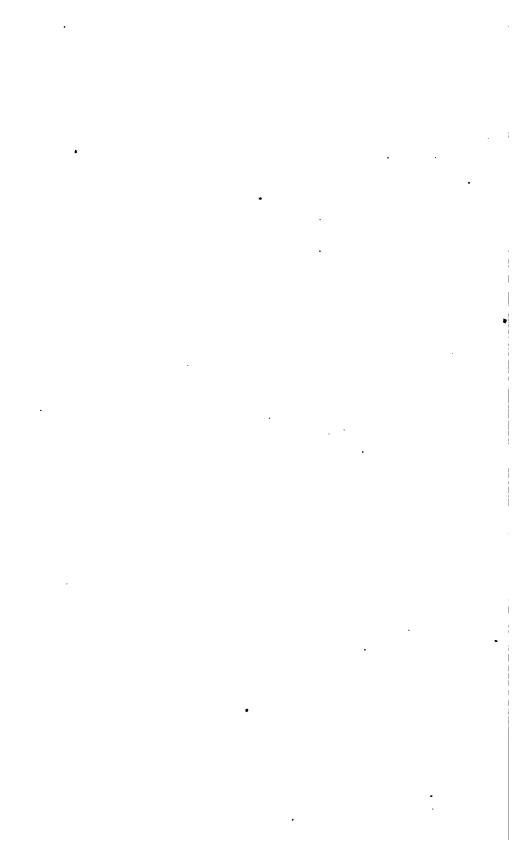
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> JOSEPH HENRY, Secretary S. I.



SMITHSONIAN MISCELLANEOUS COLLECTIONS.

DIRECTIONS

FOR

METEOROLOGICAL OBSERVATIONS,

AND THE

REGISTRY OF

PERIODICAL PHENOMENA.



WASHINGTON: SMITHSONIAN INSTITUTION. 1860.

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DIRECTIONS

POR

METEOROLOGICAL OBSERVATIONS,

ADOPTED BY THE SMITHSONIAN INSTITUTION

THE following directions were originally drawn up for the use of the observers in correspondence with the Smithsonian Institution, by Professor Guyor, of the College of New Jersey, Princeton, and are now reprinted, with a series of additions, for more general distribution. The additions are indicated by brackets, [].

SECRETARY S. I.

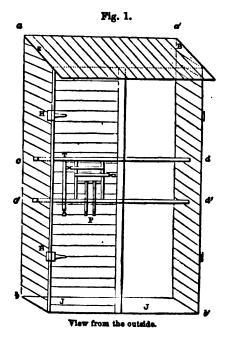
PLACING AND MANAGEMENT OF THE INSTRUMENTS.

THERMOMETER.

Placing.—Place the thermometer in the open air, and in an open space, out of the vicinity of high buildings, or of any obstacle that impedes the free circulation of the air. It should be so situated as to face the north, to be always in the shade, and be at least from nine to twelve inches from the walls of the building, and from every other neighboring object. The height from the ground may be from ten to fifteen feet, and, as far as possible, it should be the same at all the stations. The instrument should be protected against its own radiation to the sky, and against the light reflected by neighboring objects, such as buildings, the ground itself, and sheltered from the rain, snow, and hail. The following arrangement will fulfil these requirements (Fig. 1):—

Select a window situated in the first story, fronting the north, in a room not heated or inhabited; remove the lattice blinds, if there be any, and along the exterior jambs of the window place perpendicularly two pieces of board (a b—a' b'), projecting to

a distance of from twenty to twenty-four inches from the panes. At half this distance, ten or twelve inches from the panes, and at the height of the eye of the observer, when in the chamber, pass from one piece of board to the other two small wooden transverse bars (c d, c' d'), each an inch broad, for the purpose of supporting the instruments. Upon the outer edge of the boards fasten, in the usual way (H H), the latticed blinds which were removed from the jambs, or two others provided for the purpose. That blind behind which the instruments are to be placed, is to serve as a screen, and must be fastened, almost entirely closed, so as to make a little more opening; the other will remain entirely open, to allow a free access of air and light, and is not to be closed except in great storms. The whole must be covered with a small inclined roof of boards (B E), placed at least fifteen or twenty inches above the instrument. part (J J), or the basis, may remain open.



[The foregoing is a convenient arrangement by which the observations can be taken without exposing the observer to the

weather. To prevent radiation from the room, the windows during the intervals of observations may be closed with an inside wooden shutter. The outside of the lattice-work should be painted white, to reflect off the light and heat which may fall upon it.]

The thermometer must be placed exactly perpendicular, the middle of the scale being at the height of the eye against the

two small wooden bars, so that the top of the scale being fixed by a screw to the upper bar, the bulb may pass at least two or three inches beyond the lower bar. The instrument is attached to the last by a little metallic clasp. (Fig. 2.) It will thus be placed ten or twelve inches from the panes, from the screen, and the other parts of the window.

[In a later arrangement, a single transverse bar is used. This being placed at the necessary height, the thermometers are attached to it by small metal brackets, which support them at a distance from the bar of about two inches. The metal brackets are permanently screwed to the bar, and the thermometers are fastened to them by small finger-screws, by

which they can be detached at pleasure. The order of placing them is shown in the cut.

Reading .- To read the thermometer, the eye must be placed exactly at the same height as the column of mercury. Unless this precaution is taken, there is a liability to errors, the greater in proportion to the thickness of the glass of the stem and the shortness of the degrees. The reading should be made at all times, and especially in the winter, through the panes, and without opening the window; otherwise the temperature of the chamber will inevitably influence the thermometer in the open air. The degrees must be read, and the fractions carefully estimated in tenths of degrees. After having rapidly taken the observation, another should be made to verify it. If there are several other instruments to observe, and the thermometer is to be read first, the first reading may be made some minutes before the hour; the second, after the reading of the psychrometer; and if there is a difference, the mean number is to be entered in the journal. When, notwithstanding the shelter, the bulb of the thermometer is moistened by rain or fog, or covered with ice or snow, it is





necessary to wipe it rapidly, and not to record the degree until the instrument has been allowed to acquire the true temperature of the air.

Verification.—Verify the zero point, at the beginning and end of winter. For this purpose, fill a vessel with snow, immerse the bulb of the thermometer in the middle of it, so as to be surrounded on every side by a layer of several inches of snow, slightly pressed around the instrument. The stem must be placed exactly perpendicular, and covered with snow as far up as the freezing-point on the scale. Let it stand so for half an hour or more, and then read it, taking great care to place the eye at the same height as the summit of the mercurial column. If the top of the column does not coincide with the freezingpoint of the scale, the exact amount of the difference must be ascertained, and the correction immediately applied. same time enter in the journal, under its appropriate head, the day on which the experiment is made, its quantity, and the hour at which the application of it was commenced. It is necessary to add, that since the zero point of the thermometer is not that of the temperature of snow as it is frequently found . when exposed to the atmosphere, but that of melting snow, the experiment must be made in a place above the temperature of freezing. Instead of snow, pounded ice may be employed.]

Green's thermometers have an arrangement by which the tube can be slipped down the small quantity necessary to correct for this change. The end of the tube is fitted into a small plate of German silver, and this fastened by a screw to the scale. If, on testing the thermometer, the mercury be found to stand above 32°, free the screw one or two turns without taking it out, and push down the plate the necessary amount to bring the mercury to coincide. The thermometer must be handled with great care in making this adjustment, and it may be well, for additional security against accident, to loosen all the screws which fasten the bands around the tube; it will then slide in them more freely. After completing the adjustment, they may again be set moderately tight. The object of this adjustment being only to avoid the trouble of making a correction, it is not advisable to attempt it, if the observer thinks that he risks, in so doing, the safety of his instrument. As the tubes of these standard thermometers are kept for a considerable time before fixing the zero point, in

most cases the moving will not be required. After the first year the zero point changes little, and practically, when exposed only to atmospheric influences, may be considered permanent.]

SELF-REGISTERING THERMOMETERS.

Placing.—These two thermometers, indicating the maxima and minima, are to be placed beside the common thermometer, in a horizontal position, with the bulbs opposite and free, on two small perpendicular supports uniting the two bars, as shown in Fig. 1.

Reading.—For the reading, place the eye in such a position that the visual ray may be perpendicular to the extremity of the index; enter the indications with the fractions of degrees, if there are any, and, after having verified them again, bring back, by means of the magnet, the indexes of the two thermometers to the summit of their respective columns.

Verification.—Compare the indications of the two thermometers frequently, and especially the spirit thermometer, with those of the common thermometer; verify the zeros at least twice a year, and, if there is a difference, adjust the zero anew, if the instrument permits, to eliminate the correction, as has been stated above for the simple thermometer, or take this correction into account in the register.

[The maximum thermometer is subject to derangement by the mercury getting to the side of the steel index and wedging it fast. When such is the case, put the bulb in ice, if it is necessary to bring the mercurial column so low, or cool it sufficiently to get all the mercury down that will pass the index; then move the magnet along the tube with a slight knocking or jarring motion, and try to get the index into the chamber at the top of the stem. If you get the index free of the wedge, but with mercury above it, heat the bulb until all the disjointed mercury and index are driven into the chamber, then keep the index up by the magnet, and the mercury will go back as the bulb cools. The great point of attention is to get and keep the index free of the wedge. The mercury being above is of little consequence, as it can readily be heated up into the chamber; in doing this, most watchfulness is required in not suffering the index to wedge

by the driving mercury. If the index is so wedged that it cannot be moved by these methods, then grasp the thermometer firmly in the hand, and swing it quickly, as if you wished to throw the mercury into the chamber at the top; the index, with more or less mercury, will be found in the chamber: if not, repeat the swinging until it is there. Then heat up the bulb until the mercury joins that in the chamber, keep the index up by the magnet, and let the mercury, by cooling, go back in unbroken line.

In using the magnet to move the index up into contact with the mercury, care must be taken not to urge it too strongly, or it may enter the mercury.

In using the spirit-thermometer, the same care is necessary as with the mercurial, since the index may sometimes be forced out of the spirit, entangling the vapor and the alcohol. this is the case, the thermometer must be taken down and held vertically; a few taps or jars will bring the spirit together. The spirit-thermometer requires attention, also, in the following particular. The vapor above the column is apt, in time, to condense at the end of the tube, commonly at the very end. When the spirit-thermometer stands lower than the mercurial one, this may be suspected and looked for. When so found, the thermometer should be taken down and shaken until the alcohol runs down; it should then be kept in an upright position for some time, to drain. If it is found difficult to shake down the condensed vapor, the end of the tube may be carefully and slowly heated with a small lamp, or a small rod of heated iron held at a short distance, keeping the bulb and lower part as cold as possible; the alcohol by vaporization will then condense at the surface of the spirit in connection with the bulb. Occasionally, in cold climates, spiritthermometers are deranged by the air absorbed by the alcohol becoming free in the bulb at a low temperature. When this occurs, bring the thermometer to as low a temperature as may be convenient; then hold it in such a position that the air-bubble comes to the juncture of the bulb and tube, warm the bulb till all the air is in the tube; then, by shaking the thermometer, or by gentle knocking, the spirit will flow down, and the air speck come to the top.

This does not occur in spirit-thermometers that are closed with a vacuum, and the spirit at the time well freed from air.

In this case, however, the above-named difficulty from vaporization takes place more readily than when closed with air. These derangements of the spirit-thermometer are readily rectified, and only require occasional examination to detect them.

Both the maximum and minimum thermometers may be adjusted without the magnet, by raising one end sufficiently to allow the index to slide down by its own weight.*

The ordinary maximum thermometer (Rutherford's) not working well, even in the hands of many careful observers, has occasioned several attempts to make one without an index.

Mr. Green has lately contrived one. The object is effected by inclosing in the bulb a glass valve, which is floated by the mercury to the juncture of the bulb and tube. On an increase of heat the mercury from the bulb passes this valve, but on contraction from a decreasing temperature, the portion in the column is obstructed, and remains stationary, indicating the maximum point attained.

To set the instrument for another observation, it is held bulb downwards, and with a gentle jerk the mercury falls and joins that in the bulb; it is then placed horizontal in the usual way.

A movable valve-piece is introduced rather than a fixed obstruction or stricture, as in a new and ingenious maximum thermometer by Messrs. Negretti and Zambra, of London, in expectation that the observer will find greater ease and satisfaction in readjusting the instrument for observation. †

Professor Phillips, of England, has also devised one. His plan is to cut off a portion of the column of mercury by an intervening small bubble of air. An increase of heat drives this detached portion forward, and leaves it there on a decrease of heat.

This form is also made by Mr. Green, and possesses some advantages peculiar to it; but, until experience decide otherwise, we doubt if it can be put in order after accidental derangement, by every observer. The former plans are not open to this objection.

^{*} The index of the spirit-thermometer is frequently made of a small cylinder of enamel, which cannot be moved by the magnet.

[†] These thermometers being new in plan, particular instructions in regard to suspending and setting them will be given with each instrument by the maker, Mr. James Green, New York.

PSYCHROMETER.

Placing.—The psychrometer, or wet-bulb thermometer, must be situated under the same conditions as the thermometer. It should be placed on the same wooden bars, several inches off, and outside of the thermometer. (See Fig. 1.)

The bulbs should also be entirely free, and at a distance from the bars.

In case of violent winds, the instrument may be sheltered by the movable blind, which may also serve as a fan to promote evaporation when the air is too still.

The cloth which surrounds the bulb ought to be of medium fineness, not too coarse; it should form a covering of equal thickness on all sides, and should not be drawn too closely upon the glass. Linen is preferable to cotton, which retains the dust. The covering should be changed every two or three months, and the bulb cleaned. [The linen may be washed, without removal, by means of a jet of clean water from a small syringe.]

Observation.—For the observation, take first a small vessel full of water, which should be left on the window, that the water may be at the temperature of the air; bring it near to the bulb, and immerse the bulb several times into the water. All the space between the bulb and the bottom of the scale must be wet, and care must be taken that the wrapping is thoroughly moistened, without, however, a too large drop remaining suspended at the bulb. The water used must be pure; the best is rain-water, filtered, because it does not hold any salt in solution, which might incrust the cloth after evaporation.

In some arrangements of the psychrometer, the wet-bulb is kept constantly wet by conducting water to it from a small vessel, by capillary attraction, along a string of cotton wick. A series of comparative observations was made at this Institution, last summer, on these two modes of wetting the bulb, which gave the same result within a fraction of a degree from the mean of the records of a month. The observers connected with the Coast Survey prefer the method of dipping the covered bulb.

After wetting the bulb, shut the window, and leave the psychrometer for a time.

While the wet bulb is slowly acquiring the temperature of

evaporation, the observer is occupied with other observations. though watching the psychrometer to make sure of the moment when it has become stationary. In summer, from four to ten minutes are needed for this, according to the size of the bulb; but in winter, when the water freezes on the bulb, it must be moistened from fifteen to thirty minutes before the observation, which should not be made until the ice around the bulb is quite formed and dry. The best way is to keep round the bulb a layer of ice, constant and uniform, which should be neither too thick nor too thin; then the observation may take place imme-When the temperature is in the neighborhood of the freezing-point, the observation of the psychrometer requires very peculiar care; the reason of which we have elsewhere explained. During a fog, the wet-bulb thermometer may sometimes be higher than the dry-bulb; then the air is over-saturated, and contains, besides the vapor at its maximum of tension, water suspended in a disseminated liquid state. This is, however, not a frequent occurrence.

If the air is very still, it is well to increase the evaporation by setting the air in motion by a fan. If the wind is too strong, the instrument should be protected by the movable blind. The reading must be made rapidly, and, as much as possible, at a distance, and without opening the window; for the proximity of the observer, either by the heat radiating from his body, or by his breath, as well as the temperature and the hygrometrical state of the air issuing from the chamber, which is always different from that of the external air, especially in winter, would infallibly act upon the instruments, and would falsify the observation.

Verification.—The two thermometers must be carefully compared from time to time, and if a difference is found, the instruments must be adjusted, or it must be taken into the account, and the observations corrected when entered in the journal.

BAROMETER.

Placing.—The barometer should be placed in a room, of a temperature as uniform as possible; not heated, nor too much exposed to the sun. The instrument must be suspended at the height of the eye, near a window, in such a manner as to be lighted perfectly, without exposure either to the direct rays of

the sun, or to the currents of the air, which always take place at the joinings of the windows. When the barometer has to be fixed to the wall, as is the case with all the common stationary and wheel barometers, care must be taken to secure the tube in a position perfectly vertical, regulating it by the plumb-line, first in front, then at the sides, at least in two vertical planes cutting

Fig. 3.



each other at right angles. When the instrument is so constructed as to take its equilibrium itself, as the Fortin barometers and those of J. Green, recently made under the direction of the Smithsonian Institution, it is enough to hang it on a strong hook. These conditions being fulfilled, the rest of the arrangement may be varied according to the nature of the localities. For the Fortin and Green barometers, the following arrangement is convenient, and may be almost everywhere adopted. (See Fig. 3.)*

A small oblong box $(a \ b)$, some inches longer than the barometer, and a little broader than its cistern, is firmly set against the wall (w w'), near the window, in such a manner as to open in a direction parallel to the panes; at the summit (a) it has a strong hook (h h'), which extends beyond the box about two or three inches, and on which the barometer is suspended. The instrument remains generally in the box, which is closed by a movable cover, and which protects it from external injuries. from dust, and from the direct radiation of warm bodies, or the currents of air from the window, and diminishes the effect of the too sudden variations of temperature. When it is to be observed, the barometer is taken by the upper end of the tube, and the suspending ring is made to slide towards the end of the

^{*} The standard barometer at the Smithsonian Institution is stationary and inclosed within a narrow case, the front and two sides of which open out by means of hinges so as fully to expose the instrument at the time of the observation.

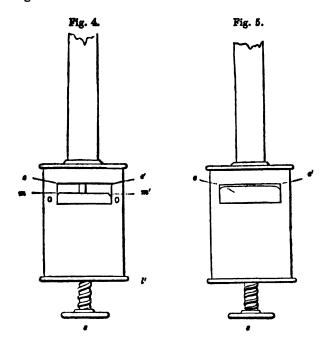
hook. The instrument is then in the full light of the window, in front of which the observer places himself; the summit of the mercurial column, as well as the surface of the mercury in the cistern, are completely lighted, and the reading becomes easy and certain. Moreover, the slight oscillating movement impressed on the instrument, by changing its place, breaks the adherence of the mercury to the glass, and thus prepares a good observation. After the reading, the barometer is again slipped gently into the box, and this is closed.

Observation.—The different operations of the barometer of constant level should be made in the following order:—

- a. Before all, incline the instrument gently, so as to render the mercurial column very movable; then, after having restored it to rest, strike several slight blows upon the casing, in such a manner as to impress on the mercury gentle vibrations. The adherence of the mercury to the glass will thus be destroyed, and the column will take its true equilibrium.
- b. Note the degree and the tenths of degrees of the thermometer attached to the instrument; for it will be seen that the heat of the observer's body soon makes it rise.
- c. Bring, by means of the adjusting screw (Fig. 4), the surface of the mercury to its constant level. In Green's first barometers, the metallic envelop of the cistern is pierced through $(o\ o')$, and allows the surface of the mercury contained in the glass cistern to be seen. The plane which passes through the upper edge $(e\ e')$ of this opening is the true level, or the zero of the scale, to which the surface of the mercury must be restored.

For this, take hold, with the left hand, of the lower edge of the cistern (l l'), taking great care not to disturb its vertical position; apply the right hand to the adjusting screw (s), and, turning it gently, bring by degrees the level surface, of the mercury to the upper edge (s e') of the opening of the cistern, until there remains between the two only an almost imperceptible line of light, as in the Fig. 5 (s e'). Then leave the instrument to itself, to re-establish its verticality, if it had been accidentally deranged, and placing the eye exactly at the height of the mercury, examine whether the contact is exact. For this operation, it is important to have a good light; the cistern ought to be placed higher than the lower edge of the window, so that the light may reach it directly. It is necessary also to take care

not to confound the slight line of light which marks the opposite edge of the cistern, with the light reflected by the surface of the mercury against the inner walls; the former is always sharp and well defined; the latter vague and indefinite. When, before adjusting the level, the mercury is higher than the upper edge, it is necessary to begin by lowering it beneath the level (see Fig. 4), so as to leave an interval of light, which is then gradually shut out, as has been described. When the observation is to be made in the night, place the lamp before, and not behind, the instrument, and somewhat higher than the eye; and if the wall itself is not light enough, place behind the cistern, or the top of the column, a viece of white paper, which reflects the light.



In the barometers with an ivory point, as the Fortin, Newman, and Green barometers, the extremity of this point is the zero of the scale, which must be brought into exact contact with the surface of the mercury. We commonly judge that this takes place when we see the actual rounded summit of the point co-

incide exactly with its image reflected below by the mercury. This method may be very good when the surface of the mercury is perfectly pure and brilliant; but this is very rare. It is generally dimmed by a slight layer of oxide, which makes the coincidence of the point with its image uncertain. It is safer to judge of the contact in a different manner. From the moment when the point does more than touch the surface, it forms around itself, by capillary action, a small depression, which, breaking the direction of the reflected rays, becomes immediately very easy to discover. It is enough, then, to raise the mercury so as slightly to immerse the point; then to lower it gradually until the little depression disappears. If care is taken to make a good light fall on that portion of the mercury which is under the point, and to use the aid of a magnifier, the adjustment of the point thus made becomes not only easy, but very certain, and the errors to which we are liable are almost insensible, for they do not exceed two or three hundredths of a millimetre, or a thousandth of an inch.

d. The level being thus adjusted to the zero of the scale, we proceed to observe the height of the summit of the column. Take hold of the instrument with the left hand, above the attached thermometer, without moving it from the vertical; strike several slight blows in the neighborhood of the top of the column; then, by means of the screw, lower the slide which carries the vernier, until the plane passing through the two lower opposite edges of it is exactly tangent to the summit of the meniscus—that is, the convexity which terminates the column. We know that this is the case when, placing the eye exactly at the height of the summit of the column, we still see the summit of the column, without there being any trace of light between the summit and the edge of the ring. To convince ourselves that the barometer has remained quite vertical during its operation, we leave it to itself, and when it is at rest, we look again to see whether the ring has remained tangential to the summit of the column. If it has not, the verticality has been disturbed; it must be adjusted anew. It is necessary, at the same time, to examine if the adjustment of the surface of the mercury in the cistern has remained the same. The attached thermometer will also be read anew, and if it indicates a temperature noticeably higher than at the commencement of the observation, a mean value between the two indications must be adopted. An exact observer can never dispense with these verifications.

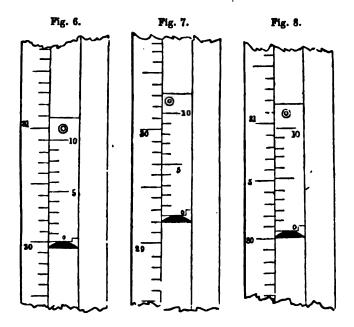
e. Nothing more, then, remains than to read the instrument. In the English barometers, the inches and tenths of inches are read directly on the scale, the hundredths and thousandths on the vernier. In the French barometers, with the metrical scale, the centimetres and millimetres are read on the scale, and the fractions of millimetres on the vernier. We begin by reading on the scale the number of inches and tenths of an inch, or of millimetres, there are, as far up as the line which corresponds to the lower edge of the vernier, and which marks the summit of the column. In the Green barometers, this line marks at the same time the zero of the vernier. If this line does not coincide with one of the divisions of the scale, we read the fraction of the following division on the vernier:—

The principle of the vernier is very simple. If we wish to obtain tenths, we divide into ten parts a space on the vernier comprising nine parts of the scale (see Fig. 6); each division of the vernier is thus found shorter by a tenth than each division of the scale. Now, if we start from the point where the zero of the vernier and its tenth division coincide exactly with the first and the ninth division of the scale, and if we cause the vernier to move gradually from the ninth to the tenth division of the scale, we shall see the first, the second, the third, and the other divisions of the vernier as far as the tenth, coincide successively with one of the divisions of the scale. Now, the divisions of the scale to which those of the vernier correspond, being equal parts. it follows that the space in question has been successively divided into ten parts, or tenths, by these successive coincidences. the scale bears millimetres, the vernier will give tenths of millimetres; if it has tenths of an inch, the vernier will give hundredths. By changing the proportions, it may be made to indicate by the vernier smaller fractions, as twentieths of millimetres. or five-hundredths of an inch. &c.

To read the vernier, we must look out for the line that coincides with one of the divisions of the scale; the number of this division of the vernier, proceeding from zero, indicates the number of tenths of millimetres, or of hundredths of an inch, which must be added to the whole number given by the scale. If none of the divisions of the scale coincides exactly, we estimate by

the eye, in decimals, the quantity by which the vernier must be lowered to obtain a coincidence, and this is added to the fraction already obtained. This will be hundredths of millimetres in the metrical barometer, and thousandths of inches in the English barometers.

The following figures will serve as an example; the instrument an English barometer.



In Fig. 6 the regulating line, which is the lower edge of the vernier ring, coincides exactly with the line of thirty inches on the scale. The zero and the tenth division of the vernier are also in exact coincidence; that is to say, there is no fraction. We shall read then 80.000 inches.

In Fig. 7 the regulating line does not fall upon any of the divisions of the scale, but between twenty-nine inches and two-tenths and twenty-nine inches and three-tenths of an inch. There is then a fraction which must be read on the vernier. Seeking which of these divisions coincides with that of the scale, we find that it is the fifth; we shall write then 29.250 inches.

In Fig. 8 we see that the height falls between thirty inches

and thirty inches and one-tenth; no line of the vernier also coincides exactly; but the line 7 is a little above, the line 8 is a little below, one of the lines of the scale; the fraction falls, then, between seven and eight hundredths. Estimating in tenths the distance the vernier passes over between the coincidence of seven and that of eight, we thus obtain the tenths of an hundredth, or the thousandths. In this latter case, the distance above seven is less than the half; we shall then read 30.073. It will always be easy to judge whether the top approaches nearer the upper coincidence than the lower coincidence; in the former case, the fraction is greater than .005; in the latter it is smaller than The error which will be committed in this estimate will remain less than .005; with practice and a little skill, it will hardly ever exceed .002, always supposing the scale is well graduated. For this reading, as well as for the others, it is particularly important to have the eye exactly at the height of the line to be determined.

The same process of reading is applied to the metrical scale; the vernier then gives tenths directly, and by estimate, the hundredths of millimetres. In the English instruments, the inches must be separated by a (.) and three decimals written, even when the last is a zero; s. g. 30.250, and not 30.25; the zero indicates that the thousandths have been taken into account, but that there are none. In the metrical scale put the (.) after the millimetres, and admit two decimals, s. g. 761.25.*

During the whole time of the observation of the barometer, the observer must endeavor to protect it as much as possible from the heat which radiates from his body. But the best way is to learn to observe rapidly. All the operations of which we have just spoken take longer to describe than to execute; one or two minutes, if the instrument be in place, three minutes if it is to be taken from its case and put back again, are sufficient for a practised observer to make a good observation

Altitude.—The height of the barometer above the ground, or above some fixed point, which may serve as an invariable point of reference, ought to be exactly determined. Such a point, for instance, may be the base of a public edifice, the level of low

^{*} For the method of reading the vernier of Green's standard barometer, see the description of the instrument, page 54.

water of a neighboring river, the ordinary level of the surfacewater of a canal, the upper part of a wharf in mason-work, &c. If the barometer has changed place, it is again necessary to measure exactly its height above the same point of reference; the latter will serve to fix the height of the barometer and of the station above the level of the ocean; this datum being of the greatest importance. Every change of this nature should be carefully noted in the journal.

It is greatly to be desired that the place of the barometer, once determined, should not be changed, either from one story to snother, or from one house to another. If circumstances compel this to be done, we should begin, before taking it from its place, by raising the mercury in the cistern by means of the screw, so as to fill the cistern and the tube; it must then be gently taken from the hook, turned upside down, and carried with the cistern up, taking great care not to strike it against anything. If it were transported without these precautions, even from one chamber to another, great risk would infallibly be run of breaking it, or letting in air, and thus rendering it useless.

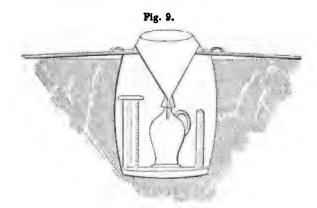
Verification.—From time to time the barometer should be so inclined as to cause the mercury to strike gently against the top of the tube. If it gives a dry and clear sound, it is free from air, and the instrument is in good condition. If the sound is flat and muffled, there is a little air in the barometric vacuum; and the fact should be noticed in the journal. Every occasion should be seized to compare it anew with a standard barometer, to ascertain whether it has undergone any change.

OMBROMETER.

Placing.—The ombrometer, or rain-gage, is a funnel, accompanied by a graduated cylindrical glass vessel, and by a reservoir. It should be placed in an open space. Trees, high buildings, and other obstacles, if too near, may have a considerable influence in increasing or diminishing the quantity of rain which falls into the funnel. The surface of the receiver should be placed horizontally about six inches above the ground. The most simple mode of establishing it is the following:—

Place in the ground a cask or barrel (Fig. 9), water-tight, the

top rising above the ground about three inches; cover it with boards slightly inclined in the form of a roof, which project on all sides beyond the edge of the barrel at least a foot. A circular opening in the middle receives the funnel, the borders of



which rest on the board. At the bottom of the barrel, to receive the water, is an earthen or metallic vessel, with a narrow neck, (an ordinary earthen jug will answer,) in which is placed the end of the funnel, exactly filling the opening. It must contain two or three quarts. The funnel is fastened by means of two clasps to the board, which must be covered up with sod, to make it like the ground itself. If circumstances render it necessary to place the ombrometer higher, the height must be carefully noted in the journal. If it is placed upon a sloping roof, it should be on the top, and not at the edges, or at the angles, and must be raised several feet above the roof itself.

Observation.—To make the observation, remove the funnel, and pour the water from the jug into the large graduated glass cylinder. The opening of the funnel being one hundred square inches, one inch of rain in depth gives one hundred cubic inches of water; and each division of the glass containing a cubic inch of water, each of them represents a hundredth of an inch of rain fallen into the ombrometer. These degrees are large enough to permit us to estimate the thousandths of an inch. The divisions of the smaller graduated glass cylinder will measure directly the thousandths of an inch, and it may serve, in case of accident, as a substitute for the larger one. The two glass vessels may be

placed in the barrel itself, if it is of sufficient size. They must be placed in a reversed position, on two upright pegs, to let them drip out. As soon as the observation is made, it should be noted in pencil, not trusted to the memory; and written in the journal upon entering the house.

SNOW-GAGE.

Observation.—The snow-gage should be supported vertically, in an open place, between three short wooden posts, its opening being about two feet from the ground. It should be employed in the following manner:—

When only a very small quantity of snow falls, or of snow alternating with rain, or of dry and fine snow, driven by the wind, it should be collected in the snow-gage, as would be done in the ombrometer. But when the snow falls in a sufficient quantity to cover the ground more than an inch deep, the vessel must be emptied, and plunged, mouth downwards, into the snow, until the rim reaches the bottom. A plate of tinned iron, or a small board, may then be passed between the ground and the mouth of the gage, and the whole reversed. In this way a cylinder of snow, of which the base is superficially one hundred inches, will be cut out, and received into the vessel. The operation may be facilitated by placing on the ground a platform of strong board or plank, two or three feet square, on which the snow is received.

The place selected for this purpose must be one where the snow has not been heaped up, or swept away by the wind, and where it presents, as near as possible, the mean depth of the layer that has fallen. In order to take only the snow which may fall in the interval between two observations, the board should be swept after each measurement, and the place designated by stakes.

Reading.—In the reading of the graduated vessels, the general surface of the liquid must be considered as the true height, and not the edges, which are always raised along the walls of the vessel by capillary attraction.

The collected snow must be melted by placing the gage, covered with a board, to prevent evaporation, in a warm room;

and the quantity of water produced measured by pouring it into the glass cylinder. It need hardly be said, that if rain and snow fall the same day, no account will be taken except of what the snow-gage receives, unless the ombrometer has been observed separately after the rain, and the snow-gage after the snow. Care must be taken, in these cases, not to count twice the same quantity of fallen water.

The rain-water and melted snow-water must be separately entered in the journal in the columns reserved for each.

During abundant rain-falls, it is well to measure the water more than once a day, or at least immediately after the rain; and the quantity of the rain fallen, together with the time it has lasted, is to be noted separately in the column of remarks.

When it freezes, it will be necessary to protect the receiver by filling in the interior of the barrel with straw.

[A series of observations have been made at the Smithsonian Institution with rain-gages of different sizes and different forms, the result of which, as far as the observations have been carried, is to induce a preference for the smallest gages. The one which was first distributed by the Institution and the Patent Office to the observers, is represented in Fig. 10. It consists of the

Fig. 10.

funnel a, terminated above by a cylindrical brass ring, bevelled into a sharp edge at the top, turned perfectly round in a lathe, and of precisely five inches diameter. The rain which falls within this ring is conducted into a two-quart bottle, b, placed below to receive it. To prevent any water which may run down on the outside of the funnel from entering the bottle, a short

tube is soldered on the lower part of the former and encloses the neck of the latter. The funnel and bottle are placed in a box or small cask e, e, sunk to the level of the ground, which is covered with a board d, d, having a circular hole in its centre to receive and support the funnel. To prevent the rain-drops which may fall on this board from spattering into the mouth of the funnel, some pieces of old cloth or carpet, c, c, may be tacked upon it.

The object of placing the receiving ring so near the surface of the earth, is, to avoid eddies caused by the wind, which might disturb the uniformity of the fall of rain.

In the morning, or after a shower of rain, the bottle is taken up and its contents measured in the graduated tube f, and the quantity in inches and parts recorded in the register. The gage, or tube, which was first provided for this purpose, will contain, when full, only one-tenth of an inch of rain, the divisions indicating hundredths and thousandths of an inch. As this, however, is found to be too small for convenience, another gage, which will contain an inch of rain, and indicating tenths and hundredths, will be sent to observers.

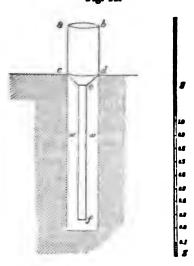
Another and simpler form of the gage has since been adopted by the Institution and the Patent Office, to send by mail to distant observers. It is one of those which have been experimented on at the Institution, and is a modification of a gage which was received from Scotland, and which has been recommended by Mr. Robert Russell.

It consists of-

- 1. A large brass cylinder a, b, c, d, two inches in diameter, to eatch the rain.
- 2. A smaller brass cylinder e, f, for receiving the water and reducing the diameter of the column, to allow of greater accuracy in measuring the height.
- 3. A whalebone scale s, s, divided by experiment, so as to indicate tenths and hundredths of an inch of rain.
- 4. A wooden cylinder w, w, to be inserted permanently in the ground for the protection and ready adjustment of the instrument.

To facilitate the transportation, the larger cylinder is attached to the smaller by a screw-joint at s.

Fig. 11.



Directions for use.—To put up this rain-gage for use: 1. Let the wooden cylinder be sunk into the ground in a level unsheltered place until its upper end is even with the surface of the earth. 2. Screw the larger brass cylinder on the top of the brass tube and place the latter into the hole in the axis of the wooden cylinder, as shown in the figure, and the arrangement is completed.

The depth of rain is measured by inserting the scale into the gage and noting the height to which it has been wetted by the water when it is withdrawn. In order, however, that the water may wet the scale, the superficial grease should be removed by rubbing it with a moist cloth, previous to use. In case the water cannot be made to adhere to the scale, a slip of pine or other wood may be made of the same size of the scale, and this inserted in its stead. The quantity of water may then be measured by applying the slip of wood to the scale.

Should the fall of rain be more than sufficient to fill the smaller tube, then the excess must be poured out into another vessel, and the whole measured in the small tube in portions.

Care should be taken to place the rain-gage in a level field or open space, sufficiently removed from all objects which would prevent the free access of rain, even when it is falling at the most oblique angle during a strong wind. A considerable space also around the mouth of the funnel should be kept free from plants, as weeds or long grass, and the ground so level as to prevent the formation of eddies or variations in the velocity of the wind.

To ascertain the amount of water produced from snow, a column of the depth of the fall of snow, and of the same diameter as the mouth of the funnel, should be melted and measured as so much rain.

The simplest method of obtaining a column of snow for this purpose is to procure a tin tube, about two feet long, having one end closed, and precisely of the diameter of the mouth of the gage.

With the open end downward, press this tube perpendicularly into the snow until it reaches the ground or the top of the ice, or last preceding snow; then take a plate of tin, sufficiently large to cover it, pass it between the mouth of the tube and the ground, and invert the tube. The snow contained in the tube, when melted, may be measured as so much rain. When the snow is adhesive, the use of the tin plate will not be necessary.

From measurements of this kind, repeated in several places when the depth of the snow is unequal, an average quantity may be obtained.

As a general average, it will be found that about ten inches of snow will make one of water.]

Mr. Guest, of Ogdensburgh, N. Y., recommends, from an experience of six years, the following as the best plan for ascertaining the amount of melted snow. Procure a cylindrical tin tube of the exact diameter of the mouth of the rain-gage and two or three feet long, so that the snow cannot be blown out. Place this vertically in a properly exposed position, and firmly secure it against the action of the wind, which would otherwise blow it over in a violent storm. After the snow has ceased to fall, bring the vessel with its contents into the house, near a fire, which will gradually melt the snow, and afterwards measure the water produced by means of the rain-gage.

WIND-VANE.

Placing.—The wind-vane should be set in a place as free and open as possible, away from every obstacle, and especially from high buildings. It should exceed in elevation, by at least eight or ten feet, the neighboring objects. To facilitate observations at night, the following arrangement may be adopted:—

The wind-vane is composed of a leaf of zinc about three feet in length, in the form of a butterfly's wing, exactly counterbalanced by a leaden ball. It is carried upon a cylindrical axis of pine wood, or of any other light and strong material, two inches in diameter, which, if possible, passes down through the roof into the observer's chamber, otherwise along the exterior wall of the building to a window. The axis terminates by a steel pivot turning freely on a cast-iron plate. This plate supports a dial divided into degrees, besides indicating the eight principal points of the compass. The axis carries an index placed in the same plane as the feather of the wind-vane, which enables us to read upon the dial, as well by night as by day, the direction of the wind. The whole rests on a strong wooden shelf, firmly fastened to the window by supports. Above, the rod is firmly fixed to a strong upright staff, or, better, on the roof, with strong braces, by means of a piece of wood containing friction rollers, which allow the shaft to turn freely and without effort. Similar pieces with friction rollers, placed at different distances along the wall, keep the axis vertical.

Great care must be taken to secure the perfect verticality of the shaft, and to this end it is necessary to fix it by a plumb-line in two different planes cutting each other at right angles. The index at the foot of the rod should be placed on the same side with the point of the wind-vane, and in the same plane as the feather. The pivot should turn very freely in the hole that receives it, and into which a drop of oil should be poured.

Finally, we must carefully adjust the points of the dial, which is supported with the iron plate, upon a board fastened upon a shelf by means of a strong screw. In making this adjustment by means of a compass, the magnetic variation of the locality must be taken into account; each observer should have the line of the true north traced on his window.

If the dial is exposed to the open air, it must be protected against the snow and tee, which would impede the play of the pivot and of the index. A small ring of wood placed around the pole, under one of the friction rollers, will prevent the windwane from being raised, and the pivot from being displaced during the most violent winds.

[As a flat vane is always in a neutral line, a more accurate and sensitive one is made by fastening two plates together at an angle of about ten degrees, forming a long wedge. Thus,

The longer the vane, the shorter the pulsations, and the steadier the action will be. For a small sized vane, it may be ten or twelve inches wide, and four feet long.]

Observation.—The observation of this instrument demands In winds of considerable strength the vane is never some care. at rest, or fixed in the same direction; it oscillates incessantly, and its oscillations increase in amplitude with certain winds, and with the violence of the wind. We must then note the mean direction between the extremes. When the wind is very feeble, perhaps it may not have sufficient force to set the vane in motion; in this case, as when the air is calm, great mistakes might be made by registering the direction marked by the index; for its position indicates, not the direction of the existing wind, but that of the last wind that had the power to set the instrument in When the index is immovable, and there is no oscillation, we must give up its indications, and refer to the movement of light bodies, as that of the leaves of trees and the smoke of chimneys, to determine the direction of these feeble currents of air. During the night the direction of the wind may be easily ascertained by raising the hand in the air, with one finger wet. The least motion in the air increases evaporation, and a sensation of cold is experienced on the side of the finger turned towards the wind.

The direction of the wind must be noted, following the eight principal points of the compass—north, northeast, east, southeast, south, southwest, west, and northwest. For the additional observations during storms, the degrees may be indicated, in order to follow more exactly the rotation of the wind, or at least

sixteen points of the compass, viz: N. NNE. NE. ENE. E. ESE. SE. SSE. S. SSW. SW. WSW. W. WNW. NW. NNW.

The lower, or surface wind, often has a different direction from that which prevails in the upper regions of the atmosphere, and this is generally the case when the wind turns, and the weather is going to change, also during storms and great atmospheric movements. The direction, then, of the lower and the higher layers of clouds must be separately noted in the several columns of the journal reserved for this purpose. If the direction is the same in the whole extent of the atmosphere, the same letters will be marked in the three columns. If the absence of clouds does not permit us to judge how the wind is above, a dash must be substituted for the letter, indicating that the observation has been made. A blank always signifies an observation omitted.

To avoid an error in the estimate of the direction of the clouds, it will be well to observe their course between two fixed points, as a window frame, the fixed lines of which will facilitate the observation. Another very convenient method is to place a small mirror horizontally, with lines traced on it indicating the points of the compass; the image of the clouds passing over these will indicate their direction.

The manner in which the wind turns, or rather the order in which the winds succeed each other in the course of the day, must be watched very carefully. It will be seen that they commonly follow in regular order; they pass from the east by the south to the west, and from the west, by the north, to the east. Nevertheless, they sometimes go back in the opposite direction, particularly during storms. A little memorandum, summing up in a few words at the end of each day this course of the wind, together with the hours of the wind's changes, is very valuable. It may be entered in the column of remarks.

The force of the wind must be estimated as nearly as possible according to the following degrees:—

0. A perfect calm.

The simple initial letter of the wind, for instance N. (north), indicating its direction without any number, means a slight movement of the air hardly to be called a wind, and only just sufficient to allow an estimate of its direction.

- 1. A light breeze which moves the foliage, and sometimes fans the face.
- 2. A wind which moves the branches of the trees, somewhat retards walking, and causes more or less of a slight rustling sound in the open air.
- 3. A wind which causes strong boughs and entire trees to rock, makes walking against it difficult; which causes a stronger rustling sound to be heard, and which often blows in gusts, and carries light bodies up into the air.
- 4. A storm-wind, during which the trees are in constant motion; branches and boughs covered with foliage are broken off, and in a violent storm sometimes even entire trees are broken, or uprooted; leaves, dust, &c., are continually borne up and carried far away; during which time there is an uninterrupted loud rustling sound, with strong gusts; walking windward is extremely difficult, and now and then chimneys, fences, &c., are thrown down, windows broken in, &c.

These degrees correspond nearly to the following numbers of Beaufort's scale, which is generally used among seamen:—

1. the same as 1. Light breeze,
2. " " 4. Moderate breeze,
3. " " 8. A fresh gale,
4. " " 11. A storm-wind,

of Beaufort's
scale.

[The force of the wind is now estimated and registered according to the direction on the blank forms.]

SKY.

The blue color of the sky has an intimate connection with the hygrometrical state and the electrical tension of the air; it may be noted by the expressions, dark, light, and grayish.

Haze and dry mist.—The transparency of the air is often disturbed by a kind of vapor, which gives a whitish tint to the sky and dims the rays of the sun. This phenomenon, known in Europe under different names, appears frequently after long droughts; in this country it seems to characterize the Indian summer. In Europe, and elsewhere, an intensely dry mist, which is, probably, a different phenomenon, sometimes follows great earthquakes or volcanic eruptions. The observer will carefully

enter phenomena of this kind, and the circumstances under which they appear or disappear. If he has an opportunity, as in a high station, he should endeavor to ascertain if there is an upper limit, and what is the thickness of the layer of haze or dry mist. Observations made in the Alps prove that the atmosphere is often entirely free from it at a height of two thousand feet, when it is very intense in the plain. Does a thunder-storm or rain always cause it to disappear? Do the prairie fires have any relation with kindred phenomena? Does it appear more frequently in certain seasons than in others?

HYDRO-METEOROLOGICAL PHENOMENA.

DEW.

The dews, especially when they are abundant, and The white frosts, or frozen dew, particularly the first and last of the year, and their intensity, must be entered.

FOG.

Fog.—The moment must be noted when it forms and when it dissipates, as falling fog, rising fog; its density, as dense fog, slight fog.

Mists hanging over forests, moors, meadows, rivers, or the

Notice must be carefully taken of the time of their appearance or disappearance; these are the most important facts in regard to them.

These fogs must not be confounded with the dry fog, which belongs to another class of phenomena, which have been spoken of above.

CLOUDS.

For noting these the observer must go out to a place entirely free, in case his residence has too confined a horizon.

The cloudiness or the quantity of clouds, after some practice,

can be easily estimated, in accordance with the following scale. Thus, we understand by—

- 0. A clear sky, entirely free from clouds;
- 10. The whole sky covered with clouds, or a dense fog, or rain; and by 1, 2, 3, 4, 5, 6, 7, 8, 9, the different degrees of cloudiness which lie between these:
- 1. Denotes, for instance, nine times as much blue sky as clouds;
- 5. An equal amount of clouds and blue sky;
- 9. Nine times more clouds than blue sky.
- If, on account of the locality, it is impossible for the observer to estimate the quantity of clouds in this way, he can make use of the following expressions, which will mark at the same time the medium character of the aspect of the sky during each day:
 - Wcl. Wholly clear; a sky entirely free from clouds.
 - Cl. Clear; when at least two-thirds of the sky is unclouded.
- M. Medium; the clouded part of the sky nearly equal to the blue.
 - C. Cloudy; a larger part cloudy than clear.
 - Ov. Overcast; the clouds rarely broken.
 - Cov. Covered sky; without any visible spot of blue.

The form of the clouds will be indicated by the terminology of Howard.

According to this, they are distinguished by their external forms into three kinds: the cirrus, cumulus, and the stratus, to which belong four transition forms, the cirro-cumulus, the cirro-stratus, the cumulo-stratus, and the nimbus. The most remarkable of these forms may be characterized in the following manner:—

The cirrus, or cat-tail of the sailors, is composed of loose filaments, the whole of which sometimes resembles a pencil, sometimes curly hair, sometimes a fine net, or a spider's web.

The cumulus, or summer cloud, the cotton-bale of the sailors, often shows itself under the form of a hemisphere resting on a horizontal base. Sometimes these half spheres are piled upon one another, forming those large accumulated clouds in the horizon which resemble, at a distance, mountains covered with anow.

The stratus is a horizontal band, which is formed at sunset and disappears at sunrise.

The cirro-cumulus are those small rounded clouds, which are

often called fleecy; when the sky is covered with clouds of that kind it is said to be mottled.

The cirro-stratus is composed of small bands, formed of closer filaments than those of the cirrus, for the rays of the sun often find it difficult to penetrate them. These clouds form horizontal beds, which, at the zenith, seem composed of a great number of loose clouds, while at the horizon a long and very narrow band is seen.

The cumulo-stratus is a mass of heaped up and dense cumuli. At the horizon they often assume a dark or bluish tint, and pass into the condition of nimbi, or rain clouds.

The nimbus is distinguished by its uniform gray tint, its fringe and indistinct edges; the clouds composing it are so blended that it is impossible to distinguish them.

But besides these principal forms, there are several intermediate, to which it is difficult to assign a name. They must be referred to the form which they most resemble.

They may be entered in the journal by means of the following abbreviations:—

St.	i. e.	Stratus.
Cu.	44	Cumulus.
Cir.	"	Cirrus.
Cir. st.	66	Cirro-stratus.
Cu. st.	66	Cumulo-stratus
Cir. cu.	44	Cirro-cumulus.
Nim.	64	Nimbus.

If several of these forms are visible, the most frequent should be underlined, and the others should follow the order of their frequency. The distribution of the clouds in the sky should be noted, whether they are dispersed or accumulated in a special region of the heavens, in the horizon, at the zenith, &c

RAIN.

It is necessary to note as accurately as possible the hour at which the rain begins and ends; if it is a continued rain, or at intervals and in showers; if it is general or only partial, preceded, followed, or accompanied by fogs; the size of the drops and the force of the rain should be also noted. For these different cases, the following designations may be adopted:—

Rainy, when the fall of some drops and the appearance of the weather is such as to indicate the approach of rain.

Continued rain.

Interrupted rain.

Shower, which lasts not more than a quarter of an hour.

General rain, which prevails over the whole extent of the horizon.

Partial rais, which falls from the clouds that pass over only a small extent of country.

The force of the rain may be indicated by the following gradations:—

Drizzling rain, which falls in very small drops, almost like those of mist.

Slight or fine rain.

Moderate rain.

Heavy rain.

Violent rain, heavy and strong pelting rain.

The size of the drops seems to depend chiefly upon the height of the clouds, and consequently upon the seasons and the circumstances of the temperature.

The snow.—The period of the first and last snow, the size of the flakes, their forms.

Sleet, which consists in small balls of snow, white and opaque, commonly without a crust of ice, like the opaque nucleus found within hail-stones, falling more frequently in spring and in autumn.

Frozen rain drops should be distinguished from the preceding forms; they make little balls of transparent ice.

Hoil.—Indicate the size, form and average weight of the hail-stones. The number of different strata observed in the larger stones. Whether any of them contain particles of sand or any other foreign matter. The extent and course of the phenomenon.

THUNDER-STORMS.

The time of beginning and ending of the storm must be indicated as exactly as possible; the point of the horizon whence it rises, the direction of the clouds, of the wind and its variations, and, if possible, the quantity of rain before and during the storm;

of hail, &c., which falls; note if it passes over the place of the observation, or at a distance; if it is accompanied, or not, with strong electrical detonations and numerous lightnings. It will be well to ascertain the state of the meteorological instruments every five minutes during the storm, especially of the barometer and the thermometer.

[At the Institution the barometer generally sinks during the coming on of a storm, and rises suddenly at the first fall of rain.]

In the journal, the occurrence of a storm will be indicated on the opposite page of the blank, with the hour when it took place. If special observations have been made with the instruments, they will also be entered on the opposite side of the sheet, taking care to note the day and the hour. If the observations require a more detailed description, it may be made on a separate sheet.

TORNADOES AND LAND-SPOUTS.

These whirlwinds, or violent and circumscribed storms, give rise to very complex phenomena, which are difficult to observe. All the meteorological circumstances, however, should be minutely noted; among others the following:—

The course of the barometer, which almost always sinks much and rapidly; that of the thermometer, which usually indicates an elevation of temperature; the region of the heavens in which the thunder-storm frequently accompanying them is formed; the form and color of the clouds; the direction and intensity of the wind; the frequency, the size, and the form of the lightnings; finally, the apparent shape of the land-spout, its variations, its course, and its effects upon the trees and upon the ground.*

ADDITIONAL OBSERVATIONS DURING STORMS.

Everybody knows the importance of a knowledge of the laws of those great movements of the atmosphere which embrace almost the whole extent of the continent. It is only in following them, step by step; by observing their different phases at different

^{*} For more detailed instructions upon the observations of land-spouts, see the Annuaire Météorol. de France, 1849, p. 225.

places, and by combining the facts obtained, that the meteorologist can be enabled to discover the laws which preside over these great phenomena. For this, the three regular observations a day are insufficient; it is then earnestly recommended to observers, who desire to contribute effectually to the solution of this great problem, not to content themselves with the prescribed number, but to add as many more as possible during the continuance of remarkable storms; noting not only the state of the instruments from hour to hour, if possible, but following with attention all the meteorological changes. These observations must be entered on the reverse of the sheet, under the head of Casnal Phenomena, which is particularly reserved for this purpose.

The principal points to which attention should be directed are the following:—

The barometer announces by a considerable fall the approach of a storm. Then it begins to rise during its continuance, and only resumes its nominal equilibrium after its close. Remark especially the following points:—

Was the storm preceded by a noticeable or sudden rise previous to the fall;

Note the state of the barometer, and the time when the fall becomes more rapid;

Its state, and the time, when it is lowest and when the rise begins;

The highest point which it reaches during, or immediately after the storm.

If alternations of rising and falling take place, the fact should be mentioned and the time noted.

The thermometer.—The fluctuations of the thermometer in the same time as those of the barometer should also be noted, and their connection with the changes of the wind be observed.

The wind.—It is of the greatest importance to observe the course of the winds through the entire height of the atmosphere during the whole continuance of the storm, by means of the wind-vane and of the clouds in the different layers of the atmosphere.

The hour when the wind begins, and the direction whence it comes;

The moment of its greatest violence;

The instant it changes its direction, and when it takes the direction it keeps to the end of the storm.

It should be stated if the wind blows in a continuous manner or in squalls, and what is its force.

If there should be one or more moments of calm, the hour and duration will be indicated.

Great care must be taken at each observation to note also the direction of the different layers of clouds, which will very often be found different from that of the wind below, for the whole duration of the storm.

The clouds.—Are there certain forms of clouds which announce the approach of a storm? It is necessary, in this connection, to watch the formation of the cirrus, the cirro-cumulus, cirro-stratus, their arrangement in parallel lines, their course, and their directions. Note the quarter of the sky first covered with clouds; the moment when it is entirely covered; if there are later clear spots or not; the moment when the sky clears off.

The rain.—Note the hour at which the rain or the snow begins and ends; measure the quantity fallen while the storm lasts.

ACCIDENTAL METEORIC PHENOMENA.

These will be entered in the tables, in the place reserved for this purpose on the opposite side of the sheet. If the space is not sufficient for the description to be given, the phenomenon should be simply noted, and reference made to a separate account for details. Thus:—

The solar and lunar haloes—that is, the colored circles sometimes observed round the sun and moon. Distinguish the small ones, the ring of which measures only a few degrees, from the large or real haloes, the ring of which has a diameter of about forty-four degrees. It must be stated whether they are connected with other circles, as is sometimes the case. Care must be taken not to mistake a part of a grand halo for a rainbow. Note whether these appearances are, or are not, ordinarily followed by rain.

The Porhelia and Paraselenes (mock-suns and moons).—Describe exactly their forms and the state of the heavens at the moment of their appearance.

Rasnbows, simple or double.

An extraordinary redness of the sky, either in the morning or

evening; the particular color of the sun and of the moon at their rising, especially in fair days.

Heat lightnings without thunder, and sometimes without clouds; indicate their direction and the aspect of the clouds in their neighborhood.

The Aurora Borealis, or northern light, for the observation of which the special instructions, page 48, must be followed.

Shooting-stars.—The observer must be particularly attentive to their frequency, during the periods near the 10th and 11th of August, and the 10th and 15th November, in which it is supposed that they are more numerous than at any other time. He will designate the quarter of the heavens from which they seem to issue, and their direction.

Fireballs.—Describe their aspect, their size, their course in the heavens, and note the exact hour of their appearance.

All the other luminous phenomena, which present any extraordinary appearance, should be noted down.

These descriptions should be made in simple and well-defined terms. The observer will take great care to enter scrupulously what he sees without drawing any conclusion, or attempting any explanation of the phenomenon. He ought to reflect that, in order to make a good observation, he must keep his mind in a state of perfect freedom in respect of any preconceived theory, and to consider the phenomenon before him as being one of the data for the foundation of the science, and that the knowledge of the truth will depend upon the fidelity of his observation.

TIME OF OBSERVATIONS.

The time of observations will be the mean time at each station The observations will be made three times daily, viz:—

At 7 o'clock a. m.

2 " p. m.

9 " p. m.

The mean of these three hours will be very nearly the true mean, as it would be obtained by observation made every hour of the day and night.

The rain gage will be observed only once a day, unless very abundant rains should make a second measurement necessary.

The best time will be 2 o'clock p. m., the observation being made daily; if another hour is selected, it should, when once fixed, remain the same.

The maxima and minima thermometers will be read once a day, always at the same hour. The most suitable hour will be 9 o'clock in the evening.

If an observer desires to examine the daily oscillations of the barometer, he will also observe at 10 a. m. and 4 p. m., which give the daily maximum and minimum. It will be well to note also, at the same time, the state of the hygrometer.

If he desires to complete the data upon the diurnal course of the temperature, he will add observations of the thermometer at 10 a. m. and 6 p. m. In all cases it is desirable that, if an observer has leisure to increase the number of the hours of observations, he should fix them at equal intervals between the principal hours indicated above.

Besides these observations at regular hours, additional observations ought to be made during remarkable storms, as has been remarked above.

It is very important that the observations should be made at the exact hour, fixed by a well regulated watch. All the instruments should be read rapidly, so that the observations may be as simultaneous as possible.

The order in which they are to be observed will be as follows:-

A few minutes before the hour, observe the thermometer before opening the window; then wet the psychrometer. While it is taking the temperature of evaporation, note the height of the barometer, observe the wind, the course of the clouds, their quantity, the aspect of the sky, &c.; then read the temperature of the psychrometer.

The observations must be recorded for each instrument at the moment when they are made, without trusting anything to the memory. A strict rule should be laid down for one's self, to note exactly the indications of the instruments, without subjecting them mentally to any corrections or any reductions; these should not be applied until all the elements are at hand.

If the observer has been unavoidably hindered from making the observations at the exact hour, he will note in the column of hours the number of minutes of the delay. If he is obliged to procure a substitute, he must choose one accustomed to this kind of observation; but before entering his records, he will carefully examine them. To distinguish the observations made by his substitute, he will enter them in red ink.

As it is of the greatest importance that the series of observations should not be interrupted, and that there should be no omissions, each observer will do well to instruct beforehand one or more substitutes, who may be able upon occasion to take his place. If, in spite of these precautions, the observation has necessarily been omitted, its place will be left blank in the journal. In this case the observer must never fill up these blanks with calculations, according to his judgment; he should consider the conscientious observance of this rule indispensable to truth and good faith. He should remember, besides, that if he acts differently, he not only lessens the value of these results, but brings into doubt and disfavor the fidelity of his other observations, and takes from them what constitutes their greatest value for science—confidence.

THE REGISTER.

In the register the first page is devoted to regular observations; the second to additional observations, to periodical or extraordinary phenomena, and to monthly recapitulations. The headings of the columns indicate clearly the use of each.

For each instrument the columns follow each other in the order in which the observations are to be made, and one column is reserved to enter the observation just as it is made, and before any correction or reduction. As each sheet is to be regarded as an independent document, it should carry with it all that is necessary to correct the observations therein contained, and to render them authentic. Thus, the date of the year, the month, the precise locality, the latitude and longitude, the elevation of the instruments from the ground and above the sea, the nature and condition of the instruments which have been employed, and the amount of their corrections; finally, the signature of the observer should be repeated on every leaf. It will be sufficient, for this, to fill the blank spaces left after the different printed titles in the blank forms. The observer should the less neglect this important duty, as it is an affair of only a few strokes of the pen each

month, without which his labor would run the hazard of losing its value.

Barometer.—The degree of the attached thermometer and the observed height of the barometer will be inscribed in the first two columns. This height will be reduced to freezing-point, or 32° Fahrenheit, or zero Centigrade, by means of tables, and the whole correction of the instrument will be applied to it. It will then be inscribed in the third column, entitled corrected height at freezing-point. These corrected heights, and never any others, must be employed to form the mean, which will be inscribed in the fourth column.

Thermometer.—In the thermometrical observations the quantities above zero will be always written without a sign; the negative quantities will be all individually marked with the sign minus (—), whether they follow each other or are isolated. In the first column, entitled daily mean, will be inscribed the mean of the three observations of the day, i. e. their sum divided by 3, admitting two decimals.

Psychrometer.—In the first two columns will be entered the indications of the dry and wet thermometer, after having applied to each of them the correction of the instruments, if there be any. By means of the psychrometrical tables will be found the force of the vapor and the degree of relative moisture, each of which has its column.

We have indicated above the manner of noting the direction of the winds.

As to the force of the surface wind, which alone can be estimated with some degree of precision, it will be expressed by adding to the letter which designates the direction, the figure indicating its force: e. g., N, without a figure, signifies a slight air, hardly perceptible, coming from the north; N₁, a slight breeze; N₂, a strong wind, &c. The other two columns will have only letters, or a dash (—) if the observation has not been possible.

The quantity of clouds, or the *cloudiness* estimated from zero, or a perfectly clear sky, to 10, sky entirely overcast, has a separate column.

It is the same with rain and melted snow, which will be separately entered. A third column is reserved for the total quantity

of both. The thickness of the layer of fallen snow may be indicated in inches and tenths.

As to the broad column for Casual Phenomena, although it is desirable, considering the small space the form of the table allows, to employ abbreviations to express the state of the sky and the different meteorological phenomena; nevertheless, we must limit ourselves to a small number, chosen from among the expressions which most frequently occur, such as those found at the bottom of the blank forms. If abbreviations are too much multiplied, we lose in clearness and certainty what we gain in conciseness. A meteorological journal should not resemble a page of algebra, where a badly formed letter or a misplaced sign renders the expression unintelligible.

For the additional observations the same rule should be followed.

In the space mentioned above, periodical and extraordinary phenomena will be inscribed, with their dates and the hour of their appearance.

Every change of position, or in the condition of the instruments, should be carefully entered, with the precise date at which it took place. If there has been none, instruments all in order will be entered. By the side of the indication of the correction of the instruments will be placed, correction applied or correction not applied, according as the observations of utained in the sheet shall have been corrected or not. The finished sheet will be signed by the observer.

The reductions, the corrections, and the calculations of means, must be made day by day and at the end of each month with the greatest punctuality. The necessary tables will be placed at hand by the side of the journal, and each observation reduced, and the correction, if any, applied immediately.

This is not only the least troublesome method, but the only one which permits the observer to control the observations and the reductions, and to discover the accidental errors of the pen and of the reading in the record.

The observer cannot be too thoroughly convinced that a meteorological journal which contains only rough observations, is only half made; in this condition it is wholly unfit to serve any scientific purpose. The observations cannot be compared rigorously with each other, nor with those of other stations. The

only means for the observer to give its true value to his labor, is to make the corrections, the reductions, and the calculations of the means himself. It is for want of having thus been elaborated that voluminous collections of observations, the fruits of long years of toil, remain useless and forgotten in the dust of libraries, because the meteorologist finds it impossible to make use of them without first undertaking those calculations, the amount of which absolutely transcends the powers of an individual, and would discourage the most ardent zeal, while they would have cost the observer only an instant each day, if he had made them at the time of the observations.

The calculations desirable are as follows:---

- 1. Each barometrical observation must be reduced immediately to the temperature of zero Centigrade, or 32° Fahrenheit, by means of the tables, and the total correction of the barometer, if there is any, will be applied.
- 2. The diurnal means of the several instruments, resulting from the sum of the three observations made at these different hours, divided by three, must be entered each day in the respective columns, after the observation of 9 p. m. It is needless to say that these means should be drawn solely from observations reduced and corrected.
- 3. The monthly means for each hour separately—that is, the monthly mean of the observations of 7 s. m., and that of 2 p. m., and of the observations of 9 p. m.
- 4. The monthly means drawn from the means of each day; the monthly extremes of the instruments; the monthly amount of the rain, hail, or snow; the mean cloudiness of the sky; the prevailing wind, &c.
- 5. The annual means and amounts, and the respective extremes for the civil year.

It will be interesting to calculate, also, if the observer is so disposed, the mean of the seasons of the meteorological year, which begins December 1, to November 30, of the following civil year.

The meteorological seasons are, then:— Winter—December, January, February. Spring—March, April, May. Summer—June, July, August.

Autumn-September, October, November.

In calculating all these different results, we should take, in order to be very exact, the means of the sums of all the observations during the period of time in question, by reason of the inequality of the length of the months.

The sums which form the basis of all these means should be inscribed in the tables in the place reserved for them.

The preceding calculations, after a little practice, will not appear difficult, and may be quickly performed; but it can hardly be too often urged upon the observer to make them without delay; otherwise, this task, which is slight if accomplished daily, would become very heavy, if left to accumulate for several months. It is only by making the correction himself that the observer can institute his own comparisons, and really study the course of the meteorological phenomena. His interest will increase still more with the feeling that he is cooperating in a great work, which concerns at once his whole country and the science of the world, and the success of which depends upon the accuracy, fidelity, and devotion of all who take part in it.

A copy of the observations of each month must be forwarded during the first week of the following month. It should be carefully collated by two persons, one of whom reads the figures aloud. Each observer will receive for this purpose a double series of blank forms, one of which will be retained by him.

Many of the phenomena connected with the state of the atmosphere are of great interest for comparative climatology, especially in a practical point of view. The periodical phenomena of vegetation and of the animal kingdom, such as the epoch of the appearance and the fall of the leaves, of the flowering and ripening of the more generally cultivated fruits; the seed time and harvest of plants; the coming and going of migratory birds; the first cry of the frogs, the appearance of the first insects, &c.; the moment of the closing of rivers, lakes, and canals by ice, and of their opening; the temperature of springs at different periods of the year; the temperature in the sun compared to that observed in the shade; that of the surface, and that below the surface of the ground. All observations of this kind are valuable.

The observer will find it very instructive to project curves which indicate the diurnal, monthly, or annual variations of tem-

peratures, of atmospheric pressure, of moisture, &c., as well as thermometrical, barometrical compasses, or circles, &c.

These graphic representations are of the greatest utility for the comparisons, speaking to the eye more clearly than simple figures.

Besides the above directions for keeping an ordinary Meteorological Journal, more special instructions for the study of peculiar meteorological phenomena are prepared by the Smithsonian Institution: as on

Thunder-storms, Tornadoes, and Water-spouts, Aurora Borealis, Parhelia, Parasalenes, Haloes, Rainbows, Temperature of the soil, Periodical phenomena of the vegetable and animal kingdoms, Graphic representations of meteorological phenomena, &c. If any observer should feel inclined to devote himself to the study of any one of these physical problems, he may receive, on application, the special instructions relating to the point which he wishes to investigate. [These instructions now form a part of this pamphlet.]

[The directions given in the preceding article are not intended to supersede those printed on the sheet of blank forms issued jointly by the Smithsonian Institution and the Patent Office, but to impart additional instruction, particularly to those who are furnished with a full set of instruments and desire to attain as much precision as possible.]

SPECIAL DIRECTIONS

TO THE

METEOROLOGICAL OBSERVERS

OF THE

SMITHSONIAN INSTITUTION.

In the reduction of the meteorological records presented to this Institution, much additional labor has resulted from the occasional omission in the registers, of some important facts, and in a want of perfect uniformity in noting the phenomena. We beg, therefore, to call attention to the following remarks:—

- 1. Failure to record latitude and longitude, name and station of the observer, and date on each sheet; the observer probably supposing it sufficient to insert them once on the first sheet sent, and so omitting them afterwards. This often renders it necessary to search back through all the series of registers to some one that contained them—perhaps in a former year. They should be inserted on every sheet.
- 2. Designating the same place by different names, thus rendering it impossible to distinguish whether it were one place or two, unless by accidentally noticing the similarity in the name of the observer or in the latitude and longitude. Such changes of name should be avoided when practicable, and when necessarily made special attention should be called to it.
 - 3. Diversity in the mode of recording the Barometer, as follows:
 - (a) Integers recorded in full, thus 29.85. (This is the proper mode.)
 - (b) Integers omitted when the same as in the entry next above, thus 38.
 - (c) Integers omitted when the same as in the entry next to the left.

- -(d) Integers omitted when the same as in the entry next preceding in the order of time.
 - (e) Integers omitted except where they are different from the usual ones at the place of observation.
 - (f) Integers inserted occasionally and apparently without any system whatever.
- (g) A constant suppressed, and the excess or deficiency recorded, as + or -.

The proper mode is that indicated by (a).

- 4. Diversity in the mode of recording the Thermometer, when it is below zero, as follows:—
 - (a) Indicated by the sign minus placed before it, thus —16°. (This is the proper mode.)
 - (b) Indicated by the same sign placed after it, thus 160—.
 - (c) Indicated by writing it under a zero—thus $\frac{0}{160}$.
 - (d) Indicated by writing it after a zero, with a comma between, thus 0,16°.
 - (e) Indicated by the word 'below,' or the abbreviation b written before or after it—thus 16° below, 16° b, b 16°, or below 16°.

The first (a) is the proper mode.

- 5. Departure from the printed instructions in recording the degree of cloudiness, some observers reversing the figures and using 10 to denote a clear sky and 0, one entirely overcast; and others omitting the record altogether in the columns of cloudiness when the sky is clear, and in place of it sometimes inserting the word "clear" in the columns of "Remarks," or elsewhere. Both lead to error, and should be avoided—the zero should always be inserted "in the narrow column," as directed, when the sky is clear.
- 6. Diversity in the use of the character zero (0) in recording the motion of the clouds, as follows:—
 - (a) Used to signify a calm, or that there is no perceptible motion. (This is the correct use.)
 - (b) Used to signify that the sky is clear, instead of inserting it in the proper column.
 - (c) Used to signify that no observation was taken.

(d) Used to signify that the direction in which the upper current was moving could not be determined on account of the sky being either perfectly clear or entirely overcast.

The first (a) is the correct use.

- 7. Want of full and proper records of the direction of the wind, some observers recording the direction only after each change, and then omitting it so long as it continues the same, merely inserting a figure to denote the force. It is better to make the record in full. Other observers record the direction towards which the wind or clouds are moving instead of indicating that from which they come. A WIND from the North, or CLOUDS moving from the North, are to be denoted by N, and from the South by S, &c.
- 8. Different kinds of thermometers or different exposures used for the dry and wet-bulb thermometers, so that the observations are not comparable readily, if at all.
 - 9. Diversity in the use of the dash and the sign (") as follows:-
 - (a) To signify that the entry next above is to be repeated.
 - (b) To signify that the entry next to the left is to be repeated.
 - (c) To signify that the entry next preceding in the order of time is to be repeated.
 - (d) To signify nothing at all, but merely to fill a blank.

The use of these characters has caused much trouble in the reduction, and the true remedy would be to avoid them altogether, by making each record complete in itself.

10. Illegibility of the records, either from defective chirography or from being entered in pencil marks and partially erased.

CIRCULAR RELATIVE

20

EARTHQUAKES.

The Smithsonian Institution is desirous of collecting information in reference to all phenomena having a bearing on the physical geography of this continent; and, in behalf of the Board of Regents, it is respectfully requested that you will furnish us with any information which you may possess, or be able to obtain, in regard to the earthquake which lately occurred in your neighborhood.

It will be interesting to determine the geographical limits of the disturbance, and to ascertain whether it was confined to any particular geological formation. If the direction of the shock was observed at a few places, the centre of commotion could be determined; and if the time were accurately known at different points, the velocity of the earth-wave could be calculated. Hence, an answer is requested to the following questions, viz:—

- 1. Was the agitation felt by yourself, or by any other person in your vicinity?
 - 2. What was the approximate time of the occurrence?
 - 3. What was the number, and duration, of the shocks?
 - 4. What was the direction of the motion?
- 5. What was the character of the disturbance? was it vertical, horizontal, or oblique? was it an actual oscillation? an upheaval and depression, or a mere tremor?
- 6. Was there any noise heard? and if so, what was its character?
- 7. Was the place of observation on soft ground, or on a hard foundation near the underlaying rocks of the district?

(46)

- 8. Were any facts observed having apparently an immediate or remote bearing on this phenomenon?
- 9. What was the intensity of the force in reference to producing motion in bodies and cracks in walls?

Nor.—Please reply to the *first* question, if to no other—for an answer to it is necessary, in order to determine the limits of the commotion.

The direction of the impulse may have been ascertained by observing the direction in which molasses, or any viscid liquid, was thrown up against the side of a bowl. The remains of the liquid on the side of a vessel would indicate the direction some time after the shock occurred.

INSTRUCTIONS FOR OBSERVATIONS

OF THE

AURORA.*

GENERAL REMARKS.

Though the aurora borealis has received attention during a considerable portion of the last two centuries, definite information is still wanting on several points which may serve as the basis of a sound induction as to its cause. These relate particularly to the actual frequency of the appearance of the meteor; its comparative frequency in the different months of the year and different hours of the day; the connection of the appearance of the meteor with other atmospherical phenomena; the elevation and extent of visibility of the arch; and whether the same or different phases are presented to individuals at different stations at the same moment of time; finally, the precise influence of the arches, streams, &c., on the magnetic condition of the earth; and whether any unusual electrical effects can be observed during the appearance of the meteor.

Auroral phenomena may be divided into the following classes:-

- 1. A faint light in the north, without definite form or boundary.
 - 2. A diffused light, defined by an arch below.
 - 3. Floating patches of luminous haze—sometimes striated.
- 4. One or more arches, resembling the rainbow, of uniform white color, retaining the same apparent position for a considerable time, and varying in luminosity.

^{*} These instructions are principally adopted from those used in the Observatory at Toronto, Canada.

- 5. A dark segment, appearing under the arch.
- 6. Beams, rays, streamers, waves, transverse and serpentine bands, interrupted or checkered arches, frequently tinged with color, and showing rapid changes in form, place, and color.
 - 7. Auroral corona, or a union of beams south of the zenith.
 - 8. Dark clouds accompanying the diffuse light.
 - 9. Sudden appearance of haze over the whole face of the sky.

The following may serve as a scale of brightness:-

1. Faint. 2. Moderate. 8. Bright. 4. Very bright.

GENERAL DIRECTIONS.

- 1. Make a regular practice of looking for auroras every clear evening, from 8 to 10 o'clock, or later. Record the result, whether there be an aurora or not.
- 2. Note the time of observation, and compare the watch used with a good clock, as soon after as is convenient.
 - 3. Make a return of the latitude and longitude of the station.
 - 4. Note the class to which the auroral phenomenon belongs.
- 5. If it be an arch, note the time when the convex side reaches any remarkable stars, when it passes the zenith, disappears, &c.
- 6. If the arch be stationary for a time, mark its position among the stars on the accompanying map, so that its altitude may be determined.
- 7. If it be a streamer or beam, mark its position on the map, and the time of its beginning and ending.
- 8. If motion be observed in the beams, note the direction, whether vertically or horizontally, to the east or west.
- 9. Note the time of the formation of a corona, and its position among the stars.
- 10. Note the time of the appearance of any black clouds in the north near the anrora; also, if the sky be suddenly overcast with a mist at any time during the auroral display.
 - 11. Give the direction and force of the wind at the time.
 - 12. Note if any electrical effects are observed.
- 13. Note the effect upon a delicately suspended magnetic needle.

USE OF THE MAP.*

- 1. To define the place and the extent of the aurora, the observer should familiarize himself with the relative position of the stars in the northern sky, by frequent inspection of the accompanying map, or a celestial globe.
- 2. Let the observer place the map before him, with the constellations in the positions in which they actually appear at the time of the observation. This may be done by holding up a plumb-line between the eye and the pole star, noticing the stars which it cuts; then a light pencil drawn through these stars and the pole on the map will be the centre of the heavens, or place of the meridian at the moment.
- 8. Mark carefully the place among the stars of the arch of the aurora, and show its width by parallel curved lines. Make a note of the time.
- 4. Draw a light curved line, following, as nearly as can be judged, the outline of the arch down to the horizon, on each side.
- 5. If the arch changes its position, mark its new places at intervals, noting the time of each observation.
- 6. Letter each position A, B, C, &c., and note the time and other particulars on the back or margin of the map, or in the register.
- 7. Beams or coruscations, or streamers of white or colored light, may be marked by lines at right angles to the above, with arrow heads pointing towards the place among the stars to which they tend, or where they would meet, if prolonged.
- 8. To aid in the estimation of angular distances the spaces between certain conspicuous stars have been marked on the map, which will furnish a scale to assist the eye, when actual measurement may be impracticable.
- 9. The course of brilliant meteors, when they fall within the portion of the heavens included on the map, may be marked by a line, the length of which will show the path of the meteor; the course should be indicated by an arrow, and the time recorded.

The map, when filled, together with any written observations,

^{*} Copies of the map will be furnished by the Institution.

may be returned to the Smithsonian Institution, indorsed Meteorology.

MAGNETIC APPARATUS.

Few observers will probably be furnished with a regular set of magnetical instruments. A temporary apparatus may, however, be fitted up at comparatively little expense and trouble. this purpose a steel plate, such as was used a few years since for ladies' busks, may be magnetized, and suspended edgewise in the vertical plane, by a few fibres of untwisted silk, in a box to prevent agitation by the air, furnished with a glass window on one side, through which observations may be made. the motions perceptible, a small mirror should be cemented on the side of the magnet opposite the window. In front of this mirror, and at the distance of ten or fifteen feet, an ordinary spyglass is fastened to a block, and under the glass, to the same block, a graduated scale, with arbitrary divisions marked upon it, is attached. The arrangement is such that the divisions of the scale may be seen through the telescope, reflected from the mirror, and consequently the slightest motion of the needle, and of the mirror cemented to it, gives a highly magnified apparent motion to the scale. The mirror may be formed of a flat piece of steel, highly polished by means of calcined magnesia; or, in default of a mirror of this kind, a piece of plate looking-glass may be employed, provided one can be procured sufficiently true. The suspension threads should be three or four feet long. instrument should not be placed very near large masses of iron, and care should be taken not to change the position of any articles of iron which are within the distance of fifteen or twenty feet, otherwise a change in the position of the needle will be produced. For a similar reason the box should be constructed without iron nails. The above described instrument will indicate changes in the direction of the magnetic meridian. similar instrument, deflected at right angles to the magnetic meridian by the torsion of two suspended threads, will furnish an apparatus for indicating changes of horizontal magnetic force.

ELECTRICAL APPARATUS.

To ascertain whether any change takes place in the electrical state of the atmosphere during the appearance of an aurora, the end of a long insulated wire, suspended from two high masts or two chimneys by means of silk threads, may be placed in connection with a delicate gold leaf electrometer. Any change in the electrical state of the atmosphere, simultaneous with the aurora, will be indicated by the divergence of the leaves. Two slips of gold-leaf attached by a little paste to the lower end of a thick wire, passing through a cork in a four-ounce vial, will answer for this purpose. The arrangement of the leaves will be best made by a bookbinder, who is expert in the management of gold-leaf.

[A continuous series of photographic registers of the motion of the magnetic needle is now kept up at the joint expense of the Coast Survey and this Institution, which will serve for comparison with any observations which may be made on the aurora.]

Prof. Olmsted, in a recent paper published by the Smithsonian Institution, classifies different auroras as follows:—

"Class I. This is characterized by the presence of at least three out of four of the most magnificent varieties of form, namely, arches, streamers, corona, and waves. The distinct formation of the corona is the most important characteristic of this class; yet, were the corona distinctly formed, without auroral arches or waves, or crimson vapor, it could not be considered as an aurora of the first class.

"CLASS II. The combination of two or more of the leading characteristics of the first class, but wanting in others, would serve to mark class the second. Thus the exhibition of arches and streamers, both of superior brilliancy, with a corona, while the waves and crimson columns were wanting, or of streamers with a corona, or of arches without a corona, without streamers or columns (if such a case ever occurs), we should designate as an aurora of the second class.

"CLASS III. The presence of only one of the more rare characteristics, either streamers or an arch, or irregular coruscations, but without the formation of a corona, and with but a

moderate degree of intensity, would denote an aurora of the third class.

"CLASS IV. In this class we place the most ordinary forms of the aurora, as a mere northern twilight, or a few streamers, with none of the characteristics that mark the grander exhibitions of the phenomenon."

The same author remarks:-

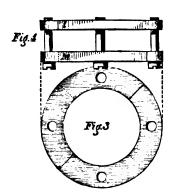
"On the evening of the 27th of August, 1827, after a long absence of any striking exhibition of the aurora borealis, there commenced a series of these meteors, which increased in frequency and magnificence for the ten following years, arrived at a maximum during the years 1835, 1836, and 1837, and, after that period, regularly declined in number and intensity until November, 1848, when the series appeared to come to a close. The recurrence, however, of three very remarkable exhibitions of the meteor in September, 1851, and of another of the first class as late as February 19th, 1852, indicates that the close was not so abrupt as was at first supposed; but still there was a very marked decline in the number of great auroras after 1848, and there has been scarcely one of the higher class since 1853.

"A review of the history of the foregoing series of auroras appears to warrant the conclusion that it constituted a definite period, which I have ventured to call the "Secular Period," having a duration of little more than twenty years; increasing in intensity pretty regularly for the first ten years, arriving at its maximum about the middle of this period, and as regularly declining during the latter half of the same period."

If this view be correct, it would appear that but few brilliant displays of the aurora may be expected for a number of years to come.

with the glass tube, indicates the temperature of the mercury in the barometer tube, not that of the external air. This central position of the thermometer is selected that the mean temperature of the whole column may be obtained; a matter of importance, as the temperature of the barometric column must be taken into account in every scientific application of its observed height.

The cistern (Fig. 2) is made up of a glass cylinder F, which allows the surface of the mercury q to be seen, and a top plate G, through the neck of which the barometer-tube t passes, and to which it is fastened by a piece of kid leather, making a strong but flexible joint. To this plate, also, is attached a small ivory point h, the extremity of which marks the commencement or zero of the scale above. The lower part, containing the mercury, in which the end of the barometer-tube t is plunged, is formed of two parts i j, held together by four screws and two divided rings l m, in the manner shown in the Figures 2, 3, and



4. To the lower piece j is fastened the flexible bag N, made-of kid leather, furnished in the middle with a socket k, which rests on the end of the adjusting-screw O. These parts, with the glass cylinder F, are clamped to the flange B by means of four long screws P and the ring R; on the ring R screws the cap S, which covers the lower parts of the cistern, and supports at the end the adjusting-screw P. P, and P, are of boxwood; the

other parts of brass or German silver. The screw O serves to adjust the mercury to the ivory point, and also, by raising the bag, so as to completely fill the cistern and tube with mercury, to put the instrument in condition for transportation.

In Fortin's barometer, and also Delcro's modification of it, a cement is used to secure the mercury against leakage at the joints. This, sooner or later, is sure to give way; and tested under the extremes of the thermometrical and hygrometrical range of this climate especially, has made this defect more evi-

This was removed by the substitution of iron in the place of wood; but it was soon found impracticable, in this form of cistern, to prevent damage from rust. These objections led to the present plan of construction, which effectually secures the joints The surfaces concerned are all without the use of any cement. made of a true figure, and simply clamped together by the screws, a very thin leather washer being interposed at the joints. This would not be permanent, however, but for the especial care taken in preparing the boxwood. The boxwood rings are all made from the centres of the wood, and concentric with its They are worked thin and then toughened, as well as growth. made impervious to moisture, by complete saturation with shel-This is effected by immersing them in a suitable solution The air being withdrawn from the pores of the wood, is replaced by the lac. This, however, with the after-drying or baking, requires care; but when properly done, the wood is rendered all but unchangeable.

Another peculiarity consists in making the scale adjustable to correct for capillarity, so that the barometer may read exactly

with the adopted standard, without the application of any correction; and this, too, without destroying the character of the barometer as an original and standard instrument. Near the 30 inches line, Figure 6, is a line v, on the main tube; this last line is distant exactly thirty inches from the tip of the ivory point; therefore, when these lines coincide, or make one line, the scale is in true measurement position; or the 30 mark is exactly thirty inches from the tip of the ivory point in the cistern. In this position, the amount of correction due to capillarity being ascertained, the scale is then moved that quantity and clamped firm. The barometer will now give the readings



corrected for capillarity, and thus avoid at once the labor of applying a correction, and the risk of error from an accidental neglect of it.

It must be borne in mind that this correction applies only to the particular tube, and while preserved in good condition.

If this tube is injured and again used, or another tube put in its place, the scale should then be moved until the lines coincide,

the amount of correction for the repaired or the new tube being estimated until a good comparison can be made directly or intermediately with the Smithsonian standard.

The connecting the parts i and j by rings and screws, Figs. 2, 3, and 4, rather than by a single screw cut on the edge, is an improvement, as the single wood-screw is apt, after a time, to adhere so firmly that it is often difficult, and sometimes impossible, with safety to the parts, to separate it.

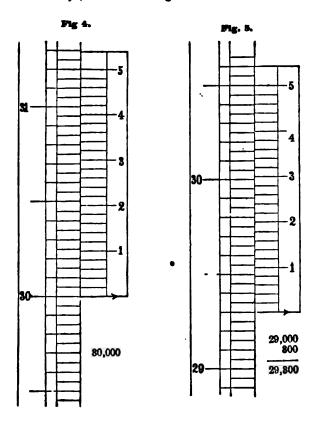
It is not advisable to disturb the cistern, unless it becomes difficult, from the oxide of mercury which gradually forms, to make the adjustment of the mercury to the ivory point, as there is more or less risk in doing so. Any one accustomed to such mechanical affairs, with due attention to the plan, can, however, take out the mercury from the cistern, refilter, clear the parts of adhering oxide, and replace them; the instrument all the time being kept vertical, with the cistern at top, as the mercury must not be allowed to come from the tube.

To insure a good vacuum by the complete expulsion of all air and moisture, the boiling of the mercury in the tube is done in vacuo; and care should be taken to preserve it in good condition.

To put up the barometer for observation, suspend the barometer by the ring A in a good light, near to and at the left side of a window, and, when practicable, in a room not liable to sudden variations of temperature. Record the temperature, and then, by the screw O, lower the mercury in the cistern until the surface is in the same plane with the extremity of the ivory point. As this extremity of the point is the zero of the scale, it is necessary, at each observation, to perfect this adjustment. It is perfect when the mercury just makes visible contact. If the surface is lowered a little, it is below the point; and if raised a small amount, a distinct depression is seen around the point. This depression is reduced to the least visible degree. A few trials will show that this adjustment can always be made to a thousandth of an inch.

The adjustment effected, bring the lower edge of the vernier C, Fig. 5, by means of the milled head D, into the same plane with the convex summit of the mercury in the tube. Looking through the opening, with the eye on a level with the top of the mercury in the tube, when the vernier tube is too low, the light

is cut off; when too high, the light is seen above the top of the mercury. It is right when the light is just cut off from the summit, the edge making a tangent to the curve. A piece of white paper placed behind, and also at the cistern, will be found to give a more agreeable light by day, and is, besides, necessary for night observations; the lamp being placed before the instrument and above the eye, to reflect the light.

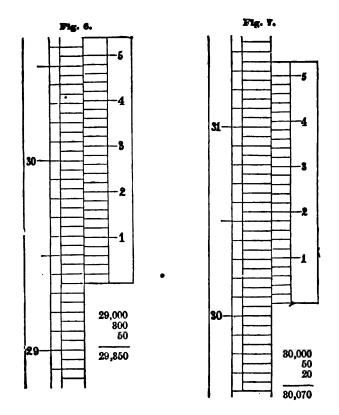


The method of reading off will perhaps be best explained by a few examples. Suppose, after completing the adjustments, the scale and vernier to be in the position shown in Fig. 4, on this page, it will be seen that the lowest or index line of the vernier coincides exactly with the line marked 30 on the scale. The reading, therefore, is 30.000 inches.

If, as in Fig. 5, we find the line of the vernier coinciding with the third line of the tenths above 29, we read 29.300.

If, as in Fig. 6, on this page, we find the index at 29 inches 8 tenths and 5 hundredths, we read 29.850.

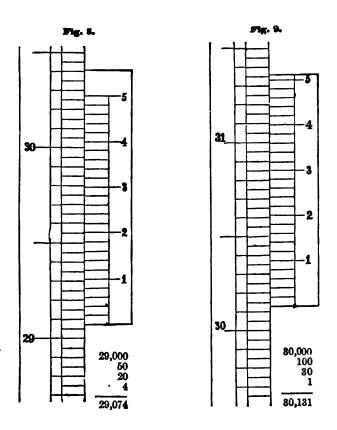
If, as in Fig. 7, we find the index at 30 inches no tenths 5 hundredths and something more, this additional quantity we



shall find by looking up the vernier scale, until we come to some one line on it, coinciding with a line on the other scale. In this instance it is the line marked 2, and indicates 2 hundredths, to be added to the other numbers, making 30.070.

If, as in Fig. 8, we find 29 inches no tenths 5 hundredths, and on the vernier the second line above that marked 2, is found to coincide with the scale, each of these short lines indicates 2

thousandths—consequently, are so counted; the reading s therefore 29.074.



Or it may be, as in Fig. 9, where we have 30 inches 1 tenth, and the line on the vernier mark 3 coinciding nearly, but not perfectly, with a line on the scale, it is a little too high; the 2 thousandth short line next above is, however, a like quantity too low; so the true reading must be the number between them—that is, 1 thousandth, making together 30.131.

These examples include all the combinations the scale allows. A little practice with the barometer, with reference to the examples, will soon enable the learner to read off the scale with facility. At first it will be best to write down the inches and

parts in full, as in the diagrams, not trusting the memory with the whole, until experience shall have given confidence.

Be careful never to lower the mercury in the cistern much below the necessary quantity, as it increases the risk of air entering the tube.

When the barometer is to be removed for transportation, or change of position, before taking it down, the mercury is to be screwed up until the cistern and tube are just full. If it is screwed more than this, the mercury may be forced through the joints of the cistern. It should then be inverted, and carried cistern-end upwards.

This instrument is well adapted for service as a mountain barometer, and when used as such, is packed in a leather case, with suitable straps for convenient carriage.

REGISTRY OF PERIODICAL PHENOMENA.

THE Smithsonian Institution, being desirous of obtaining information with regard to the periodical phenomena of animal and vegetable life in North America, respectfully invites all persons who may have it in their power, to record their observations, and to transmit them to the Institution. These should refer to the first appearance of leaves and of flowers in plants; the dates of appearance and disappearance of migratory or hybernating animals, as mammals, birds, reptiles, fishes, insects, &c.; the times of nesting of birds, of moulting and littering of mammals, of utterance of characteristic cries among reptiles and insects, and anything else which may be deemed noteworthy.

The Smithsonian Institution is also desirous of obtaining detailed lists of all the animals and plants of any locality throughout this continent. These, when practicable, should consist of the scientific names, as well as of those in common use; but when the former are unknown, the latter may alone be given. It is in contemplation to use the information thus gathered, in deducing general laws relating to the geographical distribution of species of the animal and vegetable kingdoms of North America. Any specimens of natural history will also be acceptable. Directions for their preservation have been published by the Institution, and will be sent to all who may wish them.

The points in the phenomena of plants, to which attention should be directed, are :—

- 1. Frondescence, or leafing.—When the buds first open and exhibit the green leaf.
 - 2. Flowering. When the anther is first exhibited :
 - a. In the most favorable location;
 - b. General flowering of the species.

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- 3. Fructification.—When the pericarp splits spontaneously in dehiscent fruits, or the indehiscent fruit is fully ripe.
 - 4. Fall of leaf.—When the leaves have nearly all fallen.

The dates of these various periods should be inserted in their appropriate columns.

When the observations for the year are complete, they should be returned to the Institution, with the locality and observer's name inserted in the blank at the head of the sheet.

PLANTS.

Elekat Manka	100000, Ang.	Flow	ering.	cation	ien.
List of Plants.	Prondescence or leafing.	a	b.	Fructification	Pall of
Acer rubrum, L.—Red, or soft maple. Acer dasycarpum, Khrh.—White, or silver maple. Acer saccharinum, L.—Sugar maple. Achillea millefolium, L.—Millefoil, or yarrow. Activa rubra, Willd.—Red baneberry. Activa alba, Bigelow.—White baneberry; necklace weed. Æsculus hippocastanum, L.—Horse chestnut. Æsculus glabra, Willd.—Ohio buckeye. Æsculus flava, Ait.—Yellow buckeye. Ailantus glandulosa.—Tree of heaven; ailanthus Amelanchier canadensis.—Shad bush; service berry. Amorpha fruticosa, L.—False indigo.					
Amygdalus nana, L.—Flowering almond Anemone nemorosa, L.—Wind flower; wood anemone Aquilegia canadensis, L.—Wild columbine Arctostaphylos uva-ursi, Spreng.—Bearberry Asclepias cornuti, Decaisne.—Milkweed Asimina triloba, Dunal.—Papaw Azalea nudiflora, L.—Common red honey- suckle Bignonia (Tecoma) radicans, Juss.—Trumpet creeper Castanea vesca, L.—Chestnut					·
Carya alba.—Shag-bark, or shell-bark hickory Cercis canadensis, L.—Red bud; Judas tree. Cerasus virginiana, DC.—Chokeberry. Cerasus serotina, DC.—Wild black cherry. Chionanthus virginica, L.—Fringe tree. Cimicifuga racemosa, Rll.—Black-snake root; rattlesnake root. Claytonia virginica, L.—Spring beauty. Clethra alnifolia.—White alder, or sweet pepper bush. Cornus florida, L.—Flowering dogwood* Cratægus crus-galli, L.—Cookspur thorn. Cratægus crus-galli, L.—Buglish hawthorn. Epigæ repens, L.—Trailing arbutus; ground laurel. Epilobium angustifolium, L.—Willow herb.					
Erythronium americanum, Smith.—Dog-tooth violet, or adder's tongue					

^{*} The time of the expansion of the real flower, not of the white involuces.

PLANTS-Continued.

List of Plants. Gaylussacia resinosa, Torr. and Gray.—Black huckleberry. Gerardia flava, L.—Yellow false foxglove. Geranium maculatum, L.—Crane's bill Halesia tetraptera, Willd.—Snow-drop tree Hepatica triloba, Chaix.—Round lobed liverwort Houstonia carulea, Hook.—Bluets; innocence, &co. Hypericum perforatum, L.—St. John's wort Iris versicolor, L.—Large blue flag Kalmia latifolia, L.—Mountain laurel Laurus benzoin, L.—(Benzoin odoriferum, Nees) Spice bush; Benjamin bush Leucanthemum vulgare, Lam.—Ox-eye daisy; white weed Linnae borealis, Gromov.—Twin flower Lobelia cardinalis, L.—Red cardinal flower Lonicera tartarica, L.—Foreign spurs Lupinus perehnis, L.—Wild lupine Liriodendron tulipifera, L.—Tulip tree; American poplar Magnolia glauca, L.—Small or laurel magnolis; sweet bay Mitchella repens, L.—Partridge berry Morus rubra, L.—Red mulberry Nymphea odorata, Ait.—Sweet-scented water lily Persica vulgaris, L.—Peach Podophyllum, L.—Mandrake; Mayapple Prontederia cordata, L.—Pickerel weed Pogonio ophioglossoides, Nutt.—Adder's tongue Pyrus communis, L.—Common pear-tree Pyrus malus, L.—Common spple-tree Quercus alba, L.—White oak Rhododendron maximum, L.—Great laurel Ribes rubrum, L.—Currant Robinia pseud-acacia, L.—Common locust Robinia viscosa, Vent.—Clammy locust Rubus villosus, Ait.—Black elder Sambucus canadensis, L.—Common elder Sambucus canadensis, L.—Black elder Sanguinaria canadensis, L.—Blood root. Sarracenia purpurea, L.—Side-saddle flower Saxifraga virginiensis, Michx.—Rarly saxi-	PLAN 15—Continued.	8	Flow	ering.	on.	
Gaylussacia resinosa, Torr. and Gray.—Black huckleberry. Gerardia flava, L.—Yellow false foxglove. Geranium maculatum, L.—Crane's bill Halesia tetraptera, Willd.—Snow-drop tree Hepatica triloba, Chaix.—Round lobed liverwort Houstonia carulea, Hook.—Bluets; innocence, &c. Hypericum perforatum, L.—St. John's wort Hris versicolor, L.—Large blue flag Kalmia latifolia, L.—Mountain laurel Laurus benzoin, L.—Genzoin odoriferum, Nees) Spice bush; Benjamin bush Leucanthemum vulgare, Lam.—Ox-eye daisy; white weed Linnæa borealis, Gronov.—Twin flower Lobelia cardinalis, L.—Red cardinal flower Lobelia cardinalis, L.—Wild lupine Lurinodendron tulipifera, L.—Tulip tree; American poplar Magnolia glauca, L.—Bamall or laurel magnolia; sweet bay Mitchella repens, L.—Partridge berry Morus rubra, L.—Red mulberry Mymphæa odorata, Ait.—Sweet-scented water lily Persica vulgaris, L.—Peach Poontederia cordata, L.—Pickerel weed Pogonio ophioglossoides, Nutt.—Adder's tongue Pyrus communis, L.—Common paple-tree Quercus alba, L.—White oak Rhododendron maximum, L.—Great laurel Ribes rubrum, L.—Common locust Robinia viscosa, Vent.—Clammy locust Robinia pseud-acacia, L.—Common elder Sambucus canadensis, L.—Black elder Sambucus nigra, L.—Black elder Sanguinaria canadensis, L.—Blood root Saracenia purpurea, L.—Side-saddle flower	List of Plants.	Prondescer or leafing			Fructification.	Pall of 10sf
frage Smilacina bifolia, Ker.—Two-leaved Solomon- seal Syringa vulgaris, L.—Lilac Taraxacum dens-leonis, Desf.—Dandelion Tilia americana, L.—Bass wood; American lime, or linden	nuckleberry. Gerardia flava, L.—Yellow false foxglove. Geranium maculatum, L.—Crane's bill Halesia tetraptera, Willd.—Snow-drop tree Hepatica triloba, Chaix.—Round lobed liverwort Houstonia cærulea, Hook.—Bluets; innocence, &c. Hypericum perforatum, L.—St. John's wort Iris versicolor, L.—Large blue flag Kalmia latifolia, L.—Mountain laurel Laurus benzoin, L.—(Benzoin odoriferum, Nees) Spice bush; Benjamin bush Leucanthemum vulgare, Lam.—Ox-eye daisy; white weed Linnæa borealis, Gromov.—Twin flower Lobelia cardinalis, L.—Red cardinal flower Lobelia cardinalis, L.—Foreign spurs Lupinus perennis, L.—Wild lupine Liriodendron tulipifera, L.—Tulip tree; American poplar Magnolia glauca, L.—Small or laurel magnolia; sweet bay Mitchella repens, L.—Partridge berry Morus rubra, L.—Red mulberry Morus rubra, L.—Red mulberry Morus rubra, L.—Red mulberry Morus rubra, L.—Red mulberry Persica vulgaris, L.—Peach Podophyllum, L.—Mandrake; Mayapple Pontederia cordata, L.—Pickerel weed Pogonio ophioglossoides, Nutt.—Adder's tongue Pyrus communis, L.—Common pear-tree Pyrus malus, L.—Common apple-tree Quercus alba, L.—White oak Rhododendron maximum, L.—Great laurel Ribes rubrum, L.—Currant Robinia pseud-acacia, L.—Common locust Robinia viscosa, Vent.—Clammy locust Robinia pseud-acacia, L.—Common elder Sambucus canadensis, L.—Black elder Sanguinaria canadensis, L.—Blood root Sarracenia purpurea, L.—Black elder Sarginaria canadensis, L.—Blood root Sarracenia purpurea, L.—Black elder Sarifraga virginiensis, Michx.—Rarly saxifrage Smilacina bifolia, Ker.—Two-leaved Solomon- seal Syringa vulgaris, L.—Lilac Taraxacum dens-leonis, Desf.—Dandelion Tilia americana, L.—Bass wood; American	Pr-			Fr	TV d.

BIRDS

Birds.	Arrival in spring.	Commencement of nesting.	Commencement of incubation	Appearance of young.	Departure in Automo.
Acanthylis pelasgia, Boie.—Chimney-bird . Agelaius phaniceus, L.—Red-winged blackbird Anser canadensis, L.—Wild goose Hirundo purpurea, L.—Martin . Hirundo rufa, L.—Barn swallow . Pandion carolinus, Gm.—Fish-hawk . Quiscalus ferrugineus, L.—Rusty blackbird . Quiscalus versicolor, L.—Crow blackbird . Sialia wilsonii, Sw.—Blue-bird . Turdus migratorius, L.—Robin . Tyrannula fusca, Sw.—Pewee . Dolichonyx oryzivora, Sw.—Reed-bird, rice-bird, boblink . Mimus felivox, Sw.—Cat-bird . Tyrannus intrepidus, Vieill.—Ring-bird . Troglodytes aedon.—House wren . Antrostomus vociferous.—Whippowill .		•			

REPTILES—first appearance, cries, and general peculiarities of habits.

Bufo americanus, and other species of toads.

Rana, the various kinds of frogs.

Hyla and Hylodes, the several kinds of tree-frogs.

Turtles, lizards, snakes.

FISHES-first appearance and spawning.

Salmo salar, L., salmon.
Alosa, shad.
Clupea, herring.
Anguilla, eel.
Acipenser, sturgeon.

INSECTS—their first appearance and cries.

Platyphyllum concavum, Harr., catydid. Cicada, locusts—the several kinds Ecanthus niveus, Harr., tree-crickets Grasshoppers, in their variety. Fire-flies.

GENERAL PHENOMENA OF CLIMATE.

Phenomena of a general character, of which the date of appearance cannot be mistaken, are very valuable. Series of years have in some cases been carefully observed, which would greatly add to the value of the current record, if forwarded with it. The following are of this class:—

- 1. Breaking up of ice in large rivers or bays.
- 2. Date of greatest rise and lowest fall of water in large rivers, especially when periodic, as in parts of the interior.
- 3. General leading and fall of leaf in deciduous forests. In most parts of the North and interior these are well marked and easily designated periods.
- 4. Commencement of growth and the end of growth or destruction of grasses in general; as on plains or prairies.
- 5. First growth, flowering, and maturity, of important annual staples, with their period in days from the commencement to the end of vital action.

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Wet and dry bulb thermometer, 8. Whirlwinds, 32. Winds, 25, 26, 33, 38, 45. Wind-vane, 24, 25.

Psychrometrical Table:

FOR DETERMINING THE

ELASTIC FORCE OF AQUEOUS VAPOR

AND THE

RELATIVE HUMIDITY OF THE ATMOSPHERE

FROM

INDICATIONS OF THE WET AND THE DRY-BULB THERMOMETER FAHRENHEIT.

وشه الداء الداري

BY

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WASHINGTON:
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1856.

THE following table is based on the formulæ of Reginault, as used by Prof. Guyot, in the preparation of his Psychrometrical Tables, for the Smithsonian Institution viz.:—

$$x = f - \frac{.480 (t - t')}{610 - t'} h$$
, for temperatures above the freezing-point,

and
$$x = f - \frac{.480(t-t')}{689-t'}h$$
, for those below;

in which h represents the height of the barometer, t the temperature indicated by the dry bulb centigrade thermometer, t that indicated by the wet bulb thermometer, t the elastic force of aqueous vapor in a saturated air at the temperature t, and x the actual force at the time of the observation.

Adapting these formulæ to the Fahrenheit thermometer, the former will read

$$x = f - \frac{.480 \times \frac{6}{9} (t - t')}{610 - \frac{6}{9} (t' - 32)} h = f - \frac{.480 (t - t')}{1130 - t'} h,$$

and the latter,

$$x = f - \frac{.480 \times \frac{6}{9}(t-t)}{689 - \frac{6}{9}(t-32)} h = f - \frac{.480(t-t')}{1240.2 - t'} h.$$

If we put h = 755 millimetres, = 29,725 English inches, these formulæ may be reduced for the latter measure to the following forms:—

$$x=f-\frac{14.268(t-t')}{1130-t'}$$
; and $x=f-\frac{14.268(t-t')}{1240.2-t'}$.

In using the table, look out the degree of the wet-bulb thermometer at the top, and the difference between the wet and dry bulb thermometers at the left. Under the former and opposite the latter, find, in their appropriate columns, the force of vapor, and the relative humidity.

i		1	n.	eanwa /	AP 707	W 100 D	TI D ST	BRMOMI	W. T.	, A 11 10 10 10 10 10 10 10 10 10 10 10 10	7 WT#		
	abeit.							1				l .	
	Pabre		1°		10°				8°		170		16°
	t — t' Fabrenheit,	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in Inches.	Relative Humidity.	Force of Vapor, in inches	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in Inches.	Relative Humidity.
	0° 1 1	-011 -006	100 50 2	-012 -006 -001	100 52 6	-012 -007 -001	100 54 9	-018 -007 -002	100 55 12	-018 -008 -002	100 57 16	-014 -008 -008	100 59 19
	alt.		10 1	EGREES	OF TH	e wet	BULB 1	THERMO:	METER	yahri	NHEIT		
	hronh	-2	5°	-2	4°	<u>-</u> 9	8°	9	33°	- 2	31°	-2	30°
	t — V Fahrenbelt.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Fare of Vapor, in inches.	Relative Humidity.
	0° 1 1 1 1 1 2	-015 -009 -008	100 60 22	-015 -010 -004	100 62 25	-016 -010 -005	100 68 28	-017 -011 -005	100 64 80	-017 -012 -006	100 66 88 1	-018 -012 -007 -001	100 67 85 5
	aft.	DEGREES OF THE WET BULB THERMOMETER.—FA							—Pahri	en Heit			
	ahrenh	-1	9 °	_1	8°	-1	70	_1	6 °	-1	15°	-1	4°
	t — Y Fahrenheit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Pures of Vapor, in Inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
	0° 1 1 1 1 2 2	-019 -018 -007 -002	100 69 87 9	-020 -014 -008 -008	100 70 40 12	-021 -015 -009 -008	100 71 48 16	-022 -016 -010 -004	100 72 45 19	+028 +017 +011 +005	100 78 47 28	-024 -018 -012 -006 -001	100 74 49 26 8
=	elt.		Di	EGREES	OF TH	e wer :	BULB 1	HERMOI	eter.	—yahri	NHEIT	•	
	Fabrenbelt.	-1	8°	-1	2°	1	11°	_1	0 °		D°		80
	t-v1	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
	0° 1 1 1 1 1 2 2 1 2 1 2 1	-025 -019 -018 -007 -002	100 75 51 29 6	-026 -020 .014 -009 -008	100 76 58 81 10	-027 -021 -015 -010 -004	100 77 55 84 18	-028 -022 -017 -011 -005	100 78 57 86 17	-029 -024 -018 -012 -006 -001	100 79 58 89 20 2	-081 -025 -019 -013 -008 -002	100 80 60 41 28 6

¥.		;	DBGREE	3 OF T	HB WEI	BULB	THERM	OMETE	R.—JAHI	RENHE	rr.	
abrenbe		7°		8°		9°		4°	_	B°	_:	3°
t - t' Fabrenbelt.	Force of Vapor, in Inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0° 1 1 11 2 2 21 3	-082 -026 -021 -015 -009 -008	100 80 62 43 26 10	-088 -028 -022 -016 -011 -005	100 81 68 46 29 18	-085 -029 -024 -018 -012 -006 -001	100 82 65 48 82 17 2	-066 -081 -025 -019 -014 -008 -002	100 83 66 50 84 20 5	-088 -082 -027 -021 -015 -010 -004	100 83 67 52 87 28 9	-040 -084 -028 -028 -017 -011 -006	100 84 68 58 89 26 12
4)	BGREES	OF TE	IE WET	BULB	THERMO	METER	.—yahr	BNHEP	E.	
- V Fahrenbeit.	1	٥	4	0								
t - 4 F	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in Inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0° 1 1 1½ 2 2½ 8½ 4	-042 -036 -080 -025 -019 -018 -008 -002	100 84 69 55 42 28 16 4	-044 -088 -082 -026 -020 -015 -009 -008	100 85 70 56 48 80 18 6	-046 -040 -034 -028 -022 -017 -011 -005	100 85 71 57 45 82 21 9	-048 -042 -086 -080 -024 -019 -018 -007 -001	100 86 72 59 47 85 28 12 2	-050 -044 -038 -082 -027 -021 -015 -009 -008	100 86 78 60 49 87 26 15 6	-052 -046 -041 -085 -029 -028 -017 -012 -006	100 87 74 61 51 89 29 19
		D	EGREES	OF TE	e wet	BULB	THERMO	METER	.—PAHR	enhet	r.	
hrenhe	5	•	6	•	7	•	8	•	8	0	10)°
t — V Fahrenheft.	Porce of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0° 1 1 1 2 2 2 2 4 4 4 5 5 1	-055 -049 -048 -087 -081 -026 -020 -014 -008 -002	100 87 76 62 52 42 82 22 18 4	-067 -051 -045 -040 -084 -028 -022 -017 -011 -005	100 87 76 64 54 44 85 25 16 7	-060 -054 -048 -042 -086 -081 -025 -019 -018 -007 -002	100 88 77 66 56 46 87 27 19 10 2	062 -057 -051 -045 -089 -088 -028 -022 -016 -010 -004	100 88 77 68 57 48 89 80 21 13 6	-065 -059 -054 -048 -042 -086 -080 -025 -019 -018 -007 -001	100 89 78 69 59 49 41 82 24 16 9	-068 -062 -057 -051 -045 -089 -088 -028 -022 -016 -010	100 89 79 70 60 51 48 84 27 19 12

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i i		1	MGREES	OF TE	IB WET	BULB	THURMO	MITER	.—7ARR	ENHE!	ľ.	, ===
t — V Pahrenhedt.	11	lo	19	P	18	0	14	0	14	0	16	80
4	Force of Vapor, in Inches.	Relative Humbility.	Force of Vapor, in inches.	Rolative Humidity.	Force of Vapor, in inches.	Relative Humldity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidiky.	Force of Vapor, in inches.	Relative Humidity.
0° 1 1 1 1 2 2 2 2 3 3 4 4 4 5 5 1 6 6 2 7 7 1 2	-071 -066 -060 -054 -042 -087 -081 -025 -013 -007 -002	100 90 80 71 62 63 45 87 29 22 15 8	-075 -069 -068 -057 -046 -040 -084 -028 -028 -017 -011 -005	100 90 81 72 63 65 46 89 81 24 18 11 5	-078 -072 -067 -061 -049 -043 -088 -032 -026 -020 -014 -008 -008	100 91 81 78 64 56 48 41 84 27 20 18 8	-082 -076 -070 -065 -058 -047 -041 -036 -036 -030 -024 -018 -012 -006 -001	100 91 82 74 65 58 50 48 86 29 28 17 11 6	-086 -080 -074 -068 -068 -057 -051 -045 -039 -084 -028 -022 -016 -010 -004	100 91 83 76 67 59 52 45 88 82 25 20 14 9	090 -084 -078 -072 -067 -061 -055 -049 -043 -038 -032 -026 -020 -014 -008	100 91 88 76 68 60 53 47 40 84 28 22 17 12 7
t t' Fabrenheit.		1	EGRENS	OF TE	LE WET	BULB	THERMO	METER	PAHR	enher	r.	
Yahr.	17		18		18		20)°	21		22	
1 +	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0° 1 1 1 1 2 2 1 8 3 2 4 4 1 5 5 6 6 1 7 7 1 8 8 1 9 9 1 1	-094 -088 -082 -077 -071 -065 -059 -058 -042 -086 -030 -024 -018 -012 -007 -001	100 92 84 76 69 62 55 48 42 86 81 25 20 15 10	-098 -098 -087 -081 -075 -069 -064 -058 -052 -046 -040 -034 -028 -023 -017 -005	100 92 84 77 70 63 56 50 44 88 88 27 22 17 12 8	-108 -097 -091 -085 -080 -074 -068 -062 -051 -044 -089 -089 -027 -021 -015 -010	100 92 85 78 71 64 58 52 46 40 85 29 24 20 15 11 7	-108 -102 -096 -090 -084 -079 -078 -067 -061 -055 -049 -048 -032 -026 -020 -014 -009 -008	100 92 85 78 71 65 59 53 47 42 87 81 27 22 17 18 9 5	-118 -107 -101 -095 -089 -088 -077 -071 -066 -060 -054 -042 -037 -031 -025 -019 -018 -007	100 98 86 79 72 66 60 54 49 43 89 84 29 24 20 16 12 8	-118 -112 -106 -100 -094 -088 -082 -077 -071 -065 -059 -058 -048 -048 -048 -024 -012 -006	100 98 86 79 78 67 61 56 51 40 86 81 27 22 18 14

sett.		D	DGR BES	OF TE	OF WEST	BULB '	THERMO	METER	PAHRI	en H bit	·.	
t' Fabrenbeit.	28	go .	24	l°	25	0	20	80	. 21	ro	28	90
t-t/1	Force of Vapor, in inches.	Relative Humidity.										
0° 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	·128 ·117 ·111 ·105	100 98 86 80	·129 ·128 ·117 ·111	100 98 87 81	-185 -129 -128 -117	100 98 87 82	·141 ·185 ·129 ·128	100 98 88 82	·147 ·141 ·185 ·129	100 98 88 82	·153 ·147 ·142 ·186	100 94 88 83
2 2 2 3 8	·100 ·094 ·088 ·082	74 68 62 57	-105 -099 -098 -088	75 69 68 58	·111 ·105 ·099 ·098	75 70 64 59	·117 ·111 ·105 ·099	76 71 66 61	128 -117 -111 -106	77 72 67 62	·130 ·124 ·118 ·112	78 78 68 68
4 41 5 51	-076 -070 -065 -059	52 47 42 87	-082 -076 -070 -064	58 48 44 89	-087 -082 -076 -070	54 50 45 41	-098 -088 -082 -076	56 51 47 48	-100 -094 -088 -082	57 58 49	106 ·100 ·094 ·089	58 54 50 46
6 61 7 71	-058 -047 -041 -085	88 29 25 21	-058 -058 -047 -041	85 81 27 28	-064 -058 -052 -046	87 88 29 25	-070 -064 -058 -052	89 85 81 27	-076 -070 -064 -069	40 87 88 29	-088 -077 -071 -065	42 88 85 81
8 81 9	-029 -028 -017 -011	17 18 10 6	-085 -029 -028 -017	19 15 12 9	-041 -085 -029 -028	21 18 14 11	-047 -041 -085 -029	24 20 17 14	-058 -047 -041 -035	26 22 19 16	-059 -058 -047 -041	28 24 21 18
10 101 11 111	-006	8	-012 -006	6 8	-017 -011 -005	8 5 2	-028 -017 -011 -005	11 8 5 2	-029 -028 -017 -011	18 10 8 5	-086 -080 -024 -018	15 18 10 7
12 121									-006	2	-012 -006	5 2

belt.		1	BORERS	OF TE	ib wet	BULB	THERMO	MUTE	.—yaha	enhei	r.	
	25	°	. 80)°	81	lo	82	B°	88	Bo.	84	ļ°
-	Force of Vapor, in Inches.	Belative Humidity.	Force of Vapor, in Inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in Inches.	Relative Humbdity.	Force of Vapor, in inches.	Belative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0° 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	·160 ·154 ·148 ·142	100 94 89 84	·167 ·161 ·155 ·149	100 95 89 84	-174 -168 -162 -156	100 95 89 85	·181 ·175 ·168 ·162	100 94 89 84	188 182 175	100 95 89 84	-196 -190 -188 -177	100 95 90 85
2 21 8 81	-186 -130 -125 -119	78 74 69 64	·148 ·187 ·181 ·126	79 74 70 65	·150 ·144 ·188 ·188	80 75 71 66	·155 ·149 ·142 ·186	79 74 70 65	-162 -156 -149 -148	80 75 71 66	·170 ·164 ·157 ·151	80 76 71 67
4 41 5 51	·118 ·107 ·101 ·095	60 56 51 48	·120 ·114 ·108 ·102	61 57 58 49	·127 ·121 ·115 ·109	62 58 54 51	·129 ·128 ·116 ·110	61 67 58 49	·186 ·180 ·128 ·117	62 58 54 50	·144 ·188 ·181 ·124	68 59 55 51
6 6 <u>1</u> 7 7 <u>1</u>	-089 -088 -077 -072	44 40 86 88	-096 -090 -084 -078	45 42 88 85	-108 -097 -091 -085	47 48 40 87	-108 -097 -090 -084	45 41 88 84	-110 -104 -097 -091	46 48 89 86	·118 ·111 ·105 ·098	48 44 41 87
8 <u>1</u> 9 9 <u>1</u>	-066 -060 -064 -048	26 28 21	+072 +067 +061 +065	82 28 25 23	-079 -074 -068 -062	84 80 27 25	-077 -071 -064 -058	81 28 25 22	-084 -078 -071 -065	88 80 27 24	-092 -085 -079 -072	84 81 28 26
10 101 11 111	-042 -036 -080 -024	18 15 12 10	-049 -048 -087 -081	20 17 14 12	-056 -050 -044 -088	22 19 17 14	-051 -045 -088 -082	19 16 14 11	-058 -052 -045 -089	21 18 16 18	-066 -059 -058 -046	28 20 18 15
12 12 1 18 18	-019 -013 -007 -001	7 5 2 0	-025 -019 -018 -008	9 7 5 8	-032 -026 -020 -015	12 10 7 5	-025 -019 -012 -006	9 6 4 2	-082 -026 -019 -018	11 8 6 4	-040 -088 -027 -020	18 11 8 6
14 14 <u>1</u> 15			-002	1	-008 -009	8	•••••	*****	-006	2	-014 -007 -001	4 2 0

4		I	obgreis	OF TH	IB WBT	BULB	THERMO	Merer	.—Pahr	ENHEL	r.	
hhren	88	,°	84	30	81	Yo	86	90	· 84	°	44	P°
t — t' Pabrenbelt.	Force of Vapor, in inches.	Belative Humidity.	Force of Vapor. in inches.	Relative Humidity.	Force of Tapor, in Inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Fores of Vapor, in inches.	Relative Humidity.	Force of Vapor, in Inches.	Relative Humidity.
0° 1 1 1 1 2 2 2 2 3 8 4 4 1 5 5 5 1 6 6 1 1 1 1 1 1 1 1 1 1 1 1 1	-204 -197 -191 -184 -178 -171 -165 -158 -152 -145 -189 -182 -126 -119 -113 -106 -100 -098 -087 -080 -074 -067 -061 -054 -048 -041 -085 -028 -022	100 95 90 85 81 76 72 68 68 69 56 52 49 45 42 89 86 88 80 27 25 22 19 17 16 18 10 8	212 206 199 186 180 178 167 167 160 154 147 140 118 108 101 108 101 108 108 109 108 108 108 108 108 108 108 108 108 108	100 95 90 86 81 77 78 68 64 61 57 58 50 47 43 40 87 82 29 26 24 21 19 16 14 12 10 8 8	-221 -214 -208 -201 -195 -188 -182 -175 -162 -155 -149 -142 -187 -180 -124 -117 -108 -097 -090 -068 -077 -061 -044 -081 -025 -018 -012	100 95 91 86 82 777 78 69 65 61 58 54 45 42 89 86 88 80 28 25 20 18 16 14 12 10 8 8	229 -228 -216 -210 -208 -197 -190 -184 -177 -171 -164 -157 -151 -144 -188 -181 -125 -118 -112 -105 -099 -092 -086 -079 -078 -066 -060 -058 -047 -040 -083 -027 -020 -014	100 95 91 86 82 78 70 66 62 59 55 52 49 46 48 48 22 29 27 24 22 20 18 16 14 12 10 8 7	-288 -282 -225 -219 -212 -206 -198 -186 -180 -173 -166 -160 -152 -146 -189 -183 -120 -113 -107 -101 -004 -068 -062 -055 -049 -029 -029 -029 -020 -016 -010	100 95 91 87 82 78 74 71 67 68 60 56 58 50 47 44 41 89 86 88 81 28 24 22 19 17 15 14 12 10 9	-248 -241 -285 -228 -222 -215 -209 -189 -182 -176 -169 -163 -156 -150 -143 -157 -110 -104 -078 -071 -084 -078 -071 -085 -088 -088 -088 -088 -088 -088 -088	100 95 91 87 88 79 75 71 68 64 61 67 54 48 46 48 40 87 85 82 82 82 82 81 19 17 16 16 17 18 19 10 10 10 10 10 10 10 10 10 10
18 18]									-008	1	-012 -006	8

elt.		1	degrees	OF 17	HE WET	BULB	THURMO	Meter	.—FAHR	en hei'	r.	
. — t' Fabroabelt.	41	lo	49	B ₀	48	°	44	lo	48	50	40	3°
1	Yapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in Inches.	Relative Humidity.	Porce of Vapor, in inches.	Relative Humidiky.	Force of Vapor, in inches.	Relative Humidity.
0° 1 11 2 21 8 81 4 41 5 5 1 6 61 7 7 1 8 81 1 1 1 1 1 1 1 1 1 1 1 1 1 1	+257 -257 -244 -237 -224 -218 -218 -219 -192 -185 -179 -172 -165 -159 -152 -146 -139 -120 -118 -120 -118 -120 -118 -106 -100 -098 -087 -067 -064 -048 -044 -048 -044 -048 -049 -048 -049 -048 -049 -048 -049 -048 -049 -048 -049 -048 -049 -048 -049 -048 -049 -048 -049 -048 -049 -048 -049 -048 -049 -048 -049 -048 -049 -048 -049	100 96 91 87 88 76 72 68 65 62 58 55 52 49 47 44 41 89 86 84 81 29 27 26 21 19 17 15 18 19 19 19 19 19 19 19 19 19 19 19 19 19	-267 -267 -261 -254 -248 -241 -284 -228 -221 -215 -208 -202 -195 -189 -162 -166 -149 -142 -186 -110 -108 -007 -090 -088 -077 -071 -044 -088 -031 -044 -088 -031 -044 -038	100 96 92 88 84 80 76 72 69 66 62 59 56 53 50 48 45 42 40 87 85 83 80 28 22 20 19 17 15 18 10 99 76 66 86 87 87 88 88 88 88 88 88 88 88 88 88 88	-278 -271 -265 -258 -251 -245 -245 -225 -218 -212 -205 -199 -178 -166 -159 -178 -166 -158 -140 -188 -127 -120 -118 -120 -118 -107 -100 -094 -087 -088 -048	100 96 92 88 84 80 77 78 66 63 60 57 54 48 41 89 86 84 48 41 89 86 82 80 28 80 28 17 15 16 16 16 17 18 18 18 18 18 18 18 18 18 18	-289 -282 -275 -269 -282 -256 -249 -242 -288 -216 -210 -203 -196 -190 -183 -177 -170 -168 -157 -151 -144 -187 -181 -124 -088 -071 -085 -072 -065 -058 -058	100 96 92 88 84 81 77 74 70 67 64 61 58 56 52 40 47 45 42 40 88 83 81 29 27 22 20 18 17 15 18 19 19 19 19 19 19 19 19 19 19 19 19 19	-800 -298 -286 -280 -276 -267 -260 -258 -247 -221 -214 -208 -201 -194 -188 -181 -176 -162 -155 -148 -142 -135 -129 -122 -115 -109 -1026 -069 -069 -069 -066 -049	100 96 92 88 85 81 78 74 71 68 65 62 59 56 53 51 48 46 48 41 89 87 84 41 82 22 28 21 20 18 17 15 14 12 11 10 8	*811 *805 *298 *291 *265 *278 *272 *265 *252 *245 *289 *212 *206 *199 *118 *166 *160 *179 *178 *166 *160 *188 *147 *140 *188 *127 *120 *114 *107 *101 *108 *107 *101 *106 *107 *101 *106 *107 *101 *106 *107 *101 *106 *107 *101 *106 *107 *107 *101 *106 *107 *107 *101 *106 *107 *107 *107 *107 *107 *108 *109	100 96 92 89 85 81 76 71 68 65 63 60 57 54 42 49 47 44 42 40 88 86 84 82 28 28 21 20 18 16 16 11 11
19½ 20 20½ 21 21½ 22 22½ 23 28½	H001	0	-911 -905	2	-021 -015 -009 -002	4 2 1 0	-082 -026 -019 -018 -008	5 4 2 2 1	-048 -087 -080 -028 -017 -010 -004	7 6 5 4 8 2 1	-064 -048 -041 -085 -028 -022 -015 -008 -002	9 7 6 5 4 8 2

			BGREES	OF TH	E WET	BULB '	THERMO	METER	PAHRI	ENHEIT	·	
— f' Fabruchett.	47	ro	48	30	48	0	50	90	51	l°	52	. <u>——</u> ;•
[A-t	Force of Vapor, in inches.	Relative Humidity.										
0° 1	-828 -816 -810	100 96 92	•885 •829 •822	100 96 92	-848 -841 -885	100 96 98	-861 -854 -848	100 96 98	-874 -868 -861	100 96 98	-888 -882 -875	100 96 98
11 2 21 8	-808 -297 -290 -288	89 85 82 78	·815 ·809 ·802 ·296	89 85 82 79	-828 -821 -815 -808	89 86 88 79	-841 -834 -828 -821	89 86 83 80	-854 -848 -841 -885	90 86 88 80	-869 -862 -855 -849	90 87 84 81
84 4 43	-277 -270 -264	75 72 69	·289 ·282 ·276	76 78 70	802 295 288	76 78 70	-815 -808 -801	77 74 71	-828 821 -815	77 74 71	-842 -886 -829	78 75 72
5 51 6	257 -251 -244	66 68 60	·269 ·268 ·256	67 64 61	·282 ·275 ·269	67 65 62	·295 ·288 ·282	68 65 68	-808 -802 -295	69 66 68	-822 -816 -809	69 67 64
6 <u>1</u> 7 7 <u>1</u> 8	·287 ·281 ·224 ·218	58 55 52 50	·249 ·248 ·286 ·280	59 56 58 51	·262 ·255 ·249 ·242	59 57 54 52	·275 ·268 ·262 ·255	60 58 55 58	·288 ·282 ·275 ·269	61 58 56 54	-802 -296 -289 -288	61 59 57 54
9 1 9 8 <u>1</u>	·211 ·204 ·198	48 45 48	·228 ·216 ·210	· 46 44	·286 ·229 ·222	50 47 45	·249 ·242 ·285	51 48 46	·262 ·255 ·249	51 49 47	·276 ·269 ·268	52 50 49
10 10 <u>1</u> 11 11 <u>1</u>	·191 ·185 ·178 ·171	89 87 85	·208 ·197 ·190 ·188	42 40 88 86	·216 ·209 ·208 ·196	48 41 89 87	229 222 216 209	44 42 40 88	·242 ·285 ·229 ·222	45 48 41 89	-256 -249 -248 -286	46 44 42 40
12 121 18 181	·165 ·158 ·152 ·145	88 81 29 27	·177 ·170 ·164 ·157	84 82 80	-189 -183 -176	85 88 82 80	·202 ·196 ·189 ·182	86 85 88	·216 ·209 ·208	87 86 84	-280 -228 -216	88 87 85
14 14 14 15	·188 ·132 ·125	26 24 22	·150 ·144 ·187	29 27 25 24	·170 ·168 ·156 ·150	28 27 25	·176 ·169 ·168	29 28 26	·196 ·189 ·188 ·176	82 81 29 27	·210 ·208 ·197 ·190	88 82 80 29
15½ 16 16½ 17	·119 ·112 ·106 ·099	21 19 18 16	·181 ·124 ·118 ·111	22 21 19 18	·148 ·187 ·180	28 22 21 19	·156 ·149 ·148 ·186	25 28 22	·169 ·168 ·156	26 25 28	-188 -177 -170	27 26 24
17 <u>1</u> 18 18 <u>1</u>	-092 -086 -079	15 14 12	-104 -098 -091	16 16 16	-128 -117 -110 -104	18 17 15	·180 ·128 ·116	21 19 18 17	-150 -148 -186 -130	22 20 19 18	-168 -157 -150 -144	28 22 20 19
19 19 <u>1</u> 20	-078 -066 -059	11 10 9	-085 -078 -071	18 11 10	-097 -090 -084	14 18 12	·110 ·108 ·097	15 14 18	·128 ·117 ·110	17 16 14	-187 -180 -124	18 17 16
201 21 21 211 22	-053 -046 -040 -088	8 7 6	-065 -058 -052 -045	9 8 7 6	-077 -071 -064 -057	11 10 8 7	-090 -088 -077	12 11 10 9	-108 -097 -090 -088	18 12 11 10	·117 ·110 ·104	15 18 12 11
221 28 281	-027 -020 -018	8 2 2	-088 -082 -025	4 8	-051 -044 -088	6 5 5	-064 -057 -050	8 7 6	-077 -070 -064	9 8 7	-091 -084 -077	10 10 9
24 24 <u>1</u> 25	-007 -001	0	-019 -012 -005	1 0	-081 -024 -018	8 2	-044 -087 -080	5 4 8	-057 -050 -044	6 6 5	-071 -064 -067	8 7 6

#			DEGREES	OF T	HE WET	BULB	THERM()M BTE	R,—₽АНВ	ENHEI	т.	
- * Fabreabelt.	58	jo	54	ļ°	55	,0	56	3 0	57	ro	58	°
t — t	Force of Vapor, in inches.	Relative Humidity.	Porce of Vapor, in inches.	Relative Humidity.								
0° 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-408	100	·418	100	-488	100	-449	100	466	100	-488	100
	-896	96	·411	97	-427	97	-448	97	-459	97	-476	97
	-890	98	·405	94	-420	94	-486	94	-452	94	-469	94
	-883	90	·898	90	-418	90	-429	91	-446	91	-462	91
2 2½ 8 8 8½	-876 -370 -868 -857	87 84 81 78	891 885 878 872	87 84 81 78	-407 -400 -894 -887	87 84 82 79	428 416 410 408	88 85 82 79	489 488 426 419	88 85 82 80	•456 •449 •442 •436	88 85 88 80
4	-850	75	-865	76	-880	76	896	76	-418	77	-429	77
41	-343	72	-858	78	-874	78	890	74	-406	74	-422	75
5	-837	70	-852	70	-867	71	883	71	-899	72	-416	72
5	-830	67	-845	68	-860	68	376	69	-892	69	-409	70
6	-828	65	-888	65	-854	66	-870	66	-886	67	-408	67
6 <u>1</u>	-817	62	-832	68	-847	64	-868	64	-879	65	-896	65
7	-810	60	-325	61	-840	61	-856	62	-878	62	-889	68
7 <u>1</u>	-804	57	-819	58	-834	59	-850	60	-866	60	-888	61
8	297	55	·812	56	-827	57	-848	57	-859	58	-876	59
8 <u>1</u>	290	58	·805	54	-821	55	-887	55	-858	56	-869	56
9	284	51	·299	52	-814	58	-880	58	-846	54	-862	55
9 <u>1</u>	277	49	·292	50	-807	51	-828	51	-840	52	-856	58
10	·270	47	·285	48	-801	49	-816	49	·838	50	·849	51
10 <u>1</u>	·264	45	·279	46	-294	47	-810	48	·826	48	·848	49
11	·257	48	·272	44	-287	45	-808	46	·819	47	·886	47
11 <u>1</u>	·251	41	·265	42	-281	48	-296	44	·818	45	·829	46
12	-244	89	·259	40	·274	41	-290	42	·806	48	-828	44
12 <u>1</u>	-287	88	·252	89	·268	40	-288	41	·800	41	-816	42
18	-281	86	·246	87	·261	88	-277	89	·298	40	-809	41
18 <u>1</u>	-224	84	·289	85	·254	86	-270	87	·286	88	-808	89
14	·218	88	·282	84	·248	85	-268	86	280	87	·296	88
141	·211	81	·226	82	·241	88	-257	84	278	85	·289	86
15	·204	80	·219	81	·234	82	-250	88	266	84	·288	85
151	·198	28	·212	29	·228	80	-248	81	259	82	·276	88
16	·191	27	·206	28	·221	29	-287	80	258	81	·270	82
16 <u>1</u>	·184	25	·199	27	·214	28	-280	29	246	80	·263	81
17	·178	24	·198	25	·208	26	-228	27	240	28	·256	29
17 <u>1</u>	·171	28	·186	24	·201	25	-217	26	288	27	·249	28
18	·165	22	·179	28	·195	24	210	25	-226	26	·248	27
18 <u>1</u>	·158	20	·178	22	·188	28	204	24	-220	25	·286	26
19	·151	19	·166	20	·181	22	-197	28	-218	24	·229	25
19 <u>1</u>	·145	18	·160	19	·175	20	-190	21	-207	22	·228	28
20	-188	17	·153	18	·168	19	·188	20	-200	21	-216	22
201	-181	16	·146	17	·161	18	·177	19	-198	- 20	-210	21
21	-125	15	·189	16	·155	17	·170	18	-186	19	-208	20
21	-118	14	·188	15	·148	16	·164	17	-180	18	-196	19
22	·112	18	·126	14	·141	15	·157	16	·178	17	·190	18
221	·105	12	·120	18	·185	14	·150	15	·167	16	·188	18
23	·098	11	·118	12	·128	18	·144	14	·160	16	·176	17
281	·092	10	·106	11	·122	12	·187	14	·158	15	·169	16
24	-085	9	-100	10	·115	12	·131	18	·147	14	-168	15
241	-079	8	-098	10	·108	11	·124	12	·140	18	-156	14
25	-072	7	-086	9	·101	10	·117	11	·188	12	-150	18

坦		1)BGREES	OF TI	ie wet	BULB	THERM	METER	L-FAHR	enhei	r.	
- V Pahrenhott.	56	0	60)°	61	Į°	62	3 °	68	P º	64	
t − v	Force of Vapor, in inches.	Belative Humddity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humbility.	Force of Vapor, in inches.	Relative Humbdity.	Force of Vapor, in inches.	Relative Humidity.
0°	·500	100	·518	100	·587	100	-556	100	·576	100	·596	100
	·498	97	·511	97	·530	97	-549	97	·569	97	·590	97
1	•487	94	-505	94	·528	94	-548	94	-568	94	·588	94
14	•480	91	-498	91	·517	91	-586	92	-556	92	·576	92
2	478	88	•491	88	·510	88	-529	89	-549	89	-570	89
21	466	85	•485	86	·508	86	-528	86	-542	87	-568	87
8	460	83	•478	88	·497	83	-516	84	-536	84	-556	84
81 4	·458	80 77	·471	81 77	490	81 78	·509	81 78	·529	82 79	·550 ·548	82 79
4½	•440	75	•458	75	·476	75	·496	77	-516	77	-586	77
5	•483	78	•451	78	·470	78	·489	75	-509	75	-529	75
54	•427	71	•444	71	·468	71	·483	72	-502	72	-528	72
6	420	68	•488	68	·457	69	·476	69	496	70	-516	70
6 <u>1</u>	418	66	•481	66	·450	67	·469	67	490	68	-509	68
7	407	68	•425	64	·448	65	·462	65	482	66	-508	66
7 <u>1</u>	•400	61	·418	62	·487	68	·456	68	·476	64	·496	64
8	•898	59	·411	60	·480	61	·449	61	·469	62	·489	62
9 1	-886	57	•405	58	•423	59	-442	59	·462	60	488	61
9	-880	56	•898	56	•416	57	-486	57	·455	58	476	59
8 1	-878	54	•891	54	•410	55	-429	55	·449	56	469	57
10	-867	52	-885	58	-408	54	-422	54	·442	55	-468	56
101	-860	50	-878	51	-897	52	-416	52	·486	58	-456	54
11	-858	48	-871	49	-890	50	-409	50	·429	51	-449	52
11½ 12	-847 -840	46 45	-865 -858	47 46	888	48 47	·402 ·896	49 48	·422 ·415	49 48	·448	50 49
124	-888	48	·851	44	-870	45	-889	46	-409	46	-429	47
18	-827	42	·345	42	-868	48	-882	44	-402	45	-422	46
184	-820	40	·838	41	-856	42	-876	42	-895	48	-416	44
14	-818	89	-831	89	-850	40	-869	41	-889	42	-409	48
141	-806	87	-824	88	-848	89	-862	40	-882	40	-402	41
15	-800	86	-818	87	-836	87	-856	88	-875	89	-896	40
15 <u>1</u>	·298	85	·811	85	-880	86	·849	87	·869	88	-889	89
16	·287	88	·805	84	-828	85	·842	86	·862	86	-882.	87
16½	·280	82	·298	88	·816	84	-836	84	-855	85	-876	86
17	·278	80	·291	81	·810	82	-829	83	-849	84	-869	85
17½	·267	29	·285	80	·803	81	-822	82	-842	88	-862	84
18	·260	28	·278	29	·296	80	-815	81	-835	82	-855	82
18]	·258	27	·271	28	·290	29	-809	80	-828	80	-849	81
19	·247	26	·264	27	·288	28	-802	28	-822	29	-842	80
19½	-240	25	·258	26	·276	26	-295	27	-815	28	-835	29
20	-284	28	·251	24	·270	25	-289	26	-808	27	-829	28
20¼	-227	22	·245	23	·268	24	-282	25	-802	26	-822	27
21	-220	21	·238	22	·256	28	·275	24	·295	25	-815	26
21	-218	20	·281	21	·250	22	·269	28	·288	24	-809	25
22	-207	19	·225	21	·248	22	·262	22	·282	28	-802	24
221 28 281	200 198 187	19 18 17	218 -211 -205	20 19 18	·286 ·280 ·228	21 20 19	-255 -249 -242	22 22 21 20	·275 ·268 ·262	22 22 22 21	·295 ·289 ·282	28 22 22
24 24 24 25	180 178 167	16 15 14	·198 ·191 ·185	17 16 15	·216 ·209 ·208	18 17 16	·284 ·228 ·222	19 18 17	·255 ·248 ·241	20 19 18	·275 ·268 ·262	21 20 19

岩		1	BORRES	OF TE	u wer	BULB	THURMO	METER	.—YAHR	en H.B.I.	P.	
— t' Fabrenbeit.	61	,0	66	90	61	ro	68	°	68	•	70	»
- t	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Rolative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0° 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-618 -611 -604 -598	100 97 94 92	-689 -688 -626 -619	100 97 96 92	-662 -655 -648 -642	100 97 95 92	-686 -678 -671 -665	100 97 96 92	-708 -702 -695 -688	100 97 95 92	·788 ·726 ·720 ·718	100 97 95 92
2 2½ 8 8↓	-591 -584 -577 -571	89 87 85 82	-612 -606 -599 -592	90 88 85 88	-685 -628 -621 -615	90 88 85 88	-658 -651 -644 -688	90 88 86 88	-682 -675 -668 -662	90 88 86 88	-706 -700 -698 -666	90 88 86 88
4 41 5 5	-564 -557 -561 -544	79 77 75 78	-586 -579 -572 -566	80 78 76 74	-608 -601 -595 -588	80 78 76 74	-681 -624 -617 -611	81 79 77 75	-665 -648 -641 -685	81 79 77 75	-680 -678 -666 -659	81 79 77 75
6 6 <u>1</u> 7 7 <u>1</u>	-587 -580 -524 -517	71 69 66 64	-559 -552 -545 -589	72 70 67 65	-581 -574 -568 -561	72 70 67 65	-604 -597 -591 -584	78 71 68 66	·628 ·621 ·614 ·608	78 71 68 67	-652 -646 -689 -682	78 71 69 67
8 8 <u>1</u> 9 9 <u>1</u>	-510 -504 -497 -490 -484	68 61 59 58	-582 -525 -519 -512 -505	68 61 60 58	-554 -548 -541 -534	64 62 60 59	·577 ·571 ·564 ·557	64 68 61 59	-601 -594 -588 -581	65 68 62 60	-626 -619 -612 -606	65 64 62 60
10 10 <u>1</u> 11 11 <u>1</u> 12	-477 -470 -468 -457	54 52 51 49	-505 -498 -492 -485 -478	56 55 58 52	·527 ·521 ·514 ·507	57 55 54 52	-550 -544 -587 -580	58 56 54 58	·574 ·567 ·561 ·554	58 57 55 58	·599 ·592 ·585 ·578	59 57 56 54
12 <u>1</u> 18 18 <u>1</u> 14	-450 -448 -487 -480	48 46 45	472 -465 -468 -462	50 48 47 46 44	-501 -494 -487 -481 -474	51 49 48 46	-528 -517 -510 -508	51 50 48 47	-547 -541 -584 -527	52 50 49 48	·572 ·565 ·558 ·552	52 51 50 48
141 15 161 161	428 -417 -410 -408	42 41 89 88	445 488 482	48 41 40 89	-467 -460 -454 -447	48 42 41 40	-497 -490 -488 -476 -470	45 44 48 42 40	·520 ·514 ·507 ·500 ·498	46 45 48 42 41	-545 -588 -581 -525 -518	47 45 44 48 42
16 <u>1</u> 17 17 <u>1</u> 18	-896 -890 -888 -876	87 86 84 88	-417 -410 -404 -897	88 86 85	440 488 427 420	88 87 86 85	468 456 450	89 88 87 86	·487 ·480 ·478 ·467	40 89 88 86	·511 ·504 ·498	41 89 88 87
18 <u>1</u> 19 19 <u>1</u> 20	-870 -868 -866 -860	82 81 80 29	-890 -884 -877 -871	88 82 81 80	•418 •407 •400	84 83 82 81	486 429 428 416	85 88 82 81	460 458 446	85 84 88 82	484 -478 -471 -464	86 85 84 88
20 <u>1</u> 21 21 <u>1</u> 22	-848 -886 -880 -828	28 27 26 25	-864 -858 -851 -844	29 28 27 26	-886 -880 -878 -866	80 29 28 27	409 408 896 889	80 29 29 28	488 426 419 418	81 80 29 28	457 451 444 487	82 81 80 29
22½ 28 28½ 24	-816 -809 -808 -296	24 24 28 22	-888 -831 -824 -817	25 24 28 28	860 858 846 840	26 25 24 28	-882 -876 -869 -862	27 26 25 24	-406 -899 -898 -886	28 27 26 25	•480 •424 •417 •410	28 27 27 27
241 25	·289 ·288	21 20	·811 ·804	22 21	-888 -826	28 22	856 849	28 22	·879 ·872	24 28	·404 ·897	25 24

bedt.		ľ	egrees	OF TH	e wet	BULB	THERMO	METER	.—УАНВ	en Heit	! .	
t — t' Fabreahait.	71	lo.	72	Po	78	S °	74	°	76	60	76	80
t-#)	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0° 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	·769	100	·785	100	·812	100	-839	100	-868	100	-897	100
	·762	98	·778	98	·805	98	-838	98	-861	98	-890	98
	·745	95	·771	95	·798	95	-826	95	-854	95	-884	95
	·789	98	·765	98	·792	93	-819	98	-847	98	-877	98
2 2 3 8 8	·782 ·725 ·718 ·712	90 88 86 88	-758 -751 -745 -788	90 88 86 84	·785 ·778 ·772 ·765	90 88 86 84	·812 ·805 ·799 ·792	91 88 86 84	-841 -884 -827 -820	91 88 86 84	-870 -868 -856 -850	91 89 87 85
4	·705	81	·781	81	•758	82	·785	82	-813	82	-848	88
41	·698	79	·725	79	•751	80	·778	80	-807	80	-886	81
5	·691	77	·717	77	•744	78	·772	78	-800	78	-829	79
5	·685	75	·711	75	•788	76	·765	76	-798	76	-828	77
6	-678	78	-704	78	·781	74	•758	74	·787	74	816	75
6	-671	71	-697	71	·724	72	•751	72	·780	78	809	74
7	-664	69	-691	69	·717	70	•745	70	·778	71	802	72
7	-658	67	-684	67	·711	68	•788	69	·766	69	795	70
8 ¹ 8 ¹ 8	-651 -644 -688 -681	66 64 62 61	-677 -670 -664 -657	66 64 62 61	-704 -697 -691 -684	66 65 68 61	·781 ·724 ·717 ·711	67 65 64 62	·759 ·758 ·746 ·789	67 66 64 62	-789 -782 -775 -768	68 67 65 68
10	624	59	-650	59	·677	60	·704	60	·788	61	•762	62
101	617	58	-648	58	·670	58	·698	59	·726	59	•755	60
11	610	56	-687	56	·668	57	·691	57	·719	58	•748	59
111	604	54	-680	54	·657	55	·684	56	·712	56	•741	57
12	-597	58	-628	58	-650	54	-677	54	·705	55	-785	56
12 <u>1</u>	-590	51	-616	51	-648	52	-670	53	·699	54	-728	55
13	-584	50	-610	50	-687	51	-664	52	·692	52	-721	53
13 <u>1</u>	-577	49	-608	49	-680	50	-657	50	·685	51	-714	52
14	·570	47	-596	47	-628	48	-650	49	-678	50	·707	51
14½	·564	46	-590	46	-616	47	-648	48	-671	48	·701	49
15	·557	45	-588	45	-609	46	-687	47	-665	47	·694	48
15½	·550	48	-576	43	-608	45	-630	45	-658	46	·687	47
16	·548	42	-569	42	-596	48	-628	44	-651	45	-680	46
16 <u>1</u>	·586	41	-562	41	-589	42	-616	43	-645	44	-674	45
17	·580	40	-556	40	-582	41	-610	42	-688	42	-667	48
17 <u>1</u>	·528	89	-549	89	-576	40	-608	41	-681	41	-660	42
18	·516	88	542	88	-569	89	-596	40	-624	40	658	41
18 <u>1</u>	·510	87	586	87	-562	88	-589	89	-617	89	646	40
19	·508	86	529	86	-556	87	-582	88	-611	88	640	89
19 <u>1</u>	·496	85	522	85	-549	86	-576	87	-608	87	683	88
20 20 21 21 21	489 482 476 469	84 88 82 81	-515 -508 -502 -495	84 88 82 81	-542 -585 -528 -522	85 84 88 82	569 562 556 549	86 85 84 88	597 591 584 577	86 85 84 88	-626 -620 -618 -606	87 86 85 84
22	462	80	488	81	-515	81	-542	82	-570	88	-599	83
22½	456	29	482	30	-508	80	-585	81	-568	82	-592	82
28	449	28	•475	29	-502	29	-528	80	-557	81	-586	81
28½	442	27	•468	28	-495	28	-522	29	-550	80	-579	80
24 24 24 25	486 429 422	26 26 2 5	•461 •455 •448	27 26 25	·488 ·481 ·474	28 27 26	·515 ·508 ·502	28 27 26	-548 -586 -580	29 28 27	-572 -565 -559	29 28 27

pel t		I	DGREES	OF TI	IB WET	BULB	THERMO	METER	L—FAHR	en het	r.	
- V Fabroabelt.	77	ro	78	jo	78	0	80	po	81	•	82	b.
t – v 1	Force of Vapor, in inches.	Relative Humbdity.	Force of Vapor, in inches.	Relative Humbdity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humbility.	Force of Vapor, in inches.	Relative Humidity.
0° 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-927	100	958	100	-990	100	1-028	100	1-057	100	1.092	100
	-920	98	•951	98	-984	98	1-017	98	1-050	98	1.085	98
	-914	95	•945	95	-977	96	1-010	96	1-044	96	1.079	96
	-907	98	•988	93	-970	98	1-008	98	1-087	98	1.072	94
2	-900	91	-981	91	-968	91	-996	91	1.080	91	1-065	91
2½	-898	89	-924	89	-966	89	-989	89	1.028	89	1-068	89
3	-886	87	-918	87	-960	87	-988	87	1.016	87	1-061	87
8½	-880	85	-911	85	-948	85	-976	85	1.010	86	1-045	86
4 4 4 5 5	-878 -866 -859 -858	88 81 79 77	-904 -897 -891 -884	88 81 79 77	-986 -929 -928 -916	88 81 79 77	-969 -962 -955 -949	88 81 79 78	1-008 -996 -989 -982	88 81 80 78	1.088 1.081 1.024 1.017	84 82 80 78
6	-846	75	877	75	-909	75	-942	76	-976	76	1-010	76
61	-839	78	870	78	-902	74	-985	74	-969	74	1-004	75
7	-882	72	868	72	-895	72	-928	72	-962	78	-997	78
71	-825	70	867	70	-889	70	-921	71	-955	71	-990	71
8 <u>1</u> 9 91	-819 -812 -805 -798	68 67 65 63	-850 -848 -886 -829	68 67 65 68	-882 -875 -868 -861	69 67 66 64	-915 -908 -901 -894	69 68 66 64	-948 -942 -985 -928	69 68 66 65	-988 -976 -970 -968	70 68 67 65
10	·792	62	828	62	-855	62	-887	68	-921	68	956	64
10 <u>1</u>	·785	60	816	60	-848	61	-881	61	-914	62	•949	62
11	·778	59	809	59	-841	60	-874	60	-908	60	•942	61
11 <u>1</u>	·771	57	802	57	-884	58	-867	59	-901	59	•986	59
12	-764	56	-796	56	-827	57	-860	57	-894	58	-929	58
12½	-768	55	-789	55	-821	56	-854	56	-887	56	-922	57
13	-751	58	-782	58	-814	54	-847	55	-880	55	-915	56
184	-744	52	-775	52	-807	58	-840	58	-874	54	-908	54
14	·787	51	-768	51	-800	52	-838	52	-867	58	-902	58
14 <u>1</u>	·781	49	-762	50	-798	50	-826	51	-860	51	-895	52
15	·724	48	-755	48	-787	49	-820	50	-858	50	-888	51
15 <u>1</u>	·717	47	-748	47	-780	48	-813	49	-846	49	-881	50
16	-710	46	·741	46	·778	47	-806	47	-840	48	-874	48
16 <u>1</u>	-704	45	·784	45	·766	46	-799	46	-888	47	-867	47
17	-697	44	·728	44	·760	45	-792	45	-826	46	-861	46
17 <u>1</u>	-690	42	·721	48	·758	44	-786	44	-819	45	-854	45
18	-688	41	·714	42	·746	48	·779	48	812	44	-847	44
181	-676	40	·707	41	·789	42	·772	42	806	48	-840	48
19	-670	89	·700	40	·782	41	·765	41	799	42	-888	42
191	-668	88	·694	89	·726	40	·758	40	792	41	-827	41
20 201 21 21 211	-656 -649 -648 -686	87 86 86 85	-687 -680 -678 -667	88 87 86 85	·719 ·712 ·705 ·698	89 88 87 86	·752 ·745 ·788 ·781	89 88 87 86	·785 ·778 ·772 ·765	40 89 88 87	-820 -818 -806 -799	40 89 88 88
22	-629	84	-660	84	-692	85	·724	85	·758	86	798	87
221	-622	88	-668	88	-685	84	·718	85	·751	85	786	86
23	-615	82	-646	88	-678	88	·711	84	·744	84	779	85
281	-609	81	-689	82	-671	82	·704	83	·788	84	772	84
24	-602	80	-688	81	-664	82	-697	82	·781	88	•765	88
24 1	-695	29	-626	80	-658	81	-690	81	·724	82	•759	82
25	-688	28	-619	29	-651	80	-684	80	·717	81	•752	81

ij		D	BGREES	OF TE	E WET	BULB	THERMO	METER	FAHR	ENHE	r.	
t — t' Pahrenheit.	88	PO	84	84°		,0	86	90	81	ro	86	
# -	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Reletive Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in Inches.	Relative
00	1.128	100	1.165	100	1.208	100	1.242	100	1.282	100	1.824	10
<u>, 1</u>	1.121	98	1.158	98	1.196	98	1.285	98	1.275	98	1.817	9
1 1	1·114 1·108	96 94	1·151 1·145	96 94	1·189 1·188	96 94	1·228 1·222	96 94	1·269 1·262	96 94	1.810 1.808	9
2	1.101	91	1.188	92	1.176	92	1.215	92	1.255	92	1.296	9
$2\frac{1}{2}$	1.094	90	1.181	90	1.169	90	1.208	90	1.249	90	1.290	9
8	1.087	88	1.124	88	1.162	88	1.201	88	1-241	88	1.283	8
81	1.080	86	1.117	86	1.155	86	1.194	86	1.285	86 84	1.276	
4 .4}	1.074	84 82	1·111 1·104	84 82	1·149 1·142	84 82	1·188 1·181	84 82	1·228 1·221	88	1·269 1·262	8
5	1.060	80	1.097	80	1.185	80	1.174	81	1.214	81	1.255	8
51	1.058	78	1.090	79	1.128	79	1.167	79	1-207	79	1.248	7
6	1-046	77	1-068	77	1.121	77	1.160	77	1.200	78	1.242	7
61	1.089	75	1.076	75	1.114	75	1.158	76	1.198	76	1.285	7
7 71	1.088	78 72	1.070 1.068	74 72	1·108 1·101	74 72	1·146 1·140	74 72	1·187 1·180	7 <u>4</u> 78	1·228 1·221	7
8	1-019	70	1.056	70	1.004	71	1.183	71	1.178	71	1.214	7
81	1.012	69	1.049	69	1.087	69	1.126	69	1.166	70	1.208	7
9	1.005	67	1.042	67	1.080	68	1.119	68	1.159	68	1.201	6
91	-999	66	1.086	66	1-074	66	1.112	66	1.158	67	1.194	6
10	-992	64	1.029	64	1.066	65	1.105	65	1.145	65 64	1.187	6
10] 11	-985 -978	68 61	1-022 1-015	68 62	1.060 1.058	68 62	1.099	64 62	1.189	68	1·180 1·178	6
114	.971	60	1.008	60	1.046	61	1-085	61	1.125	61	1.166	ě
12	-965	58	1.001	59	1-089	59	1-078	60	1-118	60	1.159	6
121	.958	57	-995	58	1.082	58	1.071	58	1.111	59	1.158	5
18 ⁻ 18]	·951 ·944	56	-998	56	1.026	57	1.065	57	1·105 1·098	57 56	1·146 1·189	5
_	987	55 54	-981 -974	55	1.019	56 55	1.051	56 55	1.091	55	1.182	5
14 14}	-981	52	-967	54 58	1.012	58	1.044	54	1.084	54	1.125	5
15	-924	51	960	52	-998	52	1.087	52	1.077	58	1.118	5
15}	917	50	954	50	· 9 91	51	1.080	51	1-070	52	1.111	5
16	-910	49	-947	49	-985	50	1.028	50	1-068	51	1.105	5
161 17	-908 -896	48 47	·940 ·988	48 47	-978 -971	49 48	1.017 1.010	49 48	1.057	50 49	1-098 1-091	5
171	-890	46	926	46	964	47	1-008	47	1-048	48	1.084	4
18	-888	45	-920	45	-957	46	-996	46	1-086	47	1-077	4
181	876	44	.918	44	-951	45	-989	45	1.029	46	1-071	4
19	-869	48	-906	48	944	44	988	44	1.028	45	1-064	4
191	-862	42	-899	42	-987	48	·976	48	1-016	44	1-057	4
20 20}	·855 ·849	41 40	·892 ·885	41 40	·980 ·928	42 41	-969 -962	42 41	1·009 1·002	48 42	1-050 1-043	4
21	-842	89	-879	89	-916	40	-955	41	-995	41	1-086	4
$21\frac{1}{2}$	885	88	872	88	·910	89	·948	40	•988	40	1.029	4
22	-828	87	-865	88	-908	88	-942	89	-981	89	1.028	4
221	-821	86	858	87	-896	87	985	88	975	88 88	1-016	8
28 ⁻ 28‡	-815 -808	85 84	-851 -845	86 85	-889 -882	87 86	·928 ·921	87 86	967 961	87	1-009	8
24	-800	84	-888	84	-875	85	.914	86	-954	86	-995	8
241	-794	88	-881	88	-869	84	908	85	-947	85	-989	8
25	.787	82	-824	88	-862	88	-800	84	·940	85	-981	8

46.		,	en res	OF T	es wer	BULB	THERM	METER	L.—PAHR	enhei	T.	
- Y Pahrenbelt.	88	۰	90	po .	91	•	92	°	98		94	l°
- A - J	Force of Vapor, in inches.	Rolative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Homidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Fores of Vapor, in inches.	Relative Humidity.
0°	1·866	100	1·410	100	1·455	100	1·501	100	1.548	100	1.597	100
	1·859	98	1·408	98	1·448	98	1·494	98	1.541	98	1.590	98
	1·852	96	1·896	96	1·441	96	1·487	96	1.585	96	1.588	96
1½	1.846	94	1.889	94	1·484	94	1.480	94	1.528	94	1.576	94
2	1.889	92	1.882	92	1·427	92	1.478	92	1.521	92	1.569	92
2½	1.882	90	1.875	90	1·420	90	1.466	90	1.514	91	1.562	91
3	1.825	88	1.868	88	1·418	88	1.469	89	1.507	89	1.556	89
8 <u>1</u>	1·818	86	1·862	86	1·406	87	1·458	87	1.500	87	1.549	87
4	1·811	85	1·855	85	1·400	85	1·446	85	1.498	85	1.542	85
4 <u>1</u>	1·804	88	1·848	88	1·898	88	1·489	88	1.486	84	1.585	84
5	1·298	81	1.841	81	1.886	82	1·482	82	1·479	82	1.528	82
5 <u>1</u>	1·291	80	1.884	80	1.879	80	1·425	80	1·478	80	1.521	80
6	1·284	78	1.827	78	1.872	78	1·418	79	1·466	79	1.514	79
6 <u>1</u>	1·277	77	1.821	77	1.865	77	1·411	77	1·459	77	1.507	77
7 7 <u>1</u> 8	1·270 1·268 1·256	75 78 72	1.814 1.807 1.800	75 74 72	1.858 1.852 1.845	75 74 72	1·405 1·898 1·891	75 74 78	1·452 1·445 1·488	76 74 78	1.498 1.487	76 74 78
8 <u>1</u>	1·249	70	1·298	71	1.888	71	1.884	71	1·481	71	1.480	72
9	1·248	69	1·286	69	1.881	69	1.877	70	1·424	70	1.478	70
91	1·286	67	1·279	68	1.824	68	1.870	68	1·417	69	1.466	69
10	1·229	66	1·278	66	1.817	67	1.868	67	1·411	67	1.459	67
10 <u>1</u>	1·222	65	1·266	65	1.811	65	1.856	65	1·404	66	1·452	66
11	1·215	64	1·259	64	1.804	64	1.850	64	1·897	65	1·445	65
11 <u>1</u>	1·208	62	1·252	62	1.297	68	1.848	68	1·890	68	1·489	64
12	1·202	61	1·245	61	1·290	61	1.886	62	1.888	62	1·482	62
12 <u>1</u>	1·195	59	1·238	60	1·288	60	1.829	60	1.876	61	1·425	61
18	1·188	58	1·281	59	1·276	59	1.822	59	1.869	60	1·418	60
13 <u>1</u>	1·181	57	1·224	57	1·269	58	1.815	58	1.868	59	1·411	59
14 14 <u>1</u> 15 15 <u>1</u>	1·174 1·167 1·161	56 55 54	1·217 1·211 1·204	56 55 54	1·262 1·255 1·249	57 56 54	1.808 1.801 1.295 1.288	57 56 55	1.856 1.849 1.842	58 56 55	1·404 1·897 1·890	58 57 56 55
16 16 <u>1</u> 17	1·154 1·147 1·140 1·188	58 51 50 49	1·197 1·190 1·188 1·176	58 52 51 50	1·242 1·285 1·228 1·221	58 52 51 50	1-281 1-274 1-267	54 58 52 51	1.885 1.828 1.821 1.814	54 58 52 51	1.888 1.877 1.870 1.868	54 58 52
17½ 18 18½ 19	1·126 1·119 1·112 1·106	48 47 46 45	1·170 1·168 1·156 1·149	49 48 47 46	1·214 1·207 1·200 1·194	48 47 46	1·260 1·258 1·246 1·289	50 49 48 47	1.808 1.801 1.294 1.287	50 49 48 47	1.856 1.849 1.842 1.885	51 50 49 48
19 1	1-099	44	1·142	45	1·187	45	1·288	46	1·280	46	1·828	47
20	1-092	44	1·185	44	1·180	44	1·226	45	1·278	45	1·821	46
201	1-085	48	1·129	48	1·178	44	1·219	44	1·266	44	1·815	45
21 21 21 22 22	1-078 1-071 1-065 1-058	42 41 40 89	1·122 1·115 1·108 1·101	42 41 41 40	1·166 1·159 1·158 1·146	48 42 41 40	1·212 1·206 1·198 1·191	48 48 42 41	1·259 1·258 1·246 1·289	44 48 42 41	1.808 1.801 1.294 1.287	44 48 48 42
28	1-051	89	1-094	89	1·189	89	1·185	40	1·282	41	1·280	41
231	1-044	88	1-087	88	1·182	89	1·178	89	1·225	40	1·278	40
24	1-087	87	1-080	88	1·125	88	1·171	88	1·218	89	1·266	89
24½	1-080	86	1-078	87	1·111	87	1·164	88	1·211	88	1·259	89
25	1-028	86	1-067	86	1·111	87	1·157	87	1·204	88	1·258	88

#		1	DEGREES	OF T	ES WET	BULB	THURMO	Mere	L—Jahr	ENHEI	r.	
-t Fahrenbeit.	96	50	90	30	91	ro	96)°	91) °	10	0°
- + + - + + - + + + + + +	Force of Vapor, in inches.	Relative RumMity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in Inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Veport, in inches.	Relative Humidity.	Porce of Vapor, in inches.	Relative Humidity.
0° 1 1	1.647 1.640 1.688 1.626	100 98 96 94	1-698 1-691 1-684 1-677	190 98 96 94	1·761 1·744 1·787 1·780	100 98 96 94	1.805 1.798 1.791 1.784	100 98 96 95	1.861 1.854 1.847 1.840	100 98 96 95	1·918 1·911 1·904 1·897	100 98 96 95
2 2 3 8 8	1.619 1.612 1.605 1.598	92 90 89 87	1-671 1-664 1-657 1-650	92 90 89 87	1·728 1·716 1·709 1·708	92 90 89 87	1.777 1.770 1.764 1.757	98 91 90 88	1.838 1.826 1.819 1.812	98 91 90 88	1.890 1.888 1.876 1.870	98 91 90 88
4 -41 5 5 5	1.592 1.585 1.578 1.571 1.564	85 88 82 80	1.648 1.636 1.629 1.622	85 88 82 80	1.696 1.689 1.682 1.675	85 88 82 80	1.750 1.748 1.786 1.729	86 84 88 81	1.805 1.799 1.791 1.785	86 84 88 81	1-868 1-867 1-849 1-842	86 84 88 81
61 7 71 8	1.567 1.550 1.548 1.686	78 77 75 78 72	1.616 1.608 1.602 1.595	78 77 76 74 78	1-668 1-661 1-654 1-647 1-640	78 77 76 74 78	1.722 1.715 1.708 1.701 1.694	79 78 77 75	1.778 1.771 1.764 1.757	79 78 77 76	1.885 1.828 1.821 1.814	79 78 77 76
8 <u>1</u> 9 9 <u>1</u> 10	1.580 1.528 1.517 1.509	71 70 69 68	1.581 1.574 1.567	71 70 69 68	1-688 1-627 1-620 1-618	71 70 69 68	1.688 1.681 1.674 1.667	72 71 70 69	1·750 1·748 1·786 1·729 1·722	74 78 72 70 69	1·807 1·800 1·798 1·786 1·779	74 78 72 70
10½ 11 11½ 12	1.502 1.495 1.488 1.481	66 65 68 62	1.558 1.546 1.589 1.582	66 65 68 62	1.606 1.599 1.592 1.585	66 65 64 68	1-660 1-658 1-646	67 66 64 68	1·715 1·708 1·702 1·695	67 66 65	1.772 1.766 1.759	69 67 66 65
12 <u>1</u> 18 18 <u>1</u> 14	1·474 1·468 1·461 1·454	61 60 59 68	1.526 1.519 1.512 1.505	61 60 59 58	1.578 1.571 1.564 1.658	62 61 60 59	1-682 1-625 1-618 1-611	62 61 60 59	1.688 1.681 1.674 1.667	68 62 61 60	1.745 1.788 1.781 1.724	68 62 61
14½ 15 15½ 16½ 16	1·447 1·440 1·488 1·426 1·419	57 56 55 54	1·498 1·491 1·484 1·477	57 56 55 54	1.561 1.544 1.687 1.580	58 57 56 55	1.605 1.598 1.591 1.584	58 57 56 55	1.660 1.658 1.646 1.689	59 58 57 56	1.717 1.710 1.708 1.696	59 58 57 56
17 17 17 18 18	1·412 1·405 1·899 1·892	58 52 51 50 49	1·470 1·464 1·457 1·450 1·448	58 52 51 50 49	1.528 1.516 1.509 1.502 1.495	54 58 52 51 50	1.577 1.570 1.568 1.556	54 58 52 52	1.682 1.625 1.619 1.612	55 54 58 52	1.689 1.682 1.676 1.669	55 54 58 58
19 ² 19½ 20 20½ 21	1.885 1.878 1.871 1.864	48 47 46 45	1·486 1·429 1·422 1·415	48 47 47 46	1.488 1.482 1.475 1.468	49 48 47 46	1.549 1.542 1.585 1.528 1.522	51 50 49 48 47	1.605 1.598 1.591 1.584 1.577	51 50 49 48 47	1.662 1.655 1.648 1.641	52 51 50 49
21½ 22 22½	1.857 1.850 1.848 1.887	45 44 48 48	1·408 1·401 1·395 1·888	45 44 44 48	1·461 1·454 1·447 1·440	45 44 44 48	1.515 1.508 1.501 1.494	46 45 45 44	1.570 1.568 1.556 1.549	46 46 45	1.684 1.627 1.620 1.613 1.606	48 47 46 46 45
28 281 24 24 241	1.880 1.828 1.816 1.809	42 42 40 40	1.881 1.874 1.867 1.860	42 42 41 40	1.488 1.426 1.420 1.418	42 42 41 40	1·487 1·480 1·478 1·466	48 42 42 41	1.542 1.586 1.529 1.522	48 48 42 41	1-699 1-698 1-686 1-679	44 48 48 42
25	1-802	89	1.858	89	1.406	89	1.469	40	1.616	40	1.572	41

Deft.		10	DGREES	OF TE	IN WHY	BULB	THERMO	MPTE	.—PAHR	ENHEL	t.	
– V Fabroabelt.	10	10	10	30	10	B°	10	1°	10	5°	10	Bo .
- 4	Force of Vapor, in inches.	Relative Humbdity.	Perce of Vapor, in Inches.	Relative Humidity.	Fores of Vapor, in Inches.	Relative Humidity.	Fores of Vapor, in Inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0°	1-977 1-970 1-968	100 98 96	2-087 2-080 2-028	100 98 96	2·098 2·092 2·065	100 98	2·162 2·155	100 98	2-226	100	2.288	100
1 1;	1-966	96	2-016	96	2-078	96 95	2·148 2·141	96 95	. • • • • • • • • • • • • • • • • • • •	•••••		•••••
2 21 8	1-949 1-942 1-985	98 91 90	2-009 2-002 1-995	98 91 90	2-071 2-064 2-067	98 91 90	2·184 2·127 2·120	98 91 90	•••••	*****		•••••
81	1-928 1-921	88 86	1.989 1.982	88 86	2-050 2-048	88 87	2·118 2·106	88 87	******			•••••
41 5	1·914 1·907	84 88	1-975 1-967	84 88	2-086 2-029	84 88	2·099 2·092	85 84		•••••	•••••	
5 <u>1</u> 5 61	1-900 1-898 1-887	82 80 79	1.960 1.964 1.947	82 80 79	2-022 2-015 2-008	82 80 79	2-065 2-078 2-071	82 81 79	•••••	•••••	•••••	•••••
7 71	1.880 1.878	78 76	1.940 1.988	78 76	2-001 1-994	78 77	2-064 2-067	78 77	*****	•••••		•••••
.8 .8	1.866 1.859	75 74	1·926 1·919	75 74	1·988 1·981	75 74	2-060 2-048	75 74			•••••	
9 9] 10	1.852 1.845 1.888	72 71 69	1.912 1.906 1.898	72 71 70	1-974 1-967 1-960	72 71 70	2-086 2-029 2-022	78 71 70	*****		•••••	
10 1 11	1·881 1·824	68 67	1.891 1.884	69 67	1-968 1-946	69 68	2-015 2-008	69 68		*****	•••••	•••••
111 12 124	1.817	66 65	1.877	66 65	1.989	67 65	2·001 1·994	67 66				
18 18 184	1.808 1.796 1.790	64 62 61	1.868 1.857 1.850	64 68 62	1.925 1.918 1.911	64 68 62	1.987 1.980 1.978	65 68 62	•••••		*****	
14 144	1·788 1·776	60 59	1.848 1.886	61 60	1-904 1-897	61 60	1.966 1.959	61 60				
15 15 <u>1</u> 16	1.769 1.762 1.755	58 57 56	1.829 1.822 1.815	59 58 57	1.890 1.888 1.876	59 58 57	1.952 1.945 1.988	59 58 57	•••••	*****		
16½ 17	1·748 1·741	55 54	1.808 1.801	56 55	1·869 1·862	56 55	1.981 1.924	56 55		•••••		******
17 <u>1</u> 18 184	1·784 1·727 1·720	58 52 52	1·794 1·787 1·780	54 58 52	1.849 1.842	54 58 58	1.917 1.910 1.908	55 54 58			*****	
19 19	1·718 1·706	51 50	1.778 1.766	51 50	1.885 1.828	52 51	1.896 1.889	52 51			*****	
20 201	1-699 1-692	49 48	1·759 1·752	49	1.821 1.814	50 49	1.882 1.875	50 49	•••••			
21 21 22	1-685 1-679 1-672	47 47 46	1.745 1.788 1.782	48 47 46	1.807 1.800 1.798	48 48 47	1.868 1.861 1.854	49 48 47			•••••	
22½ 28	1-665 1-658	45 44	1·725 1·718	45 44	1·786 1·779	46 45	1·847 1·840	46 46				••••
284 24	1-651 1-644	48	1.711	44	1.772	44	1.888	44	•••••	•••••		
241 25	1.687 1.680	42	1-697 1-690	42 42	1·759 1·751	48 48	1·819 1·812	48 48	•••••	•••••		•••••

#		D	ngrees	OF TE	D WET	BULD	THERMO	METRE	.—YAHR	enher	r.	
Fabrea	10	7 °	10	8°	10	D°	110°		1110		119°	
t-t]	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humbdity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches	Relative Humbdity.	Force of Vapor, in inches.	Relative Humidity.
00	2.860	100	2.429	100	2.500	100	2.572	100	2-646	100	2.721	100

TABLES,

METEOROLOGICAL AND PHYSICAL,

PREPARED FOR

THE SMITHSONIAN INSTITUTION.

ev I no 3,

BY

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PROFESSOR OF GEOLOGY AND PHYSICAL GEOGRAPHY, COLLEGE OF NEW JERSEY.

THIRD EDITION,

WASHINGTON: SMITHSONIAN INSTITUTION. 1859.

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- I. Thermometrical Tables, marked A.
- II. Hygrometrical Tables, "B.
- III. Barometrical Tables, "C.
- IV. Hypsometrical Tables, "D.
- V. Meteorological Corrections, " E.
- VI. Miscellaneous Tables, "F.

Each series has an independent paging running through all the tables that it contains.

The letters A, B, C, D, E, F, at the bottom of each page, indicate the series, and the figure the folio of the series to which the page belongs.

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At the head of each series is found a detailed table of its contents.



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THERMOMETRICAL TABLES.

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PREFACE

TO THE FIRST EDITION.

To PROR JOSEPH HENRY,

Secretary of the Smithsonian Institution.

SIR, -

In compliance with your instructions, I have prepared the collection of Meteorological Tables contained in the following pages. I have endeavored to render it useful, not only to the observers engaged in the system of Meteorological Observations now in operation under the direction of the Smithsonian Institution, for whom it was immediately designed, but also to any Meteorologist who may desire to compare and to work out portions of the vast amount of Meteorological Observations already accumulated in the stores of science.

The reduction of the observations and the extensive comparisons, without which Meteorology can do but little, require an amount of mechanical labor which renders it impossible for most observers to deduce for themselves the results of their own observations. The difficulty is still further increased by the diversity of the thermometrical and barometrical scales which Meteorologists, faithful to old habits rather than to science and to reason, choose to retain, notwithstanding the additional labor they thus gratuitously assume to themselves. To relieve the Meteorologist of a great portion of this labor, by means of tables sufficiently extensive to render calculations and even interpolations unnecessary, is to save his time and his forces in favor of science itself, and thus materially contribute to its advancement. But most of the tables useful in Meteorology being scattered through many volumes, which are often not of easy access, this collection will be, it is hoped, acceptable to the friends of Meteorology, and will supply a want very much felt in this department of the physical sciences.

In the selection of the matter, I have been guided by the idea that the tables which I sought for my own use might also be those most likely to be wanted by others. But I wish the following to be considered as a first collection, containing only the tables most appropriate to the present purpose. They are, therefore, arranged in different and independent series, with distinct paging, but constituting together a frame-work into which any tables may be readily inserted when wanted, either to make the collection more complete, or to present a choice of tables calculated from somewhat different elements, or adapted to various methods of calculation.

The measurement of heights by means of the barometer being intimately connected with Meteorology, it was thought not inappropriate to admit into this collection Hypsometrical Tables, destined to render this kind of calculations more easy and more rapid, and thus to increase the taste for a method so useful in physical geography. I have preferred the tables of Delcros, as uniting in the greatest degree simplicity and accuracy. Those of Gauss, Bessel, and Baily may be given afterwards.

Every table contains directions for its use, when necessary; moreover, the indication of the elements used in its calculation, and of the source from which it has been taken. When no remark is made as to this last point, the table has been expressly calculated for this volume.

Very respectfully,

Your obedient servant,

A. GUYOT.

Cambridge, Mass., December 15th, 1851.

PREFACE

TO THE SECOND EDITION.

To PROF. JOSEPH HENRY,

Secretary of the Smithsonian Institution.

Sir, -

In sending to you the Meteorological Tables composing the first edition of this volume, published in 1852, I expressed the desire that they be considered as a first collection, containing the tables most needed at the time by the meteorological observers engaged in the system carried on under the supervision of the Smithsonian Institution, but destined to be increased. It was in that expectation, I remarked, that the tables had been arranged in independent series, as a kind of framework, into which a larger number could readily be inserted. It seemed, indeed, highly desirable to offer to the Meteorologist and Physical Geographer, not only the tables they daily need for working out the results of their observations, but also such a variety of tables, computed from different elements, or by different methods, or adapted to different measures, as to enable every one to choose among them those that he most approves, and at the same time properly to compare and to appreciate the results obtained by others.

Thanks to the congenial spirit with which the elevated views of the founder of the Smithsonian Institution are carried out, that character of general usefulness is not wanting in the present volume. With your agreement, the present edition contains more than three times as much matter as the first; and a rapid indication of the additions will suffice to justify them, and to show that, in selecting or calculating the new tables, the object just mentioned was constantly kept in view

As to the tables in the first edition, I must remark that, several of them having been printed in my absence, the copy prepared for the printer, in which decimals had to be left out, failed to give always the nearest value. Though these errors are too small to have any importance whatsoever in Meteorology, a careful revision of all the tables on the original computations was made, and they were corrected in the present edition. The few actual misprints which were discovered are indicated in a table of errata to the first edition.

In the Thermometrical series six small tables have been added; they were prepared for converting into each other differential results given in degrees of any one of the three thermometrical scales, irrespective of their zero point.

The Hygrometrical series has been entirely reorganized. It only contained five tables, all in French measures, and the Appendix. It is now composed of twenty-seven, arranged in three divisions. In the first are found ten tables, based on Regnault's hygrometrical constants, both in French and in English measures, in two corresponding sets, for the use of the psychrometer, the dew-point instruments, and for computing the weight of vapor in the air. The whole set in English measures, and Table V. in French measures, have been prepared for this edition. Being based on the best elements we now possess, they are given here for ordinary use. The second division contains the seven most important tables published in the Greenwich Observations, and Glaisher's extensive Psychrometrical Table. These tables being much used in England, and the results obtained by them exhibiting no inconsiderable differences from those derived from the preceding ones, they are indispensable for comparing these results. The third division, composed of ten miscellaneous tables, furnishes the means of comparing the different values of the force and the weight of vapor, especially those which have frequently been used in Germany, and also of reducing the indications of Saussure's Hair-Hygrometer to the ordinary scale of moisture. The Appendix has remained as in the first edition, but all the tables have been revised and corrected.

The Barometrical series, now in four divisions, has been increased from twelve to twenty-eight tables. Excepting three small tables for capillary action, all the new ones have been computed for this edition. The comparison, now so much needed, of the Russian barometer with the other scales, appears here for the first time.

The Hypsometrical series is almost entirely new. It contained only Delcros's table for barometric and Regnault's table for thermometric measurements, besides two auxiliary tables and the thirteen small tables of the Appendix. It now offers twenty-three tables for barometrical measurement of heights, in which all the principal formulæ and scales are represented; three for the measurement of heights by the thermometer, in French and in English measures; and a rich Appendix of forty-four tables, more extensive and convenient than those in the old set, which afford the means of readily converting into each other all the measures usually employed for indicating altitudes.

The series of Meteorological Corrections for periodic and non-periodic variations, for all parts of the world, mostly due to the untiring industry of Professor Dove, is an addition which will surely be appreciated by those who know how difficult access to the original tables is for most Meteorol-

ogists. A few tables have been added to Dove's collection, computed by Glaisher, Captain Lefroy, and by myself. Most of the tables refer to temperature, only two to moisture. Two tables of Barometrical Corrections have been placed in the Hypsometrical series, where they were needed, until they can be joined by others to make a set in this series, which still awaits new contributions, especially for these last two departments.

The Miscellaneous series is but begun. I have prepared a list of useful tables, which would be no doubt welcome to the lovers of Terrestrial Physics, and which may be published at some future occasion, if you should then find it expedient.

The present collection being designed, not for the scientific only, but for the observers at large, the propriety of the explicit and popular form of the explanations which accompany the tables, and of the directions for using them, will readily be understood.

I close by the remark, that, in every instance, the works from which the tables were taken have been carefully noted, and due credit given to their authors. For all the tables without author's names, I am myself responsible.

I remain, Sir,

Very respectfully, yours,

A. GUYOT.

PRINCETON, N. J., December, 1857.

PREFACE

TO THE THIRD EDITION.

A NEW series of Hygrometrical Tables, based on Regnault's Table of Elastic Forces of Vapor, has been published by Mr. Glaisher, in London, 1856. As, however, the Psychrometrical Table has not been computed from Regnault's formula, but by means of empirical factors, the results differ from those contained in Table VII. B. A table containing Glaisher's empirical factors, therefore, has been added, and will be found on page 144 B.

Table XVIII. of the Barometrical set, C, page 72, of the Second Edition, for reducing to the freezing point the Barometers with glass or wooden scales, copied from the Instructions of the Royal Society of London, and which is reprinted in most of the English works on Meteorology, having been found erroneous, a new table has been computed and substituted for it. As a large number of observers still use barometers with wooden scales, it was found advisable to enable them to make the needed interpolations at sight, by giving the corrections for every degree of the thermometer, from 0° to 100° Fahr., and for barometric heights ranging between 26 and 31 inches.

The small Table VI. D, page 48, of the Hypsometrical Tables by the writer, having been found useful for rapid computation of approximate results, a larger one of the same description, which allows to make at sight every interpolation, has been added, on page 92, as Table XIX'. The scientific traveller, wishing to determine, when ascending a mountain, the elevation of the physical or geological phenomena that he meets with, such as the stations of remarkable plants, limits of zones of vegetation,—the geologist who uses the aneroid barometer for geological sections,—the engineer who wishes to know, on the ground, approximately, his results,—will find it convenient to obtain the relative heights indicated by their instrument by a simple multiplication. The use of the table is explained page D 90.

Some of the decimals in the smaller Table VI. D, page 48, above mentioned, have been slightly altered in order to make both tables agree.

In set E of Meteorological Corrections, a table of corrections derived by Professor C. Dewey from the hourly observations of Professor Snell, at Amherst College, has been added, which will be of service especially to the numerous observers in New England and in the neighboring States.

The errata indicated in the Second Edition, and a few unimportant ones found since, have been corrected. No other changes have been made in this edition.

A. GUYOT.

I.-III.

GENERAL COMPARISON

OF

THE THERMOMETRICAL SCALES,

OR

TABLES

SHOWING THE CORRESPONDING VALUES OF EACH FULL DEGREE OF FAHRENHEIT'S,

CENTIGRADE, AND REAUMUR'S THERMOMETERS, FROM

+212° TO -89° FAHRENHEIT.



COMPARISON OF THE THERMOMETRICAL SCALES.

THE first three tables of this set give a simultaneous comparison of the three scales mostly used at present in Meteorology, and especially of the portion of the scales not comprised in the more extensive tables which follow them. They form thus a complement to these last tables; but as most of the temperatures contained in them do not occur in Meteorology, the comparison of the full degrees was found sufficient.

These three tables have been taken from E. L. Schubarth's Collection of Physical Tables. Berlin, 1836.

Tables IV. to IX. being more useful to the Meteorologist, the calculation has been carried out for every tenth of a degree. Tables VII. and IX. are from the Annuaire Météorologique de France; the others have been calculated.

A comparison of the Centigrade and Fahrenheit degrees near the boiling point, for every tenth of a degree, for the sake of the comparison of standard thermometers, will be found at the end of Table VI.

Tables X. to XV. will be found useful for comparing differential results, such as ranges of temperature, and any relative amount expressed in degrees of different scales, without reference to their respective zeros.

I. COMPARISON OF FAHRENHEIT'S THERMOMETRICAL SCALE WITH THE CENTIGRADE AND REAUMUR'S.

 x^0 Fahr. = $(x^0 - 32^0)$ † Centig. = $(x^0 - 32^0)$ † Reaum.

	T		1	(Ĭ	T	
Fahren.	Centigrade.	Recomur.	Fahren.	Centigrade.	Recumur.	Fahren.	Centigrade.	Reaumur.
+212	+100.00	+80.00	+172	+77.78	+62.22	+132	+55.56	+44.44
211	99.44	79.56	171	77.22	61.78	181	55.00	44.00
210	98.89	79.11	170	76.67	61.38	130	54.44	43.56
209	98.33	78.67	169	76.11	60.89	129	53.89	43.11
208	97.78	78.22	168	75.56	60.44	128	58-83	42.67
207	97.22	77.78	167	75.00	60.00	127	52.78	42.22
206	96.67	77.88	166	74.44	59.56	126	52.22	41.78
205	96.11	76.89	165	73.89	59.11	125	51.67	41.33
204	95.56	76.44	164	78.83	58.67	124	51.11	40.89
203	95.00	76.00	163	72.78	58.22	123	50.56	40.44
202	94.44	75.56	162	72.22	57.78	122	50.00	40.00
201	98.89	75.11	161	71.67	57.33	121	49.44	39.56
200	93.38	74.67	160	71.11	56.89	120	48.89	39.11
199	92.78	74.22	159	70.56	56.44	119	48.33	88.67
198	92.22	73.78	158 -	70.00	56.00	118	.47.78	38.22
197	91.67	73.88	157	69.44	55.56	117	47.22	37.78
196	91.11	72.89	156	68.89	55.11	116	46.67	37.38
195	90.56	72.44	155	68.83	54.67	115	46.11	36.89
194	90.00	72.00	154	67.78	54.22	114	45.56	36.44
198	89.44	71.56	153	67.22	53.78	113	45.00	36.00
192	88.89	71.11	152	66.67	53.88	112	44.44	35.56
191	88-33	70.67	151	66.11	52.89	111	43.89	85.11
190	87.78	70.22	150	65.56	52.44	110	43.83	34.67
189	87.22	69.78	149	65.00	52.00	109	42.78	34.22
188	86.67	69.88	148	64.44	51.56	108	42.22	33.78
187	86.11	68.89	147	63.89	51.11	107	41.67	83.83
186	85.56	68.44	146	63.88	50.67	106	41.11	32.89
185	85.00	68.00	145	62.78	50.22	105	40.56	82.44
184	84.44	67.56	144	62.22	49.78	104	40.00	82.00
183	83.89	67.11	148	61.67	49.83	108	89.44	81.56
182	83.83	66.67	142	61.11	48.89	102	88.89	81.11
181	82.78	66.22	141	60.56	48.44	101	88.33	30.67
180	82.22	65.78	140	60.00	48.00	100	87.78	80.22
179	81.67	65.88	139	59.44	47.56	99	87.22	29.79
178	81.11	64.89	188	58.89	47.11	98	36.67	29.83
177	80.56	64.44	187	58.33	46.67	97	86.11	28.89
176	80.00	64.00	136	57.78	46.22	96	35.56	28.44
175	79.44	63.56	185	57.22	45.78	95	85.O	28.00
174	78.89	63.11	184	56.67	45.38	94	84.44	27.56
178	78.83	62.67	133	56.11	44.89	98	83.89	27.11
				1		<u> </u>	<u> </u>	l

8

 x^{0} Fahr. = $(x^{0} - 32^{0})$ Centig. = $(x^{0} - 32^{0})$ Resum.

Fahren.	Centigrade.	Resumur.	Fahren.	Centigrade.	Resumur.	Fahren.	Centigrade.	Resumu		
+92	+33.23	+26.67	+48	+ 8.89	+ 7.11	+ 4	-15.56	-12.44		
91	82.78	26.22	47	8.33	6.67	8	-16.11	-12.89		
90	82.22	25.78	46	7.78	6.22	2	-16.67	-18.38		
89	81.67	25.83	45	7.22	5.78	1	-17.22	-13.78		
88	81.11	24.89	44	6.67	5.33	0	-17.78	-14.22		
87	80.56	24.44	43	6.11	4.89	- 1	-18.33	-14.67		
86	80.00	24.00	42	5.56	4.44	- 2	-18.89	-15.11		
85	29.44	28.56	41	5.00	4.00	- 3	-19.44	-15.56		
84	28.89	28.11	40	4.44	8.56	- 4	-20.00	_16.00		
83	28.83	22,67	89	8.89	8.11	- 5	-20.56	-16.44		
82	27.78	22,22	88	8.38	2.67	- 6	-21.11	-16.89		
81	27.22	21.78	87	2.78	2.22	- 7	-21.67	_17.33		
80	26.67	21.83	36	2.22	1.78	- 8	-22.22	-17.78		
79	26.11	20.89	85	1.67	1.83	- 9	-22.78	-18.22		
78	25.56	20.44	84	1.11	0.89	-10	-28.38	-18.67		
77	25.00	20.00	83	0.56	0.44	-11	-23.89	-19.11		
76	24.44	19.56	82	0.00	0.00	-12	-24.44	-19.56		
75	23.89	19.11	81	- 0.56	- 0.44	-13	-25.00	-20.00		
74	23.83	18.67	30	- 1.11	- 0.89	-14	-25.56	-20.44		
73	22.78	18.22	29	- 1.67	- 1.88	-15	-26.11	-20.89		
72	22.22	17.78	28	- 2.22	- 1.78	-16	-26.67	-21.83		
71	21.67	17.33	27	- 2.78	- 2.22	-17	-27.22	-21.78		
70	21.11	16.89	26	- 3.33	- 2.67	-18	-27.78	-22.22		
69	20.56	16.44	25	- 3.89	- 8.11	-19	-28.83	-22.67		
68	20.00	16.00	24	- 4-44	- 3.56	-20	-28.89	-23.11		
67	19.44	15.56	23	- 5.00	- 4.00	-21	-29.44	-23.56		
66	18.89	15.11	22	- 5.56	- 4.44	-22	-80.00	-24.00		
65	18.33	14.67	21	- 6.11	- 4.89	-23	-80.56	-24.44		
64	17.78	14.22	20	- 6.67	- 5.88	-24	-31.11	-24.89		
63	17.22	13.78	19	- 7.22	- 5.78	-25	-31.67	-25.83		
62	16.67	18.88	18	- 7.78	- 6.22	-26	-32.22	-25.78		
61	16.11	12.89	17	- 8.33	- 6.67	-27	-82.78	-26.22		
60	15.56	12.44	16	- 8.89	- 7.11	-28	-33.83	-26.67		
59	15.00	12.00	15	- 9.44	- 7.56	-29	-33.89	-27.11		
58	14.44	11.56	14	-10.00	- 8.00	-80	-84.44	-27.56		
57	13.89	11.11	13	-10.56	- 8.44	-31	-35.00	-28.0 0		
56	13.33	10.67	12	-11-11	- 8.89	-32	-35.56	-28.44		
55	12.78	10.22	11	-11.67	- 9.33	-83	-86.11	-28.89		
54	12.22	9.78	10	-12.22	- 9.78	-34	-36.67	-29.38		
53	11.67	9.88	9	-12.78	-10.22	-35	-37.22	-29.78		
52	11.11	8.89	8	-13.33	-10.67	-36	-37.78	-30.22		
51	10.56	8.44	7	-18.89	-11.11	-37	-38.33	-30.67		
50	10.00	8.00	6	-14-44	-11.56	-38	-38.89	-31-11		
49 9.44 7.56 5 -15.00 -12.00 -39 -39.44 -31.56										

II. COMPARISON OF THE CENTIGRADE THERMOMETER WITH REAUMUR'S AND FAHRENHEIT'S.

 x° Centig. = $(82 + \frac{3}{4} x^{\circ})$ Fahr. = $\frac{4}{4} x^{\circ}$ Resum.

Centig.	Resumur.	Fahrenheit.	Centig.	Resumur.	Fahrenheit.	Centig.	Resumur.	Pahrenheit.
+100	+80-0	+212.0	+88	+66.4	+181.4	+ 66	+52.8	+150.8
99	79.2	210.2	82	65.6	179.6	65	52.0	149.0
98	78.4	208.4	81	64.8	177.8	64	51.2	147.2
97	77.6	206.6	80	64.0	176.0	63	50.4	145.4
96	76.8	204.8	79	68.2	174.2	62	49.6	148.6
95	76.0	208.0	78	62.4	172.4	61	48.8	141.8
94	75.2	201.2	77	61.6	170.6	60	48.0	140.0
93	74.4	199.4	76	60.8	168.8	59	47.2	138.2
92	78.6	197.6	75	60.0	167.0	58	46.4	136.4
91	72.8	195.8	74	59.2	165.2	57	45.6	184.6
90	72.0	194.0	78	58.4	168.4	56	44.8	132.8
89	71.2	192.2	72	57.6	161.6	55	44.0	181.0
88	70.4	190.4	71	56.8	159.8	54	48.2	129.2
87	69.6	188.6	70	56.0	158.0	58	42.4	127.4
86	68.8	186.8	69	55.2	156.2	52	41.6	125.6
85	68.0	185.0	68	54.4	154.4	51	40.8	128.8
84	67.2	188.2	67	58.6	152.6	50	40.0	122.0
								1

For the Continuation see Tables V. and VI.

III. COMPARISON OF REAUMUR'S THERMOMETER WITH FAHRENHEIT'S AND THE CENTIGRADE.

 x° Reaum. = $(32^{\circ} + \frac{3}{4}x^{\circ})$ Fahr. = $\frac{1}{4}x^{\circ}$ Centig.

Resumur.	Fahrenheit.	Centigrade.	Resumur.	Fahrenheit.	Centigrade.	Resumur.	Fahrenheit.	Centigrade.
+80	+212.00	+100.00	+66	+180.50	+82-50	+52	+149.00	+65.00
79	209.75	98.75	65	178.25	81.25	51	146.75	68.75
78	207.50	97.50	64	176.00	80.00	50	144.50	62.50
77	205.25	96.25	68	178.75	78.75	49	142.25	61.25
76	208.00	95.00	62	171.50	77.50	48	140.00	60.00
75	200.75	98.75	61	169.25	76.25	47	187.75	58.75
• 74	198.50	92.50	60	167.00	75.00	46	185.50	57.50
78	196.25	91.25	59	164.75	78.75	45	138.25	56.25
72	194.00	90.00	58	162.50	72.50	44	181.00	55.00
71	191.75	88.75	67	160.25	71.25	43	128.75	58.75
70	189.50	87.50	56	158.00	70.00	42	126.50	52.50
69	187.25	86.25	55	155.75	68.75	41	124.25	51.25
68	185.00	85.00	54	158.50	67.50	40	122.00	50.00
67	182.75	88.75	58	151.25	66.25	89	119.75	48.75

For the Continuation see Tables VIII. and IX.

IV. - V.

COMPARISON

OF

FAHRENHEIT'S THERMOMETER

WITH

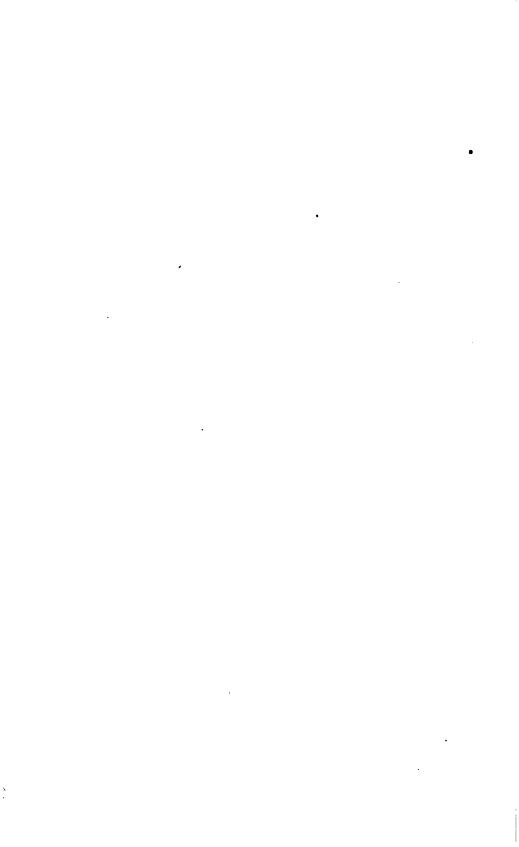
THE CENTIGRADE AND WITH THAT OF REAUMUR,

OR

TABLES

FOR CONVERTING THE DEGREES OF FAHRENHEIT INTO CENTIGRADE DEGREES AND INTO DEGREES OF REAUMUR;

GIVING THE CORRESPONDING VALUES FOR EACH TENTH OF Δ DEGREE, FROM $+122^{\circ}$ TO -76° FAHRENHEIT.



Dagress of Fahren-					Tenths of	Dogrees.				· · · · · · · · · · · · · · · · · · ·
Fahren- helf.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
+122	Centig.	Centig.	Centig.	Centig.	Centig.	Centig. +50.28	Centig. +50.88	Centig.	Centig. +50.44	Centig.
121	+50.00	+50.06 49.50	+50.11 49.56	+50.17 49.61		49.72	49.78	+50.39 49.83	49.89	+50.50 49.94
120	48.89	49.94	49.00	49.06	49.67 49.11	49.17	49.22	49.28	49.88	49.39
119	48.83	48.39	48.44	48.50	48.56	48.61	48.67	48.72	48.78	48.83
118	47.78	47.83	47.89	47.94	48.00	48.06	48.11	48.17	48.22	48.28
117	47.22	47-28	47.83	47-89	47.44	47.50	47.56	47.61	47.67	47.72
116	46.67	46.72	46.78	46.83	46.89	46.94	47.00	47.06	47.11	47.17
115	46.11	46.17	46.22	46.28	46.83	46.89	46.44	46.50	46.56	46.61
114	45.56	45.61	45.67	45.72	45.78	45.83	45.89	45.94	46.00	46.06
113	45.00	45.06	45.11	45.17	45.22	45.28	45.88	45.39	45.44	45.50
112	44.44	44.50	44.56	44.61	44.67	44.72	44.78	44.83	44.89	44.94
111	43.89	43.94	44.00	44.06	44.11	44.17	44.22	44.28	44.83	44.89
110	43.88	48.89	48.44	48.50	48.56	48.61	48.67	48.72	43.78	43.88
109	42.78	42.83	42.89	42.94	43.00	48.06	48.11	48.17	48.22	48.28
108	42.22	42.28	42.33	42.89	42.44	42.50	42.56	42.61	42.67	42.72
107	41.67	41.72	41.78	41.88	41.89	41.94	42.00	42.06	42.11	42.17
106	41.11	41.17	41.22	41.28	41.83	41.89	41.44	41.50	41.56	41.61
105	40.56	40.61	40.67	40.72	40.78	40.88	40.89	40.94	41.00	41.06
104	40.00	40.06	40.11	40.17	40.22	40.28	40.88	40.89	40.44	40.50
103	39-44	39.50	89.56	89.61	89.67	89.72	39.78	89.83	39.89	89.94
102	38.89	88.94	89.00	39. 06	39.11	89.17	89.22	89.28	89.88	89.39
101	38.83	88.39	38.44	88.50	38.56	38.61	88.67	38.72	88.78	38.83
100	37.7 8	37.83	87.89	87.94	88.00	88.06	88.11	88.17	88.22	38.28
99 98	87.22	87.28	87.83	87.89	87.44	87.50	87.56	37.61	37.67	87.72
20	36.67	36.72	86.78	86.88	86.89	36.94	87.00	37.06	87.11	87.17
97	36.11	86.17	36.22	86.28	36.33	86.89	86.44	86.50	86.56	36.61
96	85.56	85.61	85.67	85.72	35.78	85.88	85.89	35.94	86.00	86.06
95	85.00	35.06	85.11	85.17	35.22	85.28	85.88	85.89	85.44	85.50
94 98	84.44	84.50	84.56	84.61	84.67	84.72	84.78	84.88	84.89	84.94
98	33. 89	88.94	84.00	84.06	84.11	84.17	84.22	84.28	34.33	84.39
92	88.83	88.89	83.44	83.50	88.56	88.61	83.67	88.72	88.78	88.83
91	82.78	82.83	82.89	82.94	88.00	83.06	88.11	83.17	88.22	83.28
90	82.22	\$2.28	82.88	32.89	82.44	82.50	32.56	32.61	82.67	82.72
89	31.67	81.72	81.78	81.88	81.89	31.94	32.00	82.06	32.11	88.17
88	81.11	81.17	81.22	81.28	\$1.88	31.39	31.44	31.50	31.56	31.61
87	30.56	80.61	80.67	30.72	30.78	30.83	80.89	20.94	81.00	31.06
86	80.00	80.06	30.11	80.17	30.22	80.28	80.88	80.89	80.44	30.50
85	29.44	29.50	29.56	29.61	29.67	29.72	29.78	29.83	29.89	29.94
84	28.89	28.94	29.00	29.06	29.11	29.17	29.22	29.28	29.33	29.89
83	28.88	28.39	28.44	28.50	28.56	28.61	28.67	28.72	28.78	28.83
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

Degrees of	,				Tenths o	Dogrees.				
Pahren- heit.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Centig.	Centig.	Centig.	Centig.	Centig.		Centig.	Centig.	Centig.	Centig.
+82	+27.78 27.22	+27.88 27.28	+27.89	+27.94 27.89		+26.06 27.50	+28.11	+28.17	+28.22	+28.28
81 80	26.67	26.72	27.88 26.78	26.83	27.44 26.89	26.94	27.56 27.00	27.61 27.06	27.67 27.11	27.72 27.17
79	26.11	26.17	26.22	26.28	26.83	26.89	26.44	26.50	26.56	26.61
78	25.56	25.61	25.67	25.72	25.78	25.88	25.89	25.94	26.00	26.06
77 76	25.00 24.44	25.06 24.50	25.11 24.56	25.17 24.61	25.22 24.67	25.28 24.72	25.33 24.78	25.89 24.88	25.44 24.89	25.50 24.94
75	28.89	28.94	24.00	24.06	34.11	24.17	24.22	24.28	24.88	24.89
74	28.83	28.39	28.44	28.50	23.56	23.61	28.67	28.72	25.78	23.63
78	22.78	22.68	22.89	22.94	28.00	28.06	28.11	28.17	28.22	23.28
	00 00) 00 00	00 00	00.00	00.44	22,50	00 70	66.01	00.00	
72	22.22 21.67	22.28 21.72	22.88 21.78	22.89 21.88	22.44 21.89	21.94	22.56 22.00	22.61 22.06	22.67	22.72
71 70	21.07	21.72	21.78	21.28	21.33	21.89	21.44	21.50	22.11 21.56	22.17 21.61
69	20.56	20.61	20.67	20.72	20.78	20.88	20.89	20.94	21.00	21.06
68	20.00	20.06	20.11	20.17	20.22	20.28	20.88	20.39	20.44	20.50
67	19.44	19.50	19.56	19.61	19.67	19.72	19.78	19.83	19.89	19.94
66	18.89	18.94	19.00	19.06	19.11	19.17	19.22	19.28	19.33	19.89
63	18.83	18.39	18.44	18.50	18.56	18.61	18.67	18.72	18.78	18.88
64	17.78	17.83	17.89	17.94	18.00	18.06	18.11	18.17	18.22	18.28
63	17.22	17.28	17.83	17.89	17.44	17.50	17.56	17.61	17.67	17.72
62	16.67	16.72	16.78	16.83	16.89	16.94	17.00	17.06	17.11	17.17
61	16.11	16.17	16.22	16.28	16.33	16.39	16.44	16.50	16.56	16.61
60	15.56	15.61	15.67	15.72	15.78	15.83	15.89	15.94	16.00	16.06
59	15.00	15.06	15.11	15.17	15.22	15.28	15.33	15.89	15.44	15.50
58	14.44	14.50	14.56	14.61	14.67	14.72	14.78	14.88	14.89	14.94
57	13.89	13.94	14.00	14.06	14.11	14.17	14.22	14.28	14.33	14.39
56	18.83	18.39	18.44	18.50	18.56	18.61	18.67	18.72	18.78	18.83
55	12.78	12.83	12.89	12.94	18.00	13.06	18.11	18.17	18.22	18.28
54	12.22	12.28	12.83	12.39	12.44	12.50	12.56	12.61	12.67	12.72
58	11.67	11.72	11.78	11.88	11.89	11.94	12.00	12.06	12.11	12.17
52	11.11	11.17	11.22	11.28	11.83	11.89	11.44	11.50	11.56	11.61
51	10.56	10.61	10.67	10.72	10.78	10.88	10.89	10.94	11.00	11.06
50	10.00	10.06	10.11	10.17	10.22	10.28	10.33	10.89	10.44	10.50
49	9.44	9.50	9.56	9.61	9.67	9.72	9.78	9.88	9.89	9.94
48	8.89	8.94	9.00	9.06	9.11	9.17	9.22	9.28	9.33	9.39
47	8.83	8.89	8.44	8.50	8.56	8.61	8.67	8.72	8.78	8.83
46	7.78	7.83	7.89	7.94	8.00	8.06	8.11	8.17	8.22	8.28
45	7.22	7.28	7.33	7.89	7.44	7.50	7.56	7.61	7.67	7.72
44	6.67	6.72	6.78	6.88	6.89	6.94	7.00	7.06	7.11	7.17
43	6.11	6.17	6.22	6.28	6.33	6.89	6.44	6.50	6.56	6.61
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

Degrees of Fahren-		Tenths of Dogress.									
Fahren- beit.	•.	1.	2.	8.	4.	5.	6.	7.	8.	9.	
. 40	Centig. +5.56	Centig. +5.61	Centig. +5.67	Centig. +5.72	Centig. +5.78	Centig. +5.88	Centig. +5.89	Centig. +5.94	Centig. +6.00	Centig. +6.06	
+42 41	5.90	5.06	5.11	5.17	5.22	5.26	5.88	5.89	5.44	5.50	
40	4.44	4.50	4.56	4.61	4.67	4.72	4.78	4.88	4.89	4.94	
89	8.89	8.94	4.00	4.06	4.11	4.17	4.22	4.28	4.38	4.89	
88	8-83	8.29	8.44	8.50	3.56	8.61	3.67	3.72	3.78	8.88	
37	2.78	2.83	2.89	2.94	8.00	8.06	8.11	8.17	8.22	8.28	
36	2-22	2.28	2.23	2.89	2.44	2.50	2.56	2.61	2.67	2.72	
35	1.67	1.72	1.78	1.88	1.89	1.94	2.09	2.06	2.11	2.17	
34	1.11	1.17	1.22	1.28	1.83	1.39	1.44	1.50	1.56	1.61	
223	0.56	0.61	0.67	0.72	0.78	0.88	0.89	0.94	1.00	1.96	
82	0.00	0.06	0.11	0.17	0.22	0.26	0.83	0.39	0.44	0.50	
81	- 0.56	- 0.50	- 0.44	- 0.89	- 0.83	0.28	- 0.22	- 0.17	- 0.11	- 0.06	
20	- 1.11	- 1.06	- 1.00	- 0.94	- 6.89	- 0.83	- 0.78	- 0.72	- 0.67	- 0.61	
29 28	- 1.67 - 2.22	- 1.61 - 2.17	- 1.56 - 2.11	- 1.50 - 2.06	- 1.44 - 2.06	~ 1. 3 9 ~ 1. 9 4	- 1.88 1.89	- 1.28 - 1.88	- 1.22 - 1.78	- 1.17 - 1.72	
23	3.23	2.17	- Z.11	_ 3.00	- 2200	- 1.54	_ 1.59	- 1.85	- 1.78	- 1.72	
27	- 2.78	- 2.72	- 2.67	 2.6 1	- 2.56	- 2.50	- 2.44	- 2.89	_ 2.33	- 2.28	
26	- 3.83	- 8.28	- 3.22	- 8.17	- 8.11	- 8.06	- 8.00	- 2.94	- 2.89	- 2.83	
25	- 8.89	- 3.83	- 3.78	- 8.72	- 8.67	- 8 .61	- 8.56	- 8.50	- 8.44	- 8.39	
24	- 4.44	- 4.89	- 4.33	- 4.28	- 4.22	- 4.17	- 4.11	- 4.06	- 4.00	- 3.94	
23	5.00	- 4.94	- 4.89	- 4.88	- 4.78	- 4.72	- 4.67	- 4.61	- 4.56	- 4.50	
22	- 5.56	- 5.50	- 5.44	- 5.89	- 5.88	- 5.2 8	- 5.22	_ 5.17	- 5.11	- 5.06	
21	- 6.11	- 6.06	- 6.00	- 5.94	5.89	- 5.83	- 5.78	- 5.72	- 5.67	- 5.61	
20	- 6.67	- 6.61	- 6.56	- 6.50	- 6.44	- 6.89	- 6.83	- 6.28	- 6.22	- 6.17	
19	- 7.22	- 7.17	- 7.11	- 7.06	- 7.00	- 6.94	- 6.89	- 6.83	- 6.78	- 6.72	
18	- 7.78	- 7.72	- 7.67	- 7.61	- 7.56	- 7.50	- 7.44	- 7.89	- 7.88	- 7.2 8	
17	- 8.33	- 8.28	- 8.22	- 8.17	- 8.11		- 8.00	- 7.94	- 7.89	- 7.83	
16	- 8.89	- 8.83	- 8.78	- 8.72	- 8.67	- 8.61	- 8.56	- 8.50	- 8.44	- 8.39	
15	9.44	- 9.39	- 9.33	- 9.28	- 9.22	9.17	- 9.11	- 9.06	- 9.00	- 8.94	
14 13	-10.00 -10.56	- 9.94 -11.50	- 9.89 -10.44	- 9.83 -10.89	- 9.78 -10.88	- 9.72 -10. 2 8	- 9.67	- 9.61 -10.17	- 9.56 -10.11	- 9.50 -10.06	
10	10.00		10.43	10.03	-10.00	LOUD	10.22	-10.17	_10.11	-10.00	
12	-11.11	-11.06	-11.00	-10.94	-10.89	-10.88	-10.78	-10.72	-10.67	-10.61	
11	-11.67	-11.61	-11.56	-11.50	-11.44	-11. 3 9	-11.33	-11.28	-11.22	-11.17	
10	-12.22	-12.17	-12.11	-12.06	-12.00	-11.94	-11.89	-11.83	-11.78	-11.72	
9	-12.78	-12.72	-12.67	-12.61	-12.56	-12.50	-12.44	-12.39	-12.33	-12.28	
8	-13.33	-13.28	-18.22	-18.17	-18.11	-13.06	-13.00	-12.94	-12.89	-12.83	
7	-13.89	-13.83	-13.78	-13.72	-13.67	-13.61	-13.56	-13.50	-18.44	-18.39	
6	-14.44	-14.89	-14.83	-14.28	-14.22	-14.17	-14.11	-14.06	-14.00	-13.94	
Б	-15.00	-14.94	-14.89	-14.83	-14.78	-14.72	-14.67	-14.61	-14.56	-14.50	
4	-15.56	-15.50	-15.44	-15.89	-15.83	-15.28	-15.22	-15.17	-15.11	-15.06	
3	-16.11	-16.06	-16.00	-15.94	-15.89	-15.83	-15.78	-15.72	-15.67	-15.61	
1	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.	

Contig. Cont					Dogress.	Tenths of					Degrees of
+ 2	9.	8.	7.	6.	5.	4.	8.	2.	1.	_	Degrees of Fahren- heit.
1											
0									I	ll .	i
	1							ı		ll l	
	1	I	i	1	l	1		ı		II	1
- 2										11	
- 3				10.0.	10.01	10.00	20.00	20.72	10.00	10.00	- 1
-3 −19.44 −19.50 −19.66 −19.61 −19.67 −19.72 −19.78 −19.83 −19.89 -4 −20.06 −20.61 −20.67 −20.72 −20.78 −20.89 −20.89 −20.94 −21.00 -6 −21.11 −21.17 −21.22 −21.28 −21.38 −21.89 −21.44 −21.50 −21.66 -7 −21.67 −21.72 −21.78 −31.83 −21.89 −21.94 −22.00 −22.06 −22.11 -8 −22.22 −22.28 −22.89 −22.99 −22.44 −22.00 −22.06 −22.11 -9 −22.78 −22.89 −22.89 −22.44 −22.00 −22.06 −22.17 −22.72 −22.67 −22.67 −22.67 −22.67 −22.72 −22.88 −22.89 −22.44 −22.00 −22.06 −22.17 −22.66 −22.61 −22.67 −22.67 −22.50 −22.56 −23.61 −22.67 −22.72 −22.80 −23.11 −22.17 −24.28<	-19.89	-19.33	-19.28	-19.22	-19.17	-19.11	-19.06	-19.00	-18.94	-18.89	- 2
- 5	-19.94	-19.89	-19.83	-19.78	-19.72	-19.67	-19.61	-19.56	-19.50	-19.44	1
- 6	1		-20.89	-20.83		-20.22	20.17	-20.11	-20.06	-20.00	- 4
- 7	1							20.67	-20.61	-20.56	- 5
-8 -22.22 -22.28 -22.38 -22.39 -22.44 -22.50 -22.56 -22.61 -22.67 -9 -22.78 -22.88 -22.89 -22.94 -23.00 -23.06 -23.11 -23.17 -23.22 -10 -23.89 -23.94 -24.00 -24.06 -24.11 -24.17 -24.22 -23.72 -23.78 -11 -23.89 -23.94 -24.00 -24.06 -24.11 -24.17 -24.22 -24.28 -25.28 -25.38 -25.39 -25.44 -26.00 -25.66 -25.67 -25.72 -25.78 -25.28 -25.28 -25.28 -25.28	-21.61	-21.56	-21.50	-21.44	-21.39	-21.83	-21.28	-21.22	-21.17	-21.11	- 6
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Degrees of					Tenths o	f Degrees.				
Fahren- heit.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
-37	Centig38.33	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.
-38	-38.89	-38.39 -38.94	-88.44 -89.00	-38.50 -39.06	-38.56 -39.11	-38.61 -39.17	-88.67	-38.72	-38.78	-88.88
-39	-39.44	-39.50	-39.56	-39.61	-39.67	-39.72	-39.22 -39.78	- 39.2 8 - 39.83	-39.83 -39.89	-89.89
-40	-40.00	-40.06	-40.11	-40.17	-40.22	-40.28	-40.83	-40.89	-40.44	-89.94 -40.50
-41	-40.56	-40.61	-40.67	-40.72	-40.78	-40.83	-40.89	-40.94	-41.00	-41.06
	H	1					10.00			42.00
-42	-41.11	-41.17	-41.22	-41.28	-41.83	~41.89	-41.44	-41.50	-41.56	-41.61
-43	-41.67	-41.72	-41.78	-41.83	-41.89	-41.94	-42.00	-42.06	-42.11	-42.17
-44	-42.22	-42.28	-42.83	-42.89	-42.44	-42.50	-42.56	-42.61	-42.67	-42.72
-45	-42.78	-42.93	-42.89	-42.94	-43.00	-48.06	-48.11	-48.17	-48.22	-43.28
-46	-43.83	-43.39	-48.44	-43.50	-43.56	-43.61	-48.67	-43.72	-43.78	-43.88
	40.00			l		l				
-47 -48	-43.89	-43.94	-44.00	-44.06	-44.11	-44.17	-44.22	-44.28	-44.38	-44.89
-49	-11.44	-44.50	-44.56	-44.61	-14.67	-14.72	-14.78	-44.83	-44.89	-44.94
-19 -50	-45.00 -45.56	-45.06 -45.61	-45.11 -45.67	-45.17 -45.72	-45.22 -45.78	-45.28 -45.83	-45.38	-45.89	-45.44	-45.50
-51	-46.11	-46.17	-46.22	-46.28	-46.33	-46.89	-45.89 -46.44	-45.94 -46.50	-46.00	-46.06
•	40.11	-40.17	40.22	-40.25	-40.55	10.00	-40.44	-40.00	-16.56	-46.61
-52	-46.67	-46.72	-46.78	-46.83	-46.89	-46.94	-47.00	-17.06	-47.11	-47.17
-53	-47.22	-47.28	-47.83	-47.39	-47-44	-17.50	-47.56	-47.61	-47.67	-47.72
-54	-47.78	-47.83	-47.89	-47.94	-48.00	-48.06	-48.11	-48.17	-48.22	-48.28
-55	-48.33	-48.39	-48.44	-48.50	-48.56	-48.61	-48.67	-48.72	-48.78	-48.83
-56	-48.89	-48.94	-49.00	-49.06	-49.11	-49.17	-49.22	-49.28	-49.83	-49.89
	ì	i			1	1	İ			}
-57	-49.44	-49.50	-49.56	-49.61	-49.67	-49.72	-49.78	-49.83	-49.89	-49.94
-38	-50.00	-50.06	-50.11	-50.17	-50.22	-50.28	-50.88	-50.39	-50.44	-50.50
-59	-50.56	-50.61	-50.67	-50.72	-50.78	-50.83	-50.89	-50.94	-51.00	-51.06
60	-51.11	-51.17	-51.22	-51.28	-51.33	51.39	-51.44	-51.50	-51.56	-51.61
-61	-51.67	-51.72	-51.78	-51.83	-51.89	-51.94	-52.00	-52.06	-52.11	-52.17
-62	-52.22		-52.33							
-63	-52.78	-52.28		-52.39	-52.44	-52.50	-52.56	-52.61	-52.67	-52.72
-64	-53.83	-52.83 -53.39	-52.89 -53.44	-52.94	-53.00	-53.06 -53.61	-53.11	-53.17	-58.22	-53.28
-65	-53.89	-53.94	-54.00	-53.50 -54.06	-53.56 -54.11	-54.17	-53.67 -54.22	-53.72 -54.28	-53.78 -54.33	-53.83 -54.89
-66	-54.44	-54.50	-54.56	-54.61	-54.67	-54.17 -54.72	-54.78	-54.8 8	-54.89	-54.94
	0.000	02.00		04.01	04.01	1 04:12	04.70	04.00	-04.00	04.04
-67	-55.00	-55.06	-55.11	-55.17	-55.22	-55.28	-55.33	-55.39	-55.44	-55.50
68	-55.56	-55.61	-55.67	-55.72	-55.78	-55.83	-55.89	-55.94	-56.00	-56.06
-69	-56.11	-56.17	-56.22	-56.28	-56.83	-56.39	-56.44	-56.50	-56.56	-56.61
-70	-56.67	-56.72	-56.78	-56.88	-56.89	-56.94	-57.00	-57.06	-57.11	-57.17
-71	-57.22	-57.28	-57.83	-57.89	-57.44	-57.50	-57.56	-57.61	-57.67	-57.72
i		1		l			1			1
-72	-57.78	-57.83	-57.89	-57.94	-58.00	-58.06	-58.11	-58-16	-58.22	-58.28
-73	-58.88	-58.39	-58.44	-58.50	-58.56	-58.61	-58.67	-58.72	-58.78	-58.83
-74	-58.89	-58.94	-59.00	-59.06	59.11	-59.17	-59.22	-59.28	-59.33	-59.39
-75	-59.44	-59.50	-59.56	-59.61	-59.67	-59.72	-59.78	-59.88	-59.89	-59.94
-76	-60.00	-60.06	-60.11	-60.17	-60.22	-60.28	6 0.83	-6 0.39	-60.44	-60.50
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
					1~	•	-			
A					17	-				

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Degrees of		- 			Tenths of	a Degree.				
Fahren- heit.	●.	1.	2.	8.	4.	5.	6.	٧.	8.	9.
	Resumur.	Beaumur.	Resumur.	Regumur.	Recumur.	Resumur.	Resumur.	Resumur.	Resumur.	Resumu
+122	+40.00	+40.04	+40.09	+40.13	+40.18	+40.22	+40.27	+40.81	+40.86	+40.40
121	89.56	89.60	89.64	89.69	89.78	89.78	39.82	39.87	89.91	39.96
120	89.11	39. 16	39.20	89.24	89.29	39.23	39.38	89.42	89.47	89.51
119	88.67	38.71	38.76	88.80	38.84	38.89	38.93	38.98	89.02	89.07
118	38.22	88.27	38.31	38.36	38.40	88.44	88.49	88.58	38.58	\$8.62
117	87.78	87.82	37.87	87.91	87.96	88.00	88.04	88.09	38.13	38.18
116	87.88	37.38	87.42	87.47	87.51	87.56	87.60	87.64	37.69	87.78
115	\$6. 89	86.98	86.9 8	87.02	87.07	87.11	37.16	37.20	87.24	87.29
114	86.44	36.49	36.58	86.58	86.62	86.67	86.71	86.76	86.80	86.84
113	86.00	86.04	86.09	36.18	36.18	86.22	86.27	86.31	36.36	86.40
112	35.56	85.60	85.64	85.69	85.78	85.78	85.82	85.87	35.91	85.96
111	85.11	85.16	35.20	25.24	35.29	85.83	85.38	85.42	85.47	85.51
110	84.67	84.71	84.76	84.80	84.84	84.89	34.93	84.98	85.02	85.07
109	34.22	84.27	84.31	84.86	84.40	84.44	84.49	84.53	84.58	84.62
108	88.78	83.82	88.87	88.91	83.96	84.00	84.04	34.09	84.18	84.18
107	88.88	33.88	88.42	38.47	88.51	83.56	88.60	88.64	33.69	83.78
106	82.89	82.98	82.98	88.02	83.07	83.11	83-16	83.20	33.24	33.29
105	82.44	82.49	82.58	82.58	82.62	82.67	82.71	32.76	32.80	82.84
104	82.00	82.04	82.09	82.18	82.18	82.22	82.27	82.31	32.36	82.40
103	81.56	81.60	81.64	81.69	81.73	81.78	81.82	31.87	81.91	81.96
102	31-11	81.16	31. 2 0	81.24	31.29	31.38	31.88	81.42	81.47	31.51
101	80.67	80.71	80.76	80.80	20.84	80.89	30.98	80.98	81.02	81.07
100	30.22	80.27	80.31	30.36	80.40	80.44	80.49	80.53	80.58	80.62
99	29-78	29.82	29.87	29.91	29.96	80.00	80.04	80.09	80.18	80.18
98	29.88	29.88	29.42	29.47	29.51	29.56	29.60	29.64	29.69	29.78
97	28.89	28.98	28.98	29.02	29.07	29.11	29.16	29.20	29.24	29.20
96	28.44	28.49	28.53	28.58	28.62	28.67	28.71	28.76	28.80	28.84
95	28.00	28.04	28.09	28.18	28.18	28.22	28.27	28.31	28.36	28.40
94	27.56	27.60	27.64	27.69	27.78	27.78	27.82	27.87	27.91	27.96
98	27.11	27.16	27.20	27.24	27.29	27.33	27.38	27.42	27.47	27.5
92	26.67	26.71	26.76	26.80	26.84	26.89	26.98	26.98	27.02	27.0
91	26.22	26.27	26.31	26.86	26.40	26.44	26.49	26.58	26.58	26.6
90	25.78	25.82	25.87	25.91	25.96	26.00	26.04	26.09	26.18	26.18
89	25.33	25.88	25.42	25.47	25.51	25.56	25.60	25.64	25.69	25.7
88	24.89	24.93	24.98	25.02	25.07	25.11	25.16	25.20	25.24	25.29
87	24.44	24.49	24.58	24.58	24.62	24.67	24.71	24.76	24.80	24.8
86	24.00	24.04	24.09	24.18	24.18	24.22	24.27	24.81	24.86	24.40
85	28.56	28.60	23.64	28.69	23.78	23.78	23.82	23.87	28.91	23.96
84	23.11	23.16	23.20	23.24	28.29	23.33	23.38	23.42	28.47	23.51
83	22.67	22.71	22.76	22.80	22.84	22.89	22.93	22.98	28.02	23.07
82	22.22	22.27	22.81	22.86	22.40	22.44	22.49	22.53	22.58	22.62
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

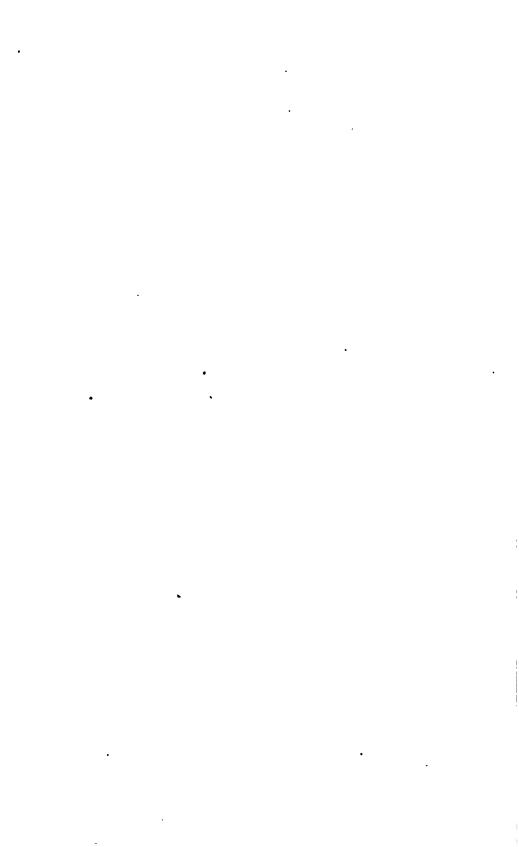
Degrees of Fahren-	Tenths of a Degree.											
Fahren- heit.	0.	. 1.	2.	8.	4.	5.	6.	7.	8.	9.		
.01		l .		Resumur. +21.91	1		Resumer. +22.04	Resumur. +22.09	Resumur.			
+81	+21.75 21.33	+21.82 21.38	+21-87 21.42	21.47		+22.00 21.56			+22.18	+22.18		
80 79		20.93	20.98	21.02	21.51		21.60	21.64	21.69	21.78		
78	20.89	20.49	20.58	20.58	21.07 20.62	21.11	21.16	21.20	21.24	21.29		
77	20.00	20.45	20.09	20.18	20.02	20.07	20.27	20.76	20.86	20.40		
"	20.00	20.03	20.00	20.15	20.40	20.52	20.27	40.01	20.00	20.40		
76	19-56	19.60	19.64	19.69	19.78	19.78	19.82	19.87	19.91	19.96		
75	19.11	19.16	19.20	19.24	19.29	19.33	19.38	19.42	19.47	19.51		
74	18.67	18.71	18.76	18.80	18 84	18.89	18.93	18.98	19.02	19.07		
78	18.22	18-27	18.31	18.86	18.40	18.44	18.49	18.53	18.58	18.62		
72	17.78	17.82	17.87	17.91	17.96	18-00	18.04	18.09	18.13	18.18		
				ĺ			1	1	ŀ			
71	17.38	17.88	17.42	17.47	17.51	17.56	17.60	17.64	17.69	17.78		
70	16.89	16.98	16.98	17.02	17.07	17.11	17.16	17.20	17.24	17.29		
69	16.44	16.49	16.58	16.58	16.62	16.67	16.71	16.76	16.80	16.84		
68	16.00	16.04	16.09	16.13	16.18	16.22	16.27	16.31	16.86	16.40		
67	15.56	15.60	15.64	15.69	15.78	15.78	15.82	15.87	15.91	15.96		
66	15.11	15.16	15.20	15.24	15.00	15.88	15.38	15.42	15.47	1		
65	14.67	14.71	14.76	14.80	15.29 14.84	14.89	14.93	14.98	15.02	15.51		
64	14.22	14.27	14.70	14.36		14.44	14.49			15.07		
63	18.78	13.82	13.87	18.91	14.40 13 96	14.00	14.04	14.58	14.58	14.62		
62	13.38	13.36	13.42	18.47	18.51	13.56	13.60	13.64	13.69	13.78		
02	10.30	19.00	10.40	10.17	18.51	10.50	10.00	18.04	10.09	13.78		
61	12.89	12.98	12.98	18.02	18.07	18.11	18.16	13.20	13.24	18.29		
60	12.44	12.49	12.58	12.58	12.62	12.67	.12.71	12.76	12.80	12.84		
59	12.00	12.04	12.09	12.18	12.18	12.22	12.27	12.31	12.86	12.40		
58	11.56	11.60	11.64	11.69	11.78	11.78	11.82	11.87	11.91	11.96		
57	11.11	11.16	11.20	11.24	11.29	11.88	11.38	11.42	11.47	11.51		
						l			İ			
56	10.67	10.71	10.76	10.80	10.84	10.89	10.98	10.98	11.02	11.07		
55	10.22	10.27	10.31	10.36	10.40	10.44	10.49	10.58	10.58	10.62		
54	9.78	9.82	9.87	9.91	9.96	10.00	10.04	10.09	10.18	10.18		
58	9.33	9.38	9-42	9.47	9.51	9.56	9.60	9.64	9.69	9.78		
52	8.89	8.98	8.98	9.02	9.07	9.11	9.16	9.20	9.24	9.29		
2.			0 50	0 *0		0.00		0 ===	0.00	6.0		
51 50	8.44	8.49	8.58	8.58	8.62	8.67	8.71	8.76	8.80	8.84		
	8.00	8.04	8.09	8.18	8.18	8.22	8.27	8.81	8.86	8.40		
49	7.56	7.60	7.64	7.69	7.73	7.78	7.82	7.87	7.91	7.96		
48 47	7.11	7.16	7.20	7.24	7.29	7.33	1	7.42	7.47	7.51		
47	6.67	6.71	6.76	6.80	6.84	6.89	6.93	6.98	7.02	7.07		
46	6.22	6.27	6.31	6.36	6.40	6.44	6.49	6.58	6.58	6.62		
45	5.78	5.82	5.87	5.91	5.96	6.00	6.04	6.09	6.13	6.18		
44	5 33	5.38	5.42	6.47	5.51	5.56	5.60	5.64	5.69	5.73		
43	4.89	4.98	4.98	5.02	5.07	5.11	5.16	5.20	5.24	5.29		
42	4.44	4.49	4.53	4.58	4.62	4.67	4.71	4.76	4.80	4.84		
41	4.00	4.04	4.09	4.13	4.18	4.22	4.27	4.81	4.86	4.40		
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.		

19

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Degrees of Fahren-	Tenthe of a Degree.									
Fahren- heit.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Resumur	Resumur.	Reaumur.	Resumur.	Resumur.	Resumur.	Resumur.	Resumur.	Reaumur.	Resumer.
+40	+ 3.56	+ 8.60	+ 3.64	+ 3.69	+ 8.78	+ 3.78	+ 3.82	+ 3.87	+ 3.91	+ 8.96
89	3.11	3.16	3.20	8.24	8.29	3.88	3.38	8.42	8.47	8.51
38	2.67	2.71	2.76	2.80	2.84	2.89	2.93	2.98	3.02	3.07
37	2.22	2.27	2.81	2.36	2.40	2.44	2.49	2.58	2.58	2.62
36	1.78	1.82	1.87	1.91	1.96	2.00	2.04	2.09	2.18	2.18
35	1.83	1.38	1.42	1.47	1.51	1.56	1.60	1.64	1.69	1.73
84	0.89	0.93	0.98	1.02	1.07	1.11	1.16	1.20	1.24	1.29
88	0.44	0.49	0.53	0.58	0.62	0.67	0.71	0.76	0.80	0.84
82	0.00	0.04	0.09	0.18	0.18	0.22	0.27	0.31	0.36	0.40
31	- 0.44	- 0.40	- 0.36	- 0.31	- 0.27	- 0.22	- 0.18	- 0.13	- 0.09	- 0.04
80	- 0.89	- 0.84	- 0.80	- 0.76	- 0.71	- 0.67	- 0.62	- 0.58	- 0.53	- 0.49 - 0.98
29	1.83	- 1.29	- 1.24	- 1.20	- 1.16	- 1.11	- 1.07	- 1.02	- 0.98	
28	- 1.78	- 1.78	- 1.69	- 1.64 - 2.09	- 1.60 - 2.04	1.56	- 1.51	- 1.47	- 1.42	- 1.38
27 26	- 2.22 - 2.67	- 2.18 - 2.62	- 2.18 - 2.58	- 2.53	- 2.49	- 2.00 - 2.44	- 1.96 - 2.40	- 1.91 - 2.86	- 1.87 - 2.31	- 1.82 - 2.27
25	- 8.11	- 8.07	- 3.02	- 2.98	- 2.93	– 2.89	- 2.84	- 2.80	- 2.76	- 2.71
24	- 3.56	- 8.51	- 8.47	- 3.42	- 8.88	- 3.83	- 3.29	- 8.24	- 3.20	- 3.16
23	- 4.00	- 8.96	- 3.91	- 8.87	- 3.82	– 8.7 8	- 8.73	- 8.69	- 8.64	- 3.60
22	- 4.44	- 4.40	- 4.36	- 4.31	- 4.27	- 4.22	- 4.18	- 4.13	- 4.09	- 4.04
21	- 4.89	- 4.84	- 4.80	- 4.76	- 4.71	- 4.67	- 4.62	- 4.58	- 4.53	- 4.49
20	- 5.83	- 5.29	- 5.24	- 5.20	- 5.16	- 5.11	- 5.07	- 5.02	- 4.98	- 4.93
19	- 5.78	- 5.73	- 5.69	- 5.64	- 5.60	- 5.56	- 5.51	- 5.47	- 5.42	- 5.38
18	- 6.22	- 6.18	- 6.13	- 6.09	- 6.04	- 6.00	- 5.96	- 5.91	- 5.87	- 5.82
17	- 6.67	- 6.62	- 6.58	- 6.53	- 6.49	- 6.44	- 6.40	- 6.36	- 6.31	- 6.27
16	- 7.11	- 7.07	7.02	- 6.98	- 6.93	- 6.89	- 6.84	- 6.80	- 6.76	- 6.71
15	- 7.56	- 7.51	- 7.47	- 7.42	- 7.3 8	- 7.83	- 7.29	- 7.24	- 7.20	- 7.16
14	– 8.00	- 7.96	- 7.91	- 7.87	- 7.82	- 7.78	- 7.73	- 7.69	- 7.64	- 7.60
13	- 8.44	- 8.40	- 8.36	- 8.81	- 8.27	- 8.22	- 8.18	- 8.13	- 8.09	- 8.04
12	- 8.89	- 8.84	- 8.80	- 8.76	- 8.71	- 8.67	- 8.62	- 8.58	- 8.53	- 8.49
11	- 9.33	- 9.29	- 9.24	- 9.20	- 9.16	- 9.11	9.07	- 9.02	- 8.98	- 8.98
10	- 9.78	- 9.73	- 9.69	- 9.64	- 9.60	- 9.56	- 9.51	- 9.47	- 9.42	- 9.38
9	-10.22	-10.18	-10.13	-10.09	-10.04	-10.00	- 9.96	- 9.91	- 9.87	- 9.82
8	-10.67	-10.62	-10.58	-10.53	-10.49	-10.44	-10.40	-10.36	-10.31	-10.27
7	-11.11	-11.07	-11.02	-10.98	-10.93	-10.89	-10.84	-10.80	-10.76	-10.71
6	-11.56	-11.51	-11.47	-11.42	-11.88	-11.83	-11.29	-11.24	-11.20	-11.16
5	-12.00	-11.96	-11.91	-11.87	-11.82	-11.78	-11.73	-11.69	-11.64	-11.60
4	-12.44	-12.40	-12.36	-12.31	-12.27	-12.22	-12.18	-12.18	-12.09	12.04
8	-12.89	-12.84	-12.80	-12.76	-12.71	-12.67	-12.62	-12.58	-12.53	-12.49
2	-13.88	-18.29	-13.24	-13.20	-13.16	-18.11	-18.07	-12.02	-12.98	-12.93
1	-13.78	-18.73	-18.69	-13.64	-13.60	-13.56	-18.51	-13.47	-13.42	-13.38
+ 0	-14.22	-14.18	-14.18	-14.09	-14.04	-14.00	-13.96	-13.91	-13.87	-13.82
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

Degrees of Fahren-	Tenths of a Degree.									
he it.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Resumur.	Resumur.	Resumur.	Resumur.	Resumur.	Resumur.	Resumur.	Recumur.	Resumur.	Reaumur.
- 0	-14.22	-14.27	-14.31	-14.36	-14.40	-14.44	-14.49	-14.53	-14.58	-14.62
-1	-14.67	-14.71	-14.76	-14.80	-14.84	-14.89	-14.98	-14.98	-15.02	-15-07
- 2	-15.11	-15.16	-15.20	-15.24	-15.29	-15.33	-15.88	-15.42	-15.47	-15.51
- 3	-15.56	-15.60	-15.64	-15.69	-15.73	-15.78	-15.82	-15.87	-15.91	-15.96
- 4	-16.00	-16.04	-16.09	-16.13	-16.18	-16.22	-16.27	-16.81	-16.86	-16.40
- 5	-16.44	-16.49	-16.53	-16.58	-16.62	-16.67	-16.71	-16.76	-16.80	-16.84
- 6	-16.89	-17.93	-16.98	-17.02	-17.07	-17.11	-17.16	-17.20	-17.24	-17.29
- 7	-17.33	-17.38	-17.42	-17.47	-17.51	-17.5 6	-17.60	-17.64	-17.69	-17.78
-8	-17.78	-18.82	-17.87	-17.91	-17.96	-18.00	-18.04	-18.09	-18.13	-18.18
- 9	-18.22	-18.27	-18.31	-18.36	-18.40	-18.44	-18.49	-18.58	-18.58	-18.62
-10	-18.67	-18.71	-18.76	-18.80	-18.84	-18.89	-18.93	-18.96	-19.02	-19.07
-11	-19.11	-19.16	-19.20	-19.24	-19.29	-19.83	-19.38	-19.42	-19.47	-19.51
-12	-19.56	-19.60	-19.64	-19.69	-19.78	-19.78	-19.82	-19.87	-19.91	-19.96
-13	-20.00	-20.04	-20.09	-20.13	-20.18	-20.22	-20.27	-2 0.81	-20.86	-20.40
-14	-20.44	-20.49	-20.53	-20.58	-20.62	-20.67	-20.71	-20.76	-20.80	-20.84
-15	-20.89	-20.98	-20.98	-21.02	-21.07	-21.11	-21.16	-21.20	-21.24	-21.29
-16	-21.33	-21.38	-21.42	-21.47	-21.51	-21.56	-21.60	-21.64	-21.69	-21.73
-17	-21.78	-21.82	-21.87	-21.91	-21.96	-22.00	-22.04	-22.09	-22.13	-22.18
-18	-22.22	-22.27	-22.31	-22.36	-22.40	-22.44	-22.49	-22.53	-22.58	-22.62
-19	-22.67	-22.71	-22.76	-22.80	-22.84	-22.89	-22.93	-22.98	-23.02	-23.07
-20	-23.11	-23.16	-23.20	-23.24	-28.29	-23.83	-28.88	-23.42	-28.47	-23.51
-21	-23.56	-23.60	-23.64	-23.69	-28.73	-23.78	-28.82	-23.87	-23.91	-23.96
-22	-24.00	-24.04	-24.09	-24.18	-24.18	-24.22	-24.27	-24.81	-24.36	-24.40
-23	-24.44	-24.49	-24.58	-24.58	-24.62	-24.67	-24.71	-24.76	-24.80	-24.84
-24	-24.89	-24.93	-24.98	-25.02	-25.07	-25.11	-25.16	-25.20	-25.24	-25.29
-25	-25.33	-25.38	-25.42	-25.47	-25.51	-25.56	-25.60	-25.64	-25.69	-25.78
-26	-25.78	-25.82	-25.87	-25.91	-25.96	-26.00	-26.04	-26.09	-26.13	-26.18
-20 -27	-26.22	-25.8Z -26.27	-26.81	-26.36	-26.40	-26.44	-26.49	-26.58	-26.58	-26.62
-28	-26.67	-26.71	-26.76	-26.80	-26.84	-26.89	-26.93	-26.98	-27.02	-27.07
-29	-27.11	-27.16	-27.20	-27.24	-27.29	-27.38	-27.88	-27.42	-27.47	-27.51
-30	-27.56	-27.60	-27.64	-27.69	-27.73	-27.78	-27.82	-27 .87	-27.9 1	-27.96
-30 -31	-28.00	-28.04	-28.09	-28.18	-28.18	-21.10 -28.22	-28.27	-28.31	-28.86	-28.40
-31 -32	-28.44	-28.49	-28.53	-28.58	-28.62	-28.67	-28.71	-28.76	-28.80	-28.84
-32 -33	-28.89	-28.93	-28.98	-29.02	-29.07	-29.11	-29.16	-29.20	-29.24	-29.29
-85 -84	-29.83	-28.93 -29.88	-25.95 -29.42	-29.02	-29.51	-29.11 -29.56	-29.60	-29.64	-29.69	-29.73
		00.00	00 0=	00 44	00.00	90.00	_90.04	_90 00	-30.13	-80·18
-35	-29.78	-29.82	-29.87	-29.91	-29.96	-80.00	-80.04 -80.49	-80.09 -80.53	-80.58	-30.62
-36	-30.22	-80.27	-30.81	-80.86	-30.40 -30.40	-80.44			-81.02	-81.07
-37	-30.67	-30.71	-30.76	-80.80	-30.84	-80.89	-80.98 -91.88	-80.98 91.49	-81.02 -81.47	-81.07 -81.51
-38	-81.11	-3 1.16	-31.20	-31.24	-81.29 -91.79	-81.38	-31.38 -31.82	-31.42 -31.87	-81.47 -81.91	-31.96
-39 -40	-31.56 82.00	-31.60 -80.04	-81.64 80.09	-31.69 -80.13	-81.73 -80.18	-31.78 -80.22	-80.27	-30.81	-80.86	- 8 0.40
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	1	<u> </u>	1	<u> </u>				<u> </u>		



VI.-VII.

COMPARISON

OF

THE CENTIGRADE THERMOMETER

WITH

THE THERMOMETERS OF FAHRENHEIT AND OF REAUMUR,

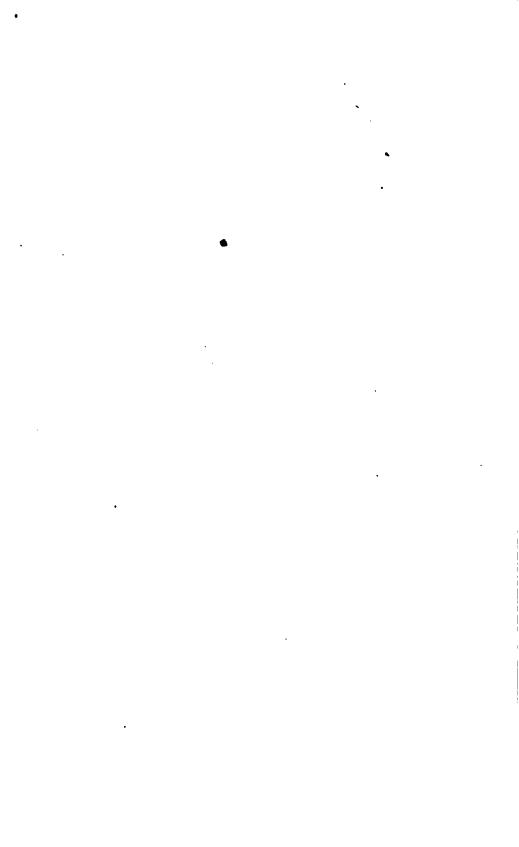
OR

TABLES

FOR CONVERTING CENTIGRADE DEGREES INTO DEGREES OF FAHRENHEIT

AND OF REAUMUR;

GIVING THE CORRESPONDING VALUES FOR EACH TENTH OF A DEGREE, FROM +50° TO -54° CENTIGRADE.



	Tenths of Degrees.											
Centigrade Degrees.	9.	1.	2.	8.	4.	5.	6.	7.	8.	9.		
450	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fabrea.	Fahren.	Fabren.	Fahren. +123.44	Fahren.		
+50 49	+122.00 120.20	120.88	120.56	120.74	120.92		121.28	121.46	121.64	121.82		
48	118.40	118.58	118.76	118.94	119.12		119.48	119.66	119.84	120.02		
47	116.60	116.78	116.96		117.82			117.86		118.22		
46	114.80	114.98	115.16	115.84	115.52	115.70	115.88	116.06	116.24	116.42		
45	113.00	113.18	113.36	113.54	118.72	118.90	114.08	114.26	114.44	114.62		
44	111.20	111.88	111.56	111.74	111.92	112.10	112.28	112.46	112.64	112.82		
43	109.40	109.58	109.76	109.94	110.12	110.80	110.48	110.66	110.84	111.02		
42	107.60	107.78	107.96	106.14	108.82	108.50	108.68	108.86	109.04	109.22		
41	105.80	105.98	106.16	106.84	106.52	106.70	106.88	107.06	107.24	107.42		
40	104.00	104.18	104.86	104.54	104.72		105.08	105.26	105.44	105.62		
39	102.20	102.88	102.56	102.74	102.92		108.28	108.46	108.64	103.82		
38	100.40	100.58	100.76	100.94	101.12		101.48	101.66	101.84	102.02		
37	98.60	96.78	98.96	99.14	99.82	99.50	99.68	99.86	100.04 98.24	100.22		
86	96.80	96.98	97.16	97.84	97.52	97.70	97. 88	98.06	90.24	98.42		
35	95.00	95.18	95.86	95.54	95.72	95.90	96.08	96.26	96.44	96.62		
84	98.20	98.88	98.56	98.74	98.92	94.10	94.28	94.46	94.64	94.82		
23	91.40	91.58	91.76	91.94	92.12	92.80	92.48	92.66	92.84	93.02		
32	89.60	89.78	89.96	90.14	90.82	90.50	90.68	90.86	91.04	91.22		
31	87.80	87.98	88.16	88.84	88.52	88.70	88.88	89.06	89.24	89.42		
30	86.00	86.18	86.86	86.54	86.72	86.90	87.08	87.26	87.44	87.62		
29	84.20	84.88	84.56	84.74	84.92	85.10	85.28	85.46	85.64	85.82		
28	82.40	82.58	82.76	82.94	83.12		83.48	88.66	88.84	£4.02		
27	80.60	80.78	80.96	81.14	81.32		81.68	81.86	82.04	82.22		
26	78.80	78.98	79.16	79.84	79.52	79.70	79.88	80.06	80.24	80.42		
25	77.00	77.18	77.86	77.54	77.72	77.90	78.08	78.26	78.44	78.62		
24	75.20	75.88	75.56	75.74	75.92		76.28	76.46	76.64	76.82		
23	78.40	78.58	78.76	78.94	74.12		74.48	74.66	74.84	75.02		
28	71.60	71.78	71.96	72.14	72.32	72.50	72.68	72.86	78.04	78.22		
21	69.80	69.98	70.16	70.84	70.52	70.70	70.88	71.06	71.24	71.42		
20	66.00	68.18	68.36	68.54	68.72	68.90	69.06	69.26	69.44	69 .62		
19	66.20	66.88	66.56	66.74	66.92	67.10	67.28	67.46	67.64	67.82		
16	64.40	64.58	64.76	64.94	65.12		65.48	65.66	65.84	66.02		
17	62.60	62.78	62.96	68.14	63.82		63.68	63.86	64.04	64.22		
16	60.80	60.98	61.16	61.84	61.52	61.70	61.88	62.06	62.24	62.42		
15	59.00	59.18	59.36	59.54	\$9.72	59.90	60.08	60.26		60.62		
14	57.20	57.88	57.56	57.74	57.92			58.46		58.82		
18	55.40	55.58	55.76	55.94			56.48	56.66		57.02		
13	53.60	58.78	53.96	54.14	54.82		54.68	54.86		55.22		
11	51.80	51.98	52.16	52.84	52.52	52.70	52.88	58.06	58.24	53.42		
	9.	1.	3.	8.	4.	5.	6.	7.	8.	. 9.		

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+10	••• ahren. 0.00 8.20 6.40 4.80 9.20 7.40 5.60 3.80 2.00 2.00 4.80 4.80	1. Fahren. +50.18 48.38 46.58 44.78 42.96 41.18 89.38 87.58 35.78 33.98 32.18 31.82 30.02 28.22 26.42 24.62	## Fahren. +50.36 48.56 46.76 44.96 43.16 41.86 89.56 87.76 35.96 84.16 82.86 81.64 29.84 28.04 26.24	8. Fahren. +50.54 48.74 46.94 45.14 48.84 .41.54 89.74 87.94 86.14 84.34 82.54 31.46 29.66 27.86	4. Fahren. +50.72 48.92 47.12 45.32 43.52 41.72 39.92 38.12 36.32 32.72 31.28 29.48	Fahren. +50.90 49.10 47.80 45.50 43.70 41.90 40.10 38.30 36.50 34.70 32.90	Fahren. +51.08 49.28 47.48 45.68 43.88 42.06 40.28 38.48 36.68 34.88 33.06	Fahren. +51.26 49.46 47.66 45.86 44.06 42.26 40.46 38.66 36.86 83.06 83.26	Fahren. +51.44 49.64 47.84 46.04 44.24 42.44 40.64 88.84 87.04 35.24 83.44	9. Fahren. +51.62 49.82 48.02 46.22 44.42 42.62 40.82 89.02 87.22 85.42 83.62
+10	0.00 8.20 6.40 4.60 2.80 1.00 9.20 7.40 5.60 8.80 2.00 0.20 8.40 6.60	+50.18 48.88 46.58 44.78 42.96 41.18 39.28 87.58 35.78 33.98 32.18 31.82 30.02 28.22 26.42	+50.36 48.56 46.76 44.96 43.16 41.36 89.56 87.76 35.96 34.16 32.36 31.64 29.84 28.04 26.24	+50.54 48.74 46.94 45.14 43.34 -41.54 39.74 87.94 36.14 34.34 31.46 29.66	+50.72 48.92 47.12 45.82 43.52 41.72 39.92 38.12 36.82 34.52 32.72	+50.90 49.10 47.80 45.50 43.70 41.90 40.10 88.80 86.50 84.70 82.90	+51.06 49.28 47.48 45.68 43.88 42.08 40.28 38.48 36.68 34.88 33.08	+51.26 49.46 47.66 45.86 44.06 42.26 40.46 28.66 36.86 83.06 38.26	+51.44 49.64 47.84 46.04 44.24 42.44 40.64 88.84 87.04 35.24 33.44	+51.62 49.82 48.02 46.22 44.42 42.62 40.82 89.02 87.22 85.42 83.62
9 48 8 46 7 44 6 42 5 41 4 39 8 32 8 32 1 83 0 82 - 0 82 - 1 80 - 2 28 - 3 26 - 4 24 - 5 23 - 6 21 - 7 19 - 8 17 - 9 15 - 10 14 - 11 12 - 12 8 - 14 6 - 15 - 16 3 - 17 - 18 - 0 - 19 - 2 2 - 20 - 4 - 21 - 5 - 22 - 7 - 9 - 9	8.20 6.40 4.60 2.80 1.00 9.20 7.40 5.60 3.80 2.00 0.20 8.40 6.60	48.88 46.58 44.78 42.98 41.18 39.88 37.58 35.78 33.98 32.18 31.82 30.02 28.22 26.42	48.56 46.76 44.96 45.16 41.86 89.56 87.76 85.96 84.16 82.86 81.64 29.84 28.04 26.24	46.94 45.14 43.34 -41.54 39.74 87.94 36.14 84.34 32.54 31.46 29.66	48.92 47.12 45.32 43.52 41.72 39.92 38.12 36.32 34.52 32.72	49.10 47.80 45.50 43.70 41.90 40.10 88.80 36.50 84.70 32.90	49.28 47.48 45.68 48.88 42.08 40.28 86.48 36.68 34.88 33.08	47.66 45.86 44.06 42.26 40.46 38.66 36.86 83.06 83.26	47.84 46.04 44.24 42.44 40.64 88.84 87.04 35.34 88.44	49.82 48.02 46.23 44.42 42.62 40.82 89.02 87.22 85.42 88.62
8 46 7 44 6 42 5 41 4 39 8 37 2 35 1 83 0 82 - 0 32 - 1 30 - 2 28 - 3 26 - 4 24 - 5 23 - 6 21 - 7 19 - 8 17 - 9 15 - 10 14 - 11 12 - 12 10 - 13 6 - 17 - 16 - 16 5 - 16 3 - 17 - 18 - 0 - 19 - 2 - 20 - 4 - 21 - 5 - 22 - 7 - 23 - 9	4.60 2.80 1.00 9.20 7.40 5.60 3.80 2.00 0.20 8.40 6.60	44.78 42.96 41.18 89.88 87.58 85.78 83.98 82.18 31.82 30.02 28.22 26.42	44.96 48.16 41.86 89.56 87.76 85.96 84.16 82.36 31.64 29.84 28.04 26.24	45.14 48.84 .41.54 89.74 87.94 86.14 84.84 82.54 81.46 29.66	45.82 48.52 41.72 89.92 88.12 36.82 84.52 82.72	45.50 43.70 41.90 40.10 38.30 36.50 84.70 32.90	45.68 48.88 42.06 40.28 88.48 86.68 84.88 83.06	45.86 44.06 42.26 40.46 88.66 86.86 83.06 83.26	46.04 44.24 42.44 40.64 88.84 87.04 35.24 88.44	46.22 44.42 42.62 40.82 89.02 37.22 85.42 88.62
6 42 5 41 4 89 8 87 2 85 1 88 0 82 - 0 82 - 1 80 - 2 28 - 3 26 - 4 24 - 5 23 - 6 21 - 7 19 - 8 17 - 9 15 - 10 14 - 11 12 - 12 10 - 13 8 - 14 6 - 15 5 - 16 8 - 17 - 18 - 10 - 2 - 20 - 4 - 21 - 5 - 22 - 7 - 23 - 9	2.80 1.00 9.20 7.40 5.60 8.80 2.00 0.20 8.40 6.60	42.96 41.18 89.88 87.58 85.78 83.98 82.18 81.82 80.02 28.22 26.42	43.16 41.86 89.56 87.76 85.96 84.16 82.86 31.64 29.84 28.04 26.24	48.84 .41.54 89.74 87.94 86.14 84.84 82.54 81.46 29.66	43.52 41.72 89.92 88.12 36.82 84.52 82.72	43.70 41.90 40.10 38.80 36.50 84.70 32.90	43.88 42.08 40.28 88.48 86.68 34.88 33.08	44.06 42.26 40.46 28.66 36.86 83.06 83.26	44.24 42.44 40.64 88.84 87.04 35.24 88.44	44-42 42-62 40-82 89-02 37-22 85-42 83-62
5 41 4 39 8 37 2 35 1 38 0 32 - 0 32 - 1 30 - 2 28 - 3 26 - 4 24 - 5 23 - 6 21 - 7 19 - 8 17 - 9 15 - 10 14 - 11 12 - 12 10 - 13 8 - 14 6 - 15 5 - 16 3 - 17 - 18 - 0 - 19 - 2 - 20 - 4 - 21 - 5 - 22 - 7 - 23 - 9	1.00 9.20 7.40 5.60 8.80 2.00 2.00 0.20 8.40 6.60	41.18 89.88 87.58 85.78 83.98 82.18 81.82 80.02 28.22 26.42	41.86 89.56 87.76 85.96 84.16 82.86 81.64 29.84 28.04 26.24	. 41.54 89.74 87.94 86.14 84.84 82.54 81.46 29.66	41.72 89.92 88.12 36.82 84.52 82.72	41.90 40.10 88.80 86.50 84.70 82.90	42.06 40.28 88.48 86.68 34.88 83.08	42.26 40.46 28.66 36.86 83.06 83.26	42.44 40.64 88.84 87.04 35.24 88.44	42.62 40.82 89.02 37.22 85.42 83.62
4 39 3 37 2 35 1 38 0 32 - 0 32 - 1 30 - 2 28 - 3 26 - 4 24 - 5 23 - 6 21 - 7 19 - 8 17 - 9 15 - 10 14 - 11 2 - 12 10 - 18 - 14 6 - 15 5 - 16 3 - 17 - 18 - 0 - 19 - 2 - 20 - 4 - 21 - 5 - 22 - 7 - 23 - 9	9.20 7.40 5.60 8.80 2.00 0.20 8.40 6.60	89.88 87.58 85.78 83.98 82.18 81.82 80.02 28.22 26.42	39.56 37.76 35.96 34.16 32.36 31.64 29.84 28.04 26.24	89.74 87.94 86.14 84.84 82.54 81.46 29.66	39.92 38.12 36.32 34.52 32.72	40.10 88.80 86.50 84.70 82.90	40.28 88.48 86.68 34.88 33.06	40.46 38.66 36.86 83.06 38.26	40.64 88.84 87.04 35.24 88.44	40.82 89.02 37.22 85.42 83.62
3 37 2 35 1 38 0 32 - 0 32 - 1 30 - 2 28 - 3 26 - 4 24 - 5 23 - 6 21 - 7 19 - 8 17 - 9 15 - 10 14 - 11 12 - 12 10 - 18 - 14 6 - 15 - 16 3 - 17 - 18 - 0 - 19 - 2 - 20 - 4 - 21 - 5 - 22 - 7 - 23 - 9	7.40 5.60 8.80 2.00 2.00 0.20 8.40 6.60	87.58 85.78 83.98 82.18 81.82 80.02 28.22 26.42	87.76 85.96 84.16 82.86 81.64 29.84 28.04 26.24	87.94 86.14 84.84 82.54 81.46 29.66	88.12 36.82 84.52 32.72	88.80 86.50 84.70 82.90	38.48 36.68 34.88 33.06	28.66 26.86 83.06 83.26	38.84 37.04 35.24 33.44	89.02 37.22 85.42 83.62
2 35 1 0 32 - 0 32 - 1 30 - 2 28 - 3 26 - 4 24 - 5 23 - 6 21 - 7 19 - 8 17 - 9 15 - 10 14 - 11 12 - 12 10 - 18 - 14 6 - 15 5 - 16 3 - 17 - 18 - 0 - 19 - 2 - 20 - 4 - 21 - 5 - 22 - 7 - 23 - 9	5.60 8.80 2.00 2.00 0.20 8.40 6.60	85.78 83.98 82.18 81.82 80.02 28.22 26.42	35.96 34.16 32.36 31.64 29.84 28.04 26.24	36.14 84.34 82.54 31.46 29.66	36.82 84.52 32.72	36.50 84.70 32.90 31.10	36.68 34.88 83.06	36.86 85.06 83.26	87.04 35.24 88.44	37.22 85.42 83.62
1 83 32 - 0 82 - 1 80 82 - 2 8 - 8 26 - 4 24 - 5 23 - 6 21 - 7 19 - 8 17 - 9 15 - 10 14 - 11 12 - 12 10 - 18 - 14 6 - 15 - 16 - 17 - 18 - 0 - 19 - 2 1 - 5 - 22 - 7 - 23 - 9	8.80 2.00 2.00 0.20 8.40 6.60	33.98 32.18 31.82 30.02 28.22 26.42	84.16 82.86 81.64 29.84 28.04 26.24	84.84 82.54 81.46 29.66	34.52 32.72 31.28	84.70 82.90 81.10	34.88 33.06	83.06 88.26	35.24 88.44	85.42 88.62
0	2.00 2.00 0.20 8.40 6.60	\$2.18 \$1.82 \$0.02 28.22 26.42	31.64 29.84 28.04 26.24	32.54 31.46 29.66	32.72 31.28	32.90 31.10	88.06	88.26	88.44	83.62
- 0 32 - 1 30 - 2 28 - 3 26 - 4 24 - 5 23 - 6 21 - 7 19 - 8 17 - 9 15 - 10 14 - 11 12 - 12 10 - 18 8 - 14 6 - 15 5 - 16 3 - 17 - 18 - 19 - 2 - 20 - 4 - 21 - 5 - 22 - 7 - 23 - 9	2.00 0.20 8.40 6.60	81.82 80.02 28.22 26.42	31.64 29.84 28.04 26.24	31.46 29.66	31.28	31.10				
- 1	0.20 8.40 6.60	30.02 28.22 26.42	29.84 28.04 26.24	29.66			30.92	80.74	90 *0	00 00
- 2 28 - 8 26 - 4 24 - 5 21 - 7 19 - 15 - 10 - 11 - 12 - 13 - 14 6 - 15 - 16 - 17 - 18 - 0 - 19 - 2 - 20 - 4 - 21 - 5 - 22 - 7 - 23 - 9	8.40 6.60	28.22 26.42	28.04 26.24		29.48				30.56	30.38
- 8 26 -4 24 -5 23 -6 21 -7 19 -10 14 -11 12 -12 -13 8 -14 6 -15 -16 -17 -18 -19 -2 -20 -4 -21 -5 -22 -7 -23 -9	6.60	26.42	26.24	27.86		29.80	29.12	28.94	28.76	28.58
- 4 24 - 5 28 - 6 21 - 7 19 - 8 17 - 9 15 - 10 - 11 - 12 - 12 - 16 - 15 - 16 - 17 - 18 - 0 - 19 - 2 - 20 - 4 - 21 - 5 - 22 - 7 - 23 - 9					27.68	27.50	27.82	27.14	26.96	26.78
- 5 28 - 6 21 - 7 19 - 8 17 - 9 15 -10 14 -11 12 -12 10 -18 8 -14 6 -15 5 -16 3 -17 -18 - 0 -19 - 2 -20 - 4 -21 - 5 -22 - 7 -23 - 9	4.60	24.62		26.06	25.88	25.70	25.52	25.84	25.16	24.98
- 6 21 19 - 8 17 - 9 15 10 14 -11 12 -12 10 -15 -16 3 -17 -18 -19 -2 -20 -4 -21 -5 -22 -7 -23 -9			24.44	24.26	24.08	28.90	28.72	23.54	23.86	23.18
- 7 19 17 - 8 17 - 9 15 - 10 14 - 11 12 - 12 10 - 18 - 14 6 - 15 - 16 - 17 1 - 18 - 0 - 19 - 2 - 20 - 4 - 21 - 5 - 22 - 7 - 23 - 9	3.00	22.82	22.64	22.46	22.28	22.10	21.92	21.74	21.56	21.38
- 8 17 - 9 15 -10 14 -11 12 -12 10 -18 8 -14 6 -15 5 -16 -17 1 -18 -0 -19 -2 -20 -4 -21 -5 -22 -7 -23 -9	1.20	21.02	20.84	20.66	20.48	20.80	20.12	19.94	19.76	19.58
- 9 15 -10 14 -11 12 -12 10 -18 8 -14 6 -15 5 -16 5 -17 1 -18 -0 -19 -2 -20 -4 -21 -5 -22 -7 -23 -9	9.40	19.22	19.04	18.86	18.68	18.50	18.82	18.14	17.96	17.78
-10	7.60	17.42	17.24	17.06	16.88	16.70	16.52	16.84	16.16	15.98
-11 12 10 -12 10 11 12 10 10 10 10	5.80	15.62	15.44	15.26	15.08	14.90	14.72	14.54	14.36	14.18
-12 10 -18 8 -14 6 -15 5 -16 3 -17 1 -18 -0 -19 -2 -20 -4 -21 -5 -22 -7 -23 -9	4.00	13.82	13.64	18.46	13.28	18.10	12.92	12.74	12.56	12.38
-18	2.20	12.02	11.84	11.66	11.48	11.80	11.12	10.94	10.76	10.58
-14 6 -15 5 -16 3 -17 1 -18 -0 -19 -2 -20 -4 -21 -5 -22 -7 -23 -9	0.40	10.22	10.04	9.86	9.68	9.50	9.82	9.14	8.96	8.78
-15 516 317 118 -0 -19 - 2 -20 -4 -21 -5 -22 -7 -23 -9	B. 60	8.42	8.24	8.06	7.88	7.70	7.52	7.34	7.16	6.98
-16	6.80	6.62	6.44	6.26	6.08	5.90	5.72	5.54	5.86	5.18
-17 1. -18 -0 -19 -2 -20 -4 -21 -5 -22 -7 -23 -9	5.00 .	4.82	4.64	4.46	4.28	4.10	8.92	8.74	8.56	8.88
-18 - 0 -19 - 2 -20 - 4 -21 - 5 -22 - 7 -23 - 9	8.20	8.02	2.84	2.66	2.48	2.30	2.12	1.94	1.76	1.58
-19 - 2 -20 - 4 -21 - 5 -22 - 7 -23 - 9	1.40	1.22	1.04	0.86	0.68	0.50	0.82	0.14	- 0.04	- 0.22 - 2.02
-20	0.40 2.20	- 0.58 - 2.38	- 0.76 - 2.56	- 0.94 - 2.74	- 1.12 - 2.92	- 1.80 - 8.10	- 1.48 - 3.28	- 1.66 - 8.46	- 1.84 - 3.64	- 2.02 - 2.82
-21 - 5 -22 - 7 -23 - 9		2.00				0.20	0.20	0.10		0.02
-22 - 7 -23 - 9		- 4.18	- 4.36	- 4.54	- 4.72	- 4.90	- 5.08	- 5.26	- 5.44	- 5.62
-23 - 9	5.80	- 5.98	- 6.16	- 6.34	- 6.52	- 6.70	- 6.88	- 7.06	- 7.24	- 7.42
		- 7.78	- 7.96	- 8.14	- 8.32	- 8.50	- 8.68	- 8.86	- 9.04	- 9.22
	9.40 1. 2 0	- 9.58 -11. 8 8	- 9.76 -11.56	- 9.94 -11.74	-10.12 -11.92	-10.80 -12.10	-10.48 -12.28	-10.66 -12.46	-10.84 -12.64	-11.02 -12.82
l				1			l			
11	3.00	-13.18	-13.36	-18.54	-13.72	-18.90	-14.08	-14.26	-14.44	-14.62
- 11		-14.98	-15.16	-15.84	-15.52	-15.70	-15.88	-16.06	-16.24	-16.42
li li	4.80	-16.78 -18.58	-16.96 -18.76	~17.14 ~18.94	-17.32 -19.12	-17.50 -19.80	-17.68 -19.48	-17.86 -19.66	-18.04 -19.84	-18 .22 -20.02
11	6.60	-20.88	-20.56	-20.74	-10.12 -20.92	-21.10	-21.28	-21.46	-21.64	-21.82
		1.	9.	8.	4.	5.	6.	7.	8.	9.

A

					Tenthe of	Degrees.				
Centigrade Degrees.	•,	1.	9.	8.	4.	5.	6.	7.	8.	9.
	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.
-30	-22.00	-22.18	-22.86	-22.54	-22.72	-22.9 0	-23.08	-28.26	-23.44	-33.62
-31	-23.80	-28.98	-24.16	-24.84	-24.52	-24.70	-24.88	-25.06	-25.24	-25.42
-32	-25.60	-25.7 8	-25.9 6	-26.14	-26.32	-26.50	-26.68	-26. 86	-27.04	-27.22
33	-27.40	-27.58	-27.76	-27.94	-28.12	-28.30	-28.48	-28.66	-28.84	-29. 02
-34	-29.20	-29.38	-29.56	-29.74	-29.92	-80.10	-30.2 8	-30.46	-80.64	-30.82
-35	-31.00	-81.18	-31.86	-81.54	-81.72	-81.90	-32.08	-82.26	-82.44	-82.62
-36	-82.80	-32.98	-33.16	-83.34	-83.52	-33.70	-33.88	-84.06	-84.24	-34.42
-37	-34.60	-34.78	-34.96	-85.14	-35.32	-35.50	-35.68	-85.86	-36.04	-86.22
-38	-36.40	-36.58	-36.76	-36.94	-37.12	-87.30	-37.48	-87.66	-37.84	-88.02
-89	-38.20	-38.88	-38.56	-38.74	-88.92	-39.10	-39.28	-89.46	-39.64	-89.82
-40	-40.00	-40.18	-40.36	-40.54	-40.72	-40.90	-41.08	-41.26	-41.44	-41.62
-41	-41.80	-41.98	-42.16	-42.34	-42.52	-42.70	-42.88	-43.06	-43.24	-43.42
-42	-43.60	-43.78	-43.96	-44.14	-44.82	-44.50	-44.68	-44.86	-45.04	-45.22
-43	-45.40	-45.58	-45.76	-45.94	-46.12	-46.80	-46.48	-46.66	-46.84	-47.02
-44	-47.20	-47.38	-47.56	-47.74	-47.92	-48.10	-48.28	-48.46	-48.64	-48.82
				3,110						
-45	-49.00	-49.18	-49.86	-49.54	-49.72	-49.90	-50.08	-50.26	-50.44	-50.62
-46	-50.80	-50.98	-51.16	-51.84	-51.52	-51.70	-51.88	-52.06	-52.24	-52.42
-47	-52.60	-52.78	-52.96	-58.14	-58.82	-58.50	-53.68	-58.86	-54.04	-54.22
-48	-54.40	-54.58	-54.76	-54.94	-55.12	-55.80	-55.48	-55.66	-55.84	-56.02
-49	-56.20	-56.38	-56.56	-56.74	-56.92	-57.10	-57.28	-57.46	-57.64	-57.82
-	-50.20	-00.00		202	00.02	"""	J20	330	554	-,
-50	-58.00	-58.18	-58.86	-58.54	-58.72	-58.90	-59.08	-59.26	-59.44	-59.62
-50 -51	-59.80	-59.98	-60.16	-60.84	-60.52	-60.70	-60.88	-61.06	-61.24	-61.42
-52	-61.60	-61.78	-61.96	-62.14	-62.32	-62.50	-62.68	-62.86	-63.04	-63.22
-52 58	-63.40	-63.58	-63.76	-63.94	-64.12	-64.80	-64.48	-64.66	-64.84	-65.02
-54	-65.20	-65.38	-65.56	-65.74	-65.92	-66.10	-66.28	-66.46	-66.64	-66.82
-94	-05.20	-00.00	-05.00	-00.74	-00.92	-00.10	-00.20	-00.40	-00.04	-00.02

TABLE FOR COMPARING THE CENTIGRADE AND FAHRENHEIT'S THERMOMETERS NEAR THE BOILING POINT.

Centigrade Degrees.	6.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Fahren.	Fahren.	Fahren.	Fahren.	Pahren.	Pahren.	Fahren.	Fahren.	Fahren.	Fahren.
100	212.00	212.18	212.86	212.54	212.72	212.90	213.06	213.26	213.44	213.62
99 -	210.20	210.88	210.56	210.74	210.92	211.10	211.28	211.46	211.64	211.82
98	208.40	208.58	208.76	208.94	209.12	209.30	209.48	209.66	209.84	210.02
97	206.60	206.78	206.96	207.14	207.32	207.50	207.68	207.86	208.04	208.22
96	204.80	204.98	205.16	205.84	205.52	205.70	205.88	206.06	206.24	206.42
95	203.00	203.18	203.86	203.54	203.72	203.90	204.08	204.26	204.44	204.62
94	201.20	201.38	201.56	201.74	201.92	202.10	202.28	202.46	202.64	202.82
93	199.40	199.58	199.76	199.94	200.12	200.30	200.48	200 66	200.84	201.02
92	197.60	197.78	197.96	198.14	198.32	198.50	198.68	198.86	199.04	199.22
91	195.80	195.98	196.16	196.34	196.52	196.70	196.88	197.06	197.24	197.42
90	194.00	194.18	194.36	194.54	194.72	194.90	195.08	195.26	195.44	195.62
89	192.20	192.38	192.56	192.74	192.92	193.10	198.28	193.46	193.64	193.82

VII. CONVERSION OF CENTIGRADE DEGREES INTO DEGREES OF REAUMUR.

	Tenths of Degrees.											
Centigrade Degrees.	0.	1.	9.	3.	4.	5.	6.	7.	8.	9.		
± 40	Resum.	Resum.	Resum.	Resum.	Reaum.	Resum.	Recum.	Resum.	Reaum.	Reaum. +32.72		
±40	+32.00	±82.06	±82.16	+82.24		+82.40	± 32.4 8	± 82. 56	+82.64			
39	81.20	81.28	81.36	81.44	81.52	31.60	81.68	81.76	81.84	81.92		
38	80.40	80.48	80.56	30.64	80.72	80.80	80.88	30.96	81.04	81.12		
87	29.60	29.68	29.76	29.84	29.92	80.00	80.08	80.16	80.24	80.32		
36	28.80	28.88	28.96	29.04	29.12	29.20	29.28	29.36	29.44	29-52		
35	28.00	28.08	28.16	28.24	28.82	28.40	28.48	28.56	28.64	28.72		
84	27.20	27.28	27.36	27.44	27.52	27.60	27.68	27.76	27.84	27.92		
23	26.40	26.48	26.56	26.64	26.72	26.80	26.88	26.96	27.04	27.12		
82	25.60	25.68	25.76	25.84	25.92	26.00	26.08	26.16	26.24	26.82		
81	24.80	24.88	24.96	25.04	25.12	25.20	25.28	25.86	25.44	25.52		
80	24.00	24.08	24.16	24.24	25.82	24.40	24-48	24.56	24.64	24.72		
29	23.20	28.28	28.86	23.44	23.52	28.60	28.68	28.76	23.84	23.92		
28	22.40	22.48	22.56	22.64	22.72	22.80	22.88	22.96	28.04	28.12		
27	21.60	21.68	21.76	21.84	21.92	22.00	22.08	22.16	22.24	22.32		
26	20.80	20.88	20.96	21.04	21.12	21.20	21.28	21.36	21.44	21.52		
23	20.00	20.08	20.16	20.24	20.32	20.40	20.48	20.56	20.64	20.72		
24	19.20	19.28	19.86	19.44	19.52	19.60	19.68	19.76	19.84	19.92		
23	18.40	18.48	18.56	18.64	18.72	18.80	18.88	18.96	19.04	19.12		
22	17.60	17.68	17.76	17.84	17.92	18.00	18.08	18.16	18.24	18.32		
21	16.80	16.88	16.96	17.04	17.12	17.20	17.28	17.86	17.44	17.52		
20	16.00	16.08	16.16	16.24	16.32	16.40	16.48	16.56	16.64	16.72		
19	15.20	15.28	15.86	15.44	15.52	15.60	15.68	15.76	15.84	15.92		
18	14.40	14.48	14.56	14.64	14.72	14.80	14.88	14.96	15.04	15.12		
17	18.60	13.68	13.76	13.84	13.92	14.00	14.08	14.16	14.24	14.32		
16	12.80	12.88	12.96	18.04	18.12	18.20	18.28	13.36	13.44	18.52		
15	12.00	12.08	12-16	12.24	12.32	12.40	12.48	12.56	12.64	12.72		
14	11.20	11.28	11.36	11.44	11.52	11.60	11.68	11.76	11.84	11.92		
18	10.40	10.48	10.56	10.64	10.72	10.80	10.88	10.96	11.04	11.12		
12	9.60	9.68	9.76	9.84	9.92	10.00	10.08	10.16	10.24	10.32		
11	8.80	8.88	8.96	9.04	9.12	9.20	9.28	9.36	9.44	9.52		
10	8.00	8.08	8.16	8.24	8.82	8.40	8.48	8.56	8.64	8.72		
9	7.20	7.28	7.86	7.44	7.52	7.60	7.68	7.76	7.84	7.92		
8	6.40	6.48	6.56	6.64	6.72	6.80	6.88	6.96	7.04	7.12		
7	5.60	5.68	5.76	5.84	5.92	6.00	6.08	6.16	6.24	6.32		
6	4.80	4.88	4.96	5.04	5.12	5.20	5.28	5.36	5.44	5.52		
5	4.00	4.08	4.16	4.24	4.82	4.40	4.48	4.56	4.64	4.72		
4	8.20	8.28	3.86	8.44	8.52	3.60	3.68	3.76	3.84	3.92		
3	2.40	2.48	2.56	2.64	2.72	2.80	2.88	2.96	3.04	3.12		
2	1.60	1.68	1.76	1.84	1.92	2.00	2.08	2.16	2.24	2.32		
1	0.80	0.88	0.96	1.04	1.12	1.20	1.28	1.36	1.44	1.52		
0	0.00	0.08	0.16	0.24	0.32	0.40	0.48	0.56	0.64	0.72		
	0.		·		l	<u> </u>		·				

VIII.-IX.

COMPARISON

OF

REAUMUR'S THERMOMETER

WITH

THE THERMOMETER OF FAHRENHEIT AND THE CENTIGRADE THERMOMETER,

OR

· TABLES

FOR CONVERTING DEGREES OF REAUMUR INTO DEGREES OF FAHRENHEIT

AND INTO CENTIGRADE DEGREES;

GIVING THE CORRESPONDING VALUES FOR EACH TENTH OF A DEGREE, FROM $\pm 40^{\circ}$ TO $\pm 40^{\circ}$ REAUMUR.

	Tenths of Degrees.											
Degrees of Resumur.	•.	1.	9.	8.	4.	5.	6.	7.	8.	9.		
	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.		
+40	1	+122.22		-								
39 38	119.75 117.50	119.97 117.72	120.20 117.95	120.42 118.17	120.65 118.40		121.10 118.85	121.82 119.07	121.55 119. 3 0	121.77 119.52		
87	115.25		115.70	115.92			116.60			117.27		
86	118.00	118.22	113.45	113.67	113.90		114.35	114.57	114.80	115.02		
"	1 110100	110122	100120		220.20		222.00			-10102		
35	110.75	110.97	111.20	111.42	111.65	111.87	112.10	112.82	112.55	112.77		
84	108.50	108.72	108.95	109.17	109.40	109.62	109.85	110.07	110.80	110.52		
83	106.25	106.47	106.70	106.92	107.15		107.60	107.82	108.05	108.27		
82	104.00	104.22	104.45	104.67	104.90	1	105.35	105.57	106.80	106.02		
81	101.75	101.97	102.20	102.42	102.65	102.87	108.10	108.82	103.55	108.77		
		00	00.0-	100 15	100 45	100.00	100 0-	105.0	100 00	107		
80	99.50 97.25	99.72	99.95 97.70	100.17	100.40 98.15		100.85	101.07	101.30 99.05	101.52		
29 28	97.25	97.47 95.22	95.45	97.92 95.67	95.90	98.37 96.12	98.60 96.85	98.82 96.57	96.80	99.27 97.02		
20	92.75	92.97	98.20	93.42	93.65		94.10	94.82	94.55	94.77		
26	90.50	90.72	90.95	91.17	91.40	91.62	91.85	92.07	92.30	92.52		
-					- 2. 20							
25	88.25	88.47	88.70	88.92	89.15	89.87	89.60	89.82	90.05	90.27		
24	86.00	86.22	86.45	86.67	86.90	87.12	87.85	87.57	87.80	88.02		
23	83.75	83.97	84.20	84.42	84.65	84.87	85.10	85.82	85.55	85.77		
22	81.50	81.72	81.95	82.17	82.40	82.62	82.85	88.07	83.30	88.52		
21	79.25	79.47	79.70	79.92	80.15	80.87	80.60	80.82	81.05	81.27		
20	77.00	77.22	77.45	77.67	77.90	78.12	78.85	78.57	78.80	79.02		
19	74.75	74.97	75.20	75.42	75.65	75.87	76.10	76.82	76.55	76.77		
18	72.50 70.25	72.72 70.47	72.95 70.70	78.17 70.92	78.40 71.15	73.62 71.87	78.85 71.60	74.07	74.30 72.05	74.52 72.27		
17 16	68.00	68.22	68.45	68.67	68.90	69.12	69.85	69.57	69.80	70.02		
• .	00.00	00.22	00.40	00.07	00.00	00.12	03.00	03.01	00.00	10.02		
15	65.75	65.97	66.20	66.42	66.65	66.87	67.10	67.32	67.55	67.77		
14	68.50	63.72	68.95	64.17	64.40	64.62	64.85	65.07	65.80	65.52		
· · 18	1.25	61.47	61.70	61.92	62.15	62.87	62.60	62.82	63.05	63.27		
J2.	59.00	59.22	59.45	59.67	59.90	60.12	60.85	60.57	60.80	61.02		
11	756.75	56.97	57.20	57.42	57.65	57.87	58.10	58.82	58.55	58.77		
٠, ١	7											
16	54.50	54.72	54.95	65.17	55.40	55.62	55.85	56.07	56.80	56.52		
9	52.25	52.47	52.70	52.92	53.15	53.87	53.60	58.82	54.05	54.27		
8	50.00 47.75	50.22 47.97	50.45 48.20	50.67 48.42	50.90 48.65	51.12 48.87	51.85 49.10	51.57 49.82	51.80 49.55	52.02 49.77		
6	45.50	47.97	45.95	46.17	46.40	46.62	46.85	47.07	47.80	47.5?		
•	20.00	W. 72	-50.00	₩.11	40,40	40.02	20.00		41.00	2110,		
5	43.25	48.47	48.70	43.92	44.15	44.87	44.60	44.82	45.05	45.27		
4	41.00	41.22	41.45	41.67	41.90	42.12	42.85	42.57	42.80	43.02		
8	88.75	88.97	89.20	89.42	89.65	89.87	40.10	40.82	40.55	40.77		
2	36.50	86.72	86.95	87.17	87.40	87.62	87.85	88.07	88.30	88.52		
L	84.25	84.47	84.70	84.92	85.15	85.87	35.60	35.82	36.05	86.27		
			9									
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.		

A

					Tenths o	f Degrees.				
Degrees of Resummr.	0.	1.	2.	3.	4.	5,	6.	7.	s.	9.
+ 0	Fahren. +32.00	Fahren. +32.22	Fahren. +32.45	Fahren. +32.67	Fahren, +82.90	Fahren. +33.12	Fahren. +83.85	Fahren. +83.57	Fahren. +33.80	Fahren. +34.02
-0	82.00	31.77	81.55	31.32	\$1.10	30.87	30.65	80.42	80.20	29.97
-1	29.75	29.52	29.80	29.07	28.85	28.62	28.40	28.17	27.95	27.72
- 2	27.50	27.27	27.05	26.82	26.60	26.87	26.15	25.92	25.70	25.47
- 8	25.25	25.02	24.80	24.57	24.85	24.12	23.90	23.67	28.45	23.22
- 4	23.00	22.77	22.55	22.32	22.10	21.87	21.65	21.42	21.20	20.97
•						1			1	20.01
- 5	20.75	20.52	20-80	20.07	19.85	19.62	19.40	19.17	18.95	18.72
- 6	18.50	18.27	18.05	17.82	17.60	17.87	17.15	16.92	16.70	16.47
- 7	16.25	16.02	15.80	15.57	15.25	15.12	14.90	14.67	14.45	14.22
- 8	14.00	13.77	18.55	18.82	18.10	12.87	12.65	12.42	12.20	11.97
- 9	11.75	11.52	11.80	11.07	10.85	10.62	10.40	10.17	9.95	9.72
_10	9.50	9.27	9.05	8.82	8.60	8.37	0.15	7.92	7.70	7 4~
-10 -11	7.25	7.02	6.80	6.57	6.85	6.12	8.15 5.90	5.67	5.45	7.47 5.22
-11 -12	5.00	4.77	4.55	4.32	4.10	8.87	8.65	8.42	8.20	2.97
-12	2.75	2.52	2.30	2.07	1.85	1.62	1.40	1.17	0.95	0.72
-14	0.50	0.27	0.05	- 0.17	- 0.40	- 0.62	- 0.85	- 1.07	- 1.80	- 1.52
	0.50	0.27	0.00	- 0.17	- 0.40	0.02	_ 0.00	_ 1.07	- 1.50	- 1.02
-15	- 1.75	- 1.97	- 2.20	- 2.42	- 2.65	- 2.87	- 8.10	- 8.82	- 3.55	- 8.77
-16	- 4.00	- 4.22	- 4.45	- 4.67	- 4.90	- 5.12	- 5.85	- 5.57	- 5.80	- 6.02
-17	- 6.25	- 6.47	- 6.70	- 6.92	- 7.15	- 7.87	- 7.60	- 7.82	- 8.05	- 8.27
-18	- 8.50	- 8.72	- 8 .9 5	- 9.17	- 9.40	- 9.62	- 9.85	-10.07	-10.80	-10.52
-19	-10.75	-10.97	-11.20	-11.42	-11.65	-11.87	-12.10	-12.32	-12.55	-12.77
-20	-18.00	-18.22	-18.45	-13.67	-13.90	-14.12			-14.80	-15.02
-21	-15.25	-15.47	-15.70	-15.92	-16.15	-16.87		-16.82	-17.05	-17.27
-22	-17.50	-17.72	-17.95	-18.17	-18.40	-18.62			-19.30	-19.52
-23 -24	-19.75	-19.97	-20.20 -22.45	-20.42	-20.65	-20.87 -23.12		-21.82	-21.55 -23.80	-21.77
-24	-22.00	-22.22	-42.40	-22.67	-22.90	-20.12	-25.80	-23.57	-23.5U	-24.02
25	-24.25	-24.47	-24.70	-24.92	-25.15	-25.87	-25.60	-25.82	-26. 05 -	-26.27
-26	-26.50	-26.72	-26.95	-27.17		-27.62	-27.85	-28.07	-28.2 0 ·	
-27	- 2 8.75	-28.97	-29.20	-29.42	-29 .65	-29.87	-80.10	-80.82	-3035	-80.77
-28	-\$1.00	-81.22	-81.45	-81.67	-81.90	-82.12	-82.85	-82.57	-32,80	-88.02
-29	-33.25	-83.47	-88.70	-33.92	-84.15	-84.87	-34.60	-34.82	-85.06	-83.27
	1	i		'					1,37	b.
-30	-85.50	-85.72	-85.95	-8 6.17	-86.40	-86.62	-86 .85	-87 .07	-87.80	~8 7752.
-31	-87.75	-87.97	-88.20	-8 8.42	-88.65	-88.87		-39.32	-89.55	-89.77
-32	-40.00	-40.22	-40.45	-40.67	-40.90	-41.12		-41.57	-41.80	-43.02
-33	-42-25	-42.47	-42.70	-42.92	-48.15	-48.87	-48.60	-43.82	-44.05	-44.27
-84	-44.50	-44.72	-44.95	-45.17	-45.40	-45.62	-45.85	-46.07	-46.80	-46.52
-35										
	-46.75	-46.97	-47.20	-47.42	-47.65	-47.87	-48.10	-48.32	-48.55	-48.77
-36	-49.00	-49.22	-49.45	-49.67	-49.90	-50.12	-50.35	-50.57	-50.80	-51.02
-37	-51.25	-51.47	-51.70	-51.92	-52.15	-52.87	-52.60	-52.82	-53.05	-58.27
-38	-58.50	-58.72	-58.95	-54.17	-54.40	-54.62	-54.85	-55.07	-55.80	-55.52
-39	-55.75	-55.97	-56.20	-56.42	-50.65	-56.87	-57.10	-57.32	-57.55	-67.77
	0,	1.	2.	8.	4.	5.	G.	7.	8.	9.

11. CONVERSION OF DEGREES OF REAUMUR INTO CENTIGRADE DEGREES.

Contignost Con		Tentile of Degrees.											
±40 ±50.06 ±50.18 ±50.25 ±60.86 ±60.06 ±60.83 ±50.75 ±60.88 ±51.00 ±51.10 <th>Degrees of Resumur.</th> <th>0.</th> <th>1.</th> <th>2.</th> <th>8.</th> <th>4.</th> <th>5.</th> <th>6.</th> <th>7.</th> <th>8.</th> <th>9.</th>	Degrees of Resumur.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.		
Record R	+40										Centig. +51.13		
37 46.25 46.88 46.50 46.63 46.75 46.88 47.00 47.13 47.25 47.13 47.25 47.13 47.25 47.13 47.25 47.13 47.25 47.13 47.25 47.13 47.25 47.13 47.25 47.13 45.26 46.88 46.00 46.31 45.26 46.88 44.00 44.13 44.25 44.88 44.50 44.63 44.75 44.81 34.20 42.13 42.25 42.88 44.00 44.13 42.25 44.84 44.00 44.13 44.25 44.88 44.00 42.13 42.25 44.84 44.00 44.13 44.25 44.84 44.00 44.13 44.25 44.84 44.00 44.13 44.25 44.84 44.00 44.13 44.25 44.84 44.00 44.13 44.25 44.83 44.07 44.10 44.10 44.10 44.10 44.10 44.10 44.10 44.10 44.10 44.11 44.25 44.83 40		48.75	_	_	I—	ı—	_		_	_	49.88		
36 45.00 45.13 45.25 45.88 45.00 46.38 45.75 45.88 46.00 46.3 35 43.75 43.88 44.00 44.13 44.25 44.88 44.60 44.63 44.75 44.8 34 42.50 42.63 42.75 42.88 45.00 43.13 43.25 43.88 48.50 43.13 43.25 43.88 48.50 43.13 43.25 43.88 48.50 42.13 42.25 42.13 42.25 42.13 42.25 42.13 42.25 42.13 42.25 42.13 42.25 42.13 42.25 42.13 42.25 42.13 42.25 42.13 42.25 42.13 42.25 42.13 42.25 42.33 40.00 40.48 40.00 40.48 40.00 48.13 43.25 43.88 40.00 48.13 43.25 43.88 40.00 46.3 46.79 40.88 41.00 44.13 44.25 44.88 44.00 44.13	88	47.50	47.63	47.75	47.88	48.00	48.13	48.25	48.88	48.50	48.63		
35 43.75 43.88 44.00 44.18 44.25 44.88 44.50 44.63 44.75 44.83 44.75 44.88 44.50 44.63 44.75 42.83 43.25 43.88 44.50 42.13 42.25 42.33 42.25 42.33 42.25 42.33 42.25 42.33 42.25 42.33 42.25 42.33 42.25 42.33 42.25 42.33 42.25 42.33 42.25 42.33 42.25 42.33 42.25 42.33 42.25 42.33 42.25 42.33 42.25 42.33 42.25 42.33 44.25 44.48 44.75 44.48 44.60 44.13 44.25 44.48 44.67 44.48 44.60 44.83 44.60 44.41 44.42 44.41 44	87	46.25	46.88	46.50	46.63	46.75	46.88	47.00	47.13	47.25	47.38		
84 42.60 42.63 42.75 42.83 43.00 43.13 43.25 43.88 46.50 42.13 42.25 32.83 39.00 38.13 38.25 38.83 88.50 38.13 38.25 38.83 38.50 38.13 38.25 38.83 38.50 38.13 38.25 38.83 38.50 38.13 38.25 38.83 38.50 38.13 38.25 38.83 38.00 38.13 38.25 38.83 38.00 38	86	45.00	45.13	45.25	45.88	45.50	45.68	45.75	45.88	46.00	46.13		
38 41.25 41.88 41.60 41.63 41.75 41.88 42.00 42.13 42.25 42.33 32 40.00 40.13 40.25 40.38 40.60 40.483 40.75 40.89 41.00 41.33 31 38.76 38.88 39.00 39.13 39.25 39.88 39.50 39.63 39.75 39.33 30 37.60 37.63 37.75 37.88 38.00 38.13 38.25 38.88 38.00 37.13 37.25 38.22 38.20 38.35.00 38.35.00 38.35.00	85	43.75	43.88	44.00	44.18	44.25	44.88	44.50	44.63	44.75	44.88		
32 40.00 40.13 40.25 40.38 40.50 40.483 40.75 40.88 41.00 41.33 31 38.75 38.88 39.00 39.13 39.25 39.88 39.50 39.43 39.75 39.33 30 37.60 37.63 37.75 37.88 38.00 38.13 38.25 38.88 38.50 38.62 36.63 36.75 36.88 37.00 37.13 37.25 37.37 37.38 36.00 38.13 38.25 38.50 38.63 36.00 38.13 38.25 38.50 37.38 38.00 38.13 38.25 36.88 36.00 38.43 34.75 34.45 34.48 34.50 34.83 34.75 34.75 34.75 34.75 34.75 34.75 34.75 34.75 34.75 34.75 34.75 34.75 34.75 34.75 34.75 34.75 34.75 34.75 34.75 34.83 34.75 34.75 34.83 34.75 34.75	84	42.50	42.63	42.75	42.88	43.00	48.13	43.25	43.88	48.50	43.63		
31 38.75 38.88 39.00 39.13 39.25 39.88 39.60 38.33 38.75 38.13 30 37.60 37.63 37.75 37.88 38.00 38.13 38.25 38.88 38.50 38.13 29 36.25 36.38 36.60 36.63 36.75 36.88 37.00 37.13 37.25 37.25 28 36.00 35.13 35.25 35.38 36.50 36.63 35.75 35.88 36.00 36.33 26 32.50 32.63 32.75 32.88 33.00 38.13 33.25 33.88 33.60 38.33 38.21 34.43 34.45 34.43 34.47 34.43 34.53 34.45 34.43 34.47 34.43 34.47 34.43 34.47 34.43 34.47 34.43 34.47 34.43 34.47 34.43 34.47 34.43 34.47 34.43 34.47 34.43 34.47 34.47 34.43 34.47 </th <th>38</th> <th>41.25</th> <th>41.38</th> <th>41.50</th> <th>41.63</th> <th>41.75</th> <th>41.88</th> <th>42.00</th> <th>42.18</th> <th>42.25</th> <th>42.38</th>	38	41.25	41.38	41.50	41.63	41.75	41.88	42.00	42.18	42.25	42.38		
30 37.60 37.63 37.75 37.88 38.00 38.13 38.25 38.88 38.50 37.13 37.25 32.25 32.35 32.35 32.35 32.35 32.35 32.35 32.35 32.35 32.35 32.35 32.35 32	82	40.00	40.13	40.25	40.38	40.50	40.68	40.75	40.88	41.00	41.13		
29 36.25 36.38 36.60 36.63 36.75 36.83 37.00 87.13 37.25 37.1 28 36.00 35.13 35.25 35.38 35.50 35.68 35.75 35.88 36.00 36.63 27 32.75 33.88 34.00 34.13 34.25 34.88 34.60 34.63 34.75 34.13 26 32.50 32.63 32.75 32.88 38.00 33.13 33.25 33.88 33.50 33.88 32.50 33.88 3	81	88.75	88.88	39.00	89.18	89.25	89.88	89.50	89.63	89.75	39.88		
28 35.00 35.13 35.25 35.88 34.00 34.13 34.26 34.88 34.60 34.63 34.75 34.63 34.75 34.63 34.75 34.63 34.75 34.63 34.75 34.63 34.75 34.63 34.75 34.63 34.75 34.63 34.75 34.63 34.75 34.63 34.75 34.63 34.75 34.63 34.75 34.63 34.75 34.88 34.60 34.63 34.75 34.83 32.00 32.18 32.25 32.32 33.83 30.00 30.83 30.00 30.68 30.76 30.88 31.00 31. 22.25 22.38 29.50 29.63 29.75 29.75 29.75 29.75 29.75 29.75 29.75 29.75 29.75 29.75 29.75 29.75 29.75 29.75 29.75 29.75 29.75 29.75 29.275 29.275 29.275 29.275 29.275 29.275 29.275 29.275 29.275 29.275											88.63		
27 33.75 33.88 34.00 34.13 34.25 34.88 34.50 34.63 34.75 34.8 26 32.50 32.63 32.75 32.88 33.00 33.12 33.25 33.88 33.50 33.4 25 31.25 31.38 31.50 31.63 31.75 31.88 32.00 32.18 32.25 32.3 24 30.00 30.18 30.25 80.38 30.60 30.68 30.75 30.88 31.00 31. 23 28.75 28.88 29.00 29.13 29.25 29.38 29.60 29.63 29.75 29.1 22 27.50 27.63 27.75 27.88 26.00 28.18 28.25 28.38 28.50 22.63 29.75 29.1 20 25.00 25.13 25.25 25.88 25.50 25.63 25.75 25.88 26.00 26.1 29.21 21.25 21.38 23.50 23.38 23.50<											37.38		
26 32.50 32.63 32.75 32.88 33.00 33.13 33.25 33.88 38.50 33.41 25 31.25 31.38 31.50 31.63 31.75 31.88 32.00 32.18 32.25 32.18 24 30.00 30.18 30.25 80.38 30.60 30.68 30.75 30.88 31.00 31.25 23 28.75 28.88 29.00 29.13 29.25 29.38 29.50 29.63 29.75 29.1 22 27.50 27.63 27.75 27.88 28.00 28.18 28.25 28.38 28.50 28.63 21 26.25 26.38 26.60 26.63 26.75 26.88 27.00 27.13 27.25 27.3 20 25.00 25.13 25.25 25.88 25.50 25.63 25.75 25.88 26.00 26.1 19 23.75 23.88 21.00 21.13 22.25 22.13 <th></th> <th>1</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>86.13</th>		1									86.13		
25 31.25 31.38 31.60 31.63 31.75 31.88 32.00 32.18 32.25 32.18 32.25 32.18 32.25 32.18 32.25 32.31 32.25 30.00 30.18 30.25 30.88 30.50 30.68 30.75 30.88 30.00 32.18 32.25 32.38 29.50 29.68 29.75 29.85 29.50 28.18 28.20 29.38 29.50 22.63 22.75 22.88 23.00 28.18 28.25 25.88 26.00 26.18 24.75 24.68 24.75 24.68 24.75 24.68 24.75 24.68 24.75 24.68 24.75 24.68 24.75 24.68 24.75 24.68 24						1		1			84.88		
24 30.00 30.18 30.25 80.88 30.60 30.68 30.75 30.88 31.00 31. 28 28.75 28.88 29.00 29.13 29.25 29.38 29.50 29.63 29.75 29.1 22 27.50 27.63 27.75 27.88 28.00 28.18 28.25 28.38 28.50 23.6 21 26.25 26.38 26.60 26.63 26.75 26.88 27.00 27.13 27.25 27.3 20 25.00 25.13 25.25 25.88 25.50 25.63 25.75 25.88 26.00 26.18 19 23.75 23.88 24.00 24.13 24.25 24.38 24.50 24.63 24.75 24.43 18 22.50 22.63 22.75 22.88 23.00 23.13 23.25 23.38 23.50 23.22 23.13 17 21.25 21.88 21.60 21.63 21.75 21.88 22.00 22.13 22.25 22.21 16 20.00	26	82.50	82.63	82.75	82.88	83.00	33.13	83.25	83.88	88.50	38.68		
23 28.75 28.88 29.00 29.13 29.25 29.38 29.50 29.63 29.75 29.75 27.88 28.00 28.18 28.25 28.38 28.50 28.65 26.88 26.50 26.68 26.75 26.88 27.00 27.18 27.25 27.3 20 25.00 25.13 25.25 25.88 25.50 25.63 25.75 25.88 26.00 26.13 24.25 24.88 24.50 24.63 24.75 24.88 24.50 24.63 24.75 24.88 24.50 24.63 24.75 24.88 24.50 24.63 24.75 24.88 24.50 24.63 24.75 24.88 24.50 24.63 24.75 24.88 24.50 24.63 24.75 24.63 24.75 24.88 22.00 22.13 22.25 23.38 23.50 23.88 23.00 22.13 22.25 22.31 22.25 22.33 20.00 22.13 22.25 22.33 20.00 22.13	25	31.25	31.38	31.50	81.63	31.75	81.88	82.00	82.18	32.25	32.38		
22 27.50 27.63 27.75 27.88 29.00 29.18 28.25 28.38 28.50 28.62 21 26.25 26.88 26.50 26.63 26.75 26.88 27.00 27.18 27.25 24.48 24.50 24.68 24.75 24.43 24.50 24.68 24.75 24.43 24.25 24.28 24.00 22.13 22.25 23.28 23.00 23.18 23.25 23.28 23.50 22.00 22.13 22.25 22.31 22.25 22.31 22.25 22.31 22.25 22.31 22.25 22.33 20.50 20.68 20.75	24	30.00	80.18	80.25	80.38	80.50	30.68	80.75	80.88	81.00	31.18		
21 26.25 26.88 26.50 26.63 26.75 26.88 27.00 27.13 27.25 27.3 20 25.00 25.13 25.25 25.88 25.50 25.63 25.75 25.88 26.00 26.19 19 23.75 23.88 24.00 24.13 24.25 24.88 24.50 24.63 24.75 24.41 18 22.50 22.63 22.75 22.88 23.00 23.13 23.25 23.88 23.50 23.18 23.25 23.88 23.50 23.13 23.25 23.88 23.50 23.18 23.25 23.88 23.50 23.18 23.25 23.88 23.50 23.18 23.25 23.88 23.50 23.21 23.25 23.88 23.50 23.21 23.25 23.88 23.50 23.21 23.25 23.88 23.50 23.21 23.25 23.28 23.50 23.21 23.25 23.88 23.00 23.18 23.20 23.21 2	28	28.75	28.88	29.00	29.13	29.25	29.38	29.50	29.68	29.75	29.88		
20 25.00 25.13 25.25 25.88 25.50 25.63 25.75 25.88 26.00 26.13 26.00 26.13 24.13 24.25 24.88 24.50 24.68 24.75 24.68 24.75 24.88 24.50 24.68 24.75 24.88 24.50 24.68 24.75 24.88 24.50 24.68 24.75 24.88 24.50 24.68 24.75 24.88 24.50 24.68 24.75 24.88 24.50 24.68 24.75 24.88 24.50 24.68 24.75 24.88 24.50 24.68 24.75 24.88 24.50 24.68 24.75 24.68 24.75 24.88 24.50 24.68 24.75 24.68 24.75 24.68 24.75 24.68 24.75 24.68 24.75 24.68 24.75 24.88 24.50 24.88 23.50 23.88 23.50 23.88 23.50 23.88 22.00 22.18 22.25 22.21 22.25 22.21 22.25 22.21 22.25 22.21 22.25 22.25 22.21 22.25 22	22	27.50	27.63	27.75	27.88	28.00	28.18	28.25	28.38	28.50	28 63		
19 23.75 23.88 24.00 24.13 24.25 24.88 24.50 24.63 24.75 24.81 18 22.50 22.63 22.75 22.88 23.00 23.13 23.25 23.38 23.50 23.61 17 21.25 21.38 21.50 21.63 21.75 21.88 22.00 22.13 22.25 22.31 16 20.00 20.13 20.25 20.38 20.50 20.63 20.75 20.88 21.00 21.3 15 18.75 18.88 19.00 19.13 19.25 19.38 19.50 19.63 19.75 19.3 14 17.50 17.63 17.75 17.88 18.00 18.13 18.25 18.38 18.50 18.4 13 16.25 16.83 16.50 16.63 16.75 16.88 17.00 17.13 17.25 17.4 12 15.00 15.13 15.25 15.38 15.60 16.63 16.75 16.88 17.00 17.13 17.25 17.4 10	21	26.2 5	26.88	26.50	26.63	26.75	26.88	27.00	27.18	27.25	27.38		
18 22.50 22.63 22.75 22.88 23.00 23.13 23.25 23.88 23.50 23.48 17 21.25 21.88 21.60 21.63 21.75 21.88 22.00 22.13 22.25 22.3 16 20.00 20.13 20.25 20.38 20.50 20.63 20.75 20.68 21.00 21.3 15 18.75 18.88 19.00 19.13 19.25 19.38 19.50 19.63 19.75 19.4 14 17.50 17.63 17.75 17.88 18.00 18.13 18.25 18.28 18.50 18.4 13 16.25 16.83 16.60 16.63 16.76 16.88 17.00 17.13 17.25 17.1 12 15.00 15.13 15.25 15.88 15.50 15.63 15.75 15.88 16.00 16.1 11 18.75 13.88 14.00 14.13 14.25 14.83 14.50 14.63 14.75 14.43 10 12.50 12.63<	20	25.00	25.13	25.25	25.38	25.50	25.68	25.75	25.88	26.00	26.13		
17 21.25 21.88 21.60 21.63 21.75 21.88 22.00 22.13 22.25 22.15 16 20.00 20.13 20.25 20.38 20.50 20.63 20.75 20.88 21.00 21.1 15 18.75 18.88 19.00 19.13 19.25 19.38 19.50 19.68 19.75 19.4 14 17.50 17.63 17.75 17.88 18.00 18.13 18.25 18.28 18.50 18.6 13 16.25 16.38 16.50 16.63 16.75 16.88 17.00 17.13 17.25 17.4 12 15.00 15.13 15.25 15.38 16.50 15.63 15.75 15.88 16.00 16.1 11 18.75 18.83 14.00 14.13 14.25 14.88 14.50 14.63 14.75 14.43 10 12.50 12.63 12.75 12.88 13.00 13.13 13.25 18.38 18.50 18.6 9 11.25 11.38 11.50	19	28.75	23.88	24.00	24.18	24.25	24.88	24.50		24.75	24.88		
16 20.00 20.13 20.25 20.38 20.50 20.63 20.75 20.88 21.00 21.3 15 18.75 18.88 19.00 19.13 19.25 19.38 19.50 19.68 19.75 19.4 14 17.50 17.63 17.75 17.88 18.00 18.13 18.25 18.28 18.50 18.6 13 16.25 16.88 16.50 16.63 16.75 16.88 17.00 17.13 17.25 17.4 12 15.00 15.13 15.25 15.38 16.50 15.63 15.75 15.88 16.00 16.1 11 18.75 18.88 14.00 14.13 14.25 14.38 14.50 14.63 14.75 14.43 10 12.50 12.63 12.75 12.88 13.00 13.13 13.25 18.38 18.50 18.6 10 12.50 12.63 12.75 12.88 13.00 13.13	18	22.50	22.63	22.75	22.88	23.00	28.18	23.25	23.88	23.50	23.63		
15 18.75 18.88 19.00 19.13 19.25 19.38 19.50 19.68 19.75 19.8 14 17.50 17.63 17.75 17.88 18.00 18.13 18.25 18.88 18.50 18.6 13 16.25 16.88 16.50 16.68 16.75 16.88 17.00 17.13 17.25 17.4 12 15.00 15.13 15.25 15.38 15.60 15.63 15.75 15.88 16.00 16.13 11 18.75 18.88 14.00 14.13 14.25 14.38 14.50 14.63 14.75 14.43 10 12.50 12.63 12.75 12.88 13.00 13.13 13.25 18.38 18.50 18.4 10 12.50 12.63 12.75 12.88 13.00 13.13 13.25 18.38 18.50 18.4 10 12.50 12.63 12.75 12.88 13.00 13.13 13.25 18.38 18.50 18.4 10 10.13 10.25<		21.25	21.88	21.50	21.68	21.75	21.88	22.00	22.18		22.38		
14 17.50 17.63 17.75 17.88 18.00 18.13 18.25 18.38 18.50 18.61 18.62 18.88 17.00 17.13 17.25 17.13 17.25 17.13 17.25 17.13 17.25 17.13 17.25 17.13 17.25 17.13 17.25 17.13 17.25 17.13 17.25 17.13 17.25 17.13 17.25 17.13 17.25 17.13 17.25 17.13 17.25 17.13 17.25 17.13 17.25 17.13 17.25 17.25 17.24 18.26 18	16	20.00	20.18	20.25	20.88	20.50	20.63	20.75	20.88	21.00	21.13		
13 16.25 16.88 16.50 16.63 16.75 16.88 17.00 17.18 17.25 17.1 12 15.00 15.13 15.25 15.38 15.60 15.63 15.75 15.88 16.00 16.1 11 18.75 18.88 14.00 14.13 14.25 14.88 14.50 14.63 14.75 14.8 10 12.50 12.63 12.75 12.88 13.00 13.13 13.25 18.38 18.50 18.6 9 11.25 11.38 11.60 11.63 11.75 11.88 12.00 12.18 12.25 12.3 8 10.00 10.13 10.25 10.38 10.50 10.63 10.75 10.88 11.00 11.3 7 8.75 8.88 9.00 9.13 9.25 9.88 9.50 9.63 9.75 9.8 6 7.50 7.68 7.75 7.88 8.00 8.18 8.25	15	18.75	18.88	19.00	19.13	19.25	19.38	19.50	19.68	19.75	19.88		
12 15.00 15.13 15.25 15.88 16.60 15.63 15.75 15.88 16.00 16.1 11 18.75 18.88 14.00 14.13 14.25 14.88 14.50 14.63 14.75 14.63 10 12.50 12.63 12.75 12.88 13.00 13.13 13.25 18.38 18.50 18.6 9 11.25 11.33 11.50 11.63 11.75 11.88 12.00 12.18 12.25 12.3 8 10.00 10.13 10.25 10.38 10.50 10.63 10.75 10.88 11.00 11.3 7 8.75 8.88 9.00 9.13 9.25 9.88 9.50 9.63 9.75 9.8 6 7.50 7.68 7.75 7.88 8.00 8.13 8.25 8.88 8.50 8.6 5 6.25 6.38 6.50 6.63 6.75 6.88 7.00 7.13 7.25 7.3 4 5.00 5.13 5.25 5.38	14	17.50	17.63	17.75	17.88	18.00		18.25	18.38	18.50	18.68		
11 18.75 18.88 14.00 14.18 14.25 14.38 14.50 14.63 14.75 14.43 10 12.50 12.63 12.75 12.88 13.00 13.18 13.25 18.88 18.50 18.6 9 11.25 11.38 11.60 11.63 11.75 11.88 12.00 12.18 12.25 12.18 8 10.00 10.13 10.25 10.38 10.50 10.63 10.75 10.88 11.00 11.1 7 8.75 8.88 9.00 9.13 9.25 9.88 9.50 9.63 9.75 9.8 6 7.50 7.68 7.75 7.88 8.00 8.13 8.25 8.88 8.50 8.6 5 6.25 6.38 6.50 6.63 6.75 6.88 7.00 7.13 7.25 7.3 4 5.00 5.13 5.25 5.38 5.50 5.63 5.75 5.88 <th>13</th> <th>16.25</th> <th>16.88</th> <th>16.50</th> <th>16.63</th> <th>16.75</th> <th>16.88</th> <th>17.00</th> <th>17.18</th> <th>17.25</th> <th>17.88</th>	13	16.25	16.88	16.50	16.63	16.75	16.88	17.00	17.18	17.25	17.88		
10 12.50 12.63 12.75 12.88 13.00 13.13 13.25 18.88 18.50 18.60 9 11.25 11.38 11.50 11.63 11.75 11.88 12.00 12.18 12.25 12.3 8 10.00 10.13 10.25 10.38 10.50 10.63 10.75 10.88 11.00 11.3 7 8.75 8.88 9.00 9.13 9.25 9.88 9.50 9.63 9.75 9.8 6 7.50 7.68 7.75 7.88 8.00 8.18 8.25 8.88 8.50 8.6 5 6.25 6.38 6.50 6.63 6.75 6.88 7.00 7.13 7.25 7.3 4 5.00 5.13 5.25 5.38 5.50 5.63 5.75 5.88 6.00 6.3 3 3.75 3.88 4.00 4.13 4.25 4.38 4.50 4.63 <	12	15.00	15.13	15.25	15.88	15.50	15.63	15.75	15.88	16.00	16.13		
9 11.25 11.38 11.60 11.63 11.75 11.88 12.00 12.18 12.25 12.35 8 10.00 10.13 10.25 10.38 10.50 10.62 10.75 10.88 11.00 11.1 7 8.75 8.88 9.00 9.13 9.25 9.88 9.50 9.63 9.75 9.5 6 7.50 7.68 7.75 7.88 8.00 8.18 8.25 8.88 8.50 8.6 5 6.25 6.38 6.50 6.63 6.75 6.88 7.00 7.13 7.25 7.3 4 5.00 5.13 5.25 5.38 5.50 5.63 5.75 5.88 6.00 6.3 3 3.75 3.88 4.00 4.13 4.25 4.38 4.50 4.63 4.75 4.4 2 2.50 2.63 2.75 2.88 3.00 3.13 3.25 3.38 3.50 3.4 1 1.25 1.38 1.50 1.63 1.75 1.88 2.00 2.13 2.25 2.2 0 0.00 0.13 0.25 0.38 0.50 0.63 0.75	11	18.75	18.88	14.00	14.18	14.25	14.88	14.50	14.63	14.75	14.88		
8 10.00 10.13 10.25 10.38 10.50 10.63 10.75 10.88 11.00 11.1 7 8.75 8.88 9.00 9.13 9.25 9.88 9.50 9.63 9.75 9.5 6 7.50 7.68 7.75 7.88 8.00 8.13 8.25 8.88 8.50 8.6 5 6.25 6.38 6.50 6.63 6.75 6.88 7.00 7.13 7.25 7.3 4 5.00 5.13 5.25 5.38 5.50 5.63 5.75 5.88 6.00 6.3 3 3.75 3.88 4.00 4.13 4.25 4.38 4.50 4.63 4.75 4.4 2 2.50 2.63 2.75 2.88 3.00 3.13 3.25 3.38 3.50 3.4 1 1.25 1.38 1.50 1.63 1.75 1.88 2.00 2.13 2.25 2.3 0 0.00 0.13 0.25 0.38 0.50 0.63 0.75 0.88 1.00 1.3	10	12.50	12.63	12.75	12.88	13.00	13.18	13.25	18.38	18.50	18.68		
7 8.75 8.88 9.00 9.13 9.25 9.88 9.50 9.63 9.75 9.6 6 7.50 7.68 7.75 7.88 8.00 8.13 8.25 8.88 8.50 8.6 5 6.25 6.38 6.50 6.63 6.75 6.88 7.00 7.13 7.25 7.4 4 5.00 5.13 5.25 5.38 5.50 5.63 5.75 5.88 6.00 6.3 3 3.75 3.88 4.00 4.13 4.25 4.38 4.50 4.63 4.75 4.5 2 2.50 2.63 2.75 2.88 3.00 3.13 3.25 3.38 3.50 3.4 1 1.25 1.38 1.50 1.63 1.75 1.88 2.00 2.13 2.25 2.3 0 0.00 0.13 0.25 0.38 0.50 0.63 0.75 0.88 1.00 1.3	9	11.25	11.38	11.50	11.63	11.75	11.88	12.00	12.18	12.25	12.38		
6 7.50 7.68 7.75 7.88 8.00 8.13 8.25 8.88 8.50 8.6 5 6.25 6.38 6.50 6.63 6.75 6.88 7.00 7.13 7.25 7.3 4 5.00 5.13 5.25 5.38 5.50 5.63 5.75 5.88 6.00 6.3 3 3.75 3.88 4.00 4.13 4.25 4.38 4.50 4.63 4.75 4.5 2 2.50 2.63 2.75 2.88 3.00 3.13 3.25 3.88 3.50 3.4 1 1.25 1.38 1.50 1.63 1.75 1.88 2.00 2.13 2.25 2.3 0 0.00 0.13 0.25 0.38 0.50 0.63 0.75 0.88 1.00 1.3	8	10.00	10.13	10.25	10.38	10.50	10.63	10.75	10.88	11.00	11.13		
5 6.25 6.38 6.50 6.63 6.75 6.88 7.00 7.13 7.25 7.3 4 5.00 5.13 5.25 5.38 5.50 5.63 5.75 5.88 6.00 6.3 3 3.75 3.88 4.00 4.13 4.25 4.88 4.50 4.63 4.75 4.1 2 2.50 2.63 2.75 2.88 3.00 3.13 3.25 3.38 3.50 3.4 1 1.25 1.38 1.50 1.63 1.75 1.88 2.00 2.13 2.25 2.3 0 0.00 0.13 0.25 0.38 0.50 0.63 0.75 0.88 1.00 1.3		8.75	8.88	9.00	9.18	9.25	9.88	9.50	9.68	9.75	9.88		
4 5.00 5.13 5.25 5.38 5.50 5.63 5.75 5.88 6.00 6.3 3 3.75 3.88 4.00 4.13 4.25 4.88 4.50 4.63 4.75 4.4 2 2.50 2.63 2.75 2.88 3.00 3.13 3.25 3.88 3.50 3.4 1 1.25 1.38 1.50 1.63 1.75 1.88 2.00 2.13 2.25 2.4 0 0.00 0.13 0.25 0.38 0.50 0.63 0.75 0.88 1.00 1.3	6	7.50	7.68	7.75	7.88	8.00	8.18	8.25	8.88	8.50	8.68		
3 3.75 3.88 4.00 4.13 4.25 4.88 4.50 4.63 4.75 4.4 2 2.50 2.63 2.75 2.88 3.00 3.13 3.25 3.88 3.50 3.4 1 1.25 1.38 1.50 1.63 1.75 1.88 2.00 2.13 2.25 2.4 0 0.00 0.13 0.25 0.38 0.50 0.63 0.75 0.88 1.00 1.3			1	ı							7.38		
2 2.50 2.63 2.75 2.88 3.00 3.13 3.25 3.88 3.50 3.4 1 1.25 1.38 1.50 1.63 1.75 1.88 2.00 2.13 2.25 2.3 0 0.00 0.13 0.25 0.38 0.50 0.63 0.75 0.88 1.00 1.3	- 4	i	1	I	ı						6.18		
1 1.25 1.38 1.50 1.63 1.75 1.88 2.00 2.18 2.25 2.3 0 0.00 0.13 0.25 0.38 0.50 0.68 0.75 0.88 1.00 1.3		ľi	1	I	1			l .			4.88		
0 0.00 0.13 0.25 0.38 0.50 0.68 0.75 0.88 1.00 1.3	l l		1	,	1		K .		,	1	3.68 2.88		
		i								Ì	1.13		
0. 1. 2. 3. 4. 5. 6. 7. 6. 9.		0.			3.		5.	6,	7.	8.	9.		

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X.-XV.

TABLES

FOR

COMPARING THERMOMETRICAL DIFFERENCES

EXPRESSED IN DEGREES OF DIFFERENT SCALES,

IRRESPECTIVE OF THEIR ZERO POINT.

X. NUMBER OF DEGREES OF FAHRENHEIT = NUMBER OF CENTIGRADE DEGREES. 4° Resumur = 5° Centigrade = 9° Fahrenheit.

Degrees	Tenths of a Degree.									
of Fahren- heit.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.
0	0.00	0.06	0.11	0.17	0.22	0.28	0.88	0.39	0.44	0.50
1	0.56	0.61	0.67	0.72	0.78	0.88	0.89	0.94	1.00	1.06
2	1.11	1.17	1.22	1.28	1.33	1.39	1.44	1.50	1.56	1.61
3	1.67	1.72	1.78	1.83	1.89	1.94	2.00	2.06	2.11	2.22
4	2.22	2.28	2.33	2.39	2.44	2.50	2.56	2.61	2.67	2.72
5	2.78	2.83	2.89	2.94	8.00	3.06	3.11	8.17	8.22	8.28
6	3.88	8.39	8.44	3.50	8.56	8.61	8.67	4.72	3.78	3.88
7	8.89	8.94	4.00	4.06	4.11	4.17	4.22	4.28	4.83	4.89
8	4.44	4.50	4.56	4.61	4.67	4.72	4.78	4.88	4.89	4.94
9	5.00	5.06	5.11	5.17	5.22	5.28	5.82	5.39	5.44	5.50

XI. NUMBER OF DEGREES OF FAHRENHEIT == NUMBER OF DEGREES OF REAUNUR.

Dogrees					Tenthe of	a Degree.				
of Fahren- heit.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Resumur.	Resumur.	Resumur.	Resumur.	Resumur.	Resumur.	Resomur.	Resumur.	Recomur.	Reaumur.
0	0.00	0.04	0.09	0.18	0.18	0.22	0.27	0.81	0.86	0 40
1	0.44	0.49	0.58	0.58	0.62	0.67	0.71	0.76	0.80	0.84
2	0.89	0.98	0.98	1.02	1.07	1.11	1.16	1.20	1.24	1.29
8	1.33	1.88	1.42	1.47	1.51	1.56	1.60	1.64	1.69	1.78
4	1.78	1.82	1.87	1.91	1.96	2.00	2.04	2.09	2.18	2.18
5	2.22	2.27	2.31	2.36	2.40	2.44	2.49	2.58	2.58	2.62
6	2.67	2.71	2.76	2.80	2.84	2.89	2.93	2.98	3.02	3.07
7	8.11	3.16	8.20	8.24	3.29	8.83	3.38	8.42	3.47	3.51
8	3.56	8.60	8.64	3.69	8.78	8.78	3.82	3.87	3.91	8.96
9	4.00	4.04	4.09	4.18	4.18	4.22	4.27	4.31	4.36	4.40

XII. NUMBER OF CENTIGRADE DEGREES = NUMBER OF DEGREES OF REAUMUR.

			Tenths of a Degree.									
Centig. Degrees.	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.		
	Reaumur.	Resumur	Resumur.	Resumur.	Recumur	Resumur.	Resumur.	Resumur	Resumur.	Resumur.		
0	0.00	0.08	0.16	0.24	0.82	0.40	0.48	0.56	0.64	0.72		
1	0.80	0.88	0.96	1.04	1.12	1.20	1.28	1.36	1.44	1.52		
2	1.60	1.68	1.76	1.84	1.92	2.00	2.08	2.16	2.24	2.32		
3	2.40	2.48	2.56	2.64	2.72	2.80	2.88	2.96	8.04	8.12		
4	8.20	8.28	8.36	8.44	8.52	8.60	8.68	8.76	3.84	3.92		
5	4.00	4.08	4.16	4.24	4.82	4.40	4.48	4.56	4.64	4.72		
6	4.80	4.88	4.96	5.04	5.12	5.20	5.28	5.36	5.44	5.52		
7	5.60	5.68	5.76	5.84	5.92	6.00	6.08	6.16	6.24	6.32		
8	6.40	6.48	6.56	6.64	6.72	6.80	6.88	6.96	7.04	7.12		
9	7.20	7.28	7.86	7.44	7.52	7.60	7.68	7.76	7.84	7.92		

III. NUMBER OF CENTIGRADE DEGREES — NUMBER OF DEGREES OF FAHRENHEIT.

4° Resumur — 5° Contigrade — 9° Fahrenheit.

Contig. Dagress.	Tenths of a Degree.									
Centig. Degrees.	9.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fahr.	Fahr. 0.18	Fahr. 0.86	Fahr. 0.54	Fahr. 0.72	Fahr. 0.90	Fahr. 1.08	Fahr. 1.26	Fahr. 1.44	Fahr. 1.62
1	1.80	1.98	2.16	2.84	2.52	2.70	2.88	3.06	8.24	8.42
	8.60 5.40	3.78 5.58	3.96 5.76	4.14 5.94	4.82 6.12	4.50 6.30	4.68 6.48	4.86 6.66	5.04 6.84	5.22 7.02
4	7.20	7.88	7.56	7.74	7.92	8.10	8.26	8.46	8.64	8.82
5	9.00	9.18	9.86	9.54	9.72	9.90	10.08	10.26	10.44	10.62
6 7	10.80 12.60	10.98 12.78	11.16 12.96	11.84 18.14	11.52 18.32	11.70 18.50	11.88 13.68	12.06 13.86	12.24 14.04	12.42 14.22
8 9	14.40 16.20	14.58 16.38	14.76 16.56	14.94 16.74	15.12 16.92	15. 3 0 17.10	15.48 17.28	15.66 17.46	15.84 17.64	16.02 17.82

XIV. NUMBER OF DEGREES OF REAUMUR == NUMBER OF CENTIGRADE DEGREES.

Degrees		Tenthe of a Degree.									
of Reaum.	0.	1.	2.	8.	4.	5,	6.	7.	8.	9.	
	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	
0	0.00	0.12	0.25	0.87	0.50	0.62	0.75	0.87	1.00	1.12	
1	1.25	1.87	1.50	1.62	1.75	1.87	2.00	2.12	2.25	2.37	
2	2.50	2.62	2.75	2.87	8.00	3.12	8.25	8.37	8.50	8.62	
8	8.75	8.87	4.00	4.12	4-25	4.87	4.50	4.62	4.75	4.87	
4	5.00	5.12	5.25	5.37	5.50	5.62	5.75	5.87	6.00	6.12	
5	6.25	6.87	6.50	6.62	6.75	6.87	7.00	7.12	7.25	7.87	
6	7.50	7.62	7.75	7.87	8.00	8.12	8.25	8.87	8.50	8.62	
7	8.75	8-87	9.00	9.12	9.25	9.87	9.50	9.62	9.75	9.87	
8	10.00	10.12	10.25	10.87	10.50	10.62	10.75	10.87	11.00	11.12	
9	11.25	11.87	11.50	11.62	11.75	11.87	12.00	12.12	12.25	12.37	

XV. NUMBER OF DEGREES OF REAUMUR == NUMBER OF DEGREES OF FAHRENHEIT.

					Tenths of	the of a Degree.								
Degrees of Reaum.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.				
	Pahr.	Fabr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.				
0	0.00	0.22	0.45	0.67	0.90	1.12	1.35	1.57	1.80	2.02				
1	2.25	2.47	2.70	2.92	8.15	3.37	8.60	3.82	4.05	4.27				
2	4.50	4.72	4.95	5.17	5.40	5.62	5.85	6.07	6.80	6.52				
8	6.75	6.97	7.20	7.42	7.65	7.87	8.10	8.82	8.55	8.77				
4	9.00	9.22	9.45	9.67	9.90	10.12	10.85	10.57	10.80	11.02				
. 5	11.25	11.47	11.70	11.92	12.15	12.37	12.60	12.82	18.05	18.27				
6	13.50	13.72	18.95	14.17	14.40	14.62	14.85	15.07	15.80	15.52				
7	15.75	15.97	16.20	16.42	16.65	16.87	17.10	17.32	17.55	17.77				
8	18.00	18.22	18.45	18.67	18.90	19.12	19.35	19.57	19.80	20.02				
9	20.25	20.47	20.70	20.92	21.15	21.87	21.60	21.82	22.05	22,27				

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HYGROMETRICAL TABLES.

HTGROMETERS, or instruments used for determining the amount of aqueous vapor present in the air, are of three classes. In the first, we find the hygrometers based on the absorption of moisture by hygroscopic substances, the best of which is Saussure's Hair-Hygrometer; in the second class, the Psychrometer, or wet-bulb thermometer, which gives the temperature of evaporation; in the third, the various instruments designed for ascertaining the temperature of the dew-point. From the data furnished by each of these instruments, and a table of the elastic forces of vapor at different temperatures, the humidity of the air can be deduced with more or less accuracy.

The use of the hygroscopic substances as hygrometers having been nearly given up on account of the inaccuracy of the results, the variability of the instruments, and the difficulty, if not impossibility, of making them comparable, the psychrometer and the dew-point instruments represent the two methods now usually employed in Meteorology. The following set, therefore, contains extensive tables, in French and English measures, for deducing the hygrometrical condition of the atmosphere from the indications of the Psychrometer and of the dew-point instruments, to which have been added tables of the weight of vapor, in a given space, at different temperatures,—an element often needed in Meteorology.

As, however, the results deduced from the same data furnished by the observations may considerably differ, according to the values of the elastic force of vapor, and the formulæ used in the computation, the tables have been arranged in two series.

The first series contains Regnault's table of the elastic forces of vapor, with tables of the three kinds above mentioned, together with a corresponding set in English measures. Tables V. to X. have been computed for this volume.

The second series gives the table of elastic forces of vapor deduced from Dalton's experiments, and adopted in the Greenwich Observations, together with the various tables based on it.

HYGROMETRICAL TABLES.

A third series of miscellaneous tables furnishes the means of comparing the different values of the elastic force and weight of vapor determined by various physicists, as well as the results of Saussure's Hair-Hygrometer, with those obtained by other methods.

An Appendix, containing tables for comparing the quantity of rain-water indicated in different measures, closes the set.

Though the first series of tables, based on Regnault's table of tensions, is recommended for ordinary use, as being derived from the determinations which seem to deserve the greatest degree of confidence, it was thought expedient to give also the Greenwich tables, which have been, and still are, so extensively used in England, in order to enable meteorologists to judge of the differences which exist between the results obtained by them and those deduced from the constants of Regnault and others.

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FRENCH MEASURES,

BASED ON REGNAULT'S HYGROMETRICAL CONSTANTS.

В



TABLE

OF

THE ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN MILLIMETRES OF MERCURY FOR CENTIGRADE TEMPERATURES, BY REGNAULT.

This table contains the elastic forces of vapor corresponding to every tenth of a degree of temperature between — 35° and + 40° Centigrade, as determined by the experiments of V. Regnault, made by order of the French government, for the purpose of establishing the numerical value of the elements which enter into the computations concerning the steam-engine. These results are generally considered as the most accurate science possesses at present. They are published in the Mémoires de l'Institut, Tom. XXI.; and more correctly in Regnault's Etudes sur l'Hygrométrie, in the Annales de Chimie et de Physique. In Vol. XV. Regnault gives the table of elastic forces for every tenth of a degree from — 10° to + 35° Centigrade, which is reprinted in Table I. The numbers below — 10° and above + 35°, in the same table, have been taken from another table for every full degree, previously published in Vol. XI. p. 333 of the same periodical, and in the same volume of the Mémoires de l'Institut, extending from — 32° to + 230°.

It should be remarked, however, that the numbers below zero, in the two tables just mentioned, having been computed from different formulas of interpolation, slightly disagree. In order to establish a continuity, therefore, the numbers in Table I. corresponding to full degrees from -10° to -35° have been formed by starting from the value due to -10° in the larger table of Regnault, and subtracting from it the difference between -10° and -11° in the other table, in order to find the value of -11° , and so on, by subtracting successively the corresponding differences to -35° . For the fractions of degrees below -10° , the mean values have been adopted as sufficiently accurate for meteorological purposes.

I. ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN MILLIMETRES OF MERCURY FOR CENTIGRADE TEMPERATURES.

BY REGNAULT.

Tempera-					Tenths of	Degrees.				
ture Centigrade.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
•	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
-85	0.221	0.219	0.216	0.214	0.211	0.209	0.207	0.204	0.202	0.199
-84	0.247	0.244	0.242	0.249	0.287	0.284	0.281	0.229	0.226	0.224
-88	0.275	0.272	0.269	0.267	0.264	0.261	0.258	0.255	0.258	0.250
-82	0.805	0.302	0.299	0.296	0.298	0.290	0.287	0.284	0.281	0.278
-81	0.887	0.884	0.831	0.827	0.824	0.321	0.218	0.815	0.811	0.808
-80	0.371	0.368	0.864	0.861	0.857	0.854	0.851	0.847	0.844	0.840
-29	0.409	0.405	0.401	0.898	0.394	0.890	0.886	0.382	0.879	0.375
-28	0.449	0.445	0.441	0.487	0.433	0.429	0.425	0.421	0.417	0.418
-27	0.498	0.489	0.484	0.480	0.475	0.471	0.467	0.462	0.458	0.458
-26	0.540	0.585	0.581	0.526	0.521	0.516	0.512	0.507	0.502	0.498
-25	0.590	0.595	0.580	0.575	0.570	0.565	0.560	0.555	0.550	0.545
-24	0.645	0.639	0.634	0.628	0.623	0.617	0.612	0.606	0.601	0.595
-23	0.704	0.698	0.692	0.686	0.680	0.674	0.669	0.668	0.657	0.651
-22	0.768	0.762	0.755	0.749	0.742	0.786	0.730	0.728	0.717	0.710
-21	0.838	0.831	0.824	0.817	0.810	0.808	0.796	0.789	0.782	0.775
-20	0.912	0.905	0.897	0.890	0.882	0.875	0.868	0.860	0.853	0.845
-19	0.998	0.985	0.977	0.969	0.961	0.952	0.944	0.986	0.928	0.920
-18	1.080	1.071	1.068	1.054	1.045	1.026	1.028	1.019	1.010	1.002
-17	1.174	1.165	1.155	1.146	1.136	1.127	1.118	1.108	1.099	1.069
-16	1.275	1.265	1.255	1.245	1.235	1.224	1.214	1.204	1.194	1.184
-15	1.885	1.874	1.368	1.852	1.841	1.830	1.819	1.808	1.297	1.286
-14	1.503	1:491	1.479	1.468	1.456	1.444	1.482	1.420	1.409	1.897
-18	1.631	1.618	1.605	1.598	1.580	1.567	1.554	1.541	1.529	1.516
-12	1.768	1.754	1.741	1.727	1.718	1.699	1.686	1.672	1.658	1.645
-11	1.918	1.908	1.888	1.878	1.858	1.848	1.828	1.818	1.798	1.788
-10	2.078	2.062	2.046	2.080	2.014	1.998	1.962	1.966	1.950	1.984
- 9	2.261	2.242	2.228	2.204	2.186	2.168	2.150	2.182	2.114	2.096
- 8	2.456	2.486	2.416	2.896	2.876	2.358	2.887	2.818	2.299	2.280
- 7	2.666	2.645	2.624	2.608	2.592	2.561	2.540	2.519	2.498	2.477
- 6	2.890	2.867	2.844	2.821	2.798	2.776	2.754	2.782	2.710	2.688
- 5	8.131	8.106	3.082	8.059	8.084	8.010	2.986	2.962	2.988	2.914
-4	3.387	3.861	3.885	8.809	8.288	8.257	8.281	8.206	3.181	8.156
- 8	8.662	2.634	8.606	8.578	8.550	8.522	8.495	8.468	8.441	8.414
- 2	8.955	3.925	3.895	8.865	3.886	8.807	8.778	8.749	3.720	2.691
-1	4.267	4.285	4.203	4.371	4.140	4.109	4.078	4.047	4.016	3.985
-0	4.600	4.565	4.581	4.497	4 468	4.480	4.897	4.364	4.881	4.299
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

Cantigrale			-		Tenthe of	Degrees.				
Degrees	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
°	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim. 4.801	Millim.	Millim. 4.871	Millim. 4.903
0	4.600	4.633	4.667	4.700	4.788	4.767		4.886		
1	4.940	4.975	5.011	5.047	5.082	5.118	5.155	5.191	5.228	5.265
2 3	5.802 5.687	5.840 5.727	5.878 5.767	5.416 5.807	5.454 5.848	5.491 5.889	5.530 5.930	5.569	5.608 6.014	6.055
	6.097	6.140	6.188	6.226	6.270	6.818	6.857	6.401	6.445	6.490
4 5	6.584	6.580	6.625	6.671	6.717	6.763	6.810	6.857	6.904	6.951
•	0.004	0.000	0.020	0.071	0.717	0.705	0.010	0.007	0.504	0.501
6	6.998	7.047	7.095	7.144	7.198	7.242	7-292	7.842	7.892	7.442
7	7.492	7.544	7.595	7.647	7.699	7.751	7.804	7.857	7.910	7.964
8	8.017	8.072	8.126	8.181	8.236	8.291	8.847	8.404	8.461	8.517
9	8.574	8.632	8.690	8.748	8.807	8.865	8.925	8.985	9.045	9.105
10	9.165	9.227	9.288	9.850	9.412	9.474	9.587	9.601	9.665	9.728
11	9.792	9.857	9.928	9.989	10.054	10.120	10.187	10.255	10.822	10.389
12	10.457	10.526	10.596	10.665	10.734	10.804	10.875	10.947	11.019	11.090
13	11.162	11.235	11.309	11.388	11.456	11.580	11.605	11.681	11.757	11.832
14	11.908	11.986	12.064	12.142	12.220	12.298	12.878	12.458	12.588	12.619
15	2.699	12.781	12.864	12.947	18.029	13.112	18.197	18.281	13.366	18.451
. 10	D 500	10 000	10 710	10 707	18.885	18.972	14.000	14.161	14.041	14.881
16	B.536	18.628	18.710	18.797 14.697			14.062	14.151	14.241	
17	1.421	14.518	14.605		14.790	14.882	14.977	15.072	15.167	15.262
18	14.857	15.454	15.552	15.650	15.747	15.845	15.945	16.045	16.145	16.246
19 20	17391	16.449 17.500	16.552 17.608	16.655 17.717	16.758 17.826	16.861 17.985	16.967	17.078 18.159	17.179 18.271	17.285 18.883
20	11091	17.500	11.000	10.717	17.020	17.550	18.047	10.109	10.2/1	10.000
21	18.95	18.610	18.724	18-839	18.954	19.069	19.187	19.805	19.428	19.541
22	19.69	19.780	19.901	20.022	20.148	20.265	20.889	20.514	20.639	20.763
23	20.88	21.016	21.144	21.272	21.400	21.528	21.659	21.790	21.921	22.053
24	22.184	22.319	22.458	22.588	22.728	22.858	22.996	23.185	28.278	28.411
25	23.55	23.692	23.834	28.976	24.119	24.261	24.406	24.552	24.697	24.842
26	24.988	25.138	25.288	25.488	25.588	25.788	25.891	26.045	26.198	26.851
27	26.505	26.668	26.820	26.978	27.186	27.294	27.455	27.617	27.778	27.939
28	28.101		28.488	28.599	28.765	28.981	29.101	29.271	29.441	29.612
29	29.782	29.956	80.181	30.805	80.479	80.654	80.888	81.011	31.190	81.369
30	81.548	11.729	81.911	82.094	32.278	82.468	82.650	32.837	33.026	83.215
	83.406			00.000						
31	11	3.596	33.787	38.980	84.174	84.868	84.564	34.761	84.959	85.159
32	35.859 37.410	31559 87621	85.760 87.832	35.962 38.045	86.165	86.370	86.576	36.783 38.906	86.991 89.124	37.200
83 - 84	39.565	20186	40.007	40.280	88.258 40.455	88.478 40.680	88.689 40.907		41.864	39.844
35	41.827	42.69	42.293	42.527	42.768	43.000	48.238	41.185	48.717	41.593 43.959
								20.21		20.500
86	44.201	44.45	44.690	14.936	45.188	45.431	45.681	45.932	46.184	46. 187
87	46.691	1	47.208	47.462	47.721	47.981	48.243	48.506	48.770	49.035
88	49.802		49.839	50.110	50.882	50.655	50.929	51.205	51.481	51.759
39	52.039		52.602	52.885	58.170	58.456	58.748	54.082	54.822	54.613
40	54.906	55.200	55.496	55.798	56.091	56.891	56.692	56.994	57.29 8	57.603
	0.	1.	3.	8.	4.	5.	6.	7.	8.	9.

В

GIVING IMMEDIATELY THE FORCE OF AQUEOUS VAPOR AND THE RELATIVE HUMIDITY FROM THE INDICATIONS OF THE PSYCHROMETER.

CALCULATED BY M. T. HAEGHENS.

In his Etudes sur l'Hygrométrie, M. V. Regnault discusses the theoretical bases of the formula of the Psychrometer, given by M. August, which was,

$$x = f - \frac{0.568 (t - t')}{640 - t'} h,$$

in which h represents the height of the barometer; t the temperature of the air given by the dry-bulb thermometer; t' the temperature of the wet-bulb thermometer; f' the force of aqueous vapor in the saturated air at a temperature equal to t'; x the elastic force of aqueous vapor which exists in the air at the time of the observation.

After having modified some of the numerical values, which form the coefficients, M. Regnault adopted this formula,

$$x = f - \frac{0.429 (t-t)}{610-t} h.$$

But comparative experiments, made by himself, showed that by substituting the coefficient 0.480 for that of 0.429, the calculated results, and those obtained by direct observation, agree perfectly in the fractions of saturation, which are greater than 0.40. This formula thus modified, or

$$x = f - \frac{0.480(t-f)}{610-f} h$$

has been used for calculating the following tables. In that part of the tables which supposes the wet-bulb to be covered with a film of ice, or below the freezing point, the value 610 - t', which represents the latent heat of aqueous vapor, has been changed into this: 610 + 79 - t' = 689 - t'.

The only hypothesis made, is that of a mean barometric pressure h, equal to 755 millimetres. If we take into account the causes of errors inherent to the psychrometer, and to the tables of the force of vapor, by means of which the absolute force of vapor is calculated, as well as to the differences of these tensions, taken at temperatures differing only by one tenth of a degree, it will be obvious that he correction due to the variations of barometric pressure can almost always be neglected. Nevertheless, a separate table has been calculated, giving the correction to be applied to the numbers in the Psychrometrical Tables for the heights of the barometer between 650 and 800 millimetres. It will be found at the end of the tables.

The disposition of the tables is the following: —

The temperatures are noted in centigrade degrees; the elaste force of vapor in the air, or its pressure on the barometer, is expressed in millimetes of mercury; the rel-

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^{*} Etudes sur l'Hygrométrie, par M. V. Regnault. Annales de Chimie etde Physique, 3^{me} Série, Tom XV., 1845. B

ative humidity is indicated in per cent. of the full saturation of the air at the corresponding temperature of the dry-bulb thermometer t.

The first vertical column contains the indications of the wet-bulb thermometer t', beginning with the temperatures below the freezing point, when the bulb is covered with ice, from —35°, and continuing from the freezing point up to +35° centigrade, the bulb being simply wet.

The second column gives the differences of the force of vapor for each tenth (0°.1) of a degree, between each full degree of the first column. It enables the observer to find out the correction for any fraction of a degree of the wet-bulb thermometer.

The following double columns give immediately the force of vapor and the relative humidity, corresponding to each degree of the wet-bulb, placed in the first column, on the same horizontal line, and to differences of the two thermometers, or to t-t', taken at every two tenths of a degree.

The horizontal column at the bottom indicates the mean difference, for each tenth of a degree, of the force of vapor contained in the same horizontal line. It gives the correction for the intermediate differences of the thermometers; 0.1, 0.3, 0.5, 0.7, 0.9, &c., &c.

To meet the wants arising from the extreme climate of North America, the tables of Mr. Haeghens have been extended from —15° to —35° centigrade, and from +30° to +35° of temperature of the wet-bulb, and to +40° of temperature of the dry-bulb thermometer. The forces of aqueous vapor of Regnault, as given in Table I., have been used for the calculations.

Use of the Tables.

Enter the tables with the difference of the two thermometers, or t-t', and with the temperature of the wet-bulb thermometer t', taking the first three pages, when the temperature of the wet-bulb is below the freezing point; and the following ones when it is above the freezing point.

Seek first the column at the head of which you find the difference of the thermometers; go down as far as the horizontal line, at the beginning of which you see the temperature of the wet-bulb thermometer; there you find the force of vapor, and the relative humidity corresponding to your observation.

Two corrections for fractions may be required for a complete calculation of the force of vapor; one for the fractions of degrees of the wet-bulb thermometer; another for the intermediate differences of the two thermometers, viz. for 0.1, 0.3, 0.5, 0.7, &c.

The first correction for fractions of degrees of the wet-bulb thermometer is found by multiplying the decimal fraction by the number placed in the second vertical column next to the whole degree, which number is the value of a tenth of a degree. The product must be added to the value of the full degree given in the table, when the temperature of the wet-bulb is above the freezing point: it must be subtracted when the temperature is below the freezing point, and receives the sign —. This correction is too important to be neglected.

The second correction, less important, for the intermediate differences of the ther-B

mometers, which are greater by one tenth than those indicated in the tables, is given in the horizontal column at the bottom of the page. It is constant and always subtractive.

Examples of Calculation.

Difference of thermometers, or t - t'

Temperature of the wet-bulb thermometer, $t' = 11^{\circ}.0$.

We find; page 18, for t-t', fifth double column; and for t', first column,

The force of vapor in the air = $9^{mn}.31$.

Relative humidity,

== 90.

 $= 0^{\circ}.8.$

Difference of thermometers, or t-t', = 7°.2.

Wet-bulb thermometer, or t', = 17°.9.

We find, page 24, for t - t', = 7°.2, and $t' = 17^{\circ}.0$, force of vapor $10^{mm}.02$.

Additive correction for fraction 0°.9, or $9 \times 0.09 = 0$.81.

Force of vapor in the air = 10 .83.

Relative humidity, 46

Difference of thermometers, $t-t'=6^{\circ}.5$.

Wet-bulb thermometer, $t' = 23^{\circ}.6$.

We find, page 23, for $t'=23^{\circ}.0$, and t-t', or difference, = 6°.4, force of vapor $16^{\text{mm}}.94$; applying immediately the correction found at the bottom of the page for one tenth more difference, or 6°.4 $+ 0.1 = 6^{\circ}.5$, we have,

Force of vapor = $16^{nm}.94 - 0.06$, or

16**.88.

Additive correction for fraction 0.6 of the wet-bulb, $6 \times 0.13 = 0$.78.

Force of vapor in the air = 17 .66.

Relative humidity, 56.

The wet-bulb thermometer covered with ice.

Difference of thermometers, $t - t' = 2^{\circ}.8$.

Wet-bulb thermometer (ice), $t' = -8^{\circ}.5$.

Page 17 gives for $t-t'=2^{\circ}.8$, and $t'=-8^{\circ}.0$, force of vapor = 1^{max}.0.

Subtractive correction for fraction 0.5 of wet-bulb, $5 \times 0.019 = -0$.1.

Force of vapor in the air = 0 .9.

Relative humidity, 30.

Below the Freezing-Point; the Bulb covered with a Film of Ice.

						II; 100 B							
Wet-				t -	V, DM	bevance of	Wet an	d Dry Bo	lb The	run den et er	6.		
Bulb Thermo moter	Mean Vertical Differ-	• °,	.0	••	.2	••.	4	●°.	6	۰.	.8	10.	.0
Conti- grade Degrees.	ence for sach 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Role- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rein- tive Hu- mid- ity.
•	Million.	Million.		Million.		Millim.		Millim		Millim.		Millim.	
-35	0.003	0.23	100	0.12	58						ŀ		
-84	0.003	0.25	100	0.15	58	0.06	18	1		1	l		
-88	0.003	0.27	100	0.17	62	0.07	26					l I	
-82	0.003	0.80	100	0.20	66	0.10	88			1	l		i
-3 1		0.84	100	0.24	69	0.14	29	0.03	10		l		
-30	0-004	0.87	100	0.27	71	0.17	44	0.07	17		ł		1
-29	0.004	0.41	100	0.81	74	0.21	46	0.11	25	•	1		
-28	0.004	0.45	100	0.85	76	0.25	58	0.15	81	0.04	9		
-27	0.004	0.49	100	0.89	78	0.29	57	0.19	36	0.09	17		
-26	0-005	0.54	100	0.44	80	0.84	60	0.24	41	0.18	28	0.08	6
į	0.004	l	j		ŀ						Ì		l
-25	0.005	0.59	100	0.49	81	0.39	68	0.29	46	0.18	29	0.08	12
-24	0.006	0.64	100	0.54	82	0.44	66	0.84	50	0.24	84	0.14	19
-23	6.006	0.70	100	0.60	84	0.50	69	0.40	58	0.80	89	0.19	25
-22	0.007	0.77	100	0.67	85	0.56	71	0.46	57	0.86	44	0.26	81
-21		0.84	100	0.74	86	0.68	78	0.58	60	0.48	48	0.88	86
	0.008												
-20	0.006	0.91	100	0.81	87	0.71	75	0.61	68	0.50	51	0.40	40
-19	0.006	0.99	100	0.89	88 89	0.79	77	0.69	66 68	0.58	55 58	0.48	45 48
-18 -17	0.009	1.08	100	0.98	90	0.87	78 80	0.87	70	0.67 0.76	61	0.66	52
-16	0-010	1.27	100	1.17	90	1.07	81	1.97	72	0.86	62	0.76	55
-10	0.011	1.2	100	1 ****	50	1.07		1.01	••	0.00	-	1 ****	""
-15		1.38	100	1.28	91	1.18	82	1.08	74	0.97	66	0.87	58
-14	0.012	1.50	100	1.40	92	1.80	88	1.19	76	1.00	68	0.99	61
-13	0.018	1.63	100	1.58	92	1.42	84	1.82	77	1.22	70	1.11	63
-12	0.014	1.77	100	1.66	98	1.56	85	1.46	78	1.85	71	1.25	65
-11	0.015	1.92	100	1.81	98	1.71	86	1.61	80	1.50	78	1.40	67
	0.016		Į			l	i			1		_	
-10		2.08	100	1.97	94	1.87	87	1.77	81	1.66	75	1.56	69
- 9	0.019	2.26	100	2.16	94	2.05	88	1.95	82	1.85	76	1.74	71
- 8	0.021	2-46	100	2.85	94	2.25	89	2.14	88	2.04	78	1.94	78
- 7	0.034	2.67	100	2.56	94	2.46	89	2.85	84	2.25	79	2.15	74
- 6		2.89	100	2.79	95	2.68	90	2.58	85	2.47	80	2.87	76
	0.095	. 10	100		O.E.		60	0.00	94	9 77	81	2.61	77
- 5 - 4	0.026	3.13 3.89	100	3.08 3.26	95 95	2.92 3.18	90 91	2.82 3.07	86 87	2.71	82	2.86	78
- 8	0.029	3.66	100	8.56	96	8.45	92	8.35	87	8.24	88	8.14	79
- 2	0.031	8.96	100	8.85	96	8.75	92	8.64	88	3.54	84	8.48	80
- 1	0.033	4.27	100	4.16	96	4.06	92	3.95	89	8.85	85	3.74	81
- ō	0.034	4.60	100	4.50	96	4.40	98	4.29	89	4.19	86	4.08	82
	<u>'</u>	•	·	'									
1		Mon	a Horis	ontal Diff	Manco (of Farce o	₹ Vapor	tos esop	0 °.1 —	0.05 mm.	•		

Below the Freezing-Point; the Built covered with a Elim of Ros.

				t-	- ¢', Dt	Bernes o	(Wet a	nd Dry B	ulb Th	rmomete	cs.		
Wet- Bulb Thermo- meter,	Mean Vertical Differ-	10	.2	10.	4	10	.6	10	.8	20.	.0	20	.9
Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Rein- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Reia- tive Hu- mid- ity.	Force of Vapor.	Reia- tive Hu- mid- ity.	Porce of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Bela- tive Hu- mid- ity.
-35 -34	Millim.	Millim.											
-88				1								1	
-82		1 1		1 1				l				1	
-31													
-80													
-29				1				1 1					
-28				į			i					1	
-27				1		l i		1	1			1	
-26													
-25													
-24		0.04	5	1				1 1		1 1			
-23	0.066	0.09	12	1		l l							
-22	0.006	0.16	18	0.05	6	l i				1	1		
-21		0.28	24	0.12	18	i							
-20	0.007	0.80	80	0.20	18	0.09		Ì	1				
-19	0.008	0.88	24	0.28	25	0.05	9 15	0.07	6	1			
-18	0.008	0.46	39	0.26	80	0.26	21	0.16	18	0.05	4		
-17	0.009	0.56	48	0.46	85	0.35	26	0.25	18	0.15	11	0.04	8
-16	0.010	0.66	47	0.56	39	0.45	81	0.85	24	0.25	16	0.14	9
	0.011	!											
-15	0.013	0.77	50	0.66	48	0.56	86	0.46	29	0.86	22	0.25	15
-14 -13	0.018	0.88	58	0.78	46 50	0.68	40	0.58	88	0.47	27	0.87	21 25
-13	0.015	1.01	56 59	0.91 1.04	58	0.80	48 47	0.70	87 41	0.60	81 85	0.63	20
-11	0.017	1.80	61	1.19	55	1.09	50	0.99	44	0.73	89	0.78	34
	0.018					30		1.50					
-10	0.019	1.46	63	1.85	58	1.25	52	1.15	47	1.04	42	0.94	88
- 9	0.010	1.64	66	1.58	61	1.48	56	1.88	51	1.22	46	1.12	41
- 8	0.033	1.83	68	1.78	68	1.62	58	1.52	54	1.42	49	1.31	45
-7	0.024	2.04	69	1.94	65	1.83	61	1.78	56	1.68	52	1.52	48 51
- 6	0.025	2.26	71	2.16	67	2.06	68	1.95	59	1.85	55	1.74	01
- 5		2.50	78	2.40	69	2.80	65	2.19	61	2.09	57	1.98	58
- 4	0.028	2.76	74	2.65	70	2.55	67	2.45	63	2.84	59	2.24	55
- 8	0.039	3.03	75	2.98	72	2.82	68	2.72	65	2.61	61	2.51	58
- 2	0.030	8.83	77	8.22	78	8.12	70	8.01	66	2.91	63	2.80	60
- 1	0.031	8.64	78	8.58	75	8.43	71	3.32	68	8.22	65	3.11	62
		1											
		Mean	Horiso	ntal Diffe	sence of	Torce of	Vanor	for each (%1= ().05 mm.			

Mean Horisontal Difference of Force of Vapor for each $0^{\circ}.1 = 0.05$ mm.

Below the Freezing-Point; the Bulb covered with a Film of Ice.

Wet-				6-	- t', Dif	isrence of	Wet a	ad Dry B	alb The	rmomete	n.		
Bulb Thermo- meter t Centi-	Mean Vertical Differ- ence for	20	.4	80	.6	90	.8	80	.0	80	.9	80	.4
grade Degrees.	each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- tty.	Force of Vapor.	Rein- tive Hu- mid- ity.	Force of Vapor.	Rein- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
•	Million.	Millim.		Million.		Million,		Millim.		Millim.		Millim,	
-15	0.011	0.15	9	0.05	8					ł			1
-14 -13	0.013	0.27	15	0.16	9	0.06	4						
-12	0.018	0.29	20	0.29	14 19	0.19	9	0.08	10	0.11	5	l	
-11	0.016	0.68	29	0.42	24	0.47	19	0.86	15	0.26	10	0.16	6
	0.016	10.00	-	3.31				3				3.25	"
-10		0.88	33	0.78	28	0.68	24	0.52	20	0.42	16	0.82	12
- 9	0.018	1.02	87	0.91	38	0.81	28	0.70	24	0.60	20	0.50	17
- 8	0.019	1.21	40	1.10	36	1.00	82	0.90	28	C.79	25	0.69	21
- 7	0.023	1.42	44	1.81	40	1.21	26	1.11	32	1.00	29	0.90	26
- 6		1.64	47	1.54	48	1.48	40	1.88	36	1.22	33	1.12	30
- 5	0.034	1.88	50	1.77	46	1.67	48	1 22	40		36	1 02	88
- 4	0.025	2.18	52	2.08	49	1.92	46	1.57	48	1.46	40	1.86 1.61	87
- 8	0.027	2.40	55	2.80	52	2.19	48	2.09	45	1.99	48	1.88	40
- 2	0.029	2.70	57	2.59	54	2.49	51	2.88	48	2.28	46	2.17	48
- 1	0.031	8.01	59	2.90	56	2.80	54	2.69	51	2.59	48	2.48	46
				1								- 1	
1 1										1	l į		
	.	80.	.6	80.	8	40.	•	40	.9	40.	.4	40.	6
		Millim.		Millim.		Millim.		Millim.	· 	Milim.		Millim.	
-15		Ì											
-14													
-13													
-12													
-11		0.05	2										
-10	0.016		_		-								
-10 - 9	0.018	0.21 0.89	8 18	0.11	4	0.19	6	0.08					
- 8	0.019	0.58	18	0.48	14	0.19	ni l	0.05	8	0.17	5	0.06	2
- 7	0.021	0.79	22	0.69	19	0.59	16	0.48	18	0.88	10	0.27	7
- 6	0.012	1.01	26	0.91	28	0.81	20	0.70	17	0.60	15	0.49	12
	0.024		l		- 1	.							1
- 5	0.025	1.25	30	1.15	27	1.04	24	0.94	22	0.88	19	0.73	16
- 4	0.027	1.50	84	1.40	31	1.80	28	1.19	26	1.09	28	0.98	20
- 8	0.029	1.78	87	1.67	84	1.57	82	1.46	29	1.36	27	1.25	24
- 2	0.031	2.07	40	1.96	87	1.86	85	1.75	83	1.65	80	1.54	28
-1	<u>i</u>	2.38	43	2.27	40	2.17	88	2.06	36	1.96	84	1.85	81
		Mean	Horist	ental Diffe	TRIDOS 00	Tores of	(Vapor	for each	0°.1 — (0.05 mm.			

				t-t	, Diste	rence of \	Wet an	d Dry-Bu	lb The	rmometer	L.		
Wet- Bulb Thermo- meter.	Mean Vertical Differ-	•	.0	• •.	.2	●.	4	●°.	6	••.	8	1%	•
Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rola- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
-	Millim.	Millim.		Millim.	_	Millim		Millim.		Millim.		Millim.	
Ō	0.03	4.60	100	4.48	96	4.86	92	4.24	88	4.12	85	4.01	81
1	0.04	4.94	100	4.82	96	4.70	93	4.58	89	4.46	85	4.85	82
2	0.04	5.80	100	5.18	96	5:06	98	4.94	89	4.88	86	4.71 5.09	88 83
3	0.04	5.69	100	5.57	97	5.45	93	5.88	90	5.21 5.62	87 87	5.50	84
4	0.04	6.10	100	5.98	97	5.86	98	6.74	91	6.05	88	5.94	85
5		6-58	100	6.41	97	6.29	94	6.17	81	0.00	60	0.84	- 00
_	0.05		100	6.88	97	6.76	94	6.64	91	6.52	88	6.40	85
6	0.05	7.00	100		97	7.25	94	7.18	91	7.01	89	6.89	86
7 8	0.05	7.49 8.02	100	7.87	97	7.78	94	7.66	92	7.54	89	7.42	86
9	0.06	8.57	100	8.45	97	8.33	95	8.21	92	8.09	89	7.97	86
10	0.06	9.17	100	9.04	97	8.92	95	8.80	98	8.68	90	8.56	87
10	0.06	9.17	100	5.04		0.52	00	0.00	-	3.00		5.50	
11	0.00	9.79	100	9.67	97	9.55	95	9.48	92	9.81	90	9.19	88
12	0.07	10.46	100	10.34	98	10.21	95	10.09	93	9.97	90	9.85	88
13	0.07	11.16	100	11.04	98	10.92	95	10.80	98	10.68	91	10.56	89
14	0.07	11.91	100	11.79	98	11.66	95	11.54	93	11.42	91	11.80	89
15	0.08	12.70	100	12.58	98	12.46	96	12.38	98	12.21	91	12.09	89
	0.08							1	1		1		
16		13.54	100	13.41	98	18.29	96	18.17	94	13.05	92	12.98	90
17	0.09	14.42	100	14.80	98	14.18	96	14.05	94	13.93	92	13.81	90
18	0.09	15,36	100	15.23	98	15.11	96	14.99	94	14.87	92	14.75	90
19	0.10	16.35	100	16.22	98	16.10	96	15.98	94	15.86	92	15.78	91
20	0.10	17.89	100	17.27	98	17.15	96	17.02	94	16.90	92	16.78	91
	0.11	ŀ		1	1		ļ	l					ĺ
21		18.50	100	18.37	98	18.25	96	18.18	94	18.00	92	17.88	91
22	0.12	19.66	100	19.54	98	19.41	96	19.29	95	19.17	98	19.04	91
28	0.18	20.89	100	20.76	98	20.64	96	20.52	95	20.89	93	20.27	91
24	0.14	22.18	100	22.06	98	21.94	97	21.81	95	21.69	93	21.57	92
25	0.14	28.55	100	28.48	98	28.80	97	23.18	95	23.05	98	22.93	92
	0.14	l .		1									
26	0.15	24.99	100	24.86	98	24.74	97	24.62	95	24.49	98	24.37	92
27	0.16	26.51	100	26.38	98	26.26	97	26.13	95	26.01	98	25.88	92
28	0.17	28.10	100	27.98	98	27.85	97	27.78	95	27.60	98	27.48	92
29	0.18	29.78	100	29.66	98	29.58	97	29.41	95	29.28	94	29.16	92
80		81.55	100	31.42	98	31.80	97	31.17	95	80.05	94	30.92	93
	0.19								00	82.90	94	32.78	93
81	0.20	88-40	100	33.28	98	88.15	97	83.08	96	84.86	94	34.78	93
82	0.21	85.86	100	35.28	99	85.11	97 98	34.98	96 96	86.91	94	86.78	98
83	0.23	87.41	100	37.28	99	87.16	98	37.08 39.18	96	89.06	94	38.93	93
34	0.23	89.56	100	89.43	99	39.81	98	41.45	96	41.38	95	41.20	93
85		41.88	100	41.70	שש	41.58	1 20	21.50	30	41.00	80	71.20	

Mean Horizontal Difference of Force of Vapor for each 0°.1 = 0.08 mm.

				t-t	, Dist	rence of 1	Not an	d Dry-Bu	lb The	rmometen			
Wet- Bulb Thermo- meter.	Mean Vertical Differ	1°	.9	1°.	4	10.	6	1%	.8	\$°.	0	3°.	9
Canti- grade Degrees	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rein- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Reia- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.	_	Millim.	_
0	0.03	3.89	78	8.77	74	3.65	71	8.58	67	8.41	64	8.29	61
1	0.04	4.23	79	4.11	75	8.99	72	3.87	69	8.75	66	8.63	68
2	0.04	4.59	80	4.47	76	4.35	73	4.28	70	4.11	67 69	3.99 4.87	65 66
8	0.04	4.97 5.38	80 81	5.26	78	4.78 5.14	74 75	5.02	71 78	4.49	70	4.78	67
5	0.04	5.82	82	5.70	79	5.58	77	5.46	74	5.84	71	5.22	69
-	0.05	"""	32	****	"	J.05		5.30	""	J.01			-
6		6.28	83	6.16	80	6.04	77	5.92	75	5.80	72	5.68	70
7	0.05	6.77	83	6.65	81	6.58	78	6.41	76	6.29	78	6.17	71
8	0.05	7.29	84	7.17	81	7.05	79	6.98	76	6.81	74	6.69	72
9	0.06	7.85	84	7.73	82	7.61	80	7.49	77	7.87	75	7.25	73
10	0.00	8.44	85	8.32	88	8.20	80	8.08	78	7.96	76	7.84	74
	0.06	1		l					Ì				İ
11	0.07	9.07	86	8.95	83	8.82	81	8.70	79	8.58	77	8.46	75
12	0.07	9.73	86	9.61	84	9.49	82	9.37	80	9.25	78	9.12	76
13	0.08	10.43	86	10.81	84	10.19	82	10.07	80	9.95	78	9.88	76
14	0.08	11.18	87	11.06	85	10.94	88	10.81	81	10.69	79	10.57	77
15	0.08	11.97	87	11.85	85	11.73	83	11.60	81	11.48	80	11.86	78
16	0.05	12.80	88	12.68	86	12.56	84	12.44	82	12.32	80	12.19	78
17	0.09	18.69	88	13.57	86	13.44	84	18.82	88	18.20	81	13.06	79
18	0.09	14.62	88	14.50	87	14.38	85	14.26	83	14.13	81	14.01	80
19	0.10	15.61	89	15.49	87	15.37	85	15.24	83	15.12	82	15.00	80
20	0.11	16.65	89	16.53	87	16.41	86	16.29	84	16.16	82	16.04	81
	0.11							l				1	
21	0.12	17.76	89	17.63	88	17.51	86	17.39	84	17.27	88	17.14	81
22	0.12	18.92	90	18.80	88	18.67	86	18.55	85	18.43	83	18.30	82
23	0.13	20-15	90	20.02	88	19.90	87	19.78	85	19.65	83	19.58	82
24	0.14	21.44	90	21.32	88	21.20	87	21.07	85	20.95	84	20.82	82
25		22.81	90	22.68	89	22.56	87	22.44	86	22.31	84	22.19	83
	0.14	04.07	00	94.10	89	99 00	0~	99 0*	90	99 ~=	85	00.00	-
26 27	0.15	24.24	90 91	24.12 25-63	89	23.99 23.51	87 88	23.87 25.39	86 86	23.75 25.26	85	28.62 25.14	83 83
28	0.16	25.76 27.35	91	27.28	89	27.10	88	26.98	87	26.86	85	26.73	84
28 29	0.17	29.03	91	28.91	90	28.78	88	28.66	87	28.58	85	28.41	84
30	0.18	80.80	91	30.67	90	30.53	89	80.42	87	30.30	86	30.17	84
	0.19				-					22.20			
31		32.65	91	32.53	90	32.40	89	32.28	87	32.15	86	82.08	85
32	0.20	34.61	91	34.48	90	84.36	89	34.28	88	84.11	86	33.98	85
33	0.21	36.66	92	36.58	90	36.41	89	36.28	88	36.16	86	36.03	85
34	0.23	38.81	92	38.68	90	38.56	89	38.48	88	38.31	87	38.18	85
35	0.20	41.07	92	40.94	91	40.82	89	40.69	88	40.57	87	40.44	86
		Moun	Horizont	al Differe	nce of	Force of	Vapor	for each (۳.1 =	0.06 mm-			

В

		•		t-t	, Disse	rence of	Wet an	d Dry-Bu	ib The	rmometer	L.		
Wet- Bulb Thermo- meter.	Mean Vertical Differ-	2	.4	2°.	6	20.	8	8°.	.0	8°.	2	80,	4
Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Reia- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
•	Millim.	Millim.		Millim.	_	Millim.	_	Millim.		Millim.		Millim.	
0	0.03	3.17	88	3.06	55	2.94	52	2.82	50	2.70	47	2.58	44
1	0.04	8.51	60	3.39	57	8.27	54	8.16	52	8.04	49	2.92	47
2	0.04	8.87	62	3.75	59	8.63	56	8.51	54	2.39	51	3.28	49
8	0.04	4.25	68 65	4.18	61 62	4.02	58 60	3.90 4.30	56 57	3.78 4.18	58	8.66	51
4 5	0.04	1.00	66	4.54	64	4.42		4.74		4.62	55 57	4.06	58
•		5.10	00	4.98	04	4.86	61	4.74	59	4.02	D/	4.50	55
6	0.05	5.56	67	5.44	65	5.32	63	5.20	61	5.08	58	4.96	56
7	0.05	6.05	69	5.93	66	5.81	64	5.69	62	5.57	60	5.45	58
8	0.05	6.57	70	6.45	68	6.33	65	6.21	68	6.09	61	5.97	59
9	0.06	7.18	71	7.01	69	6.89	67	6.77	65	6.64	63	6.52	61
10	0.06	7.72	72	7.59	70	7.47	68	7.35	66	7.28	64	7.11	62
	0.06					1							
11	0.00	8.84	73	8.22	71	8.10	69	7.98	67	7.86	65	7.74	63
12	0.07 0.07	9.00	74	8.88	72	8.76	70	8.64	68	8.52	66	8.40	64
18	0.07	9.71	75	9.58	73	9.46	71	9.34	69	9.22	67	9.10	66
14	0.08	10.45	75	10.38	73	10.21	72	10.08	70	9.96	68	9.84	67
15		11.24	76	11.12	74	10.99	72	10.87	71	10.75	69	10.63	67
	0.08												
16	0.09	12.07	77	11.95	75	11.83	78	11.71	72	11.58	70	11.46	68
17 18	0.09	12.95 13.89	77 78	12.83 13.77	76	12.71	74 75	12.59	72 73	12.47 13.40	71 72	12.34 13.28	69 70
19	0.10	14.87	78	14.75	76 77	13.64 14.63	75	13.52 14.51	74	14.38	72	14.26	70
20	0.10	15.92	79	15.79	77	15.67	76	15.55	74	15.43	73	15.30	72
20	0.11	10.02		20.75	••	15.07	10	10.00		10.40		10.00	
21		17.02	80	16.90	78	16.77	77	16.65	75	16.53	74	16.40	72
22	0.12	18.18	80	18.06	79	17.93	77	17.81	76	17.69	74	17.56	78
23	0.12	19.41	80	19.28	79	19.16	78	19.04	76	18.91	75	18.79	73
24	0.13 0414	20.70	81	20.58	79	20.45	78	20.88	77	20.21	75	20.08	74
25	0814	22.06	81	21.94	80	21.82	79	21.69	77	21.57	76	21.45	75
	0.14												
26	0.15	23.50	82	28.37	80	28.25	79	23.18	78	28.00	77	22.88	75
27	0.16	25.01	82	24.89	81	24.76	79	24.64	78	24.51	77	24.39	76
2 8	0.17	26.61	83	26.48	81	26.86	80	26.23	79	26.11	77	25.98	76
29	0.18	28.28	83	28.16	81	28.03	80	27.91	79	27.69	77	27.76	76
30	ا میں ا	30.05	83	29.92	82	29.80	81	29.67	79	29.55	78	29.42	77
31	0.19	31.90	83	31.78	82	31.65	81	31.58	80	31.40	78	31.28	77
32	0.20	33.86	84	31.78	82 82	33.61	81	33.48	80	33.36	78	33.23	78
33	0.21	35.90	84	35.77	88	35.65	81	35.52	80	35.40	79	35.27	78
34	0.22	38.06	84	37.98	83	87.81	82	37.68	81	87.56	80	37.43	78
85	0.23	40.31	84	40.18	83	40.06	82	39.93	81	39.81	80	39.68	79
		20.01		20.20		10.00	~~	30.00		20.02		22.00	

Mean Horizontal Difference of Force of Vapor for each $0^{\circ}.1 = 0.06$ mm.

.				t-t	, Dice	rence of '	Wet an	d Dry-Ba	lb The	rmometen	١.		
Wet- Bulb Thermo- meter.	Mean Vertical Differ-	*	.6	8°.	8	4 °.	•	40.	.9	4 °.	4	4 °.	6
Centi- grade Degress.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Reia- tive Hu- mid- ity.	Force of Vapor.	Rein- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Reia tive Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.	_	Millim.	
0	0.03	2.46	41	2.84	39	2.22	36	2.11	84	1.99	82	1.87	29
1	0.04	2.80	44	2.68	42	2.56	39	2.44	37	2.32	35	2.20	82
2	0.04	8.16	46	8.04	44	2.92	42	2.80	89	2.68	87	2.56	85
3	0.04	8.54	49	8.42	46	3.30	44	3.18	42	8.06	40	2.94	89
4	0.04	8.94	51	3.82	48	3.71	46	8.59	44	8.47	42	8.35	40
5		4.88	52	4.26	50	4.14	48	4.02	46	8.90	44	8.78	42
6	0.05	4.84	87	4.72	52	4.00	EV	4 40	48	4.36	46	4.24	44
7	0.05	5.83	54 56	5.21	54	4.60 5.09	50 52	4.48	50	4.85	48	4.78	46
8	0.05	5.85	57	5.78	56	5.61	54	5.49	52	5.87	50	5.25	48
9	0.06	6.40	59	6.28	57	6.16	55	6.04	58	5.92	52	5.80	50
10	0.06	6.99	60	6.87	58	6.75	57	6.63	55	6.51	58	6.39	52
	0.06	0.00	~	0.07		0.75	٠.	0.00	"	0.51	-	0.00	02
11		7.61	61	7.49	60	7.87	58	7.25	56	7.13	55	7.01	53
12	0.07	8.28	62	8.15	61	8.03	59	7.91	58	7.79	56	7.67	55
13	0.07	8.98	64	8.85	63	8.78	61	8.61	59	8.49	57	8.37	56
14	0.07	9.72	65	9.60	63	9.48	62	9.35	60	9.23	59	9.11	57
15	0.08	10.51	66	10.38	64	10.26	68	10.14	61	10.02	60	9.90	58
	0.08											1	
16		11.84	67	11.22	65	11.10	64	10.97	62	10-85	61	10.73	59
17	0.09	12.22	68	12.10	67	11.98	65	11.85	68	11.73	62	11.61	61
18	0.10	13.15	69	13.03	67	12.91	66	12.79	64	12-66	63	12.54	62
19	0.11	14-14	69	14.02	6 8	13.89	66	13.77	65	13-65	64	13.58	62
20	0.11	15.18	70	15.06	69	14.94	67	14.81	66	14-69	65	14.57	63
	0.11					ł		1	1				
21	0.12	16.28	71	16.16	69	16.04	68	15.91	67	15.79	65	15.67	64
22	0.12	17.44	71	17.32	70	17.20	69	17.07	67	16.95	66	16.88	65
23	0.13	18.67	72	18.54	71	18.42	69	18.30	68	18-17	67	18.05	66
24	0.14	19.96	73	19.84	71	19.71	70	19.59	69	19-46	68	19.84	66
25		21.32	78	21.20	72	21.07	71	20.95	70	20-83	68	20.70	67
••	0.14	00.07		80.00				00.00		88.00		00.15	cc
26 27	0.15	22.75	74	22.63	78	22.50	71	22.38	70	22.26	69 70	22.18	68
28	0.16	24.27	74	24.14	78	24.02	72	28.89	71	23.77 25.36	70	23.64 25.24	68 69
29	0.17	25.86 27.44	75 75	25-73 27-81	74	25.61 27.29	72	25.48 27.16	71	27.04	70	26.91	70
30	0.18		-							23.80		28.67	~~
-0	0.19	29.80	76	29.17	75	29.05	78	28.92	72	20.00	71	20.07	70
81		31.15	76	31.03	75	80.90	74	80.78	78	30.65	72	30.58	71
82	0.20	33.10	77	82.97	76	32.85	75	82.72	78	32.60	72	32.47	71
83	0.21	35.15	77	35.02	76	34.90	75	84.77	74	34.65	73	34.52	72
84	0.22	37.30	77	37.17	76	37.05	75	36.92	74	36.80	78	36.67	72
35	0.23	39.56	78	39.48	77	39.31	76	39.18	74	39.06	73	38.98	72
	<u>'</u>				<u> </u>		<u> </u>		لــــــــــــــــــــــــــــــــــــــ			·	

B

				t-t	, Diffi	rence of \	Wet an	d Dry-Bu	lb The	rmometer	B.	-	
Wet- Bulb Thermo- meter.	Mean Vertical Differ	4°	.8	5°.	•	5°.	9	5°.	4	5 °.	6	5°.	8
Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rein- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
	25:01-			Millim.		Millim.		Millim.		Millim.		Millim.	
ô	Millim.	Millim. 1.75	27	1.63	25	1.51	28	1.39	21	1.27	19	1.15	17
1	0.03	2.08	30	1.97	28	1.85	26	1.78	24	1.61	22	1.49	20
2	0.04	2.44	38	2.32	81	2.20	29	2.08	27	1.96	25	1.85	23
8	0.04	2.82	36	2.70	84	2.58	82	2.46	30	2.84	28	2.22	26
4	0.04	8.28	38	8.11	86	2.99	34	2.87	33	2.75	31	2.63	29
5		8.66	40	8.54	39	3.42	87	3.30	85	3.18	33	8.06	82
اما	0.05	4 10	70	4.00	41	8.88	39	8.76	87	8.64	86	3.52	84
6	0.05	4.12 4.61	48 45	4.49	48	4.37	41	4.25	40	4.18	88	4.01	86
8	0.05	5.13	47	5.01	45	4.89	43	4.77	42	4.65	40	4.58	89
9	0.06	5.68	48	5.56	47	5.44	45	5.32	44	5.20	42	5.08	41
10	0.08	6.27	50	6.15	48	6.02	47	5.90	45	5.78	44	5.66	42
	0.06			l	İ	1					1		1
11		6.89	52	6.77	50	6.65	49	6.58	47	6.40	46	6.28	44
. 12	0.07	7.55	58	7.48	52	7.81	50	7.18	49	7.06	47	6.94	46
18	0.07	8.25	55	8.13	58	8.01	52	7.88	50	7.76	49	7.64	47
14	0.08	8.99	56	8.87	54	8.75	58	8.62	51	8.50	50	8.88	49
15		9.78	57	9.65	55	9.58	54	9.41	53	9.29	51	9.17	50
	0.08					10.00		10.04		10.12	53	10.00	51
16	0.09	10.61	58 59	10.49 11.87	57 58	10.86 11.24	55 56	10.24 11.12	55	11.00	54	10.88	58
17 18	0.09	11.49 12.42	60	12.80	59	12.17	58	12.05	56	11.98	55	11.81	54
19	0.10	18.40	61	13.28	60	18.16	59	18.04	57	12.91	56	12.79	55
20	0.11	14.44	62	14.82	61	14.20	60	14.08	58	18.95	57	13.88	56
	0.11								-				
21	0.10	15.54	63	15.42	62	15.30	60	15.17	59	15.05	58	14.93	57
22	0.12	16.70	64	16.58	68	16.46	61	16.83	60	16.21	59	16.09	58
28	0.12	17.93	65	17.80	63	17.68	62	17.56	61	17.48	60	17.81	69
24	0.14	19.22	65	19.09	64	18.97	68	18.85	62	18.72	61	18.60	60
25		20.58	66	20.46	65	20.33	64	20.21	68	20-08	62	19.96	60
	0.14	00 A-	09	01 00	65	21.76	64	21.63	63	21.51	62	21.89	61
26 27	0.15	22.01 23.52	67 67	21.88 28.40	66	28.27	65	23.15	64	23.02	68	22.90	62
28	0.16	25.02	68	24.99	67	24.86	66	24.74	65	24.61	64	24.49	68
29	0.17	26.79	68	26.66	67	26.54	66	26.41	65	26.29	64	26.16	63
80	0.18	28.55	69	28.42	68	28.80	67	28.17	66	28.05	65	27.92	64
-	0.19										1		1
81	0.20	80.40	70	30.28	69	80.15	68	80.08	67	29.90	66	29.78	65
82	0.20	82.85	70	82.22	69	32. 10	68	31.97	67	31.85	66	81.72	65
88	0.22	84.40	71	34.27	70	84.15	69	84.02	68	83.90	67	83.77	66
84	0.23	36.55	71	86.42	70	86.30	69	86.17	68	86.05	67	85.92	66
85		38.80	71	88.68	70	<u> </u>	L	L	l	L	<u> </u>	<u> </u>	<u> </u>
		Moan	Horizont	al Differe	nce of	Force of	Vapor	for each (r.1 =	0.06 mm.			

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Wet				t-1	, Diffi	rence of	Wol as	d Dry-Bo	lb The	rmometer	s .		
Bulb Thermo- meter.	Mean Vertical Differ-	6	.0	●.	.9	6°.	4	€°.	6	€°.	8	70.	.0
Centi- grade Degress.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rein- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
٥	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	
0	0.03	1.04	15	0.92	13	0.80	11	0.68	9	0.56	8	0.44	6
1	0.04	1.37	18	1.25	16	1.18	15	1.01	13	0.89	11	0.78	10
2	0.04	1.78	22	1.61	20	1.49	18	1.87	16	1.25	15	1.18	18
3	0.04	2.11	25	1.99	28	1.87	21	1.75	19	1.63	18	1.51	16
5	0.04	2.51	28	2.89	26	2.27	24	2.15	28	2.03	21	1.91	19
9	0.05	2.94	30	2-82	28	2.70	27	2.58	25	2.46	24	2.34	22
6	1	8.40	33	3.28	31	2.16	29	8.04	28	2.92	26	2.80	25
7	0.05	8.89	25	3.77	88	8.65	82	3.58	30	8.41	29	3.29	28
8	0.05	4.41	87	4.28	85	4.16	84	4.04	88	8.92	81	8.80	80
9	0.08	4.96	29	4.84	38	4.71	86	4.59	85	4-47	83	4.35	82
10	0.06	5-54	41	5.42	40	5.20	88	5.18	87	5.06	85	4.94	84
	0.06								I	1			
11	0.07	6.16	48	6.04	41	5.92	40	5.80	39	5.68	87	5.56	86
12	0.07	6.82	44	6.70	48	6.58	42	6.46	41	6.84	89	6.22	88
13	0.07	7.52	46	7.40	45	7.28	48	7.16	42	7.08	41	6.91	40
14	0.08	8.26	47	8.14	46	8.02	45	7.90	44	7.77	48	7.65	41
15		9.06	49	8.92	48	8.80	46	8.68	45	8.56	44	8.44	43
	0.08								_				
16 17	0.09	9-88	50	9.75	49	9.68	48	9.51	47	9.89	45	9.27	44
18	0.09	10.76	52	10.63	50	10.51	49	10.89	48 49	10.27 11.20	47 48	10.14	46 47
19	0.10	11.69 12.67	58 54	11.56 12.55	51 58	11.44 12.42	50 51	11.32	50	12.18	49	12.06	48
20	0.11	18.71	55	13.58	54	18.46	52	18.84	52	18.22	50	13.09	49
	0.11	20.11	~	10.00	-	10.10	~	10.01	-	10.22	"	10.00	
21		14.81	56	14-68	55	14.56	54	14.44	58	14.81	52	14.19	51
22	0.19	15.96	57	15.84	56	15.72	55	15.59	54	15.47	58	15.85	52
23	0.12 0.13	17.19	58	17.06	57	16.94	56	16.82	55	16.69	54	16.57	53
24	0.14	18.48	59	18.85	58	18.23	56	18.11	55	17.98	54	17.86	58
25	`	19.84	59	19.71	58	19.59	57	19.46	56	19.84	55	19-22	54
1	0.14		ľ	1	٠ ا	1		- 1	1	i	ı	i	
26	0.15	21.26	60	21.14	59	21.01	58	20.89	57	20.77	56	20.64	55
27	0.16	22.77	61	22.65	60	22.52	59	22.40	58	22.28	57	22.15	56
28	0.17	24.86	62	24.24	61	24.11	60	28.99	59	23.86	58	28.74	57
29	0.18	26.04	62	25.91	61	25.79	60	25.66	59	25.54	58	25.41	57
~	0.19	27.80	68	27.67	62	27.55	61	27.42	60	27.30	59	27.17	58
81		29.65	61	29.53	63	29.40	62	29.28	61	29.15	60	29.03	69
82	0.90	31.59	61	31.47	68	81.34	62	31.22	61	29.10	60	30.97	59
23	0.21	33.64	65	83.51	64	28.39	63	33.26	62	83.14	61	88.01	.60
84		-5.0%		30.01		30.05	~	30020				30.01	
25	ı	l			- 1	ŀ	- 1	1	I	- 1			

Mean Horizontal Difference of Force of Vapor for each $0^{\circ}.1 = 0.06$ mm.

				t -1	r, Dist	erence of	Wet a	nd Dry-Ba	ılb Th e	rmometer	n.		
Wet- Bulb Thermo- meter.	Mean Vertical Differ-	7	·. s	70	.4	70	.6	70	.8	8°.	.0	80	.2
Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.		Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Reia- tive Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim		Millim.		Millim.		Millim.	1
0	0.03	0.82	8	0.20	8	0.09	1					0.00	١.
1 2	0.04	0.66 1.01	12	0.54	10	0.42	5	0.80	7	0.18	6	0.06 0.41	-1
8	0.04	1.39	15	1.27	13	1.15	12	1.08	l ii	0.91	9	0.79	8
4	0.04	1.79	18	1.67	16	1.55	15	1.43	14	1.81	18	1.19	11
5	0.04	2.22	21	3.10	19	1.98	18	1.86	17	1.74	16	1.62	14
	0.06			f	ŀ	1	l]	l				
6	0.05	2.78	24	2.66	28	2.44	21	2.82	20	2.20	18	2.08	17
7	0.05	8.16	26	8.04	25	2.92	24	2.80	22	2.68	21	2.56	20
8	0.06	8.68	29	3.56	27	8.44	26	3.82	25	8.20	24	8.08	22
9 10	0.06	4.28	31 88	4.11 4.70	30 22	8.99	28 30	8.87	27	3.75	26 28	3.63	25
10	0.06	4.82	88	4.70	22	4.57	30	4.45	29	4.88	28	4.21	27
11		5.44	85	5.82	84	5.19	82	5.07	31	4.95	30	4.88	29
12	0.07	6.09	37	5.97	36	5.85	84	5.73	83	5.61	82	5.49	31
18	0.07	6.79	39	6.67	37	6.55	86	6.48	85	6.31	34	6.18	33
14	0.07	7.58	40	7.41	39	7.29	38	7.17	27	7.04	36	6.92	85
15	0.08	8.31	42	8.19	41	8.07	40	7.95	39	7.88	87	7.71	36
	0.06								_				
16	0.09	9.14	48	9.02	42	8.90	41	8.78	40	8.66	39	8.58	38
17 18	0.09	10.02 10.95	45 46	9.90 10.88	44 45	9.78 10.71	48	9.66 10.58	42 43	9.53 10.46	40 42	9.41	39
19	0.10	11.93	40	11.81	46	11.69	45	11.56	44	11.44	42	10.34 11.32	41
20	0.10	12.97	48	12.85	47	12.72	46	12.60	45	12-48	44	12.86	48
_~	0.11						~	12.00	-		"	12.00	
21		14.07	50	13.94	49	18.82	48	18.70	47	13.58	46	18.45	45
22	0.19	15.22	51	15-10	50	14.98	49	14.85	48	14.78	47	14.61	46
23	0.12	16.45	52	16.82	51	16.20	50	16.08	49	15.95	48	15.83	47
24	0.14	17.73	52	17.61	52	17.49	51	17.36	50	17.24	49	17.12	48
25	- 1	19.09	58	18.97	52	18.85	52	18.72	51	18 .6 0	50	18.47	49
26	0.14	20.52	54	20.89	58	20.27	52	20.14	51	20.02	51	19.90	50
26	0.15	20.52	55	21.90	54	20.27	52 58	21.65	52	21.58	51	21.41	51
28	0.16	23.61	55	23.49	54 54	28.86	58	23.24	58	28.11	52	22.99	51
29	0.17	25.29	56	25.16	55	25.04	54	24.91	54	24.79	53	24.66	52
30	0.18	27.05	57	26.92	56	26.80	55	26.67	55	26.55	54	26.42	58
Ì	0.19		l	ł			ŀ		j		į		
31	0.20	28.90	58	28.78	57	28.65	56	28.53	55	28.40	55	28.27	54
82		30.85	59	30.72	58	80.60	57	30-47	56	30.35	56	1	Ì
83	- 1	İ	- 1		ı	ļ			- 1		i		
34 35	- 1	1		I		i	Į	1	ı		Į	1	ł
30			!		l	!	1	1					
		Ween t	James and a		of W	of 10		M					

Mean Horizontal Difference of Force of Vapor for each 0°.1 = 0.06 mm.

				t-t	, Die	rence of V	Vot an	t Dry-Bu	b The	mometen	L.		
Wet- Bulb Thermo- meter.	Mean Vertical Differ-	8	.4	₽.	6	8°.	8	9°.	•	₽.	9	9°.	4
Conti- grade Dagrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Reia- tive Hu- mid- ity.	Force of Vapor.	Rein- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
ô	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	
1			_		_		١. ١				l		
2	0.04	0.30	8	0.55	5	0.06	1 4	0.81	8	0.19	2	0.08	1
4	0.04	0.67 1.07	10	0.95	9	0.88	8	0.72	6	0.60	5	0.48	4
5	0.04	1.50	13	1.38	12	1.26	111	1.14	10	1.02	8	0.90	7
	0.05	1.00					<u>- آ</u>	l]				
6		1.96	16	1.84	15	1.72	14	1.60	13	1.48	12	1.86	10
7	0.05	2.44	19	2.82	17	2.20	16	2.08	15	1.96	14	1.84	18
8	0.05 0.06	2.96	21	2.84	20	2.72	19	2.60	18	2.48	17	2.36	16
9	0.08	8.51	24	3.39	28	8.27	21	3.15	20	8.08	19	2.91	18
10		4.09	26	8.97	25	8.85	24	8.78	28	8.61	22	8.49	21
	0.06	, , , , , , , , , , , , , , , , , , ,											
11	0.07	4.71	28	4.59	27	4.47	26	4.85	25	4,23	24	4.11	23
12	0.07	5.37	80	5.25	29	5.12	28	5.00	27	4,88	26 28	4.76	25 27
13	0.07	6.06	82	5.94	31	5.82	30	5.70	29	5.58 6.31	80	5.46 6.19	29
14	0.08	6.80	84	6.68	84	6.56	32 33	6.44 7.22	81	7.10	82	6.19	29 31
15	0.08	7.58	85	7.46	04	7.84	99	1.24	-00	7.10	32	0.51	-
16	0.05	8.41	87	8.29	36	8.17	85	8.05	84	7.92	83	7.80	82
17	0.09	9.29	89	9.17	38	9.04	87	8.92	36	8.80	85	8.68	84
18	0.09	10.22	40	10.09	89	9.97	88	9.85	37	9.73	86	9.60	35
19	0.10	11.20	41	11.07	40	10.95	89	10.83	39	10,71	88	10.58	87
20	0.11	12.28	43	12.11	42	11.99	41	11.87	40	11.74	89	11.62	38
	0.11												
21	0.12	13.33	44	13.21	43	13.08	42	12.96	41	12.84	40	12.71	40
22	0.12	14.48	45	14.36	44	14.24	48	14.12	42	18.99	41	18.87	41
23	0.13	15.71	46	15.58	45	15.46	44	15.34	48	15.21	42	15.09	42
24	0.14	16.99	47	16.87	46	16.75	45	16.62	44	16.50	44	16.37	43
25	ا ۵٫۰٬	18.35	48	18.22	47	18.10	46	17.98	45	17.86	45	17.78	44
26	0.14	10 ***	49	19.65	48	19.52	47	19.40	46	19.27	46	19.15	45
20 27	0.15	19.77 21.28	50	21.16	49	21.08	48	20.91	47	20.78	47	20.66	46
28	0.16	22.86	51	22.74	50	22.61	49	22.49	48	22.86	47	22.24	47
29	0.17	24.54	51	24.41	51	24.29	50	24.16	49	24.04	48	28.91	47
80	0.18	26.30	52	26.17	51	26.05	51	25.92	50	25.80	49	25.67	48
	0.19		1		1		1						l
81		28.16	58	28.08	52	27.91	51	27.78	51	1	i		
82		1	1		1	1		1	'		l		1
83			1	1		l .		1		1	İ	ļ	l
84		l	l				1	1					ŀ
85	l	L	<u> </u>	<u> </u>		<u> </u>	<u> </u>	<u> </u>	<u> </u>	L	l		

Mean Horizontal Difference of Force of Vapor for each $0^{\circ}.1 = 0.06$ mm.

Wet-				t-t	, Di g	reace of '	Wet an	d Dry-Bu	lb The	rmometer	.		
Bulb Thermo- meter.	Mean Vertical Differ-	9	.6	9°.	.8	10°	.0	10°	.2	10°	.4	10	.6
Centi- grade Degrees.	ence for each 0° 1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rola- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.						
0	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	
0					1	Ì	l		1		l	İ	1
2				1	1		İ	1_			i		
8				1				•				1	1
4	0.04	0.86	8	0.24	2	0.12	1		_				
5		0.78	6	0.66	5	0.54	4	0.42	3	0.80	2	0.18	1
6	0.05	1.24	9	1.12	8	1.00	7	0.88	6	0.76	5	0.64	5
7	0.05	1.72	12	1 60	11	1.48	10	1.86	9	1.24	8	1.12	7
8	0.05	2.24	15	2.12	14	2.00	18	1.88	12	1.76	11	1.64	10
9	0.06	2.79	17	2.66	16	2.54	16	2.42	15	2.30	14	2.18	18
10		8.37	20	8.25	19	8.13	18	8.00	17	2.88	16	2.76	15
11	0.06	3.98	22	3.86	21		20	3.62	19	8.50	18	8.38	18
12	0.07	4.64	24	4.52	23	8.74 4.40	22	4.28	22	4.15	21	4.03	20
13	0.07	5.33	26	5.21	25	5.09	25	4.97	24	4.85	23	4.73	22
14	0.07	6.07	28	5.95	27	5.83	26	5.71	25	5.58	25	5.46	24
15	0.08	6.85	30	6.73	29	6.61	28	6.49	27	6.37	26	6.24	26
	0.08												
16 17	0.09	7. 6 8 8.56	81 83	7.56 8.43	31 82	7.44	80 81	7.31 8.19	29 81	7.19 8.07	28	7.07 7.94	27 29
18	0.09	9.48	35	9.36	34	8.31 9.24	83	9.11	82	8.99	30	8-87	30
19	0.10	10.46	36	10.34	85	10.22	84	10.09	83	9.97	83	9.85	82
20	0.11	11.50	37	11.87	36	11.25	86	11.18	85	11.01	84	10.88	38
	0.11					1 1							
21	0.12	12.59	39	12.47	88	12.85	87	12.22	86	12.10	85	11.98	85
22 23	0.12	18.75 14.96	40	13.62 14.84	39	13.50	38	13.38 14.59	37 39	13.25 14.47	87 88	18.18 14.35	36 37
23	0.13	14.96	41	16.13	40 41	14.72 16.00	89 40	15.88	40	15.76	39	15.63	87 88
25	0.14	17.61	48	17.48	42	17.36	42	17.24	41	17.12	40	16.99	39
	0.14				_		_						
26	0.15	19.02	44	18.90	43	18.78	42	18.65	42	18.53	41	18.40	40
27	0.16	20.54	45	20.41	44	20.29	48	20.16	43	20.04	42	19.91	41
28	0.17	22.12	46	22.00	45	21.87	44	21.75	44	21.62	48	21.50	42
29 80	0.18	28.79 25.55	47 48	23.66 25.42	46 47	28.54 25.80	45 46	23.41	45	28.29	44	28.16	48
81													
32												1	
83	ł												Ì
84													
35						L!							

Mean Horizontal Difference of Force of Vapor for each $0^{\circ}.1 = 0.06$ mm.

Wet			t — t', Difference of Wet and Dry-Bulb Thermometers.													
Bulb Thermo- meter.	Mean Vertical Differ-	10°.8		11%		110	11°.9		11%		11°.6		.8			
Centigrade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rola- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Role- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.			
0, 1 2 8 4	Millim.	Millim.		Millim.		Minim.		Millim.		Millim.		Millim.				
6 7	0.05 0.05	0.52 1.00	7	0.40 0.88	8	0.28 0.76	2	0.16 0.64	1 4	0.52	8	0.40	2			
8	0.06	1.52	9	1.40	9	1.27	8	1.15	7	1.03	6	0.91	5			
9	0.06	2.06	12 14	1.94 2.52	11	1.82	10 18	1.70 2.28	10	1.58 2.16	9 11	2.04	8			
*	0.06	2004	49	4.04	1 3	A-40	10		-	2.10			**			
11		8.26	17	8.14	16	8.02	15	2.90	14	2.77	14	2.65	13			
12	0.07	8.91	19	8.79	18	8.67	17	8.55	17	8.43	16	3.81	15			
18	0.07	4-61	21	4.49	20	4.86	19	4.24	19	4.12	18	4.00	17			
14	0.07	5.84	23	5.22	22	5.10	21	4.98	21	4.86	20	4.78	19			
15	0.08	6.12	25	6.00	24	5.88	23	5.76	22	5.68	22	5.51	21			
16	0.09	6.95	27	6.83	26	6.70	25	6.58	24	6.46	23	6.84	22			
17	0.09	7.82	28	7.70	27	7.58	27	7.46	26	7.33	25	7.21	24			
18	0.10	8.75	29	8.63	29	8.50	28	8.38	27	8.26	27	8.14	26			
19	0.10	9.78	81	9.60	80	9.48	80	9.86	29	9.24	28	9.11	28			
20	0.11	10.76	33	10.64	82	10.51	81	10.89	80	10.27	30	10.15	29			
21	0.11	11.85	84	11.73	23	11.61	32	11.48	82	11.36	81	11.24	80			
22	0.12	18.01	85	12.88	84	12.76	84	12.64	33	12.51	82	12.89	82			
23	0.12	14.22	36	14.10	36	18.98	85	13.85	84	18.78	84	13.61	88			
24	0.13	15.51	88	15.39	37	15.27	86	15.15	85	15.02	85	14.90	84			
25	0.14	16.87	89	16.74	38	16.62	87	16.49	36	16.87	26	16.24	85			
	0.14	•	1			Ι΄.	l	1					١			
26	0.15	19.28	39	18.16	39	18.03	88	17.91	87	17.78	87	17.66	86			
27	0.16	19.79	40	19.67	40	19.54	89	19.42	28	19.29	88	19.17	37			
28	0.17	21.37	41	21.25	41	21.12	40	21.00	39	20.87	89	20.75	38			
29	l	28.04	42	22.91	42	l			1			l	1			
20																
31	I	l		1	ŀ		1			l	1		ľ			
82	1	1		1	1		1			ł	1					
83	l				l	1	1						1			
34 85	l	1		1	1	į .	1		ŀ			l				
33	L	L	L		L	L	<u> </u>	l	1	<u> </u>		<u> </u>	<u> </u>			
		Mean	Horisont	al Differe	nce of	Force of	Vapor	for each	0°.1 ==	0.06 mm.						

В

			t — t', Difference of Wet and Dry-Bulb Thermometers.													
Wet- Buib Thermo- meter.	Mean Vertical Differ-	19	°.0	19°	.9	19	19°.4		12°.6		12°.8		·.•			
Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity,	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.			
0	Millim.	Millim.		Millim.		Millim.	_	Millim.		Millim.		Millim.				
12	0.07	8.19	14	8.06	14	2.94	18	2.82	12	2.70	12	2.58	11			
13	0.07	8.88	16	8.76	16	8.64	15	3.51	14	3.39	14	8.27	18			
14	0.08	4.61	18	4.49	18 20	4.37	17	4.25	16	4.18	16	4.00	15 17			
15 16	0.08	5.89 6.22	20 22	6.09	20	5.15 5.97	19 21	5.03 5.85	18 20	4.90 5.78	18 19	4.78 5.61	17			
10	0.09	0.22	22	6.09	21	0.97	21	9.00	20	5.78	19	5.61	19			
17		7.09	24	6.97	23	6.84	22	6.72	22	6.60	21	6.48	21			
18	0.09	8.01	25	7.89	25	7.77	24	7.65	28	7.52	23	7.40	22			
19	0.10	8.99	27	8.87	26	8.74	26	8.62	25	8.50	25	8.38	24			
20	0.10	10.02	28	10.90	28	9.78	27	9.65	26	9.53	26	9.41	25			
21	0-11	11.12	80	10.99	29	10.87	28	10.75	28	10.62	27	10.50	27			
	0.12								١.,							
22	0.12	12.27	81	12.14	30	12.02	80	11.90	29	11.77	28	11.65	28			
28	0.13	18.48	82	18.86	31	13.23	81	18.11	30	12.99	29	12.86	29			
24	0.14	14.78 16.11	83	14.65 15.99	88	14.58	82	14.40	31	14.28	31	14.16 15.50	80			
25 26	0.14	17.54	85 86	17.42	84 85	15.87 17.29	88 84	15.74 17.17	38 34	15.62 17.04	32 83	16.92	81 88			
20	0.15	17.04	80	17.44	00	17.25	94	17.17	04	17.04	93	10.92	90			
27		19.04	37	18.92	36	18.80	85	18.67	35	18.55	84	18.42	84			
28	0.16	20.63	38			20.00		20.00	- 1				-			
		18	· 9	13°.4		13°.6		13°.8		14°.0						
				- 			_					 -				
		Millim.		Millim.		Millim.		Millim.		Millim.		Millim.				
12	0.07	2.46	10	2.84	10	2.22	9	2.09	8	1.97	8					
13	0.07	8.15	12	2.08	12	2.91	П	2.79	11	2.66	10					
14	0.08	3.88	14	8.76	14	8.64	18	3.52	18	8.40	12					
15	0.08	4.66	16	4.54	16	4.42	15	4.29	15	4.17	14					
16	0.09	5.48	18	5.86	18	5.24	17	5.12	16	5.00	16					
17		6.86	20	6.23	19	6.11	19	5.99	18	5.87	17					
18	0.09	7.28	22	7.16	21	7.08	20	6.91	20	6.79	19					
19	0.10	8.25	28	8.13	22	8.01	22	7.89	21	7.76	21	l				
20	0.10	9.29	25	9.16	24	9.04	28	8.92	28	8.80	22		ł			
21	0.11	10.38	26	10.25	25	10.13	25	10.01	24	9:89	24					
	0.12					1				1						
22	0.12	11.53	27	11.40	27	11.28	26	11.16	26	11.03	25		l			
23	0.13	12.74	28	12.62	28	12.49	27	12.87	27	12.25	26	ŀ	ļ			
24	0.14	14.02	80	13.90	29	18.77	29	18.65	28	18.58	27		1			
25	0.14	15.37	81	15.25	80	16.12	20	15.00	29	14.88	29	İ	1			
26		16.80	82	16.67	81	16.55	81	16.42	80	16.80	80					
		Mesn	Horizonte	al Differen	ce of	Force of '	Vapor 1	for each 0'	·.1 = 0	.06 mm.						

В

Correction for the Barometrical Height.

For Barom	strical		Difference of Thermometers t — t'.														
Height	Subtr'ct.	1°	3 °	30	40	5 °	60	70	80	90	10°	11°	19°	18°	14°		
				·		7	Fet-Bulb above the Freezing Point.										
Millim.	Millim.	міш.	Milli.	Mill	Mini	Milli.	Milli.	Milli.	Milli.	Mill.	Milli.	Milli.	Mill.	Milli.	Mini.		
755	755	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
750	760	0.00	0.01	0.01	0.02	0.02	0.02	0.03	0.03	0.04	0.04	0.04	0.05	0.05	0.06		
745	765	0.01	0.02	0.02	0.08	0.04					0.08	0.09	0.10	0.10	0.11		
740	770	0.01	0.03	0.04	0.05			0.08			0.12	0.18	0.14	0.16	0.17		
735	775	0.02	0.03	0.05	0.06	0.08	0.10	0.11	0.18	0.14	0.16	0.18	0.19	0.21	0.22		
			0.00	A A4	0.00	0.10	0 10	0.54	A 15	0.10	0.00	0.00	0.04	0.00	0.00		
780	780		0.04	0.08	0.08	0.10		0.14 0.17			0.20	0.22	0.24	0.26	0.28		
725	785	0.02	0.05		0.10			0.20	1 1	1	0.28	0.20	0.25	0.86	0.39		
720 715	790	0.03	0.06							0.29	0.82	0.85	0.38	0.42	0.45		
710	800	0.04	0.07		0.14	0.18				0.82	0.86	0.40	0.48	0.47	0.50		
110	~~	1							0.20	0.02							
700	14	0.04	0.09	0.13	0.18	0.22	0.26	0.81	0.85	0.40	0.44	0.48	0.53	0.57	0.62		
690	"	0.05	0.10	0.16	0.21	0.26	0.81	0.36	0.42	0.47	0.52	0.57	0.62	0.68	0.78		
680	"	0.06	0.12	0.18	0.24	0.80	0.36	0.42	0.48	0.54	0.60	0.66	0.72	0.78	0.84		
670	"	0.07	0.14	0.20	0.27	0.84	0.41	0.48	0.54	0.61	0.68	0.75	0.82	0.88	0.95		
660	"	0.08	0.15	0.28	0.80	0.8 8	0.46	0.58	0.61	0.68	0.76	0.84	0.91	0.99	1.06		
ll .	1										_						
650	"	0.08	0.17	0.25	0.34	0.42	0.50	0.59	0.67	0.76	0.84	0.92	1.01	1.09	1.18		
11	l	 	<u> </u>			L											
	•	i		ulb bel zing P	ow the)											
I		 	<u> </u>	<u> </u>		Γ—		EXAMPLE OF CALCULATION.									
755	755	0.00	0.00	0.00	0.00	0.00											
750	760	0.00		ı	0.01	0.02	1		Wel	rbeib ı	beve th	e Freezi	ng Point	-			
745	765	0.01	0.01	0.02	0.03	0.04		t' — 1	7°.0 .	ŧ.	— t' =	: 8°.2.	λ =	= 710 ^m	.		
740	770	0.01	0.02	0.08	0.04	0.05				_	for m	ean b	aromet	rical	mm.		
785	775	0.01	0.03	0.04	0.06	0.07	1	ight 7			rce of	•	•		9.41		
H		1	<u>.</u> .		١		1	Addit	ine co	rrecti	on for	710~m.	and 8°	'. 2 —	0.30		
780	780		0.04	1	4	1				Force	of va	por		. ==	9.71		
725	785	11	0.04		0.08							-					
720	790	0.02				i	1	PP11							•		
715 710	795 800	0.03	1		_		l .					-	-	at a g			
110	1 800	0.03	0.00	0.05	0.10		, P"							e the al			
709	"	0.04	0.08	0.12	0.15	0.19		•						s place s, a <i>con</i>			
690	66	11	0.09			1			•	•		_	_	s in th			
680	66	11	0.11	1		1			•					COTTE			
670	"	11	0.12		ı	1								e differ			
660	"	0.07	0.18	0.20	0.27	0.88								eviatio			
H	1		١.	1	}		wi							he accu			
650	"	0.07	0.15	0.22	0.29	0.86	ı I	the r					-		•		
1		1	1		<u> </u>	1											

III.

TABLE

GIVING AT SIGHT THE RELATIVE HUMIDITY DEDUCED FROM THE INDICA-TIONS OF THE DEW POINT INSTRUMENTS.

By M. T. HARGHENS.

This table, which has been published in the Annuaire Météorologique de France for 1850, page 86, and following, has been calculated by Mr. Haeghens, using Regnault's Tables of Elastic Forces of Vapor. It gives directly the relative humidity, when the hygrometrical observations have been made by means of dew point instruments like those of Daniell, Regnault, Bache, and others.

These hygrometers are destined to find out the temperature of the dew point, that is the temperature to which it would be necessary to lower the temperature of the air, in order that this air be completely saturated by the aqueous vapor which it contained at the time of the observation.

The force of vapor contained in the air, or its absolute humidity, is thus the maximum of force of vapor which corresponds to the temperature of the dew point; it is given directly in the Table I. of the Elastic Forces of Vapor, by Regnault.

The ratio of that maximum of force of vapor at the temperature of the dew point to the force of vapor which corresponds, in the same table, to the temperature of the surrounding air at the time of the observation, is the *relative humidity*. This ratio is given in hundredths in the following table, which relieves the observer of the trouble of calculating it.

Let t = temperature of the air surrounding the instrument.

t' = temperature of the dew point.

t - t' = the difference between these two temperatures.

The first column, on the left, contains the temperature of the air t, in centigrade degrees. The following ones, headed with the differences, t-t', between the temperatures of the air and of the dew point, give the *relative humidity* corresponding to the two elements.

	Temp. of the Air $= t$.	Dew point $= \mathscr{E}$.	Difference $t - t'$.	Relative Humidity.
Example:	10°.0	4°.4	5°.6	68

Should the temperature of the air t', or the difference t-t', fall between the numbers found in the columns, it is obvious, by glancing at the table, that an interpolation at sight will always be easy.

Temper-			ŧ-	t '=1)ifferen	ce of T	empera	tures of	the D	sw Poi	nt and	of the	Air.		-
the air.	0.0	0°.2	0°.4	0°.6	0°.8	_		1°.4		1°.8	2°.0	2°.2	2°.4	2°.6	2°. 8
t=	7.7	U .3	U .4	U .0	U .5	1°.0	1°.9	LA	1°.6	1 .0	Z .U	2 .5	2 .4	2 .0	2 .0
Centig.	100	98	97	95	94	92	90	89	88	86	85	83	82	80	79
-7	100	98	97	95	94	92	91	89	88	86	85	83	82	81	79
-6	100	98	97	95	94	92	91	89	88	87	85	84	82	81	80
-5	100	98	97	95	94	92	91	89	88	87	85	84	82	81	80
-4	100	98	97	95	94	92	91	89	88	87	85	84	83	81	80
-3	100	98	97	95	94	92	91	90	88	87	85	84	83	81	80
-2	100	98	97	95	94	93	91	90	88	87	86	84	88	82	80
-1	100	98	97	95	94	98	91	90	89	87	86	85	88	82	81
اها	100	98	97	96	94	98	91	90	89	87	86	85	83	82	81
+1	100 100	99	97	96	95	93	92	90	89	88	86	85	84	88	81 82
2	100	99 99	97 97	96 96	95 93	93 93	92 92	91 91	89 89	88 88	87 87	85 86	84	83 83	82
1	100	99	97	96	95	98	92	91	89	88	87	86	85	83	82
5	100	99	97	96	95	98	92	91	90	88	87	86	85	88	82
6	100	99	97	96	95	98	92	91	90	88	87	86	85	84	82
7	100	99	97	96	95	98	92	91	90	89	87	86	85	84	83
8	100	99	97	96	95	93	92	91	90	89	87	86	85	84	88
9	100	99	97	96	95	94	92	91	90	89	87	86	85	84	88
10	100	99	97	96	95	94	92	91	90	89	87	86	85	84	88
11	100	99	97	96	95	94	92	91	90	89	87	86	85	84	83
12	100	99	97	96	93	94	92	91	90	89	88	87	85	84	83
13	100	99	97	96	95	94	92	91	90	89	88	87	85	84	83
14	100	99	98	96	95	94	98	91	90	89	88	87	86	84	83
15	100	99	98	96	93	94	98	91	90	89	88	87	86	84	88
16	100	99	98	96	95	91	93	91	90	89	88	87	86	85	84
17	100	99	98	96	95	94	93	91	90	89	88	87	86	85	84
18	100	99	98	96	95	94	93	92	90	89	88	87	86	85	84
19	100	99	98	96	95	94	93	92	91	89	88	87	86	85	84
20	100	99	98	96	95	94	98	92	91	89	88	87	86	85	84
21	100	99	98	96	95	94	98	92	91	90	88	87	86	85	84
22	100	99	98	96	95	94	93	92	91	90	89	87	86	85	84
23	100	99	98	96	95	94	93	92	91	90	89	88	86	85	84
24	100	99	98	97	95	94	93	92	91	90	89	88	87	85	84
25	100	99	98	97	95	94	98	92	91	90	89	88	87	86	85
26	100	99	98	97	95	94	93	92	91	90	89	88	87	86	85
27	100	99	98	97	95	94	93	92	91	90	89	88	87	86	85
28	100	99	98	97	95	94	93	92	91	90	89	88	87	86	85
29	100	99	93	97	96	94	93	92	91	90	89	88	87	86	85
30	100	99	98	97	96	94	93	92	91	90 ·	89	88	87	86	85
31	100	99	98	97	96	94	93	92	91	90	89	88	87	86	85
32	100	99	98	97	96	94	98	92	91	90	89	88	87	86	85
83	100	99	98	97	96	94	93	92	91	90	89	88	87	86	85
34	100	99	98	97	96	95	98	92	91	90	89	88	87	86	85
35	100	99	98	97	96	95	93	92	91	90	89	88	87	86	85
						7									

В

Temper-				• •′ → 1	Differen	ce of T	'emnere	tures o	the D	e Poi	nt and	of the	A i -		
ature of tne air.									r —	- TO					
t=	8°.0	8°.2	8.°4	8°.6	\$°. 8	4°.0	4°.2	4°.4	4°.6	4°.8	5°.0	5°.2	5°.4	5°.6	5°. 8
Centlg.	78	77	75	74	78	72	71	69	68	67	66	65	64	68	62
-7	78	77	75	74	78	72	71	69	68	67	66	65	64	68	62
-6	78	77	76	74	78	72	71	69	68	67	66	65	64	63	62
-5	79	77	76	75	78	72	71	70	68	67	66	65	64	68	62
-4	79	77	76	75	74	78	71	70	69	68	67	66	64	63	62
-3	79	77	76	75	74	78	72	70	69	68	67	66	65	64	63
-2	79	78	77	76	74	78	72	71	70	69	68	66	65	64	63
-1	79	78	77	76	75	78	72	71	70	69	68	67	66	65	64
0	80	78	77	76	75	74	73	71	70	69	68	67	6 6	65	64
+1	80	79	78	77	75	74	78	72	71	70	69	68	66	65	64
2	81	79	78	77	76	75	74	72	71	70	69	68	67	66	65
8	81	80	78	77	76	75	74	78	72	71	70	69	68	66	65
4	81	80	79	78	77	75	74	78	72	71	70	69	68	67	66
5	81	80	79	78	77	76	75	78	72	71	70	69	68	67	6 6
6	81	80	79	78	77	76	75	74	78	72	71	70	69	68	67
7	81	80	79	78	77	76	75	74	73	72	71	70	69	68	67
8	81	80	79	78	77	76	75	74	73	72	71	70	69	6 8	67
8	82	80	79	78	77	76	75	74	73	72	71	70	69	6 8	67
10	82	81	80	78	77	76	75	74	78	72	71	70	69	68	67
11	82	81	80	79	78	76	75	74	73	72	71	70	70	69	68
12	82	81	80	79	78	77	76	75	74	78	72	71	70	69	68
13	82	81	80	79	78	77	76	75	74	78	72	71	70	69	68
14	82	81	80	79	78	77	76	75	74	73	72	71	70	69	68
15	82	81	80	79	78	77	76	75	74	73	72	71	70	69	68
16	,82	81	80	79	78	77	76	75	74	78	72	71	71	70	69
17	83	81	80	79	78	77	76	75	74	78	73	72	71	70	69
18	88	82	81	80	79	78	77	76	75	74	78	72	71	70	69
19	83	82	81	80	79	78	77	76	75	74	73	72	71	70	69
20	88	82	81	80	79	78	77	76	75	74	73	72	71	70	69
21	88	82	81	80	79	78	77	76	75	74	78	72	71	70	70
22	88	82	81	80	79	78	77	76	75	74	73	78	72	71	70
28	88	82	81	80	79	78	77	76	75	74	74	73	72	71	70
24	83 84	82	81	80	79	78	77	77	76	75	74	78	72	71	70
25		88	82	81	80	79	78	77	76	75	74	78	72	71	70
26	84	88	82	81	80	79	78	77	76	75	74	78	72	71	70
27	84	83	82	81	80	79	78	77	76	75	74	73	72	71	- 70
28	84	88	82	81	80	79	78	77	76	75	74	73	72	71	70
29 80	84 84	83 83	82 82	81 81	80 80	79 79	78 78	77	76 76	75 76	75 75	74 74	78 73	72 72	71 71
31	84	83	82	81	80	79	78	77	77	76	75	74	78	72	71
32	84	83	82	81	80	79	79	78	77	76	75	74	78	72	72
88	84	83	82	81	80	80	79	78	77	76	75	74	73	72	72
34	85	84	83	82	81	80	79	78	77	76	75	74	74	78	72
85	85	84	83	82	81	80	79	78	77	76	75	75	74	73	72
D											<u> </u>		!	<u> </u>	<u> </u>

Temper-			ŧ	_ t =	Differe	nce of I	'empera	tures o	the De	w Poin	and of	the Air			
the air.	6°0	6°.2	6°.4	6°.6	6°.8	7°.0	7°.2	7°.4	7°.6	7°.8	8°.0	8°.2	8°.4	8°.6	8°.8
Centig.						_					_		-	_	
8									l			1			
-7			59	58				•	1	1		l			
-6	61	60	59	58	57 58	56			٠.		**				
-5	61	80				57	56	55	54	58	52				
-4	62	61	60	59	58	57	56	55	54	58	52				
-3	62	61	60	59	58	57	56	55	54	58	58	52	51	50	49
-2	62	61	60	60 60	59	58	57	56	55	54	58	52	51	50	49
-1	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49
0	63	62	61	60	59	58	57	56	55	54	58	58	52	51	50
+1	63	62	61	61	60	58	58	57	56	55	54	53	52	51	51
2	64	63	62	61	60	59	58	57	56	55	55	54	58	52	51
3	64	63	62	62	60	60	59	58	57	56	55	54	53	58	52
4	65	64	63	62	61	60	59	58	57	56	56	55	54	58	52
5	65	64	63	62	62	61	60	59	58	57	56	55	54	54	58
6	66	65	64	63	62	61	60	59	58	57	57	56	55	54	58
7	66	65	64	63	62	61	60	60	59	58	57	56	55	86	54
8	66	65	64	63	62	62	61	60	59	58	57	56	56	55	54
9	66	65	64	64	63	62	61	60	59	58	58	57	56	55	54
10	67	66	65	64	63	62	61	60	59	59	58	57	56	55	55
11	67	66	65	64	63	62	61	61	60	59	58	57	56	56	55
12	67	66	65	64	68	62	62	61	60	59	58	57	57	56	55
13	67	66	65	64	64	63	62	61	60	59	59	58	57	56	55
14	67	66	66	65	64	68	62	61	60	60	59	58	57	56	56
15	67	67	66	65	64	63	62	61	61	60	59	58	57	57	56
16	68	67	66	65	64	63	68	62	61	60	59	58	58	57	56
17	68	67	66	65	64	64	63	62	61	60	59	59	58	57	56
18	68	67	66	65	65	64	68	62	61	60	60	59	58	57	57
19	68	67	67	66	65	64	63	62	62	61	60	59	58	58	57
20	68	68	67	66	65	64	63	63	62	61	60	59	59	58	57
21	69	68	67	66	65	64	64	63	62	61	60	60	59	58	57
22	69	68	67	66	65	65	64	63	62	61	61	60	59	58	58
23	69	68	67	67	66	65	64	68	62	62	61	60	59	59	58
24	69	68	68	67	66	65	64	63	63	62	61	60	60	59	58
25	69	69	6 8	67	66	65	64	64	63	62	61	61	60	59	58
26	70	69	68	67	66	65	65	64	63	62	61	61	60	59	58
27	70	69	68	67	66	66	65	64	63	62	62	61	60	59	59
28	70	69	68	67	67	66	65	64	68	63	62	61	60	60	59
29	70	69	69	68	67	66	65	64	64	68	62	61	61	60	59
80	70	69	69	6 8	67	66	65	65	64	68	62	62	61	60	59
31	70	70	69	6 8	67	66	66	65	64	68	62	62	61	60	60
82	71	70	69	68	67	67	66	65	64	64	63	62	61	61	60
33	71	70	69	68	68	67	66	65	64	64	68	62	61	61	60
84	71	70	69	69	68	67	66	66	65	64	63	62	62	61	60
85	71	70	70	69	68	67	66	66	65	64	63	68	62	61	60

В

Temper- ature of			t —	t' = D	ifferen	ce of T	empera	tures of	the D	sw Pol	nt and	of the	Air.		
the air.	9°.0	9°.2	9°.4	9°.6	9°.8	10°.0	10°.2	10°.4	10°.6	10°.8	11°.0	11 . 9	11°.4	11°.6	11°.8
Centig.	<u>`</u>												—		
-7															
−6															
-5															
-4 -3 -2 -1													'		
-3 -2														i	
-1														•	
0															
+1	50														
2	50	49	49	48	47	46									
8	51	50	49	48	48	47	46	45	45	44	43				,
4	51	51	50	49	48	47	47	46 46	45 46	44	44	43	42 43	42 42	41
5	52	51	50	49	49	48				45	44	43	-		41
6	52 53	52 52	51 51	50 51	49 50	48 49	48 48	47	46 47	45 46	45 45	44	43 44	43 48	42 42
7 8	53	52 52	52	51	50	49	49	48	47	46	46	45	44	44	43
9	54	53	52	51	50	50	49	48	48	47	46	45	45	44	43
10	54	53	52	51	51	50	49	49	48	47	47	46	45	44	44
11	54	53	53	52	51	50	50	49	48	48	47	46	46	45	44
12	54	54	58	52	51	5 1	50	49	49	48	47	47	46	45	45
13	55	54	53	52	52	51	50	50	49	48	47	47	46	46 46	45
14 15	55 55	54 54	58 54	53 53	52 52	51 51	50 51	50 50	49 49	48 49	48 48	47	46 47	46	45 45
	55				52	52	51	50	50	49	48	48	47	46	46
16 17	56	55 55	54 54	58 53	53	52	51	51	50	49	49	48	47	47	46
18	56	55	54	54	53	52	51	51	50	49	49	48	47	47	46
19	56	55	55	54	53	52	52	51	50	50	49	48	48	47	47
20	56	56	55	54	53	53	52	51	51	50	49	49	48	47	47
21	57	56	55	54	54	53	52	52	51	50	50	49	48	48	47
22	57 57	56	· 55	55 55	54	53 53	58 58	52 52	51 51	50 51	50 50	49 49	49 49	48 48	47 48
23 24	57	56 57	56	55	54	54	58	52	52	51	50	50	49	48	48
25	58	57	56	55	55	54	58	58	52	51	51	50	49	49	48
26	58	57	56	56	55	54	58	53	52	51	51	50	50	49	48
27	58	57	56	56	55	54	54	58	52	52	51	50	50	49	48
28	58	57	57	56	55	55	54	53	53	52	51	51	50	49	49
29 80	58 59	58 58	57 57	56 57	56 56	55 55	54 54	53 54	53 53	52 52	52 52	51 51	50 51	50 50	49 49
81 82	59 59	58 58	57 58	57 57	56 56	55 56	55 55	54 54	53 54	53 53	52 52	51 52	51 51	50 50	49 50
33	59	59	58	57	56	56	55	54	54	58	52	52	51	51	50
34	60	59	58	57	57	56	55	55	54	53	58	52	52	51	50
85	60	59	58	58	57	56	56	55	54	54	58	52	52	51	50

the air t = Centig		12°.2	19°.4	12°.6	190.8	190 n	100 8	100 /	100 6	100 0	140 0	140 0	140 4	140 C	140.0
-8		12 12	12 13	170 00					I A	1 L X X	II A II I	14 . 4	14 . 4		I I A " X
-8							10 .2	10 .4	10 .0	10 .0	14 10				
' _ - 7															
11															
-6 -5	1										•				
[]															
-4 -3	1														
-2															
-1			i												
0	1														
1															
+1															
8															
4	40	40	39	38	38	87									
5	41	40	89	39	38	88	87	36	36	85	35				
6	41	41	40	39	89	88	87	87	86	36	85	35	34	83	33
7	42	41	40	40	89	89	38	87	37	36	36	85	84	84	33
8	42 43	42 42	41 41	40 41	40	89 40	38 39	38 38	37 38	37 37	36 37	35 36	35 35	34 35	34 34
10	43	48	42	41	41	40	39	89	38	38	87	36	36	85	35
11	44	43	42	42	41	40	40	89	39	38	87		36	36	35
12	44	43	43	42	41	41	40	40	39	38	88	87 87	37	86	36
13	44	44	43	42	42	41	41	40	89	39	88	38	87	37	86
14	45	44	43	43	42	42	41	40	40	39	89	88	87	87	36
15	45	44	44	43	42	42	41	41	40	89	39	88	38	37	37
16	45	44	44	48	43	42	41	41	40	40	89	89	88	38	87
17	45	45	44	43	43	42	42	41	41	40	89	39	38	88	37
18 19	46 46	45 45	44	44	43 43	43 48	42	41	41	40	40	39	89	38 38	38 38
19 2 0	46	45	45	44	44	48	42 42	42 42	41	41	40	89 40	39 39	39	38
21	46	46	45	45	44	48	43	42	42			40		39	38
22	40	46	45	45	44	44	43	43	42	41	41	40	89 40	39	89
23	47	46	46	45	45	44	48	48	42	42	41	41	40	39	39
Z-1	47	47	46	45	45	44	44	43	42	42	41	41	40	40	-39
20	47	47	46	46	45	44	44	48	43	42	42	41	41	40	39
26	48	47	46	46	45	45	44	44	48	42	42	41	41	40	40
27	48	47	47	46	45	45	44	44	48	43	42	42	41	40	40
28 29	48 48	48 48	47 47	46	46 46	45 45	45 45	44	44	43	42	42	41	41	40
30	49	48	47	47	46	46	45	44	44	48 48	43 43	42 42	42 43	41	41
31	49	48	48	47	46	46	45	45				,			
32	49	49	48	47	47	46	46	45	44 45	44	48 43	43 43	42 42	42 42	41
33	49	49	48	48	47	46	46	45	45	44	44	48	43	42	42
34	50	49	49	48	47	47	46	46	45	44	44	48	43	42	42
35	50	49	49	48	48	47	46	46	45	44	44	44	48	43	42

B

TABLE IV.

FACTOR $_{p}^{100}$, FOR COMPUTING THE RELATIVE HUMIDITY, OR THE DEGREE OF MOISTURE OF THE AIR FROM 1TS ABSOLUTE HUMIDITY, GIVEN IN MILLIMETRES.

By HAEGHENS.

THE Relative Humidity, or the degree of moisture of the air, is the ratio of the quantity of vapor contained in the air to the quantity it could contain at the temperature observed, if fully saturated.

If we call

The force of vapor contained in the air = f,

The maximum of the force of vapor at the temperature of the air = F,

The point of saturation = 100,

we have the proportion,

Relative Humidity: 100::f:F,

and

 $f_{\star}^{\times 100}$ = Relative Humidity in Hundredths.

But as $\frac{f \times 100}{F} = f \times \frac{100}{F}$, it is obvious that the operation indicated by the former expression, viz. $\frac{f \times 100}{F}$, would be reduced to a simple multiplication, if we had a table of the factors $\frac{100}{F}$. Such a table is obtained by dividing the constant number 100 by each number in the Table of Elastic Forces of Vapor, and substituting the quotients to the tensions.

The following Table, taken from the Annuaire Météorologique de la France, for 1850, p. 79, gives the factor $\frac{100}{7}$ for every tenth of a degree from — 10 to $+35^{\circ}$ Centigrade, corresponding to the Forces of Vapor in Table I.

USE OF THE TABLE.

The force of vapor contained in the air being given in millimetres, multiply the number expressing it by the factor in the table corresponding to the temperature of the air at the time of the observation; the result will be the Relative Humidity in Hundretths.

Examples.

1. Suppose the temperature of the air to be = 24° Ceftigrade.

" force of vapor in the air to be = 10.76 millimetres.

Opposite 24° is found in the table the factor 4.51.

Then $10.76 \times 4.51 = 48.5$, Relative Humidity in Hundredths.

2. Suppose the temperature of the air to be = 16.7.

" force of vapor in the air to be = 12.07.

Table gives for 16.7 the factor 7.07.

Then $12.07 \times 7.07 = 85.3$, Relative Humidity.

В

FACTOR $^{100}_{\ \ F}$, to compute the relative humidity.

t =					Tenthe o	Degrees.				
of Air, Centig.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
Centraly.										
-10	48.1	48.5	49.9	49.8	49.7	50.1	50.5	50.9	51.4	51.8
9	41.2	44.6	45.0	45.4	45.7	46.1	46.5	46.9	47.3	47.7
8	40.7	41.1	41.4	41.7	42.1	42.4	42.8	48.1	43.5	48.9
7	87.5	37.8	88.1	38.4	88.7	89.0	39.4	89.7	40.0	40.4
6	84.6	84.9	35.2	85.4	85.7	86.0	36.8	86.6	36.9	37.2
5	31.9	32.2	32.4	82.7	88.0	88.2	32.5	23.8	84.0	84.8
4	29.5	29.8	80.0	80.2	30.5	80.7	81.0	81.2	81.4	81.7
3	27.3	27.5	27.7	27.9	28.2	28.4	28.6	28.8	29.1	29.8
2	23.8	25.5	25.7	25.9	26.1	26.8	26.5	26.7	26.9	27.1
1	23.4	23.6	23.8	24.2	24.0	24.8	24.5	24.7	21.9	25.1
-0	21.7	21.9	22.1	22.2	22.4	22.6	22.8	22.9	23.1	23.8
+0	21.7	21.6	21.4	21.8	21.1	21.0	20.8	20.7	20.5	20.4
1	20.2	20.1	20.0	19.8	19.7	19.5	19.4	19.8	19.1	19.0
2	18.9	18.7	18.6	19.5	18.3	18.2	18.1	18.0	17.8	17.7
3	17.6	17.5	17.3	17.2	17.1	17.0	16.9	16.7	16.6	16.5
4	16.4	16.3	16.2	16.1	15.9	15.8	15.7	15.6	15.5	15.4
5	15.3	15.2	15.1	15.0	14.9	14.8	14.7	14.6	14.5	14.4
6	14.3	14.2	14.1	14.0	13.9	13.8	13.7	13.6	18.5	18.4
7	13.4	13.3	13.2	13.1	13.0	12.9	12.8	12.7	12.6	12.6
8	12.5	12.4	12.3	12.2	12.1	12.1	12.0	11.9	11.8	11.7
9	11.7	11.6	11.5	11.4	11.4	11.8	11.2	11.1	11.1	11.0
10	10.9	10.8	10.8	10.7	10.6	10.6	10.5	10.4	10.3	10.8
11	10.2	10.1	10.1	10.0	9.95	9.88	9.82	9.75	9.69	9.63
12	9.56	9.50	9.44	9.38	9.32	9.26	9.20	9.18	9.08	9.02
13	8.96	8.90	8.84	8.79	8.73	8.67	8.62	8.56	8.51	8.45
14	8.40	8.34	8.29	8.24	8.18	8.15	8.08	8.08	7.98	7.92
15	7.87	7.82	7.77	7.72	7.68	7.63	7.58	7.58	7.48	7.48
16	7.39	7.84	7.29	7.25	7.20	7.16	7.11	7.07	7.02	6.98
17	6.98	6.89	6.85	6.80	6.76	6.72	6.68	6.63	6.59	6.55
18	6.51	6.47	6.48	6.39	6.35	6.31	6.27	6.28	6.19	6.16
19	6.12	6.08	6.04	6.00	5.97	5.98	5.89	5.86	5.82	5.79
20	5.75	5.71	5.68	5.64	5.61	5.58	5.54	5.51	5.47	5.44
21	5.41	5.37	5.84	5.31	5.27	5.24	5.21	5.18	5.15	5.12
22	5.09	5.06	5.02	4.99	4.96	4.98	4.90	4.87	4.85	4.82
23	4.79	4.76	4.73	4.70	4.67	4.65	4.62	4.59	4.56	4.58
24	4.51	4.48	4.45	4.43	4.40	4.87	4.35	4.82	4.80	4.27
25	4.25	4.22	4.20	4.17	4.15	4.12	4.10	4.07	4.05	4.03
26	4.00	3.98	3.95	3.98	8.91	8.89	8.86	8.84	8.82	3.79
27	8.77	8.75	3.78	8.71	8.69	8.66	8.64	3.62	8.60	8.58
28	3.56	8.54	3.52	8.50	8.48	8.46	8.44	3.42	8.40	3.38
29	3.36	8.84	8.32	8.80	3.28	8.26	8.24	3.22	8.21	8.19
80	3.17	8.15	3.18	8.12	8.10	8.08	8.06	8.05	8.08	8.01
81	2.99	2.98	2.96	2.94	2.98	2.91	2.89	2.88	2.86	2.84
82	2.83	2.81	2.80	2.78	2.77	2.75	2.78	2.72	2.70	2.69
33	2.67	2.66	2.64	2.63	2.61	2.60	2.58	2.57	2.56	2.54
34	2.53	2.51	2.50	2.49	2.47	2.46	2.44	2.43	2.42	2.40
35	2.39	2.38	2.86	2.35	2.34	2.33	2.81	2.30	2.29	2.28

TABLE V.

WEIGHT OF VAPOR, IN GRAMMES,

contained in a cubic metre of saturated air under a barometric pressure of 760 millimetres, and at temperatures between -20° and $+40^{\circ}$ centigrade.

The theoretic density of aqueous vapor is very nearly 0.622, or §, of the density of the air at the same temperature and pressure. Regnault's experiments gave similar results. From this ratio the weight of the vapor contained in a given volume of air, the temperature and humidity of which are known, can be computed.

If we call

t = the temperature of the air;

f = the elastic force of the vapor contained in the air at the time of the observation;

F = the maximum elastic force of vapor due to the temperature t, as given in the table;

p = the weight of the vapor contained in a litre of air at the temperature t, and with a force of vapor f;

P = the weight of vapor in a litre of air at the temperature t, and at full saturation, or F.

Then,
$$p = 0.622 \frac{1.2932235^{\circ}}{1 + 0.00367t} \cdot \frac{f}{760^{\text{min}}}$$

In which 1.293223 grammes is the weight of a litre of dry air, at the temperature of zero Centigrade, and under a barometric pressure of 760 millimetres, according to the determination of Regnault; 0.00367, the coefficient of the expansion of the air as found by the same; 760 millimetres, the assumed normal barometric pressure.

The weight of a litre of air given by Regnault in the *Mémoires de l'Institut*, Tom. XXI. p. 157, is 1.293187 grammes; but by correcting a slight error of computation (see E. Ritter, *Mémoires de la Société Physique de Genève*, Tom. XIII. p. 361), it becomes, as given above, 1.293223 grammes.

In order to obtain the weight of vapor in a cubic metre, or 1000 litres, of saturated air, the formula becomes,

$$P = 0.622 \, \frac{1293.2238^{t}}{1 + 0.00367 \, t} \cdot \frac{F}{760^{\text{mm}}}.$$

From this formula Table V. has been computed. The tensions due to the temperatures in the first column are placed opposite the weights of vapor; they are taken from Table I. It will be seen that, throughout the table, the number of grammes of vapor nearly corresponds to the number of millimetres of pressure expressing the tension.

The table of the weights of vapor given in Pouillet's *Eléments des Physique*, Tom. II. p. 707, being based on older values, gives results somewhat different. In that published by Becquerel, *Eléments de Physique Terrestre*, p. 354, Regnault's tensions and coefficient of expansion of the air have been used, but the value of the weight of vapor in a litre of air formerly determined by Biot and Arago, viz. 1.29954 grammes, has been retained.

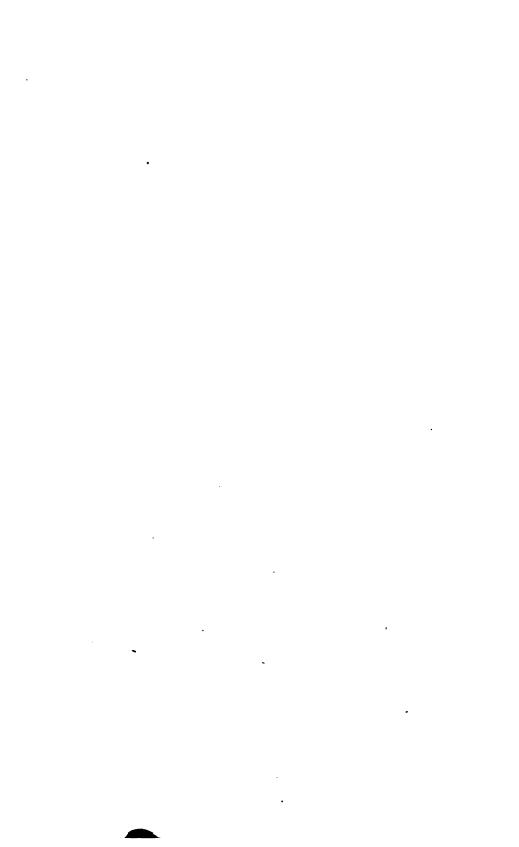
B

V. WEIGHT OF VAPOR, IN GRAMMES,

CONTAINED IN A CUBIC METRE OF SATURATED AIR,

At Temperatures between -20° and $+40^{\circ}$ Centigrads.

Temperature of	Force of	Weight _ of	Difference.	Temperature	Force of	Weight	Difference.
Dew-Point.	Vapor.	Vapor.		Dew-Point.	Vapor.	Vapor.	
Centigrade.	Millimetres.	Grammes.	Grammes.	Centigrade.	Millimetres.	Grammes.	Grammes.
-20°	0.912	1.042		+10°	9.165	9.857	
-19	0.993	1.130	0.088	11	9.792	9.962	0.605
-18	1.080	1.224	0.094	12	10.457	10.601	0.689
-17	1.174	1.325	0.101	18	11.162	11.276	0.678
-16	1.275	1.434	0.109	14	11.908	11.988	0.719
,,,			0.118				0.751
-15 -14	1.385	1.551	0.127	15	12.699	12.789	0.798
	1.503	1.678	0.184	16	13.586	13.582	0-835
-13 -12	1.631	1.813	0.145	17	14.421	14.867	0.880
-12 -11	1.768	1.957	0.167	18	15.357	15.247	0.926
-11	1.918	2.114		19	16.846	16.173	
-10	2.078	2.288	0.169	20	17.291	17.148	0.975
- 9	2.261	2.475	0.192	21	18.495	18.174	1.026
- 8	2.456	2.678	0.908	22	19.659	19.258	1.078
- 7	2.666	2.896	0.318	28	20.888	20.887	1-184
- 6	2.890	3.128	0.932	24	22.184	21.579	1.193
			0.348				1.262
- 5	8.131	8.376	0.262	25	23.550	22.831	1.818
- 4	8.887	3.638	0.281	26	24.988	24.144	1.380
- 8	8.662	3.919	0.298	27	26.505	25.524	1.447
- 2	8.955	4.217	0.817	28	28.101	26.971	1.619
- 1	4.267	4.584		29	29.762	28.489	
0	4.600	4.869	0.334	80	81.548	*** 0***	1.589
+1	4.940	5.209	0.841	81	88.405	30.079 81.744	1.666
2	5.302	5.571	0.361	82	85.859	88.491	1.747
3	5.687	5.953	0.363	88	87.410	~ 85. 491	1.827
4	6.097	6.360	0.406	84	39.565	87.280	1.918
			0.481				
5	6.584	6.791		85	41.827	89.281	2.001
6	6.998	7.247	0.466	86	44.201	41.823	2.093
7	7.492	7.781	0.484	87	46.691	48.510	2.187
8	8.017	8.248	0.841	28	49.802	45.795	2.285
9	8.574	8.795	0.841	29	52.039	48.182	2.387
+10	9.165	9.857	0.073	+40	54.906	50.674	2.492



PRACTICAL TABLES,

IX

ENGLISH MEASURES,

BASED ON REGNAULT'S HYGROMETRICAL CONSTANTS.

В

VI.

TABLE OF THE ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHRENHEIT,
REDUCED FROM REGNAULT'S TABLE.

The values of the elastic force of vapor furnished by V. Regnault, which are found in Table I. of this Hygrometrical set, are derived from a series of experiments conducted, during several years, with great care, consummate skill, and all the means of precision which are at the disposal of modern science. The methods of investigation, and all the steps in each experiment, were minutely described and submitted to the judgment of the scientific, successively in separate papers in several volumes of the Annales de Chimie et de Physique, and collectively in his final Report to the Minister of Public Works, (see above, p. 9,) which fills Volume XXI. of the Mémoires de l'Institut de France. The confidence which has been deservedly granted to these determinations by nearly all scientific men, is increased by the fact that one of the best physicists and experimenters in Germany, Professor Magnus, came, about the same time, to results so little different, that both tables, for most purposes, may be considered identical. (Compare below, Table XXII.) It seems, therefore, that these values ought to be used in our hygrometrical tables, as has been done in France, in preference to the older and less reliable determinations on which they are based.

Though Regnault's table of the elastic force of vapor is considered, even, it is believed, by a majority of scientific men in England, as the most reliable which science now possesses, the author is not aware that any extensive reduction of it to English measures, such as is wanted for meteorological purposes, has been as yet published; still less a series of tables based on these values. Such a set of hygrometrical tables in English measures, corresponding to the preceding one in French measures, is offered here, which, it is hoped, supplies a real want felt by a large number of meteorologists.

Table VI. is Regnault's Table of the Elastic Force of Vapor as given in Table I., reduced to English measures, in which the fourth decimal is given in order to secure the third, and otherwise to facilitate the computations. From these values Tables VII. to X. have been computed.

VI ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHREMERIT.

REDUCED FROM REGNAULT'S TABLE.

Temper-	Force of	. "	Temper-	Force of	f Vapor	r. Tem	200	Fore	of Vapor	Temper	1	f Vapor.
store Fahren- heit.	Tenths of	- 11		Tenths of	Degre	es. Fab	ren-	Tenth	a of Degree	II - 4	Tenthe	f Degrees.
	•	0.5	-	•	0.5	5		•	9.5	•	0	0.5
	Eng. In.	Eng. In.		Eng. In.	Eng. 1	in.		Eng.	In. Eng. I	n.	Eng. In.	Eng. In.
-31	0.0087	0.0085	-19	0.0171	0.01	67 -	8	0.02		0 + 2	0.0476	0.0485
-3 0	0.0092	0.0090	-18	0.0181	0.01	76 -	7	0.03	12 0.030	4 8	0.0498	0.0510
-29	0.0098	0.0095	-17	0.0190	0.01	85 -	6	0.03	27 0.031	9 4	0.0521	0.0588
-28	0.0104	0.0101	-16	0.0200	0.01	95 -	5	0.03	48 0.03	5	0.0545	0.0558
-27	0.0110	0.0107	-15	0.0210	0.02	05 -	4	0.03	59 0.038	61 6	0.0570	0.0584
-26	0.0117	0.0114	-14	0.0221	0.02	16 -	8	0.08	76 0.036	8 7	0.0597	0.0611
-25	0.0124	0.0120	-13	0.0282	0.02		2	0.03		- 11	0.0625	
-24	0.0131	0.0127	-12	0.0244	0.02	[]	1	0.04			0.0654	
-23	0.0138	0.0135	-11	0.0257	0.02		0	0.04			0.0684	
-22	0.0146	0.0142	-10	0.0270	0.02	63∥ +	0	0.04	34 0.04	- 11	0.0716	
-2 1	0.0154	0.0150	- 9	0.0288	0.02		1	0.04		11	0.0749	
-20	0.0163	0.0158	- 8	0.0297	0.02	90 +	2	0.04	76 0.048	7 +18	0.0783	0.0800
Temper- ature Fahren-					7	Conths of	Deg	reed.				
heit.	0.	1.	2.	3		4.	Í	5	6.	7.	8.	9.
0	Eng. In					ling. In.		. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.
14	0.0818					0.0834		887	0.0841	0.0845	0.0849	0.0853
15	0.0857					0.0878		877	0.0881	0.0885	0.0889	0.0898
16	0.0898					0.0914		918	0.0923	0.0927	0.0931	0.0986
17	0.0940					0.0958		962	0.0967	0.0971	0.0975	0.0980
18	0.0984					0.1002		1007	0.1012	0.1016	0.1021	0.1025
19	0.1030	0.108	0.104	0.10	044	0.1049	0.1	054	0.1059	0.1064	0.1068	0.1078
20	0.1078	0.108	0.108	8 0.10	098	0.1098	0.1	108	0.1108	0.1118	0.1118	0.1123
21	0.1128					0.1148		158	0.1159	0.1164	0.1169	0.1174
22	0.1179	0.118	0.119	0 0.1	195	0.1200		206	0.1211	0.1217	0.1222	0.1227
28	0.1233				249	0.1255	0.1	260	0.1266	0.1272	0.1277	0.1288
24	0.1289	0.129	0.130	0.1	806	0.1812	0.1	318	0.1824	0.1329	0.1335	0.1841
25	0.1347	0.185				0.1371		877	0.1388	0.1389	0.1395	0.1401
						_						
26	0.1407	0.141	0.141	9 0.1	126	0.1482	0.1	438	0.1444	0.1450	0.1457	0.1468
27	0.1469	0.147	0.148	2 0.1	488	0.1495	0.1	501	0.1508	0.1514	0.1521	0.1527
28	0.1584	0.154	0.15	7 0.1	558	0.1560	0.1	1567	0.1578	0.1580	0.1587	0.1598
29	0.1600	0.160	0.161	3 0.16	620	0.1627	0.1	634	0.1641	0.1647	0.1654	0.1661
30	0.1668	0.167	0.168	0.10	689	0.1696	0.1	1708	0.1710	0.1717	0.1724	0.1782
31	0.1739	0.174	1	•	760	0.1767	0.1	1775	0.1782	0.1789	0.1796	0.1804
	O.	1.	2.	8		4.		5.	6.	7.	8.	9.

2

Expressed in English Inches of Mercury for Temperatures of Fahrenheit.

Tempera-					Tenths of	l Degrees,			_	
ture of Fabren- helt.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Bug. In. 0.1840	Eng. In. 0.1847	Bug. In.	Eng. In. 0.1861	Eng. In. 0.1869	Eng. In. 0.1876
82 83	0.1811	0.1818 0.1891	0.1825 0.1898	0.1888	0.1918	0.1921	0.1854 0.1928	0.1936	0.1944	0.1951
34	0.1959	0.1967	0.1974	0.1982	0.1990	0.1998	0.1928	0.2013	0.2021	0.2029
85	0.2037	0.2045	0.2053	0.2061	0.2070	0.2077	0.2086	0.2094	0.2102	0.2111
86	0.2119	0.2127	0.2135	0.2144	0.2152	0.2161	0.2169	0.2178	0.2186	0.2195
87	0.2204	0.2212	0.2221	0.2230	0.2288	0.2247	0.2256	0.2265	0.2278	0.2282
88	0.2291	0.2300	0.2309	0.2318	0.2827	0.2836	0.2845	0.2854	0.2864	0.2373
39	0.2382	0.2391	0.2400	0.2410	0.2419	0.2428	0.2438	0.2447	0.2457	0.2466
40	0.2476	0.2485	0.2495	0.2504	0.2514	0.2324	0.2588	0.2548	0.2553	0.2563
41	0.2572	0.2382	0.2592	0.2602	0.2612	0.2622	0.2632	0.2642	0.2652	0.2662
42	0.2672	0.2682	0.2692	0.2702	0.2718	0.2728	0.2783	0.2744	0.2754	0.2764
43	0.2775	0.2785	0.2796	0.2807	0.2817	0.2828	0.2839	0.2850	0.2860	0.2871
44	0.2882	0.2898	0.2904	0.2915	0.2926	0.2937	0.2948	0.2960	0.2971	0.2982
45	0.2998	0.8005	0.8016	0.3028	0.3089	0.3050	0.8062	0.8074	0.3085	0.3097
46	0.8108	0.8120	0.8182	0.8144	0.3156	0.8168	0.3179	0.3191	0.8203	0.8215
47	0.3228	0.3240	0.3252	0.8264	0.8276	0.3289	0.3301	0.8818	0.3826	0.8338
48	0.3331	0.3868	0.3376	0.3888	0.8401	0.8414	0.3426	0.3439	0.3452	0.8465
49	0.8477	0.8490	0.8508	0.3516	0.3529	0.8542	0.3556	0.8569	0.3582	0.8595
50	0.8608	0.3622	0.8685	0.3648	0.3661	0.8675	0.8688	0.8702	0.3715	0.8729
51	0.8748	0.8756	0.8770	0.8784	0.8798	0.8812	0.8826	0.3840	0.8004	V.8000
52	0.3882	0.8896	0.8911	0.8925	0.3939	0.8954	0.3968	0.3983	0.8997	0.4012
53	0.4027	0.4041	0.4056	0.4071	0.4086	0.4101	0.4116	0.4131	0.4146	0.4161
54	0.4176	0.4191	0.4207	0.4222	0.4237	0.4258	0.4268	0.4284	0.4299	0.4315
45	0.4831	0.4846	0.4362	0.4878	0.4394	0.4410	0.4426	0.4442	0.4458	0.4474
56	0.4490	0.4507	0.4528	0.4589	0.4556	0.4572	0.4589	0.4605	0.4622	0.4688
57	0.4655	0.4672	0.4689	0.4705	0.4722	0.4789	0.4756	0.4778	0.4791	0.4808
58	0.4825	0.4842	0.4859	0.4876	0.4894	0.4912	0.4929	0.4947	0.4964	0.4982
59	0.5000	0.5017	0.5035	0.5058	0.5071	0.5089	0.5107	0.5125	0.5148	0.5161
60	0.5179	0.5198	0.5216	0.5234	0.5258	0.5271	0.5290	0.5801	0.5328	0.5846
61	0.5865	0.5384	0.5408	0.5422	0.5441	0.5461	0.5480	0.5499	0.5519	0.5588
62	0.5558		0.5597	0.5617	0.5686	0.000	0.5676		0.5716	
63	0.5756	0.5777	0.5797	0.5817	0.5838	0.5858	0.5879	0.5899	0.5920	0.5941
81	0.5962	0.5983	0.6004	0.6025	0.6046	0.6067	0.6088	0.6109	0.6131	0.6152
65	0.6178	0.6195	0.6217	0.6238	0.6260	0.6282	0.6804	0.6325	0.8347	0.6869
66	0.6392	0.6414	0.6486	0.6458	0.6481	0.6508	0.6525	0.6548	0.6571	0.6593
67	0.6616	0.6689	0.6662	0.6685	0.6708	0.6781	0.6754	0.6777	0.6800	0.6824
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Expressed in English Inches of Mercury for Temperatures of Farrenheir.

Tempera-					Tenths of	f Degrees.				
ture of Fahren- heit.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
•	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Rog. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Bog. In.
68	0.6347	0.6870	0.6894	0.6917	0.6941	0.6965	0.6989	0.7012	0.7086	0.7060
69	0.7084	0.7108	0.7133	0.7157	0.7181	0.7206	0.7230	0.7255	0.7280	0.7305
70	0.7329	0.7854	0.7879	0.7405	0.7480	0.7455	0.7480	0.7506	0.7581	0.7557
71	0.7583	0.7609	0.7634	0.7660	0.7686	0.7712	0.7789	0.7765	0.7791	0.7818
72	0.7844	0.7871	0.7897	0.7924	0.7951	0.7 97 8	0.8005	0.8082	0.8059	0.8086
73	0.8113	0.8141	0.8166	0.8196	0.8228	0.8251	0.8279	0.8807	0.8335	0.8868
74	0.8391	0.8419	0.8447	0.8476	0.8504	0.8533	0.8561	0.8590	0.8619	0.8648
75	0.8676	0.8703	0.8735	0.8764	0.8798	0.8822	0.8852	0.8881	0.9911	0.8940
76	0.8970	0-9000	0.9030	0.9060	0.9090	0.9120	0.9150	0.9180	0.9211	0.9241
77	0.9272	0.9302	0.9283	0.9364	0.9395	0.9426	0.9457	0.9488	0.9519	0.9550
78	0.9582	0.9618	0.9645	0.9677	0.9709	0.9740	0.9778	0.9805	0.9837	0.9869
79	0.9902	0.9934	0.9967	1.0000	1.0088	1.0065	1.0099	1.0182	1.0165	1.0198
80	1.0232	1.0265	1.0299	1.0332	1.0366	1.0400	1.0484	1.0463	1.0508	1.0587
81	1.0572	1.0606	1.0641	1.0675	1.0710	1.0745	1.0780	1.0815	1.0851	1.0686
82	1.0922	1.0957	1.0998	1.1028	1.1064	1.1100	1.1186	1.1172	1.1209	1.1245
83	1.1281	1.1316	1.1854	1.1891	1.1428	1.1465	1.1502	1.1589	1.1576	1.1614
84	1.1651	1.1689	1.1726	1.1764	1.1802	1.1840	1.1878	1.1916	1.1954	1.1998
85	1.2031	1.2070	1.2108	1.2147	1.2186	1.2225	1.2264	1.2808	1.2842	1.2881
86	1.2421	1.2460	1.2500	1.2540	1.2580	1.2620	1.2660	1.2700	1.2740	1.2781
87	1.2821	1.2862	1.2903	1.2944	1.2985	1.3026	1.2068	1.8109	1.3151	1.8192
88	1.3234	1.8276	1.8818	1.8361	1.8408	1.8445	1.8488	1.8531	1.8578	1.3616
89	1.3659	1.3703	1.8746	1.3789	1.3833	1.8877	1.3920	1.8964	1.4008	1.4058
90	1.4097	1.4141	1.4186	1.4230	1.4275	1.4820	1.4865	1.4410	1.4456	1.4501
91	1.4546	1.4592	1.4638	1.4684	1.4780	1.4776	1.4822	1.4869	1.4915	1.4962
92	1.5008	1.5055	1.5102	1.5149	1.5197	1.5244	1.5291	1.5839	1.5887	1.5435
93	1.5482	1.5581	1.5579	1.5627	1.5676	1.5724	1.5778	1.5822	1.5871	1.5920
94	1.5969	1.6018	1.6068	1.6117	1.6167	1.6217	1.6267	1.6817	1.6367	1.6417
95	1.6468	1.6518	1.6569	1.6620	1.6671	1.6722	1.6778	1.6825	1.6876	1.6928
96	1.6980	1.7082	1.7084	1.7137	1.7189	1.7242	1.7295	1.7848	1.7401	1.7454
97	1.7508	1.7561	1.7615	1.7669	1.7723	1.7777	1.7881	1.7886	1.7940	1.7995
98	1.8050	1.8105	1.8160	1.8215	1.8271	1.8827	1.8882	1.8438	1.8494	1.8551
99	1.8607	1.8664	1.8720	1.8777	1.8884	1.8891	1.8949	1.9006	1.9064	1.9121
100	1.9179	1.9237				1.9471				1.9707
101	1.9766	1.9826		1.9945		2.0065		2.0186	2.0247	2.0307
102	2.0368	2.0429	2.0490			2.0675		2.0798	2.0861	2.0923
103	2.0985	2.1048	2.1110	2.1178		2.1299	2.0787	2.1426	2.1489	2.1553
104	2.1617	2.1681	2.1745	2.1810	2.1874	2.1289	2.2004	2.1420	2.2185	2.2200
	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.

VII.

PSYCHROMETRICAL TABLES,

GIVING, IN ENGLISH INCHES OF MERCURY, THE ELASTIC FORCE OF VAPOR CONTAINED IN THE AIR, AND ITS BELATIVE HUMIDITY IN HUNDREDTHS;

DERIVED FROM THE INDICATIONS OF THE WET AND DRY BULB THERMOMETERS,
IN DEGREES OF FAHRENHEIT.

By A. GUYOT.*

M. V. REGNAULT, in his Etudes sur l'Hygrométrie Annales de Chimie et de Physique, 3^{mp} série, Tom. XV. p. 129, after having discussed the theoretical bases of the psychrometric formula given by August, and modified the numerical values of some of its coefficients, adopts the formula

$$x = f - \frac{0.480 (t - t')}{610 - t'} h$$

for temperatures above the freezing-point; and when the temperature of the wet thermometer is below the freezing-point, the bulb being covered with a film of ice,

$$x = f - \frac{0.480 (t - t')}{689 - t'} h$$

^{*} While this table was going through the press, a similar one, prepared by Prof. T. H. Coffin for his private use, was published by the Smithsonian Institution, in order to meet an urgent demand from many quarters. Being based on the same formula, it gives the same results, except, perhaps, in degrees below 14° Fahrenheit, where the tables show slight discrepancies. These unimportant differences arise from the fact that Prof. Coffin's table was computed from Regnault's tensions, as given in the first edition of this collection, while the author's table is based on the table of tensions as given in this second edition, in which the values below 14° Fahrenheit have been somewhat modified, for reasons given above. The following table gives also the relative humidity with one more decimal, which makes the interpolations more easy; and a column of differences for finding the values for fractions of t'. A table for reducing the results to another barometric height is added at the end of the table.

in which

x represents the force of vapor in the air at the time of the observation;

t, the temperature of the air in Centigrade degrees, indicated by the dry thermometer;

t', the temperature of evaporation given by the wet thermometer;

f, the force of vapor in a saturated air at the temperature t';

h, the height of the barometer.

Substituting the Fahrenheit scale for the Centigrade, the formula, for temperatures above the freezing-point, reads

$$x = f - \frac{0.480 \times \frac{1}{6}(t - t')}{610 - \frac{1}{4}(t' - 32^{\circ})} h = f - \frac{0.480(t - t')}{1130 - t'} h;$$

and below the freezing-point,

$$x = f - \frac{0.480 \times \frac{1}{2} (t - t')}{689 - \frac{1}{4} (t' - 32^{\circ})} h = f - \frac{0.480 (t - t')}{1240.2 - t'} h.$$

Making, further, h = 29.7 English inches, these formulæ become

$$x = f - \frac{0.480 (t - t')}{1130 - t'}$$
 29.7 = $f - \frac{14.256 (t - t')}{1130 - t'}$

and

$$x = f - \frac{0.480 (t - t')}{1240.2 - t'} 29.7 = f - \frac{14.256 (t - t')}{1240.2 - t'}.$$

The mean barometric pressure for which the table has been computed, viz. 29.7 inches, is, within a small fraction, the same as that adopted in Haeghens's Tables, No. II., which is 755 millimetres = 29.725 Eng. inches. As that slight difference in the barometric pressure cannot cause, in the most extreme cases, a difference exceeding two thousandths of an inch in the elastic forces, the results in the two tables may be considered identical.

That barometric pressure, corresponding, in our latitudes, to a mean altitude of 250 to 300 feet above the sea, is likely to suit, without correction, the largest number of meteorological stations. Should the mean height of the barometer, in consequence of the elevation of the station, much differ from that adopted in the table, a constant correction can be determined, to be applied to the numbers in the table. At the end, page 72, will be found a table which furnishes that correction for barometric heights between 20 and 31 inches, and for values of t - t' between 2° and 26° Fahrenheit.

The effect of the irregular variations of the barometer at the same station can, in most cases, be neglected; for the error due to that cause will scarcely ever exceed those which may arise from the uncertainty of the very elements on which the tables are based.

ARRANGEMENT OF THE TABLES.

The same arrangement as is found in the Psychrometrical for the Centigrade scale has been adopted.

The first column at the left contains the indications of the wet-bulb thermometer, from -31° to 105° Fahrenheit.

The second column gives the differences of the force of vapor for each tenth of a degree, between each two consecutive full degrees in the first column. It enables the observer easily to find the values for the fractions of degrees of the wet thermometer.

The following double columns furnish the forces of vapor and the relative humidity corresponding to each full degree of the wet-bulb thermometer given in the first column in the same horizontal line, and to the difference of the two thermometers, or t-t', found at the head of each column, for every half-degree from 0° to 26°.5. The relative humidity, or the fraction of saturation, is given in hundredths, which is near enough for meteorological purposes; but one decimal more has been added, though separated by a point, in order to facilitate the interpolations.

At the bottom of each page is found the mean difference, for each tenth of a degree, between the forces of vapor on the same line. It gives the means of finding the values for the intermediate differences of t - t', not found in the tables.

USE OF THE TABLES.

Enter the tables with the difference of the two thermometers, or t-t', and the temperature of the wet-bulb thermometer, given by observation.

In the column headed by the observed difference of the thermometer, t-t', and on the horizontal line headed by the observed temperature of the wet thermometer, t', are found the force of vapor, and the relative humidity corresponding to these temperatures.

For the fractions of degrees of the wet thermometer, multiply the decimal fraction by the number placed in the second column between the full degree and the next, and add the product if the temperature is above, and subtract it if it is below zero Fahrenheit.

The intermediate values of t - t' not given in the table are found by subtracting the number in the line at the bottom of the page, multiplied by the number of additional tenths, from the value given in the table. This correction, being always very small, can usually be neglected.

For the relative humidity, interpolations at sight will generally suffice.

Examples.

1. Dry thermometer, $t = 50^{\circ} \text{ F.}$ Wet thermometer, $t' = 43^{\circ} \text{ F.}$ Difference, or $t - t' = 7^{\circ} \text{ F.}$

Page 58, we find for $t-t'=7^{\circ}$ in the third double column, and for $t'=43^{\circ}$ in the first column

Force of vapor in the air = 0.186 inch.
Relative humidity in hundredths = 51

2. Dry thermometer, $t = 88^{\circ}.5$ F.

Wet thermometer, $t' = 76^{\circ}.3$ F.

Difference, $t-t'=12^{\circ}.2$ F.

Page 63, Table gives for t - t' = 12 and $t' = 76^{\circ} = 0.735$ inch.

Add for fraction of t' = 0.3, $0.003 \times 3 = 0.009$

Subtract for fraction of $t - t' = 0^{\circ}.2$, $.0013 \times 2 = -0.003$

Force of vapor in the air = 0.741

Relative humidity = 55

3. Dry thermometer, $t = -4^{\circ}.5 \text{ F}.$

Wet thermometer, $t' = 6^{\circ}.0 \text{ F}.$

Difference, $t-t'=1^{\circ}.5$ F.

Page 50, Table gives for $t - t' = 1^{\circ}.5$ and $t' = -6^{\circ} = 0.016$ inch.

Subtract for fraction of t' = 0.5, $0.0002 \times 5 = -0.001$

Force of vapor in the air = 0.015Relative humidity = 45

49

B

VII. PSYCHROMETRICAL TABLES.

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredthe,

			•	t t', below	•			and Dry Bulb co				·	
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	0 °.	.0	• °.	.5	10	.0	10	.5	90,	.0	20	.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Reia- tive Hu- mid- ity.	Force of Vapor	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0		Eng. In.		Eng. In		Eng. In.		Rng. In.		Eng. In.		Eng. In	
-31	.00003	0.009	100 100	0.008	86.0 89.6					i	l		
-80 -29	.00006	0.010	100	0.004	42.9			l	ŀ				1
-28	.00006	0.010	100	0.005	46.1			ľ			i	l	1
-27	.00006	0.011	100	0.006	49.0						1	1	ŀ
	-00006				3.5.1			ļ		}		•	
-26	00000	0.012	100	0.006	51.8			Ì	l			l	İ
-25	.00007	0.012	100	0.007	54.4]		
-24	.00007	0.018	100	0.008	56.8			•	1		}	1	
-23	.00008	0.014	100	0.008	59.0			1	1		l		
-22	.50003	0.015	100	0.009	61.0							ļ	
	.00008			l						1	ŀ		
-21		0.015	100	0.010	62.6	0.004	26.9		1	l	İ		İ
-20	.00008	0.016	100	0.011	64.2	0.005	80.8			l		1	I
-19	.00008	0.017	100	0.012	65.9	0.006	83.5						1
-18	.00009	0.018	100	0.012	67.5	0.007	86.6	i		l			1
-17	-0001	0.019	100	0.018	69.0	0.008	89.5			İ	•		
	.0001											i	
-16		0.020	100	0.014	70.4	0.009	42.8		•				
-15	.0001	0.021	100	0.015	71.8	0.010	44.9	0.004	19.4			i	
-14	.0001	0.022	100	0.017	73.0	0.011	47.4	0.005	23.0			Ī	
-18	.0001 .0001	0.028	100	0.018	74.8	0.012	49.8	0.007	26.4				
–12	*******	0.024	100	0.019	75.4	0.013	51.9	0.008	29.5				
	.0001												
-11		0.026	100	0.020	76.5	0.014	53.9	0.009	82.5				
-10	-0001	0.027	100	0.021	77.5	0.016	55.7	0.010	35.8	0.005	15.6		
- 9	-0001	0.028	100	0.023	78.5	0.017	57.7	0.012	38.3	0.006	19.1		
- 8	-0001	0.080	100	0.024	79.4	0.018	59.4	0.018	40.6	0.007	22.5		
- 7	-0001	0.031	100	0.026	80.8	0.020	61.1	0.014	48.0	0.009	25.7		
- 6	-0001	0.038	100	0.027	81.1	0.021	62.7	0.016	45.4	0.010	28.4	0.005	12.9
	•0002												
- 5	.0002	0.084		0.029									
- 4	.0003	0.086	100	0.030	82.5	0.025	65.8		ı	0.014	84.5		19.8
- 8	-0002	0.038	100	0.032	83.2	0.026	67.1	0.021	51.7		36.9	0.010	22.9
- 2	.0002	0.039	100	0.034	83.9	0.028	68.3	0.023	58.5	0.017	89.3	0.011	25.8 28.6
- 1 - 0	.0002	0.041	100 100	0.036	84.5 85.0	0.080	69.5 71.0	0.024	55.3 57.0	0.019 0.021	41.6 43.8	0.015	\$1.8
- "		0.040	100	0.038	00.0	0.082	11.0	0.020	01.0	0.021	40.0	0.010	01.0
		Мо	n Hori	sontal Di	Serence	of Force	of Vapo	or for eacl	h 0°.1 =	- 0.0012.			

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

					•			•		bermome ith a File).	
meter	Mean Vertical Difference of Force	●°,	.0	••	.5	10	.0	10	.5	20	.0	90	.5
Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rein- tive Hu- mid- ity.	Force of Vapor.	Reia- tive Hu- mid- ity.	Force of Vapor.	Reia- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity
•		Rog. In.		Eng. In.		Pag. In.		Eng. In.		Eng. In.		Eng. In	
0	0.0003	0.013	100	0.088	85.0	0.032	70.7	0.026	57.0	0.021	48.8	0.015	81.8
1	.0001	0.045	100	0.040	85.6	0.084	71.8	0.028	58.6	0.028	46.0	0.017	38.9
2	.0003	0.047	100	0.042	86.2	0.086	78.0	0.081	60.2	0.025	48.0	0.019	86.
3	.0002	0.050	100	0.044	86.7	0.088	74.0	0.088	61.8	0.027	50.0	0.022	38.
4		0.052	100	0.046	87.2	0.041	75.0	0.035	68.3	0.080	52.0	0.024	41.5
-	.0002			1				1					
5		0.055	100	0.049	87.7	0.048	76.0	0.038	64.7	0.032	58. 8	0.026	43.4
6	.0002	0.057	100	0.051	88.2	0.046	76.9	0.040	66.0	0.034	55.3	0.029	45.2
7	.0003	0.059	100	0.054	88.6	0.048	77.7	0.048	67.1	0.087	56.8	0.031	47.0
8	.0008	0.062	100	0.057	89.0	0.051	78.4	0.045	68.2	0.040	58.2	0.034	48.8
9	.0003	0.065	100	0.059	89.4	0.054	79.1	0.048	69.2	0.048	59.6	0.087	50.8
			l	i i		1							
1	-0003									ŀ			
10	.0008	0.068	100	0.062	89.8	0.057	79.7	0.051	70.1	0.046	61.0	0.040	52.2
11	.0003	0.071	100	0.066	90.1	0.061	80.4	0.054	71.1	0.049	62.3	0.043	58.8
12	-0003	0.073	100	0.069	90.4	0.063	81.0	0.058	72.1	0.052	68.5	0.046	
18	.0004	0.078	100	0.072	90.7	0.067	81.6	0.061	73.0	0.056	61.8	0.050	56.8
14		0.082	100	0.076	91.0	0.071	82.8	0.065	78.9	0.059	65.9	0.054	58.2
	-0004												
15		0.086	100	0.080	91.3	0.074	82.9	0.069	74.8	0.063	67.1	0.057	59.7
16	-0064	0.090	100	0.084	91.6	0.078	88.4	0.073	75.7	0.067	68.2	0.061	61.0
17	-0004	0.094	100	0.038	91.9	0.088	84.0	0.077	76.5	0.071	69.2	0.066	62.8
18	-9004	0.098	100	0.093	92.1	0.087	84.5	0.081	77.2	0.076	70.2	0.070	68.5
19	-0004	0.103	100	0.097	92.4	0.092	85.0	0.086	78.0	0.080	71.2	0.075	64.7
	.0005							1					
20	.0005	0.108	100	0.102	92.6	0.096	85.5	0.091	78.7	0.085	72.1	0.079	65.8
21	-0005	0.113	100	0.107	92.9	0.101	86.0	0.096	79.4	0.090	78.0	0.084	66.9
22	-0005	0.118	100	0.112	93.1	0.107	86.4	0.101	80.0	0.095	73.8	0.099	68.0
28	-0006	0.123	100	0.118	93.3	0.112	86.8	0.106	80.7	0.100	74.6	0.095	68.9
24	-0006	0.129	100	0.128	93.6	0.117	87.2	0.112	81.2	0.106	75.4	0.100	69.9
25		0.135	100	0.129	93.8	0.128	87.6	0.118	81.8	0.112	76.1	0.106	70.7
	-0006												
26		0.141	100	0.185	94.0	0.129	88.0	0.123	82.4	0.117	76-8	0.112	71.6
27	-0006	0.147	100	0.141		0.125				0.124		0.118	72.5
28	-0006	0.158	100	0.148				0.136	88.4		78.2	0.125	78.3
29	.0007	0.160	100	0.154	94.5			0.148	88.9	0.137	78.8	0.181	74.0
80	.0007	0.167	100	0.161	94.7			0.150	84.8		79.4		74.8
31	-0007	0.174	100	0.168	94.8	0.162	89.6	0.157	84.8	0.151	80.0	0.145	75:6
		Nov	n Horis	ontal Dif	ference	of Force	of Vapo	r for eacl	0°.1 =	0.0012.			

Temperature, Fahrenheit. -- Force of Vapor in English Inches. -- Relative Humidity in Hundredtha.

			,		•	fference o esing-Poi		•).	
meter	Mean Vertical Difference of Force	80.	•	8°.	.5	4%	0	40	.5	50.	.0	50	.5
t/ Fabren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rein- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rein- tive Hu- mid- ity.	Force of Vapor.	Role tive Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	
0	0.0003	0.010	19.8	0.004	7.9			l i	ŀ				
1	.0002	0.012	22.8	0.006	11.8			ŀ	l				
2	.0009	0.014	25.8	0.008	14.7					ľ			
8	.0002	0.016	28.1	0.010	17.8								
4		0.018	80.8	0.018	20.9	0.007	11.4						
	.0003		}										
5	1	0.021	88.4	0.015	28.8	0.010	14.6						
6	-0002	0.028	85.6	0.018		0.012	17.5	0.006	9.0				
7	.0001	0.026	87.7	0.020	28.8	0.014	20.2	0.009	12.0				
8	.0003	0.028	39.8	0.028	81.2	0.017	22.9	0.011	15.0				
9	.0008	0.081	41.8	0.026	28.5	0.020	25.5	0.014	17.9	0.009	10.6		
-													
	-0008	1		ŀ									
10	.0008	0.034	43.8	0.029	85.7	0.028	28.0	0.017	20.6	0.012	18.6		
11	.0003	0.087	45.7	0.082	87.9	0.026	80.4	0.020	23.8	0.014	16.4	0.009	9.9
12	-0003	0.041	47.5	0.085	40.0	0.029	82.7	0.024	25.8	0.018	19.2	0.012	12.9
13	-0004	0.044	49.2	0.089	42.0	0.033	85.0	0.027	28.8	0.022	21.9	0.016	15.8
14	1	0.048	50.9	0.042	48.9	0.087	87.1	0.081	80.7	0.025	24.5	0.020	18.4
	-0004		}		1								
15		0.052	52.5	0.046	45.7	0.040	89.2	0.085	82.9	0.029	26.9	0.023	21.5
16	.0004	0.056	54.1	0.050	47.5	0.044	41.2	0.039	85.1	0.033	29.8	0.027	28.7
17	.0004	0.060	55.6	0.054	49.2	0.049	48.1	0.048	87.2	0.037	81.6	0.032	26.2
18	-0004	0.065	57.0	0.059	50.9	0.053	44.9	0.047	39.2	0.042	83.7	0.036	28.5
19	-0004	0.069	58.4	0.068	52.5	0.058	46.7	0.052	41.2	0.046	85.8	0.040	80.7
	l											1 1	
	.0005		1		ļ								
20		0.074	59.8	0.068	54.0	0.062	48.8	0.057	43.0	0.050	87. 8	0.045	82.9
21	.0005	0.079	61.0	0.078	55.4	0.067	50.0	0.062	44.7	0.056	89.7	0.050	84.9
22	.0005	0.084	62.2	0.078	56.8	0.072	51.5	0.067	46.4	0.061	41.5	0.055	86.8
23	.0006	0.089	68.4	0.088	58.1	0.078	52.9	0.072	48.0	0.066	43.8	0.061	38.6
24	.0006	0.095	64.4	0.089	59.8	0.083	54.8	0.077	49.6	0.072	44.9	0.066	40.8
25	.0000	0.100	65.5	0.095	60.5	0.089	55.6	0.068	51.0	0.078	46.5	0.072	42.2
	0006	1 1			1								
00		0.700	66.5	ا ا	Q1 +	0.095	KØ 0	0.089	89 4	0.088	49 0	0.078	48.9
26	-0006	0.106			61.7		56.9 58.2		1	0.090	49.6	0.075	45.5
27	.0006	0.118			62.8		59.4	0.102	55.2	0.096	51.0	0.090	47.0
28	.0007	0.119	68.5	0.118	68.9	0.108	60.6	0.102	56.4	0.108	52.4	0.097	48.6
29 30	-0007	0.126 0.132	69.4 70.3	0.120 0.127	64.9 65.9	0.114 0.121	61.7	0.115	57.7	0.109	58.7	0.104	49.9
81	-0007	0.132	71.2		66.9	0.121	62.8	0.113	58.8	0.116	55.0	0.111	51.5
~		0.100		0.104	00.0	V.120	02.0	0.100	1 23.3		23.3	l	

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

_			•		•			and Dry I					
Web- Bulb Thermo- meter E'	Mean Vertical Difference of Force of Vapor	6 °.	.0	60,	.5	70	.0	70	.5	80,	.0	S °.	.5
Pahron- heit.	for each	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Reia- tive Hu- mid- ity.	Fores of Vapor.	Role- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
•		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Bog. In.		ing In.	
12	0.0008	0.007	6.8					j.		1	1	!	
18	.0004	0.010	9.9 12.8	0.000				1		l			
14	-0004	0.014	15.7	0.008	7.5	0.004				Ī			
15 16	.0004	0.018 0.022	18.4	0.012	10.4 18.8	0.006	5.4 8.4		[I			
1.	.0004	V-UZZ	10.4	0.010	19.5	0.010	0.4			1			
17		0.026	21.0	0.020	16.0	0.015	11.8	0.009	6.7	l	l '		
18	.0004	0.030	23.5	0.025	18.6	0.019	14.0	0.018	9.6	0.008	5.8		
19	.0003	0.085	25.8	0.029	21.2	0.028	16.6	0.018	12.8	0.012	8.2	0.006	4.2
20	.0005	0.040	28.1	0.084	28.5	0.028	19.0	0.022	15.0	0.017	11.0	0.011	7.1
21	.0000	0.044	30.8	0.039	25.8	0.088	21.5	0.027	17.5	0.022	13.5	0.016	9.8
	-0008		İ										
22	.0004	0.050	32.8	0.044	28.0	0.088	23.8	0.082	19.8	0.027	16.0	0.021	12.8
23	.000a	0.055	34.2	0.049	80.1	0.048	26.0	0.088	22.1	0.032	18.4	0.026	14.8
24	.0006	0.060	36.1	0.055	82.1	0.049	28.1	0.048	24.4	0.088	20.7	0.032	17.2
25 26	.0006	0.066	88.0 89.8	0.060	84.0 85.9	0.055	80.2	0.049	26.5 28.6	0.048	28.0 25.1	0.038	19.5
20	.0006	0.072	39.5	0.000	20.9	0.061	82.2	0.055	25.0	0.049	20.1	0.048	21.8
27		0.078	41.5	0.078	37.8	0.067	84.0	0.061	80.6	0.055	27.2	0.050	28.9
28	-0006	0.085	48.2	0.079	39.5	0.078	35.9	0.067	32.5	0.062	29.1	0.056	25.9
29	.0007	0.091	44.8	0.085	41.1	0.060	87.6	0.074	34.2	0.068	\$1.0	0.063	27.9
20	.0007	0.098	46.2	0.092	42.7	0.086	39.2	0.081	25.9	0.075	32 .8	0.069	29.7
31	.0007	0.106	47.6	0.099	44.3	0.098	40.8	0.088	87.5	0.082	84.4	0.076	31.4
		90	.0	90	.5	10	.0	10	.5	110	.0	110	.5
		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	
20	1	0.005	8.4				!						
21	0.0005	0.010	6.1	0.005	2.7	1							
22	.00C5	0.015	8.8	0.010	5.4	0.004	2.2						
23	.0005	0.021	11.4	0.015	8.0	0.009	4.9						
24	.0005	0.026	13.9	0.020	10.6	0.015	7.5	0.009	4.5				
25	-0006	0.032	16.2	0.026	18.1	0.020	10.0	0.015	7.1	0.009	4.2		
_	.0006								_				
26	.0004	0.088	18.5	0.082	15.4	0.026	12.4	0.021	9.5	0.015	6.8	0.009	4.1
27	-0006		1	0.088		0.032		0.027		0.021	9.2		6.5
28	-0007	0.050		0.045	1	0.039					1	0.022	8.8
29	.0007	0.057	24.9		21.9	0.045	19.0	0.040	16.3	0.084	18.7	0.028	11.
30	-0007	0.064	26.7		1	0.052	21.0 22.9	0.046	18.4 20.8	0.041	15.8	0.085	18.8
3 1		0.071	28.5	0.000	25.7	0.008	24.5	0.00%	20.0	0.048	17.8	0.042	15.8
_		Mea	a Hori	ontal Di	Serve	of Force	of Vep	or for eac	P 0-T	- 0.0012.			

PSYCHROMETRICAL TABLES.

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				t-t	, or Di	fierence o	l Wet a	and Dry 1	Balb Th	ermomet	ets.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	●°.	•	●°.	5	10,	0	10	5	90.	.0	20	.5
Fahren- helt.	for each 00.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rein- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Reia- tive Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		ling. In.	
32	0.0007	0.181	100	0.175	94.5	0.168	89.8	0.162	84.1	0.155	79.2	0.149	74.4
88	.0008	0.188 0.196	100	0.182	94.7	0.175	89.5	0.169	84.5	0.162	79.7 80.2	0.156 0.16 3	75.0
84 85	.0008	0.204	100	0.189	94.8	0.188 0.191	89.8 90.0	0.176 0.184	84.9 85.8	0.170	80.7	0.103	75.6 76.2
36	.0008	0.212	100	0.205	95.0	0.191	90.8	0.192	85.6	0.186	81.1	0.179	76.8
	.0009	0.212	100	0.200	55.5	0.133	50.0	0.102	00.0	0.200	J	0.1.0	
87	.0009	0.220	100	0.214	95.2	0.207	90.5	0.201	86.0	0.194	81.6	0.188	77.8
38	.0009	0.229	100	0.228	95.8	0.216	90.7	0.210	86.8	0.208	82.0	0.196	77.9
\$9	.0009	0.288	100	0.282	95.4	0.225	91.0	0.219	86.6	0.212	82.4	0.206	78.4
40	-0010	0.248	100	0.241	95.5	0.285	91.2	0.228	86.9	0.221	82.9	0.215	78.9
41	-0010	0.257	100	0.251	95.6	0.244	91.4	0.288	87.8	0.281	83.3	0.224	79.4
42		0.267	100	0.260	95.7	0.254	91.6	0.247	87.5	0.241	88.6	0.284	79.8
48	-0010	0.278	100	0.271	95.8	0.264	91.8	0.258	87.8	0.251	84.0	0.245	80.8
44	.0011	0.288	100	0.282	95.9	0.275	92.0	0.268	88.1	0.262	84.8	0.255	80.7
45	-0011	0.299	100	0.298	96.0	0.286	92.1	0.280	88.3	0.278	84.7	0.266	81-1
46	.0013	0.811	100	0.804	96.1	0.297	92.8	0.291	88.6	0.284	85.0	0.278	81.5
47	10019	0.828	100	0.816	96.2	0.310	92.5	0.303	88.8	0.297	85.8	0.290	81.9
48	.0018	0.835	100	0.329	96.2	0.822	92.6	0.815	89.0	0.809	85.6	0.802	82.2
49	.0013	0.848	100	0.841	96.8	0.885	92.7	0.328	89.8	0.821	85.9	0.815	82.6
50	.0018	0.861 0.874	100	0.854	96.4	0.348	92.9	0.841	89.5	0.848	86.1 86.4	0.328 0.341	82.9 83.2
51	.0014	V-0/-	100	0.868	96.5	0.361	98.0	0.854	89.7	0.648	50.4	0.541	08.2
52		0.388	100	0.382	96.5	0.875	98.2	0.869	89.9	0.862	86.7	0.855	88.6
53	.0014	0.403	100	0.896	96-6	0.389	93.8	0.383	90.1	0.876	86.9	0.870	88.9
54	-0015	0.418	100	0.411	96.7	0.404	93.4	0.398	90.2	0.391	87.2	0.885	84.2
55	.0015	0.438	100	0.426	96.7	0.420	98.5	0.418	90.4	0.407	87.4	0.400	84.4
56	.0016	0.449	100	0.442	96.8	0.486	93.6	0.429	90.6	0.422	87.6	0.416	84.7
57	.0017	0.466	100	0.459	96.8	0.452	93.7	0.446	90.7	0.489	87.8	0.432	85.0
58	-0017	0.482	100	0.476	96.9	0.469	98.9	0.468	90.9	0.456	88.0	0.449	85.2
59	0018	0.500 0.518	100	0.498	96.9	0.487	94.0	0.480	91.0	0.478	88.2	0.467 0.495	85.5 85.7
60 61	-0019	0.537	100	0.511	97.0 97.0	0.505	94.1 94.2	0.498	91.2 91.3	0.491	88.4 88.6	0.458	85.9
91	.0019	0.007	100	0.000	91.0	0.028	74.3	0.317	41.2	0.010	99.0	V.JU3	G#-8
62	20019	0.556	100	0.549	97.1	0.542	94.2	0.586	91.5	0.529	88.8	0.522	86.2
68	.0020	0.576	100	0.569	1	•	ı	0.556		0.549	89.0	0.542	86.4
64	.0090	0.596	100	0.589				0.576	91.7		89.1		86.6
65	.0031	0-617	100	0.611		0.604		•		0.591		0.584	86-8
66	.0022	0.639	100	0.638	97.8	0.626	94.6	0.619	92.0	0.612		0.606	87.0
67	******	0.662	100	0.655	97.8	0.648	94.7	0.642	92.1	0.685	89.6	0.628	87.2
		Mee	n Hori	ontal Di	Serence	of Force	of Vapo	or for eac	h 00.1	- 0.001 8 .			<u> </u>

Temperature, Fahrenheit. — Force of Vapor in English Inches — Relative Humidity in Hundredths.

				1-1	', or Di	Янгерое (of Wet	and Dry	Bulb Ti	hermoene	ters.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	● °.	•	⊕ ∘,	.5	10	.0	10.	.5	90	.0	90	.5
Pahren- heit.	for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
•		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	_	Eng In.	
6 8	0.0023	0.685	100	0.678	97.8	0.671	94.7	0.668	92.2	0.658	89.8	0.651	87.8
69	.0014	0.708	100	0.702	97.4	0.695	94.8	0.688	92.3	0.682	89.9	0.675	87.5
70	.0025	0.788	100	0.726	97.4	0.720	94.9	0.718	92.4	0.706	90.0	0.699	87.7
71	.0026	0.759	100	0.752	97.5	0.745	95.0	0.738	92.5	0.781	90.2	0.725	87.9
72	.0027	0.784	100	0.778	97.5	0.771	95.0	0.764	92.7	0.757	90.8	0.751	88.0
73		0.811	100	0.805	97.5	0.798	95.1	0.791	92.7	0.784	90.4	0.778	88.2
74	-0028	0.889	100	0.882	97.6	0.826	95.2	0.919	92.8	0.812	90.6	0.805	88.8
75	.0028	0.868	100	0.861	97.6	0.854	95.2	0.847	92.9	0.841	90.7	0.884	88.5
78		0.897	100	0.890	97.6	0.888	95.8	0.877	93.0	0.870	90.8	0.868	88.6
77	.0030	0.927	100	0.920	97.7	0.914	95.4	0.907	93.1	0.900	90.9	0.898	88.8
	-0011					1		ì			ł		
78	.0082	0.958	100	0.951	97.7	0.945	95.4	0.938	98.2	0.931	91.0	0.924	88.9
79	.0033	0.990	100	0.988	97.7	0.977	95.5	0.970	98.3	0.968	91.1	0.956	89.0
80	.0084	1.023	100	1.016	97.7	1.010	95.5	1.008	98.4	0.996	91.2	0.989	89.2
81	.0035	1.057	100	1.050	97.8	1.044	95.6	1.037	93.4	1.080	91.8	1.023	89.8
82	.0036	1.092	100	1.085	97.8	1.079	95.6	1.072	93.5	1.065	91.4	1.058	89.4
83	.0030	1.128	100	1.121	97.8	1.115	95.7	1.108	98.6	1.101	91.5	1.094	89.5
84	.0037	1.165	100	1.158	97.8	1.152	95.7	1.145	98.6	1.188	91.6	1.181	89.6
85	.0038	1.208	100	1.196	97.9	1.189	95.8	1.188	98.7	1.176	91.7	1.169	89.7
86	.0039	1.242	100	1.285	97.9	1.228	95.8	1.222	98.8	1.215	91.8	1.208	89.8
87	.0040	1.282	100	1.275	97.9	1.268	95.9	1.268	98.8	1.256	91.9	1.249	90.0
	.0041												
88	.0042	1.328	100	1.817	97.9	1.810	95.9	1.808	98.9	1.296	92.0	1.289	90.1
89	.0044	1.366	100	1.359	97.9	1.352	95.9	1.845	94.0	1.839	92.0	1.882	90.2
90	.0044	1.410	100	1.403	98.0	1.396	96.0	1.389	94.0	1.382	92.1	1.875	90.3
91	.0046	1.455	100	1.448	98.0	1.441	96.0	1.484	94.1	1.427	92.2	1.420	90.8
92		1.501	100	1.494	98.0	1.487	96.1	1.480	94.1	1.478	92.8	1.466	90.4
92	-0048	1.548	100	1.541	98.0	1.585	96.1	1.528	94.2	1.521	92.4	1.514	90.5
94	.0049	1.597	100	1.590	98.1	1.588	96.1	1.576	94.3	1.569	92.4	1.562	90.6
95	-0050	1.647	100	1.640	98.1	1.633	96.2	1.626	94.8	1.619	92.5	1.612	90.7
96	.0081	1.698	100	1.691	98.1	1.684	96.2	1.677	94.4	1.670	92.6	1.664	90.8
97	.0048	1.751	100	1.744	98.1	1.739	96.2	1.780	94.4	1.728	92.6	1.716	90.9
98	.0084	1.805	100	1.798	98.1	1.791	96.8	1.784	94.5	1.777	92.7	1.770	90.9
	.0056							1					
99		1.861	100	1.854	98.1	1.847	96.3			1.833		1.826	91.0
100	.0087 .0089	1.918	100	1.911	98.2		96.3	1.897	94.6	1.890	92.8	1.888	91.1
101	-0060	1.977	100	1.970	98.2		96.4	1	94.6	1.949	92.9	1.942	91.2
102	-0000	2.037	100	2.080	98.2	2.028	96.4	2.016	94.7	2.009	92.9	2.002	91.2
108	.0063	2.098	100	2.092	98.2		96.4	2.078	94.7	2.071	98.0	2.064	91.8
104	1	2.162	100	2.155	98.2	2.148	96.5	2.141	94.7	2.184	98.1	2.127	91.4
	•			mtal Diff				<u> </u>		<u>'</u>		,	

Temperature, Fahrenheit. -- Force of Vapor in English Inches. -- Relative Humidity in Hundredths.

				t -	t', or D	ifference	of Wet	and Dry	Bulb T	hermome	iters.		
Wet- Bulb Thermo- meter t'	of Force of Vapor	30,	.0	80	.5	40	.0	40.	.5	50	.0	50	.5
Fahren- heit.	for each 0°.1	Force of Vapor.	Rela- tive Hu- mid- ity	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rein- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mkd- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In,		Eng. In.	
82	0.0007	0.142	69.8	0.186	65.8	0.129	61.0	0.123	56.8	0.116	52.7	0.110	48.8
83	.0007	0.149	70.5	0.148	66.1	0.186	61.9	0.180	57.7	0.123	53.7	0.117	80.0
84 85	.0008	0.157 0.165	71.2 71.9	0.150	66.9	0.144	62.8 63.6	0.187	58.6 59.5	0.181	54.7	0.124	51.2 52.3
86	.0008	0.100	72.6	0.158 0.166	67.7 68.5	0.160	64.5	0.145	60.5	0.139 0.147	53.7 56.7	0.132	58.4
30	.0008	0.176	12.0	0.100	00.0	0.100	04.0	0.133	00.5	0.147	00.7	0.140	00.2
87	-0009	0.181	78.2	0.175	69.2	0.168	65.3	0.162	61.4	0.155	57.7	0.149	54.5
28	.0009	0.190	73.8	0.188	69.9	0.177	66.1	0.170	62.3	0.164	58.7	0.157	55.5
89	•0010	0.199	74.4	0.192	70.6	0.186	66.9	0.179	63.2	0.178	59.7	0.166	56.5
40	.0010	0.208	75.0	0.202	71.8	0.195	67.7	0.189	64.1	0.182	60.7	0.176	57.5
41		0.218	75.6	0.211	72.0	0.205	68.4	0.198	65.0	0.192	61.7	0.185	58.5
42	-0010	0.228	76.2	0.221	72.6	0.215	69.1	0.208	65.7	0.202	62.4	0.195	59.4
43	-0010	0.238	76.7	0.221	78.2	0.215	69.8	0.219	66.3	0.202	68.1	0.195	60.2
44	-0011	0.249	77.2	0.242	78.7	0.236	70.4	0.229	67.0	0.228	63.8	0.216	61.1
45	-0011	0.260	77.7	0.258	74.8	0.247	71.0	0.240	67.6	0.284	64.6	0.227	61.8
46	-0011	0.271	78.1	0.265	74.8	0.258	71.6	0.252	68.8	0.245	65.3	0.288	62.6
	-0012				ì								
47	-0018	0.283	78.6	0.277	75.8	0.270	72.2	0.264	68.9	0.257	66.0	0.250	63.3
48	-0018	0.296	79.0	0.289	75.8	0.282	72.7	0.276	69.6	0.269	66.7	0.268	64.0
49	-0018	0.308	79.4	0.302	76.3	0.295	73.8	0.288	70.2	0.282	67.4	0.275	64.7
50	.0018	0.321 0.835	79.8 80.2	0.315	76.7	0.308	78.8	0.801	70.9	0.295	68.1 68.7	0.288	65.4 66.0
51	-0014	0.880	80.2	0.328	77.2	0.321	74.3	0.815	71.4	0.808	00.7	0.302	00.0
52		0.849	80.5	0.342	77.6	0.335	74.7	0.329	71.9	0.322	69.2	0.815	66.6
53	.0014	0.863	80.9	0.856	78.0	0.850	75.2	0.848	72.5	0.886	69.8	0.830	67.2
54	-0013	0.378	81.2	0.371	78.4	0.365	75.6	0.858	72.9	0.851	70.3	0.845	67.8
55	-0018 -0016	0.398	81.6	0.387	78.8	0.880	76.1	0.378	78.4	0.367	70.8	0.360	68.3
56		0.409	81.9	0.408	79.1	0.896	76.5	0.889	73.9	0.888	71.8	0.376	68.9
F-7	-0016	0.400	00.0	0 410	WD #	0.710	70 O	0.406	71.0	0 200	71.0	0.892	69.4
57 58	. 0017	0.426 0.443	82.2 82.5	0.419 0.436	79.5 79.8	0.412	76.9 77.2	0.423	74.8 74.8	0.399	71.8 72.3	0.409	69.9
59	.0017	0.443	82.8	0.458	80.2	0.429	77.6	0.440	75.1	0.410	72.7	0.427	70.8
60	-0018	0.478	88.1	0.471	80.5	0.465	78.0	0.458	75.5	0.451	73.1	0.445	70.8
61	-0019	0.497	83.3	0.490	80.8	0.488	78.3	0.477	75.9	0.470	78.5	0.468	71.8
1	.0019												
62	.0090	0.516	83.6	0.509	81.1	0.502	78.6	0.496	76.8	0.489	74.0	0.482	71.7
63	.0020	0.536	i	•		0.522				0.509	1	0.502	72.1
64	-0021	0.556	84.1	1	81.7		79.8	0.536	77.0	0.529	74.7	0.528	72.5
65	.0022	0.577	84.8	1	81.9		79.6	0.557	77.8		1	0.544	72.9
66 67	.0028	0.599	84.6	li .	82.2 82.4		79.9	0.579	77.6	0.572	75.4 75.8	0.566 0.588	78.8 73.7
97		0.622	84.8	0.615	02.4	0.608	80.2	0.601	78.0	0.595	10.5	0.030	10.1
		Ме	n Hori	sontal Di	ference	of Force	of Vap	or for eac	b 0°.1	- 0.0018.		•	

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Temy.cature, Februhelt. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				tt	', or Di	fference (el Wet	and Dry	Bulb Ti	ormomet	lers.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	8 °.	.0	8°.	.5	40.	.0	40.	.5	5 °.	.0	50,	.5
Fahren- heit	for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Reia- tive Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	
68	0.0024	0.644	85.0	0.638	82.7	0.631	80.4	0.624	78.8	0.618	76.1	0.611	74.0
69	.0024	0.668	85.2	0.661	82.9	0.655	80.7	0.648	78.6	0.641	76.4	0.635	74.4
70	.0025	0.693	85.4	0.686	88.2	0.679	81.0	0.672	78.8	0.666	76.8	0.659	74.7
71	.00±6	0.718	85.6	0.711	88.4	0.704	81.2	0.698	79.1	0.691	77.1	0.681	75.1
72		0.744	85.8	0.737	88.6	0.781	81.5	0.724	79.4	0.718	77.4	0.710	75.4
73	.0037	0.771	86.0	0.764	88.8	0.757	81.7	0.751	79.7	0.744	77.6	0.737	75.7
7.1	-00-58	0.799	86.2	0.792	84.0	0.785	81.9	0.778	79.9	0.772	77.9	0.765	76.0
75	-0028	0.827	86.3	0.820	84.2	0.814	82.2	0.807	80.2	0.800	78.2	0.793	76.3
76	.0029	0.856	86.5	0.850	84.4	0.848	82.4	0.836	80.4	0.829	78.4	0.828	76.6
77	-0030	0.887	86.7	0.880	84.6	0.878	82.6	0.866	80.6	0.860	78.7	0.853	76.8
1	.0081												
78	.0032	0.918	86.8	0.911	84.8	0.904	82.8	0.897	80.8	0.890	78.9	0.884	77.1
79	.0032	0.949	87.0	0.943	85.0	0.936	83.0	0.929	81.1	0.922	79.2	0.916	77.4
80	.0034	0.982	87.1	0.976	85.1	0.969	88.2	0.962	81.3	0.955	79.4	0.949	77.6
81	.0034	1.016	87.3	1.010	85.3	1.008	88.4	0.996	81.5	0.989	79.7	0.982	77.9
82	20000	1.051	87.4	1.045	85.5	1.038	88.6	1.031	81.7	1.024	79.9	1.017	78.1
	.0036												-0.0
83	-0037	1.097	87.5	1.080	85.6	1.074	83.7	1.067	81.9	1.060	80.1	1.053	78.8
84	-0038	1.124	87.7	1.117	85.8	1.111	88.9	1.104	82.1	1.096	80.3	1.090	78.5
85	.0039	1.162	87.8	1.155	85.9	1.148	84.1	1.142	82.8	1.185	80.5	1.128	78.8 79.0
86	-0040	1.201	87.9	1.194	86.1	1.187	84.2	1.181	82.4	1.174	80.7 80.9	1.167 1.208	79.0
87		1.242	88.1	1.235	86.2	1.228	84.4	1.222	82.6	1.215	80.9	1.206	19.2
88	.0041	1.282	88.2	1.276	86.3	1.269	84.6	1.262	82.8	1.255	81.1	1.248	79.4
89	.0042	1.325	88.3	1.818	86.5	1.311	84.7	1.804	88.0	1.297	81.8	1.291	79.6
90	.0044	1.369	88.4	1.362	86.6	1.355	84.9	1.348	88.1	1.841	81.4	1.384	79.8
91	-0012	1.413	88.5	1.407	86.7	1.400	85.0	1.398	88.8	1.886	81.6	1.379	80.0
92	.0046	1.460	88.6	1.453	86.9	1.446	85.1	1.489	88.4	1.482	81.8	1.425	80.2
	-0047												
93		1.507	88.7	1.500	87.0	1.493	85.8	1.486	83.6	1.480	82.0	1.473	80.8
91	.0019	1.556	88.8	1.549	87.1	1.542	85.4	1.535	88.8	1.528	82.1	1.521	80.5
95	.0050	1.606	88.9	1.599	87.2	1.592	85.5	1.585	88.9	1.578	82.3	1.571	80.7
96	.0051	1.657	89.0	1.650	87.8	1.648	85.7	1.636	84.0	1.629	82.4	1.622	80.9
97	-0052	1.709	89.1	1.702	87.5	1.696	85.8	1.688	84.2	1.682	82.6	1.675	81.0
98	-0091	1.764	89.2	1.757	87.6	1.750	85.9	1.743	81.8	1.786	82.7	1.729	81.2
	.0058		00.0			,	00.0	1 200	04.4	1 500	00.0	,	01 0
99	.0057	1.819		1.812		1.805		1.798	84.4		ł	1.785	81.8 81.5
100	.0048	1.876	89.4	1.869	87.8	1.863	86.2	1.856	84.6		83.0		81.6
101	.0060	1.935	89.5	1.928	87.9	1.921	86.3	1.914	84.7	1.907	83.2 83.3	1.900 1.961	81.8
102	-0062	1.995	89.6	1.988	88.0	1.981 2.048	86.4	1.974 2.036	84.8	1.967 2.029	88.4	2.022	81.9
103	.0063	2.057	89.7	2.050 2.118	88.1	2.106	86.5 86.6	2.099	84.9 85.1	2.029	83.5		82.1
104		2.120	89.8	4-110	88.2	2.100	00.0	2.000	00.1	2.082	00.0	1 2.500	,
		Me	an Hori	sontal Di	ference	of Force	of Vap	or for eac	ь 0°.1	- 0.0018.			

Temperature, Fahrenheit - Force of Vapor in English Inches. - Relative Humidity in Hundredths

_				t —1	l', or Di	iSerence (e Wet	and Dry l	Balb Ti	ermome	locs.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	6°.	0	60.	5	3 ℃	.0	70.	.5	8°.	.0	80	.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity	Force of Vapor.	Rain- tive Hu- mid- ity.	Force of Vapor.	Rele- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
•		Eng. In.		Eng. In.		Eng. ln.		Eng. In.		Eng. In,		Eng. In,	
82	0.0007	0.103	45.0	0.097	41.4	0.090	37.9	0.084	84.5	0.077	81.2	0.071	28.0
83	.0007	0.110	46.8	0.104	42.7	0.097	89.8	0.091	36.0	0.084	32.8	0.078	29.6
84	.0008	0.118	47.6	0.111	44.1	0.105	40.7	0.098	87.4	0.092	84.3	0.085	31.2
85	.0008	0.126	48.8	0.119	45.8	0.118	42.0	0.106	88.8	0.100	85.7	0.098	32.
86	.0009	0.184	50.0	0.127	46.6	0.121	48.3	0.114	40.2	0.108	87.2	0.101	847
87		0.142	51.1	0.136	47.8	0.129	44.6	0.128	41.6	0.116	88.6	0.109	35.
88	-0009	0.151	52.2	0.144	49.0	0.138	45.9	0.181	12.9	0.125	40.0	0.118	87.
89	.0009	0.160	58.8	0.153	50.1	0.147	47.1	0.140	44.1	0.184	41.3	0.127	38.
40	.0009	0.169	54.3	0.163	51.3	0.156	48.8	0.149	45.4	0.148	42.6	0.186	89.
41	•0010	0.179	55.4	0.172	52.8	0.166	49.4	0.159	46.6	0.158	48.9	0.146	41.
	.0010	İ		1									
42	50010	0.189	56.8	0.182	58.4	0.175	50.5	0.169	47.7	0.162	45.0	0.156	42.
43	.0011	0.199	57.2	0.192	21.8	0.186	51.5	0.179	48.8	0.178	46.1	0.166	48.0
44	.0011	0.209	58.1	0.203	55.8	0.196	52.5	0.190	49.8	0.188	47.2	0.177	44.7
45	.0011	0.220	59.0	0.214	56.2	0.207	53.5	0.201	50.8	0.194	48.3	0.188	45.8
46	1	0.232	59.8	0.225	57.0	0.219	54.4	0.212	51.8	0.206	49.8	0.198	46.
47	.0012		00.0	0.000	E		55.2	0.224	F0 =	0.010	50.2	A 811	480 1
48	-0012	0.244	60.6	0.237	57.9 58.7	0.281	56.1	0.224	52.7	0.217	51.2	0.211 0.228	48.
49	.0013	0.269	61.3 62.0	0.249	59.4	0.248	56.9	0.249	53.6 54.5	0.230	52.1	0.228	49.
50	.0013	0.282	62.7	0.202	60.2	0.268	57.7	0.262	55.8	0.242	52.9	0.249	50.
51	-0018	0.282	63.4	0.275	60.9	0.282	58.4	0.275	56.1	0.269	58.7	0.262	51.
•1	.0014	0.295	05.4	0.200	60.9	U.282	00.4	0.275	50.1	U.208	00.7	0.202	D1.4
52	.0014	0.309	64.1	0.802	61.6	0.296	59.2	0.289	56.8	0.282	54.6	0.276	52.8
58	.0014	0.328	64.7	0.317	62.3	0.810	59.9	0.308	57.6	0.297	55.8	0.290	53.2
54	9100	0.338	65.3	0.332	62.9	0.825	60.6	0.318	58.3	0.812	56.1	0.305	58.
55	.0015	0.854	65.9	0.847	63.5	0.840	61.2	0.884	59.0	0.827	56.8	0.820	54.5
56	.0016	0.869	66.5	0.868	64.1	0.856	61.9	0.849	59.7	0.848	57.5	0.836	55
_	-0017		l	l									
57	-0017	0.886	67.0	0.879	64.7	0.373	62.5	0.866	60.8	0.859	58.2	0.353	56.1
58	.0017	0.403	67.5	0.396	65.3	0.889	63.1	0.888	60.9	0.376	58.8	0.869	56.8
59	-0017 -0018	0.420	68.0	0.413	65.8	0.407	68.6	0.400	61.5	0.893	59.5	0.887	57.
60	.0018	0.488	68.5	0.481	66.3	0.425	64.2	0.418	62.1	0.411	60.1	0.405	58.
61		0.457	69.0	0.450	66.9	0.448	64.7	0.486	62.7	0.480	60.7	0.428	58.
62	-0019	0.476	69.5	0.469	67.4	0.462	65.3	0.456	68.2	0.449	61.3	0.442	59.
68	.0020	0.495	70.0	0.489	67.8	0.482	65.8	0.475	68.8	0.469	61.8	0.462	59.
61	.0021	0.516	70.4	0.509	69.3	0.503	66.8	0.496	64.8	0.489	62.4	0.488	60.
65	.0021	0.537	70.8	0.580	68.8	0.524	66.8	0.517	64.8	0.510	62.9	0.504	61.0
66	.0022	0.559	71.2	0.552	69.2	0.545	67.2	0.589	65.8	0.582	63.4	0.525	61.
67	.0028	0.581	71.6	0.575	69.6	0.568	67.7	0.561	65.7	0.554	68.9	0.549	62.
			1 -1.5	1	23.3					1	55.5	1	

Temperature, Fahrenheit. -- Force of Vapor in English Inches -- Relative Humidity in Hundredths.

				t-t	, or Di	flerence o	(Wot s	and Dry	Balb Ti	oermome(iers.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	€0.	.0	6 °.	.5	70	.0	70	.5	80	.0	80	.5
Fahren- helt.	for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rein- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rein- tive Hu- mid- ity	Force of Vapor.	Relative Hu- mid- ity.
ō		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng In.	
68	0.0094	0.604	72.0	0.597	70.0	0.591	68.1	0.584	66.2	0.577	64.4	0.571	62.6
69	.0084	0.628	72.4	0.621	70.4	0.614	68.5	0.608	66.6	0.601	64.8	0.594	63.0
70 71	.0026	0.652 0.678	72.7 78.1	0.646	70.8	0.639	68.9 69.3	0.632	67.1 67.5	0.625		0.619	63.5
72	.0036	0.704	78.4	0.671	71.2	0.664	69.7	0.657 0.683		0.651	65.7 66.1	0.614	64.0
	.0047	0.704	10.4	0.097	71.5	0.080	00.7	0.053	67.9	0.077	00.1	0.070	64.4
73	.0028	0.780	73.8	0.724	71.9	0.717	70.1	0.710	68.3	0.708	66.5	0.697	64.8
74	.0028	0.758	74.1	0.751	72.2	0.745	70.4	0.738	68.7	0.731	66.9	0.724	65.3
75	.0020	0.787	74.4	0.780	72.6	0.778	70.8	0.766	69.0	0.760	67.3	0.758	65.7
76	.6030	0.816	74.7	0.809	72.9	0.802	71.1	0.796	69.4	0.789	67.7	0.782	66.1
77		0.946	75.0	0.889	78.2	0.832	71.4	0.826	69.7	0.819	68.1	0.812	66.4
	.0081						1						
78	.0089	0.877	75.3	0.870	78.5	0.863	71.8	0.857	70.1	0.850	68.4	0.848	66. 8
79	-0038	0.909	75.6	0.902	73.8	0.895	72.1	0.888	70.4	0.882	68.8	0.875	67.2
80	-0084	0.942	75.8	0.935	74.1	0.928	72.4	0.921	70.7	0.915	69.1	0.908	67.5
81	.0085	0.976	76.1	0.969	74.4	0.962	72.7	0.955	71.0	0.948	69.4	0.913	67.9
82	.0036	1.011	76.4	1.004	74.6	0.997	78.0	0.990	71.8	0.988	69. 8	0.977	68.2
83	.0036	1.046	76.6	1.040	74.9	1.088	78.8	1.026	71.6	1.019	70.1	1.012	68.5
84	.0087	1.083	76.8	1.077	75.2	1.070	78.5	1.068	71.9	1.056	70.4	1.012	68.8
85	.0018	1.121	77.1	1.114	75.4	1.108	78.8	1.101	72.2	1.094	70.7	1.087	69.1
86	.0038	1.160	77.8	1.158	75.7	1.147	74.1	1.140	72.5	1.188	70.9	1.126	69.4
87	-0039	1.201	77.5	1.194	75.9	1.187	74.8	1.181	72.7	1.174	71.2	1.167	69.7
•	-0040			21.202				****			''''		.,,
88	.0042	1.241	77.7	1.285	76.1	1.228	74.6	1.221	78.0	1.214	71.5	1.207	70.0
89	.0044	1.284	78.0	1.277	76.4	1.270	74.8	1.268	73.8	1.256	71.8	1.250	70.8
90	.0044	1.327	78.2	1.321	76.6	1.814	75.0	1.807	78.5	1.300	72.0	1.298	70.6
91	.0045	1.372	78.4	1.365	76.8	1.859	75.8	1.352	78.7	1.845	72.8	1.838	70.8
92		1.418	78.6	1.412	77.0	1.405	75.5	1.898	74.0	1.891	72.5	1.884	71.1
93	-9047	1.466	**	1.750		1 470			"l	1 400		, ,	~1 -
94	.0049	1.514	78.8	1.439	77.2	1.452	75.7	1.445	74.2	1.438	72.8	1.431	71.3
95	.0060	1.564	79.0 79.1	1.507	77.4 77.6	1.501	75.9 76.1	1.494	74.4	1.487	73.0	1.480	71.6
96	.0051	1.615	79.1	1.608	77.6 77.8	1.602	76.1	1.595	74.9	1.588	78.2 78.4	1.581	71.8
97	-0082	1.668	79.5	1.661	77.8	1.654	76.5	1.647	75.1	1.640	78.4 78.7	1.633	72.1 72.3
98	-0084	1.722	79.7	1.715	78.2	1.708	76.7	1.701	75.8	1.694	78.9	1.688	72.5
~	.0056		10.1		10.2	1.700	.0.7	*****	. 0.0	1.084	.0.8	1.000	12.0
99		1.778	79.8	1.771	78.4	1.764	76.9	1.757	75.5	1.750	74.1	1.748	72.7
100	-0057	1.835	80.0	1.828		1.821	77.1	1.814	75.7	1.807	74.8	1.800	72.9
101	.0059	1.898	80.2	1.887	78.7		77.3	1.878	75.9	1.866	74.5	1.859	73.2
102	-0060	1.954	80.8	1.947	78.9	1.940	77.4		76.1	1.926	74.7	1.919	73.4
108	-0061	2.015	80.5	2.008	79.0	2.001	77.6	1.994	76.2	1.997	74.9	1.980	73.6
104	-0063	2.078	90.6	2.071	79.2	2.064	77.8	2.057	76.4	2.051	75.1	2.044	73.8
	<u> </u>	Mean	Horis	ntal Diff	100000	of Force	z Vapo	or for eac	ь 0°.1 .	- 0.0018.			

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Belative Humidity in Hundredths.

				t-1	t ′, or D	lfbrence	of Wet	and Dry	Bulb T	hermome	ters.		
meter	Mean Vertical Difference of Force	9°.	•	90,	.5	100	.0	100	.5	110	.0	110	.5
fahren- heit.	of Vapor for such 0°.1.	ores of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mki- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Bela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In	
82	0 0007	0.064	25.0	0.058	22.0	0.051	19.2	0.045	16.4	0.038	13.8	0.082	11.2
88	-0097	0.071	26.7	0.065	23.8	0.058	21.0	0.052	18.8	0.045	15.7	0.089	18.5
84	•0008	0.079	28.3	0.072	25.5	0.066	22.7	0.059	20.1	0.058 0.061	17.5	0.046	15.1 16.9
35	•0006	0.087	29.9 31.4	0.080	27.1 28.7	0.074	24.4	0.067	21.8 23.5	0.069	19.8 21.1	0.062	18.
86	.0008	0.095	91.4	0.088	20.7	0.082	26. 0	0.075	Z3.0	0.009	21.1	0.002	10.
87		0.103	83.0	0.096	30.3	0.090	27.6	0.088	25.2	0.077	22.8	0.070	20.
88	.0009	0.112	84.4	0.105	31.8	0.099	29.2	0.092	26.8	0.086	24.4	0.079	22.
89	.0009	0.121	35.9	0.114	33.8	0.108	30.7	0.101	28.4	0.094	26.1	0.088	23.8
40	.0009	0.130	37.8	0.128	34.8	0.117	82.2	0.110	29.9	0.104	27.6	0.097	25
41	•0010	0.189	38.6	0.133	36.2	0.126	88.7	0.120	81.4	0.118	29.2	0.107	27.0
	.0010												
42	-0010	0.149	89.9	0.148	37. 5	0.136	8 5.0	0.180	32. 8	0.123	30.6	0.116	28.4
48	-0010	0.160	41.1	0.158	88.7	0.146	36.3	0.140	84.1	0.188	32 .0	0.127	29.8
44	•0011	0.170	42.8	0.163	89.9	0.157	37.6	0.150	85.4	0.144	88.8	0.187	31.2
45	.0011	0.181	43.4	0.175	41.1	0.168	88.8	0.161	86.7	0.155	34.6	0.148	82.5
46		0.192	44.5	0.186	42.2	0.179	89.9	0.178	87.9	0.166	35.8	0.160	88.8
47	.0012	0.204	45.5	0.198	43.8	0.191	41.1	0.185	89.0	0.178	87.0	0.171	85.0
48	-0012	0.217	46.5	0.210	44.3	0.203	42.1	0.197	40.1	0.190	38.1	0.184	86.1
49	-0012	0.229	47.5	0.222	45.8	0.216	48.2	0.209	41.2	0.208	89.2	0.196	37.2
50	.0013	0.242	48.4	0.285	46.3	0.229	44.2	0.222	42.2	0.216	40.2	0.209	88.8
51	.0018	0.255	49.3	0.249	47.2	0.242	45.2	0.236	48.2	0.229	41.2	0.222	39.5
-	-0014	0.200			****	0.242	4						
52		0.269	50.2	0.268	48.1	0.256	46.1	0.249	44.1	0.243	42.2	0.286	40.8
53	.0015	0.284.	51.1	0.277	49.0	0.270	47.0	0.264	45.1	0.257	48.2	0.250	41.8
54	-0015	0.298	51.9	0.292	49.8	0.285	47.9	0.279	46.0	0.272	44.1	0.265	42.8
55	.0015	0.814	52.7	0.307	50.7	0.800	48.7	0.294	46.8	0.287	45.0	0.281	48.2
56		0.330	53.5	0.323	51.4	0.816	49.5	0.810	47.7	0.803	45.9	0.296	44.1
	.0016	0.0.0		0.000		0.000		0.000	48.5	0.030	ا ـ م	0.818	44.9
57	.0017	0.346	54.8	0.839	52.2	0.888	50.3	0.848	49.2	0.819 0.886	46.7	0.380	44.9
58	.0017	0.868	55.0	0.373	52.9	0.850	51.1	0.360	50.0	0.886	47.5 48.2	0.847	45.7
5 9	-0018	0.380 0.398	55.7 56.4	0.378	53.6	0.367 0.385	51.8 52.5	0.879	50.7	0.854	48.2	0.365	47.5
60 61	-0018	0.398	57.0	0.410	54.3 55.0	0.408	58.2	0.396	51.4	0.390	49.7	0.383	48.1
O1	-0019	A-410	51.10	0.410	55.0	0.400	JU. A	0.000		3.000	10.1	2.300	20.1
62		0.486	57.6	0.429	55.6	0.422	58.9	0.416	52.1		50.4	0.402	48.8
63	•0020	0.455	58.2	0.449	56.8	0.442	54.5	0.485	52.8	0.429	51.1	0.422	49.8
64	•0031	0.476	58.8	0.469	56.9	0.462	55.1	0.456	58.4	0.449	51.8	0.442	50.2
65	.0021	0.497	59.8	0.490	57.5	0.483	55.8	0.477	54.1	0.470	52.4	0.463	50.8
66	.0022	0.519	59.9	0.512	58.0	0.505	56.3	0.498	54.7	0.492	53.1	0.485	51.5
67	.0028	0.542	60.3	0.534	58.6	0.527	56 .9	0.521	55.3	0.514	58.7	0.507	52.1
									,				

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				1-1	t', or Di	ifference (of Wet	and Dry 1	Bulb Ti	ermomet	ero.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	90,	.0	90,	.5	10	.0	100	.5	110	.0	11	·.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Rein- tive Hu- mid- ity.	Force of Vapor.	Reia- tive Hu- mid- ity.	Force of Vapor.	Reia- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor,	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
•		Eng. In.		Eng. In.		Eng. In.		ling. In.		Eng. In.		Eng. In.	
68	0.0024	0.564	60.8	0.557	59.1	0.550	57.4	0.544	55.8	0.587	54.2	0.580	52.7
69	.0025	0.588	61.8	0.581	59.6	0.574	58.0	0.567	56.4	0.561	54.8	0.554	53.8
70	.0025	0.612	61.8 62.8	0.605	60.1	0.598	58.5	0.592	56.9	0.585	55.4	0.578	58.8
71 72	.00:26	0.687 0.668	62.7	0.630	60.6	0.624	59.0 59.5	0.617	57.4 58.0	0.610 0.6 36	55.9 56.4	0.603	54.4
'*	.0037	0.000	· ·	0.000	V2.1	0.000	55.0	U-U10	55.0	0.000	50.4	0.029	U-1-18
73	.00-27	0.890	63.2	0.683	61.6	0.677	60.0	0.670	58.4	0.663	56.9	0.656	55.5
74	.00-27	0.718	63.6	0.711	62.0	0.704	60.5	0.697	58.9	0.691	57.4	0.684	56.0
75	.0029	0.746	64.0	0.739	62.5	0.788	60.9	0.726	59.4	6.719	57.9	0.712	56.5
76	-0030	0.775	64.4	0.769	62.9	0.762	61.8	0.755	59.8	0.748	58.4	0.741	56.9
77		0.805	64.8	0.799	68.8	0.792	61.8	0.785	60.8	0.778	58.8	0.772	57.4
78	.0031	0.836	65.2	0.829	63.7	0.823	62.2	0.816	60.7	0.809	59.2	0.802	57.8
79	.0032	0.868	65.6	0.861	64.1	0.855	62.6	0.848	61.1	0.841	59.7	0.884	58.8
80	.0033	0.901	66.0	0.894	64.5	0.897	68.0	0.881	61.5	0.874	60.1	0.867	58.7
81	.0034	0.935	66.3	0.928	64.8	0.921	63.4	0.914	61.9	0.908	60.5	0.901	59.1
82	.0935	0.970	66.7	0.963	65.2	0.956	68.7	0.949	62.8	0.943	60.9	0.986	59.5
]	.0036											ł	
83	.0037	1.006	67.0	0.999	65.5	0.992	64.1	0.985	62.7	0.978	61.8	0.972	59.9
84	-0038	1.042	67.3	1.036	65.9	1.029	64.4	1.022	63.0	1.015	61.7	1.008	80.8
85	.0039	1.080 1.119	67.7 68.0	1.078	66.2	1.067	64.8	1.060	68.4	1.058	62.0 62.4	1.046	60.7
86 87	-0040	1.160	68.3	1.112	66.5 66.8	1.106	65.1 65.4	1.099	68.7	1.092	62.7	1.085	61.0 61.4
81	.0041	1.100	00.3	1.100	00.0	1.140	00.4	1.140	64.1	1.188	02.4	1.120	01.4
88		1.200	68.6	1.194	67.1	1.187	65.8	1.180	64.4	1.173	63.1	1.166	61.7
89	-0042	1.243	68.9	1.236	67.4	1.229	66.1	1.222	64.7	1.215	68.4	1.208	62.1
90	.0044	1.286	69.1	1.279	67.7	1.278	66.4	1.266	65.0	1.259	63.7	1.252	62.4
91	-0046	1. 3 31	69.4	1.824	68.0	1.317	66.7	1.311	65.3	1.804	64.0	1.297	62.7
92		1.877	69.7	1.870	68.3	1.863	67.0	1.857	65.6	1.850	64.8	1.848	63.1
93	-0047	1.425	69.9	1.418	68.6	1.411	67.2	1.404	65.9	1.897	64.6	1.390	63.4
94	.0048	1.473	70.2	1.466	68.8	1.459	67.5	1.452	66.2	1.446	64.9	1.489	68.7
95	.0050	1.523	70.4	1.516	69.1	1.509	67.8	1.502	66.5	1.495	65.2	1.488	64.0
96	-00s1	1.574	70.7	1.567	69.4	1.560	68.0	1.558	66.7	1.546	65.5	1.589	64.2
97	-0043	1.627	70.9	1.620	69.6	1.618	68.3	1.606	67.0	1.599	65.8	1.592	64.5
98	-0054	1.681	71.2	1.674	69.8	1.667	68.5	1.660	67.8	1.653	66.0	1.646	64.8
l l	.0056							l '		1			
99	.0087			1.729		1.722		1.716		1.709	66.8		65.1
100	-0058	1.798			70.8		69.0	1.778	67.8	1.766	66.5	1.759	65.8
101	.0060		71.8		70.5		69.3	1.831	68.0	1.824	66.8	1.817	65.6
102 103	.0062	1.912 1.974	1		70.8 71.0		69-5 69-7		68.2	1.884	67.0	1.877	65.8
104	.0063		•	2.030		1.960		1.953 2.016	68.5 68.7	1.946 2.009	67.8	1.939 2.002	66.1 66.8
101		2.007	12.0	2.000		4.020	95.5	2.010	90.1	2.009	91.0	4.004	
]		Me	na Hori	sontal Di	Cerence	of Force	of Vap	or for eac	ት 0°.1	— 0.0018.			

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				1-1	', or Di	Gerence o	(Wet 1	and Dry l	Balb Ti	nermonne	ers.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	199	·.0	19	5	18	2.0	189	.5	14	·.o	14	.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Reia- tive Hu- nid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Reia- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid ity.
•		Eng. In.		Eng. In.		Eng. In.		Eng. In.		ling. In.		Eng. In.	
82	0.0007	0.023	8.8	0.019	6.4	0.012	4.1			l			
83	.0007	0.032	10.8	0.026	8.4	0.019	6.2	0.018	4.0				
84	.0007	0.040	12.7	0.038	10.4	0.027	8.2	0.020	6.0	0.014	4.1 6.1	0.015	4 9
8 5	.0008	0.048	14.6	0.041	12.8 14.2	0.084	10.1 12.0	0.028 0.036	8.0 10.0	0.021	8.1	0.013	4.2 6.2
26	.0008	0.056	16.4	0.043	A-4-4	0.042	12.0	0.000	10.0	0.029	3.1	J. J. J. J.	3.2
87		0.064	18.2	0.057	16.0	0.051	18.9	0.044	11.9	0.088	10.0	0.031	8.2
88	.0009	0.072	19.9	0.066	17.8	0.059	15.7	0.053	18.7	0.046	11.9	0.040	10.1
39	-0009	0.081	21.6	0.075	19.5	0.068	17.5	0.062	15.5	0.055	18.7	0.049	11.9
40	.0009	0.091	28.8	0.084	21.2	0.078	19.2	0.071	17.2	0.064	15.4	0.058	18.6
41		0.100	24.9	0.094	22.8	0.087	20.8	0.081	18.9	0.074	17.1	0.067	15.8
	-0010		26.4	0.103	24.8	0.097	22.4	0.090	20.5	0.084	18.6	0.077	16.8
42 43	.0010	0.110	27.8	0.103	25.8	0.107	28.9	0.100	22.0	0.095	20.1	0.087	18.3
44	-0011	0.120	29.2	0.124	27.2	0.118	25.8	0.111	28.5	0.104	21.5	0.098	19.8
45	.0011	0.142	80.5	0.135	28.6	0.129	26.7	0.122	24.9	0.115	22.9	0.109	21.2
46	-0011	0.158	31.8	0.146	30.0	0.140	28.1	0.188	26.8	0.127	24.8	0.119	22.7
	.0012											ľ	
47	.0019	0.165	33.0	0.158	81.2	0.152	29.8	0.145	27.6	0.188	25 7	0.132	21-0
48	.0013	0.177	84.2	0.170	32.4	0.164	30.6	0.157	28.8	0.151	27.0	0.144	25.4
49	-0013	0.190	85.8	0.188	88.5	0.176	31.7	0.170	80.0	0.168	28.3	0.157	26.7
50	.0014	0.202	86.4	0.196	84.6	0.189	82.9	0.188	31.2	0.176	29.5 30.7	0.169 0.183	27.9 29.1
51		0.216	87.5	0.209	85.7	0.202	84.0	0.196	82.8	0.189	00.7	0.103	29.1
52	-0014	0.229	88.5	0.228	86.8	0.216	85.1	0.210	88.4	0.208	\$1.8	0.196	30.2
53	.0014	0.244	39.5	0.237	87.8	0.231	86.1	0.224	84.5	0.217	82.9	0.211	81.4
84	.0015	0.259	40.5	0.252	28.8	0.245	37.1	0.289	85.5	0.232	84.0	0.226	82.4
55	.0015	0.274	41.5	0.267	89. 8	0.261	88.1	0.254	86.5	0.247	35.0	0.241	33.5
56	-0016	0.290	42.4	0.288	40.7	0.276	39. I	0.270	87.5	0.268	3 5.9	0.257	84.4
	.0016	0.000	40.0	0.000	43.0	0.000	40.0	0.286	38.4	0.280	36.9	0.278	35.4
57 80	-0017	0.306	48.2	0.299 0.816	41.6 42.4	0.298	40.0 40.8	0.286	39.8	0.280	37.8	0.275	86.8
58 59	-0017	0.823	44.1	0.816	48.8	0.810	41.7	0.820	40.1	0.230	38.7	0.807	87.2
60	-0016	0.358	45.7	0.851	44.1	0.845	42.5	0.888	41.0	0.381	39.5	0.825	38.1
61	-0018	0.876	46.4	0.870	44.9	0.868	43.8	0.856	41.8	0.850	40.8	0.848	39.9
	.0019												
62		0.896	47.2	0.389	45.6	0.882	44.1	0.876	42.6	0.869	11.2	0.862	39.8
62	.0020			0.409		0.402		0.895		0.889			
64	.0091	0.486	1	0.429	47.1	0.422	45.6	0.416	44.1	0.409	ı	0.402	41.8
65	.0021	0.457	49.8	0.450	47.8	0.443	46.3	0.437			1	0.428 0.445	42.1 42.8
66	-0023	0.478		0.472	ĺ	0.465		0.458	45.5	0.452		ł	43.5
67		0.501	50.6	0.494	49.1	0.487	47.6	0.481	46.2	J V. 1/4	2340	V-101	70.0
		Mo	an Hor	sontal Di	fierence	of Force	of Vap	or for eac	ь 0°.1	- 0.0018.	•		

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				£—1	t', or D	Merence	of Wet	and Dry	Bulb T	hermome	ters.		
Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	129	.0	199	.5	18	·.o	18	5	14	·.o	14	·.5
Pahron- heli.	for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng In.	
69	0.0024	0.524	51.2	0.517	49.7	0.510	48.8	0.508	46.9	0.497	45.5	0.490	44.1
69	.0094	0.547	51.8	0.541	50.8	0.534	48.9	0.527	47.5	0.520	46.1	0.514	44.8
70 71	.0025	0.572 0.597	52.4 52.9	0.565	50.9 51.5	0.558	49.5 50.1	0.551 0.577	48.1 48.7	0.545	46.8 47.4	0.538	45.5 46.1
72	.00-26	0.628	53.5	0.590	52.1	0.588	50.7	0.608	49.3	0.596	48.0	0.589	46.7
14	.00:26	0.028	55.5	0.010	JE.1	0.009	50.7	0.003	45.0	0.050	40.0	0.009	40.7
73	.0027	0.650	54.0	0.648	52.6	0.686	51.8	0.629	49.9	0.623	48.6	0.616	47.8
74	.0028	0.677	54.5	0.670	53.2	0.664	51.8	0.657	50.5	0.650	49.2	0.643	47.9
75	.0028	0.705	55.0	0.699	53.7	0.632	52.8	0.685	51.0	0.678	49.7	0.672	48.4
76	.01.30	0.785	55.5	0.728	54.2	0.721	52.9	0.714	51.5	0.708	50.8	0.701	48.9
77	l	0.765	56.0	0.759	54.7	0.752	58.4	0.745	52.1	0.789	50.8	0.731	49.5
	.0031									0.000			*A A
78	.0032	0.796 0.827	56.5 56.9	0.782	55.2 55.6	0.782	53.8	0.775 0.807	52.5	0.768 0.800	51.8	0.762	50.0 50.5
79 80	.0038	0.527	57.3	0.821	56.1	0.814 0.847	54.8 54.8	0.840	53.0 53.5	0.833	51.8 52.2	0.794	51.0
81	.0034	0.894	57.8	0.887	56.5	0.880	55.2	0.874	53.9	0.867	52.7	0.860	51.4
82	.0025	0.929	58.2	0.922	56.9	0.915	55.6	0.909	54.4	0.902	53.2	0.895	51.9
	-0036	0.525	00.2	V.822	00.3	0.515	55.0	0.505	04.4	0.502	00.2	0.030	01.0
83		σ.965	58.6	0.958	57.8	0.951	56.1	0.944	54.8	0.937	53.6	0.931	52.4
84	.0037	1.002	59.0	0.995	57.7	0.988	56.5	0.981	55.2	0.974	54.0	0.969	52.8
85	.0088	1.039	59.4	1.038	58.1	1.026	56.8	1.019	55.6	1.012	54.4	1.005	53.2
86	.0040	1.078	59.7	1.071	58.5	1.065	57.2	1.058	56.0	1.051	54.8	1.044	53.6
87	.0040	1.119	60.1	1.112	58.8	1.105	57.6	1.099	56.4	1.092	55-2	1.085	54.0
	.0041			l						ا ا			
88	.0042	1.159	60.5	1.152	59.2	1.146	58.0	1.139	56.8	1.132	55.6	1.125	54.4
89	-0044	1.202	60.9	1.195	59.6	1.188	58.8	1.181	57.1	1.174	56.0	1.167	54.8
90 91	.0045	1.245 1.290	61.8	1.288	59.9 60.2	1.231 1.276	58.7 59.0	1.225 1.269	57.5 57.9	1.218	56.3 66.7	1.211 1.256	55.2 55.6
92	.0046	1.336	61.9	1.329	60.6	1.822	59.4	1.315	58.2	1.809	57.0	1.802	55.9
~	-0047		51.0	1.525	50.0	1.026	55.4	1.010		1.505	J	1.002	50.0
93		1.383	62.2	1.376	60.9	1.370	59.7	1.363	58.5	1.356	57.4	1.849	56.3
94	-0049	1.432	62.5	1.425	61.2	1.418	60.0	1.411	58.9	1.404	57.7	1.897	56.6
95	-0050	1.482	62.7	1.475	61.5	1.468	60.4	1.461	59.2	1.454	58.1	1.447	57.0
96	-0051 -0052	1.533	63.0	1.526	61.8	1.519	60.7	1.512	59.5	1.505	58.4	1.498	57.8
97	.0084	1.585	63.8	1.578	62.1	1.571	61.0	1.564	59.8	1.558	58.7	1.551	57.6
96		1.639	68.6	1.682	62.4	1.625	61.8	1.618	60.1	1.612	59.0	1.605	57.9
-	.0056	1 605	29 A	1 600	eo =	1 001	61.6	1 67	60.4	1 66*	40 e	1 660	E 9 9
99	.0057	1.695 1.752	63.9 64.2			1.681		1.674		1.667 1.724	59.8	1.660	58.2 58.5
100 101	.0049	1.810	64.4	1.745 1.903	63.0 63.2	1.7 3 8 1.797	62.0 62.8	1.731 1.790	60.7 61.0		59.6 59.9	1.776	58.8
102	-0060	1.870	61.7		63.5	1.857	62.6	1.850	61.3		60.2	1.836	59.1
103	-0062	1.932	64.9	1.923	63.8	1.918	62.9	1.911	61.5	1	60.4	1.897	59.4
104	-0063	1.995		1.988		1.981	63.2			1.967	60.7	1.960	
	<u>'</u>	·						·					
		Mean	n Horis	ontal Diff	erence	of Force	of Vap	or for eac	h 0°.1	- 0.0018.			

Temperature, Fahrenheit. - Force of Vapor in English Inches. - Relative Humidity in Hundredths.

W.A	Mean				e, or D	iference (A M 66 1	LEAL DEY	DULU 11	METATORISM			
Wet- Bulb bermo- meter	Vertical Difference of Force of Vapor	150	·.0	15	.5	164	·.o	164	.5	179	·.0	17	·.5
ahren- beit.	for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Reis- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Reis- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid ity.
		Eng. In.		ing. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	
82 88			İ		l	i i							ı
84				1									l
85	1		1									-	
36		0.016	4.4										1
	0.0009		l										ł
87	.0009	0.025	6.4	0.018	4.6	0.000		0.01					
88	.0009	0.033	8.8	0.027	6.5	0.020	4.8 6.7	0.014	8.2 5.1	0.016	8.6	0.010	2.
89 40	.0009	0.042	10.1	0.086	8.4 10.1	0.029	8.5	0.028	6.9	0.016	5.4	0.010	3.
41	-0010	0.061	13.6	0.054	11.8	0.048	10.8	0.041	8.7	0.035	7.2	0.028	5.
••	.0010		2010						""				
42	-0010	0.071	15.1	0.064	13.4	0.058	11.9	0.051	10.8	0.044	8.8	0.038	7.
48	-0011	0.081	16.6	0.074	15.0	0.068	18.4	0.061	11.9	0.055	10.4	0.048	9.
44	.0011	0.091	18.1	0.085	16.5	0.078	15.0	0.072	18.5	0.065	12.0	0.058	10.
45 46	.0011	0.102 0.114	19.6 21.0	0.096	18.0 19.4	0.089	16.5 17.9	0.088	15.0 16.4	0.076	13.5 15.0	0.069 0.081	12. 13.
60	.0012	0.114	21.0	0.107	15.4	0.100	11.0	0.054	10.4	0.007	10.0	0.001	10.
47	-0012	0.125	22.4	0.119	20.8	0.112	19.8	0.106	17.9	0.099	16.5	0.092	15.
48	.0013	0.187	23.8	0.131	22.2	0.124	20.7	0.118	19.8	0.111	17.9	0.104	16.
49	.0013	0.150	25.1	0.148	23.6	0.187	22.1	0.180	20.7	0.124	19.8	0.117	17.
50	.0013	0.163	26.4	0.156	24.9	0.150	28.4	0.148	22.0	0.186	20.6	0.130	19.
51	.0014	0.176	27.6	0.169	26.1	0.168	24.6	0.156	28.2	0.150	21.9	0.148	20.
52		0.190	28.7	0.188	27.8	0.177	25.8	0.170	24.4	0.168	23.1	0.157	21.
58	.0014	0.204	29.9	0.197	28.4	0.191	27.0	0.184	25.6	0.178	24.8	0.171	23.
54	.0013	0.219	80.9	0.212	29.5	0.206	28.1	0.199	26.7	0.192	25.4	0.186	24.
55	.0016	0.234	82.0	0.228	20.6	0.221	29.2	0.214	27.8	0.208	26.5	0.201	25.
56		0.250	83.0	.0.243	81.6	0.287	80.2	0.280	29.9	0.223	27.6	0.217	26.
57	-0016	0.266	84.0	0.260	32.6	0.253	81.2	0.246	29.9	0.240	28.6	0.233	27.
58	.0017	0.288	84.9	0.276	38.5	0.270	82.2	0.268	80.8	0.256	29.6	0.249	28.
59	.0017	0.800	85.8	0.294	84.4	0.287	33.1	0.280	31.8	0.274	80.5	0.267	29.
60	.0018	0.818	36.7	0.311	35.8	0.805	84.0	0.298	82.7	0.291	81.4	0.285	30.
61	-0019	0.886	87.5	0.330	86.2	0.823	84.9	0.816	88.6	0.810	32.4	0.303	81.
62	-0019	0.356	28.4	0.349	87.0	0.342	35.7	0.836	0	0.829		0.322	82.
62 63	-0020	0.856	89.2		87.0 87.9	0.342	86.6			0.829	83.2 84.1	0.842	32.
64	-0020	0.896	40.0	0.889	87.9 88.7	0.882	87.4	0.376	36.1	0.869	34.9	0.362	83.
65	10021	0.417	40.7	0.410	39.4	0.408		0.396	36.9	0.890	85.7	0.388	84.
66	-0022	0.489	41.5	0.481	40.2	0.425	88.9	0.418	37.7	0.411	86.5	0.405	85.
67	-0023	0.460	42.2	0.454	40.9	0.447	39.6	0.440	38.4	0.434	87.2	0.427	36.
			1	l	l	l		l '	1	l			Ì

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				1-1	', or D	Servoce (of Wes	and Dry	Balb Ti	ermome	ters.	· · · · · · ·	·
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	150	.0	159	.5	16	.0	16	.5	170	·.o	179	·.5
Pahren- heit.	for each	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	
68	0.0034	0.488	42.8	0.477	41.6	0.470	40.8	0.468	89.1	0.456	87.9	0.450	86.8
69	.0034	0.507	43.5	0.500	42.3	0.594	41.0 41.7	0.487 0.511	39.8	0.480	88.7	0.473 0.498	87.5
70 71	.0025	0.531 0.556	44.2 44.8	0.524	42.9 48.6	0.518	42.4	0.511	40.5 41.2	0.504	89.3 40.0	0.498	38.2 38.9
72	.00:06	0.582	45.4	0.576	44.2	0.569	43.0	0.562	41.8	0.555	40.7	0.549	89.5
'-	-0027	0.002	20.4	0.070	77.0	0.000		0.002	-11-0	0.000	40.7	0.043	05.0
73		0.609	46.0	0.602	44.8	0.596	48.6	0.589	42.4	0.582	41.3	0.575	40.2
74	.0028	0.637	46.6	0.680	45.4	0.628	44.2	0.616	48.0	0.610	41.9	0.608	40.8
75	.0028 .0029	0.665	47.2	0.658	46.0	0.651	44.8	0.645	48.6	0.688	42.5	0.631	41.4
76	.0029	0.694	47.7	0.687	46.5	0.681	45.4	0.674	44.2	0.667	43.1	0.660	42.0
77	.0030	0.724	48.2	0.717	47-1	0.711	45.9	0.704	44.8	0.697	43.6	0.690	42.6
H	.0031												
78	.0032	0.755	48.8	0.748	47.6	0.741	46.4	0.785	45.8	0.728	44.2	0.721	48.1
79	.0033	0.787	49.8	0.780	48.1	0.778	47.0	0.766	45.8	0.760	44.7	0.758	43.7
80	.0034	0.820	49.8	0.813	48.6	0.806	47.5	0.799	46.4	0.792	45.8	0.786	44.2
81	.0035	0.858	50.8	0.847	49.1	0.840	48.0	0.888	46.9	0.826	45.8	0.819	44.6
82	.0086	0.888	50.7	0.881	49.6	0.875	48.5	0.868	47.4	0.861	46.3	0.854	45.1
88	.00.00	0.924	51.2	0.917	50.0	0.910	48.9	0.908	47.8	0.897	46.8	0.890	15.6
84	-0037	0.961	51.6	0.954	50.5	0.947	49.4	0.940	48.8	0.988	47.2	0.927	46.2
85	-0038	0.998	52.1	0.992	50.9	0.985	49.8	0.978	48.7	0.971	47.7	0.964	46.6
86	.0039	1.087	52.5	1.080	51.8	1.024	50.8	1.017	49.2	1.010	48.1	1.008	47.1
87	-0040	1.078	52.9	1.071	51.8	1.064	50.7	1.058	49.6	1.051	48.6	1.044	47.5
	-0041												
88	.0042	1.118	53.8	1.111	52.2	1.105	51.1	1.098	50.0	1.091	49.0	1.084	48.0
89	.0042	1.161	53.7	1.154	52.6	1.147	51.5	1.140	50.4	1.188	49.4	1.126	48.4
90	.0044	1.204	54.1	1.197	53. 0	1.190	51.9	1.188	50.9	1.177	49.8	1.170	48.8
91	-0046	1.249	54.5	1.242	53.4	1.285	52.8	1.228	51.2	1.221	50.2	1.215	49.2
92		1.295	54.8	1.288	53.7	1.281	52.7	1.274	51.6	1.267	50.6	1.260	49.6
93	-0048	1 0,0		1 907	84 4	1 990	#0 A	1.001	E0.0	1.015	K1 0	1.308	E0 0
94	-0049	1.842	55.2 55.5	1.885	54.1 54.4	1.828	58.0 58.4	1.321	52.0 52.4	1.815	51.0 51.4	1.856	5 0. 0 50.4
95	.0050	1.440.	55.9	1.884	54.8	1.426	58.7	1.420	52.7	1.418	51.7	1.406	50.7
96	-0051	1.491	56.2	1.484	55.1	1.477	54.1	1.471	58.1	1.464	52.1	1.457	51.1
97	-0053	1.544	56.5	1.587	55.5	1.580	54.4	1.528	58.4	1.516	52.4	1.509	51.5
98	-0054	1.598	56.8	1.591	55.8	1.584	54.8	1.577	53.8	1.570	52.8	1.563	51.8
~	.0056	1.000	5010	1.001	9010	1.004	A-1-0	*****	00.0	1.010	22.0	2.000	01.0
99		1.658	57.2	1.646	56.1	1.689	55.1	1.638	54.1	1.626	58.1	1.619	52.1
100	.0057	1.710	57.5		56.4	1.696	55.4	1-690				1.676	52.5
101	.0089	1.769	57.8	1.762	56.7	1.755	55.7	1.748	54.7	1.741	53.7	1.784	52.8
102	.0060	1.829	58.0	1.822	57.0	1.815	56.0	1.809	55.0	1.802	54.0	1.794	58.1
103	.0062	1.890	58.8	1.683	57.8	1.876	56.8	1.869	55.8	1.868	54-8	1.856	58.4
104	-0063	1.958	58.6	1.946	57.6	1.939	56.6	1.932	55.6	1.925	54.6	1.919	58.7
		Mot	n Hori	sontal Di	Serence	of Force	of Vap	or for eac	ь 0°.1 -	- 0.0018.			

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

		t — t', or Difference of Wet and Dry Bulb Thermometers.												
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor for each 0°.1.	18°.0		18°.5		19°.0		190.5		200.0		200.5		
Fahren- beit.		Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity	Force of Vapor.	Rein- tive Hu- mid- ity.	Force of Vapor.	Rein- tive Hu- mid- ity.	Force of Vapor.	Rein- tive Hu- mid- ity.	
0		ling. In.		Eng. ln.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		
32 33								ł		1				
84									l					
35	'								}	İ.				
36														
87				i				1						
38 39			İ											
40		0.012	2.5											
41	0.0010	0.022	4.8	0.015	8.0	0.009	1.6							
	-0010							0.015						
42	.0010	0.031	6.0	0.025	4.6	0.018	8.8	0.012	2.1		2.6			
48	1100.	0.041	7.6 9.2	0.085	6.3	0.028	5.0 6.6	0.022	8.7 5.4	0.015	4.8	0.019	3.2	
44	.0011	0.063	10.8	0.048	7.9 9.5	0.050	8.2	0.048	7.0	0.087	5.9	0.020	4.8	
46	-0011	0.074	12.3	0.068	11.0	0.061	9.7	0.054	8.5	0.048	7.5	0.041	6.3	
	.0012													
47	.0012	0.086	13.8	0.079	12.5	0.078	11.2	0.066	10.0	0.059	9.0	0.058	7.9	
48	.0013	0.098	15.2	0.091	13.9	0.085	12.7	0.078	11.5	0.072	10.4	0.065	9.8 10.7	
49	.0018	0.110	16.6 18.0	0.104	15.4	0.097	14.1 15.5	0.091 0.108	12.9 14.4	0.084	11.9 13.2	0.090	12.1	
50 51	-0013	0.128 0.136	19.8	0.117	16.7 18.0	0.110 0.123	16.8	0.117	l	0.110	14.5	0.103	13.4	
31	-0014	0.130	13.0		10.0	0.120	10.0		2000					
52		0.150	20.5	0.144	19.3	0.187	18.1	0.180	16.9	0.124	15.7	0.117	14.6	
53	.0014	0.164	21.7	0.158	20.5	0.151	19.3	0.145	18.2	0.138	16.9	0.181	15.8	
54	.0015	0.179	22.9	0.173	21.7	0.166	20.5	0.159	19.8	0.152	18.1	0.146	17.0 18.2	
55	.0015	0.194	24.0	0.188	22.8	0.181	21.6 22.7	0.174	20.5 21.6	0.168 0.184	19.2 20.4	0.161 0.177	19.3	
56	-0016	0.210	25.1	0.208	28.9	0.197	EZ. 1	0.150	21.0	0.104	20.4	J		
57		0.226	26.1	0.220	24.9	0.218	28.8	0.206	22.7	0.200	21.5	0.198	20-4	
58	-0017	0.248	27.1	0.286	25.9	0.230	24.8	0.228	28.7	0.217	22.6	0.210	21-5	
59	-0017	0.260	26.1	0.254	26.9	0.247	25.8	0.240	24.7	0.284	28.6	0.227	22.6	
60	-0016 -0019	0.278	29.0	0.271	27.9	0.265	26.8	0.258	25.7	0.251	24.6	0.245	23.6 24.5	
61		0.296	30.0	0.290	28.8	0.288	27.7	0.276	26.6	0.270	25.5	0.200	D-9-0	
62	-0019	0.816	80.9	0.809	29.7	0.802	28.6	0.295	27.5	0.289	26.5	0.282	25.4	
68	.0020	0.835		0.828		0.822		0.315	28.4	0.808	27.4	0.802	26.4	
64	-0020	0.855	32.6	0.849	81.5	0.342	80.4	•		0.829	28.2	•	27.2	
65	-0021	0.876		0.870		0.868	81.2	0.356	30.1	0.350	29.1	0.348	28.1	
66	.0022	0.898	84.2	1	1	0.885	82.0	0.878	30.9	0.371	29.9	i .	28.9	
67	.0028	0.420	34.9	0.414	83.8	0.407	82.8	0.400	81.7	0.398	80.7	0.887	29.7	
		Me	an Hor	isontal Di	Serence	of Force	of Vap	or for eac	n 0°.1	- 0.0018.				

Temperature, Fahrenheit. — Force of Vapor in English Inches — Relative Humidity in Hundredths.

	Mean Vertical Difference of Force of Vapor for each 0°.1.	t-t', or Difference of Wet and Dry Bulb Thermometers.											
		18°.0		180.5		19°.0		190.5		200.0		200.5	
Fahren- beit.		Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rola- tive Hu- mid- ity.	Force of Vapor.	Rola tive Hu- mid ity.
•		Eng. In.		Rog. In.		Bog. In.		Eng. In.		Eng. In.		Eng. In.	
68	0.0024	0.448	35.7	0.486	84.6	0.480	88.5	0.428	82.5	0.416	81.4	0.409	80.
69	.0025	0.467	36.4	0.460	85.8	0.458	34.2	0.446	88.2	0.440	82.2	0.488	31.
70 71	.0035	0.491	37.1 37.8	0.484	36.0 36.7	0.477	85.0 85.7	0.496	88.9 84.6	0.464	82.9 88.6	0.457	31. 32.
72	.00:26	0.542	38.5	0.585	87.4	0.528	36.3	0.522	35.3	0.515	34.8	0.508	83.
	.00-36	0.542	80.0	0.565	01.4	0.028	90.5	0.522	00.0	0.515	94.0	0.506	00.
73	.0027	0.569	39.1	0.562	38.0	0.555	87.0	0.548	36.0	0.542	35.0	0.535	34.
74	.0027	0.596	89.7	0.589	88.7	0.588	87.7	0.576	36.6	0.569	35.7	0.562	34.
75	-0020	0.624	40.8	0.618	89.8	0.611	88.8	0.604	87.8	0.597	36.3	0.591	35.
76	.6030	0.654	40.9	0.647	89.9	0.640	88.9	0.633	87.9	0.627	86.9	0.620	35.
77		0.683	41.5	0.677	40.5	0.670	89.5	0.663	3 8.5	0.656	87.5	0.630	86.
-	.0031	1,	40.1		47.0		40.0	0.694	89.0	0.687	88.1	0.680	
78 79	.0032	0.714	42.1 42.6	0.707	41.6	0.701 0.782	40.0 40.6	0.054	39.6	0.719	88.6	0.712	37. 37.
80	-0038	0.779	48.2	0.772	42.1	0.765	41.1	0.758	40.2	0.752	39.2	0.745	38.
81	-0084	0.818	48.7	0.806	42.7	0.799	41.7	0.792	40.7	0.785	89.7	0.779	38.
82	.0035	0.847	44.2	0.840	43.2	0.884	42.2	0.827	41.2	0.820	40.2	0.813	89.
	.0036	1		0.010		0.000		0.02.		0.020	20.2	0.010	
83	.0036	0.883	44.7	0.876	48.7	0.869	42.7	0.868	41.7	0.856	40.7	0.849	89.9
84	.0038	0.920	45.2	0.918	44.2	0.906	48.2	0.899	42.2	0.898	41.8	0.886	40
85	.0039	0.958	45.6	0.951	44.6	0.944	48.7	0.987	42.7	0.930	41.8	0.928	40.
86	.0040	0.996	46.1	0.989	45.1	0.988	44.1	0.976	48.2	0.969	42.8	0.962	41.
87		1.087	46.5	1.080	45.6	1.028	44.6	1.017	48.6	1.010	42.7	1.003	41.
-	-0041									- 000			
88 89	.0042	1.077	47.0 47.4	1.070	46.0 46.4	1.064	45.5	1.037	44.1	1.050	43.2 48.6	1.043	42.
90	-0048	1.168	47.8	1.156	46.9	1.149	45.9	1.142	45.0	1.186	44.1	1.129	48.
91	.0045	1.208	48.2	1.201	47.8	1.194	46.8	1.187	45.4	1.180	44.5	1.178	48.0
92	-0047	1.254	48.6	1.247	47.7	1.240	46.7	1.283	45.8	1.226	44.9	1.219	44.0
- -	.0048												
93		1.801	49.0	1.294	48.1	1.287	47.1	1.280	46.2	1.278	45.8	1.266	44.
94	.0049	1.849	49.4	1.842	48.4	1.885	47.5	1.829	46.6	1.822	45.7	1.815	44.8
95	.0050 .0061	1 68 99	49.8	1.892	48.8	1.385	47.9	1.378	47.0	1.371	46.1	1.864	45.5
96	.0063	1.450	50.1	1.448	49.2	1.486	48.8	1.429	47.8	1.422	46.5	1.415	45.0
97	-0054	1.502	50.5	1.495	49.5	1.489	48.6	1.482	47.7	1.475	46.8	1.468	46.0
98		1.556	50.8	1.549	49.9	1.548	49.0	1.586	48.1	1.529	47.2	1.522	46.
99	.0055	1 610	61 9	1.605	50 a	1.500	40 9	1.591	48.4	1.584	47.5	1.577	46.
100	-0057	1.612		1.662		1.598 1.655		1.648	48.8	1.641	47.9	1.684	47.0
, 101	. 0058	1.727	51.8	1.720	50.9	1.718	50.0	1.706	49.1	1,700	48.2	1.693	47.4
102	-0060	1.787	52.2	1.780	51.2	1.773	50.8	1.766	49.4	1.759	48.6	1.758	47.
103	.0062	1.849		1.842	51.5	1.835	50.7		49.8	1.821	48.9	1.814	48.0
104	-0063	1.912	52.8	1.905	51.9	1.898	51.0	1.891	50.1		49.2	1.877	48.4
		,		,			- 1						

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

			t-t', or Difference of Wet and Dry Bulb Thermometers.											
Bulb Thermo- meter t'	Thermo-Difference meter of Force t' of Vapor		91%0		91°.5		99°.0		220.5		23°.0		920.5	
Fahren- heit.	for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.		
o 32		Eng. In.		Eng. In.	1	Eng. In.		Eng. In.		Eng. In		ling. In		
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89							1			1				
40		l	ł	ł									[
41		1											1	
42				1									l	
48				1										
44		0.018	2.0			1								
45	0.0011	0.028	8.7	0.017	2.6	0.010	1.6							
46	.0011	0.035	5.2	0.028	4.2	0.022	8.1	0.015	2.1					
	.0012	0.040						A A0=				0.010		
47	.0013	0.046	6.8 8.2	0.040	5.7 7.2	0.088	4.7 6.2	0.027	8.7 5.2	0.020	2.7 4.2	0.018	1.8 8.8	
49	-0013	0.071	9.7	0.064	8.6	0.058	7.6	0.051	6.6	0.044	5.7	0.028	4.7	
50	-0013	0.084	11.0	0.077	10.0	0.070	9.0	0.064	8.0	0.057	7.1	0.061	6.1	
5 1	-0013	0.097	12.8	0.090	11.8	0.084	10.8	0.077	9.3	0.070	8.8	0.064	7.4	
	-0014													
52 53	.0014	0.110 0.125	18.5 14.8	0.104 0.118	12.5 18.7	0.097	11.5 12.8	0.091	10.6 11.8	0.084	9.6 10.9	0.077	8.7 9.9	
54	-0015	0.120	16.0	0.118	14.9	0.111	14.0	0.103	13.0	0.118	12.1	0.106	11.2	
55	.0015	0.155	17.1	0.148	16.1	0.120	15.1	0.125	14.2	0.118	13.8	0.121	12.4	
56	-0016	0.170	18.2	0.164	17.2	0.157	16.3	0.150	15.8	0.144	14.4	0.187	18.5	
	-0016	0.100	10										ا ـ ا	
57 d	-0017	0.186	19.4 20.5	0.180 0.197	18.4	0.178	17.4	0.167 0.188	16.5	0.160 0.177	15.6 16.7	0.153	14.7 15.8	
59	-0017	0.208	21.5	0.197	19.5 20.6	0.190	18.5 19.6	0.188	17.6 18.7	0.177	10.7	0.170	16.9	
60	-0018	0.288	22.5	0.281	21.6	0.225	20.6	0.218	19.6	0.211	18.7	0.205	17.8	
61	-0019	0.256	23.4	0.250	22.5	0.248	21.5	0.286	20.6	0.280	19.7	0.223	18.8	
	-0019													
62	.0020	0.275	24.4	0.269	23.5		22.4			0.249		0.242	19.7	
63 61 65 66 67	.0030	0.295	26.1	0.288 0.309	24.4 25.3	0.282 0.802	28.8 24.2	0.275 0.295	23.3	0.268 0.289	21.5	0.262 0.282	20.7 21.6	
65	-0021	0.886	27.0		26.1		25.1	0.295	24.2	0.209	23.3	0.202	22.4	
66	-0022	0.858	27.9		27.0		26.0	0.838	25.1	0.881	24.2	0.824	23.3	
67	-0023	0.880	28.7		27.8	0.867	26.8	0.860	25.9	0.858	25.0	0.846	24.2	
	Mean Horizontal Difference of Force of Vapor for each 0°.1 = 0.0018.													

PSYCHROMETRICAL TABLES.

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				t -1	t', or D	ference (of Wet	and Dry	Belb Ti	hermome	ters.		
Wet- Bulb Thermo- meter t'	Mean Vertical Difference of Force of Vapor	919	.0	21	·.5	224	·.o	22	.5	28	.0	28	.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity	Force of Vapor.	Reia- tive Hu- mid- ity.	Force of Vapor.		Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
		Eng. In.		Eng. In.		Eng. In.	,	Eng. In.		Eng. In.		Eng. In.	
68	0.0024	0.403	29.5	0.896	28.5	0.889	27.6	0.388	26.7	0.876	25.8	0.369	25.0
69	.0024	0.426	30.2	0.420	29.8	0.418	28.4	0.406	27.5	0.399	26.6	0.898	25.8
70	.0028	0.451	31.0	0.444	30.1 20.8	0.487	29.1	0.480	28.2	0.424	27.4 28.1	0.417	26.5 27.3
71	.00:26	0.476	31.7	0.469		0.462	29.9 30.6	0.455	29.0 29.7	0.449	28.8	0.442	28.0
72	.0027	0.501	32.4	0.495	81.5	0.488	30.0	0.481	28.1	0.175	20.0	0.400	20.0
73		0.528	83.1	0.521	82.2	0.515	81.8	0.508	80.4	0.501	29.5	0.494	28.7
74	.0038	0.556	83.8	0.549	32.8	0.542	31.9	0.585	31.1	0.529	30.2	0.522	29.4
75	.0028	0.584	84.4	0.577	88.5	0.570	32.6	0.564	31.7	0.557	80.9	0.550	30. 0
76	.0039	0.613	85.0	0.606	84.1	0.599	38.2	0.598	32.8	0.586	81.5	0.579	80.7
77		0.648	35.6	0.686	84.7	0.629	33.8	0.628	33.0	0.616	82.1	0.609	81.8
	.0031												n= 0
78	.0082	0.674	36.2	0.667	35.3	0.660	84.4	0.658	33.6	0.647	32.7 33.3	0.640	31.9 32.5
79	.0032	0.705	36.8	0.699	85.9 86.5	0.692	85.6 85.6	0.685 0.718	84.2	0.575	33.9	0.704	32.0
80	.0034	0.738	37.4 37.9	0.731 0.765	37.0	0.758	86.1	0.718	31.7	0.711	84.5	0.738	33.5
81 82	.0035	0.772 0.806	38.4	0.800	87.6	0.793	36.7	0.786	35.8	0.779	33.0	0.772	84.2
02	.0036	0.000	90.4	0.000	37.0	0.755	30.1	0.750	00.0	10	00.0	0.1.12	0112
83		0.842	89.0	0.935	88.1	0.829	87.2	0.822	36.4	0.813	35.5	0.808	34.7
81	.0037	0.879	39.5	0.872	88.6	0.865	87.7	0.858	86.9	0.852	86.1	0.845	35.2
85	.0038	0.917	40.0	0.910	89.1	0.903	88.2	0.896	87.4	0.889	86.6	0.882	35.8
P6	-0939	0.955	40.4	0.948	39.6	0.942	88.7	0.935	8 7.9	0.928	87.1	0.921	36.8
87	-0040	0.995	40.9	0.988	40.1	0.981	89.2	0.975	38.4	0.968	87.5	0.961	86.7
	-0041				~								
88	-0042	1.036	41.4	1.029	40.5	1.022	89.7	1.016	38.8	1.009	38.0	1.002	87.2
89	-0044	1.078	41.9	1.071	41.0	1.063	40.1	1.059	89.3	1.051	38.5 38.9	1.044	87.7
90	.0045	1.122	42.8	1.115	41.4	1.108	40.6	1.101	89.7	1.094	89.4	1.089	38.1 38.6
91 92	10019	1.166	42.7 43.1	1.160 1.206	41.9 42.8	1.153	41.0	1.146	40.2 40.6	1.139 1.185	39.8	1.132	39.0
34	-9846	1.212	40.1	1.200	44.0	1.100	21.4	1.194	40.0	1.100	55.0	*** ′′°	40.10
93		1.260	48.5	1.258	42.7	1.246	41.9	1.239	41.0	1.232	40.2	1.225	39.4
94	-0018	1.308	43.9	1.301	43.1	1.294	42.3	1.287	41.4	1.280	40.6	1.274	89.9
95	.0050	1.358	44.3	1.351	43.5	1.844	42.7	1.337	41.8	1.830	41.0	1.323	40.3
96	-0051	1.408	44.7	1.402	48.9	1.395	48.0	1.888	42.2	1.381	41.4	1.374	40.7
97	-0033	1.461	45.1	1.454	44.8	1.447	43.4	1.440	42.6	1.433	41.8	1.426	41.1
98	-0021	1.515	45.5	1.508	44.6	1.501	48.8	1.494	43.0	1.487	42.2	1.480	41.4
ا مم ا	-0056	, ,	47.0	7. FOR			4.0	, , , ,	40 -		42.6	1 700	41 0
99	-0057	1.570	43.8	1	45.0	I	44.2		43.4	1.543	48.0		41.8 42.2
100	.0059	1.627	46.2	1.620	45.4	1.618	44.5 44.9	1.607	43.7	1.600	43.8	1.593 1.651	42.5
101 102	.0060	1.686	46.5	1.679	45.7	1.672 1.732	45.2	1.665	44.4	1.658 1.718	43.7	1.711	42.9
102	-0062	1.807	47.2	•	46.4	1.793	45.6	1.786	44.8	1.779	41.0	1.772	43.2
104	.0063	1.870	47.5		46.7			1.849	45.1	1.842	44.8		l
	<u> </u>			1.550	,	1	1 23.0	1 *****		1 1042			
		Me	an Hori	izontal Di	ference	of Force	of Vap	or for eac	ь 0°.1	- 0.0018 .			

PSYCHROMETRICAL TABLES.

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				t-	t', or D	ifference	of Wet	and Dry	Bulb T	hermome	ters.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	24	·.O	24	5	25	°.0	25	°.5	26	°.0	26	s°.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rois- tive Hu- mid- ity.	Force of Vapor.		Force of Vapor.		Force of Vapor.	Rein- tive Hu- mid- ity.	Force o	
0		Eng. In.		Eng. In		Eng. In		Eng. In		ling. In.		Eng. In	
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47			l									ł	
48	0.0018	0.019	2.4	0.012	1.5	1							1
49	.0013	0.081	8.9	0.025	8.0	0.018	2.2	0.011	1.8				
50 51	-0018	0.044	5.2 6.5	0.087	4.4	0.081	8.6	0.024	2.7	0.018	2.0	0.011	1.2
»1	-0014	0.057	0.0	0.051	5.7	0.044	4.9	0.087	4.1	0.031	8.3	0.024	2.5
52	.0014	0.071	7.8	0.064	7.0	0.058	6.1	0.051	5.8	0.044	4.6	0.038	8.8
58	.0015	0.085	9.1	0.078	8.2	0.072	7.4	0.065	6.6	0.058	5.8	0.052	5.1
54 55	.0016	0.100	10.8 11.5	0.093	9.4	0.086	8.6	0.080	7.8	0.078	7.0	0.067 0.082	6.8
56	.0016	0.115	12.7	0.108	10.6 11.8	0.102 0.117	9.8 11.0	0.095	9.0 10.2	0.088 0.104	8.2 9.4	0.082	7.5 8.7
	.0016	- 1			11.0	0.22	11.0	0.222	10.2	0.101		4.501	
57	.0017	0.147	18.8	0.140	13.0	0.188	12.1	0.127	11.8	0.120	10.6	0.118	9.8
58 59	-0017	0.168	14.9 16.0	0.157 0.174	14.1	0.150	13.2	0.14 3 0.161	12.5	0.187	11.7	0.180	10.9 12.0
60	.0018	0.198	17.0	0.174	15.2 16.1	0.167 0.185	14.8 15.3	0.161	18.6 14.6	0.154	12.8 18.8	0.147 0.165	13.0
61	-0019	0.216	17.9	0.210	17.1	0.203	16.3	0.196	15.5	0.190	14.7	0.188	14.0
20	-0019			0.000		0.000		0.0		0.000		A 600	** ^
62 63	-0020	0.285	18.9	0.229	18.1	0.222	17.2		16.5	0.209	16.7	0.202	15.0 15.9
64	-0030	0.275	20.7		19.0 19.9	0.242	18.2 19.1	0.285	19.3		17.5	0.242	16.8
65	.0021	0.296	21.6	0.289	20.8	0.283	20.0	0.276	19.2	0.269	18.4	0.263	17.7
66	.0022 E	0.818	22.5	0.811	21.7	0.304	20.9	0.297	20.1	0.291	19.8	0.284	18.6
67		0.840	23.8	0.338	22.5	0.326	21.7	0.820	20.9	0.818	20.2	0.806	19.4
!	!	!	!				1						
		Mon	n Horis	ontal Diff	lerence (of Force	of Vapo	r for each	2 0°.1 =	0.0018.			

PSYCHROMETRICAL TABLES.

Temperature, Fahreabeit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

Wet	Moan			1-1	', or Di	ference (of Wet	and Dry	Balb Ti	hermome	ers.		
Bulb	Vertical Difference of Force of Vapor	24	.0	24	.5	25	·.o	25	·.5	26	·.o	26	·.5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Resp. tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Reia- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
. •		Eng. In.		Rog. In.	,	Eng. In.		Eng. In.		Eng. In.		Eng In.	
68	0.0024	0.363	24.2	0.356	23.3	0.849	22.5	0.842	21.8	0.386	21.8	0.829	20.8
69	.0024	0.386	24.9	0.379	24.1	0.378	23.3	0.866	22.6	0.859	21.8	0.852	21.1
70	.0025	0.410	25.7	0.403	24.9	0.897	24.1	0.890	23.8	0.858	22.6	0.377	21.9
71	.00-26	0.435	26.4	0.428	25.6	0.422	24.9	0.415	24.1	0.408	23.3	0.402	22.6
72	.0027	0.461	27.2	0.454	26.4	0.148	25.6	0.441	24.8	0.434	24.1	0.427	23.8
78		0.488	27.9	0.481	27.1	0.474	26.8	0.467	25.5	0.461	24.8	0.454	24.0
74	.0028	0.513	28.5	0.508	27.7	0.502	27.0	0.495	26.2	0.488	25.5	0.481	24.7
75	.0028	0.548	29.2	0.537	28.4	0.580	27.6	0.528	26.8	0.516	26.1	0.510	25.4
76	.0029 .6030	0.572	29.8	0.566	29.1	0.559	28.3	0.552	27.4	0.545	26.8	0.539	26.1
77	ł	0.602	80.5	0.595	29.7	0.589	28.9	0.582	28.0	0.575	27.4	0.568	26.7
	.0031			1		1				1			
78	.0032	0.633	81.1	0.626	80.3	0.619	29.5	0.618	28.7	0.606	28.0	0.599	27.8
79	.0038	0.665	81.7	0.658	80.9	0.651	80.1	0.644	29.8	0.638	28.6	0.631	27.9
80	-0034	0.697	82.8	0.691	81.5	0.684	80.7	0.677	29.9	0.670	29.2	0.668	28.5
81	.0035	0.781	82.8	0.724	82.1	0.717	31.8	0.711	30.5	0.704	29.8	0.697	29.1
82	.0036	0.766	88.4	0.759	82.6	0.752	31.8	0.745	81.0	0.738	80.4	0.782	29.7
83	.0026	0.801	83.9	0.795	83.2	0.788	82.4	0.781	81.6	0.774	80.9	0.767	30.2
84	-0037	0.888	84.5	0.881	88.7	0.824	82.9	0.818	82.1	0.811	81.5	0.804	80.7
85	.0038	0.876	85.0	0.869	84.2	0.862	88.4	0.855	32.7	0.848	82.0	0.842	81.3
86	-0039	0.914	85.5	0.908	84.7	0.901	83.9	0.894	88.2	0.887	82.5	0.880	81.8
87	-0040	0.954	86.0	0.947	85.2	0.940	84.4	0.934	88.7	0.927	83.0	0.920	82.8
	-0041												
88	.0042	0.995	86.4	0.988	35.7	0.981	84.9	0.975	84.2	0.968	88.5	0.961	32.8
89	.0044	1.087	36.9	1.080	36.1	1.024	35.4	1.017	34.7	1.010	83.9	1.008	33.2
90	.0045	1.081	37.4	1.074	86.6	1.067	35. 8	1.060	35.1	1.053	84.4	1.046	83.7
91	.0046	1.125	87.8	1.118	87.1	1.112	86.8	1.105	85.6	1.098	34.9	1.091	84.2
92		1.171	88.2	1.164	87.5	1.157	86.7	1.151	86.0	1.144	85.8	1.187	84.6
98	.0048	1.218	38.7	1.211	87.9	1.205	87.1	1.198	86.5	1.191	85.7	1.184	85.0
94	.0649	1.267	89.1	1.260	38.3	1.258	37.5	1.246	36.9	1.289	86.2	1.282	35.5
95	.0050	1.816	89.5	1.809	38.7	1.802	87.9	1.296	87.8	1.289	36.6	1.282	85.9
96	.0051	1.367	89.9	1.860	89.1	1.358	38.3	1.846	87.7	1.340	87.0	1.883	36.3
97	.0043	1.420	40.8	1.418	39.5	1.406	88.7	1.899	38.1	1.392	87.4	1.885	86.7
98	.0084	1.478	40.7	1.467	39.9	1.460	89.1	1,458	88.5	1.446	87.8	1.489	87.1
	.0066							, i					
99	.0037	1.529		1.522		1.515		1.508	88.9			1.494	87.5
100	.0039	1.586	41.4		40.7	1.572	89.9	1.565	89.2	1.558	88.5	1.551	37.9
101	-0060	1.644	41.8	1.637	41.0	1.680	40.8	1.628	89.6	1.616	88.9	1.609	88.2
102	.0062	1.704	42.2		41.4	1.690	40.7		40.0		89.8	1.669	88.6
108	.0063	1.765	42.5	1.758	41.8	1.751	41.0	1.745	40.8	1.788	89.6	1.731	38.9
104		1.828	423	1.821	42.1	1.814	41.4	1.807	40.7	1.800	40.0	1.793	89.3
		Mon	Horis	ontal Diff	erence	of Force	of Vap	or for eac	ь O°.1	- 0.0018.			

PSYCHROMETRICAL TABLES.

Correction for Barometrical Height above or below the Normal Height of 29.7 inches.

For				Dim	rence of	Thurm	moters,	or t-1	/ Fahre	abelt.				
Baromet- rical Height.	20	40	60	80	100	190	140	16°	18°	200	220	240	26°	
				·	Wet 1	Bulb abo	ve the \$	reesing	Point.		•			
Eng. In.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	
81.0	001	002	003	005	006	007	008	009	010	012	018	014	015	
30.5	.001	.001	.002	.003	.004	.004	.005	.006	.006	.007	.008	.009	.009	
80.0	000	000	001	001	001	002	002	002	002	003	003	003	004	
29.5 29.0	+.000	+.000	+.001	+.001	+.001	+.001	+.001	+.001	+.002	+.002	+.002	+.002	+.002	
28.6	.001	.001	.002	.008	.008	.004	.004	.005	.006	.006	.007	.018	.008	
23.0	.001	.002	.003	.004	.003	.000	.007	.009	.010	.011	.UIZ	.018	.014	
28.0	.001	.003	.005	.006	.008	.009	.011	.012	.014	.015	.017	.018	.020	
27.5	.002	.004	.006	.007	.010	.012	.014	.016	.018	.020	.022	.024	.026	
27.0	.002	.003	.007	.009	012	.014	.017	.019	.022	.024	.027	.029	.031	
26.5	.003	.006	.008	.011	.014	.017	.020	.028	.026	.029	.031	.034	.037	
26.0	.003	.006	.010	.013	.016	.020	.023	.026	.030	.088	.086	.040	.048	
25.5	.004	.007	.011	.014	.019	.022	.025	.030	.034	.037	.041	.045	.049	
			,	ļ					l				1	
25.0	.004	.008	.012	.016	.021	.025	.028	.038	.088	.042	.046	.050	.035	
24.0	.003	.010	.015	.020	.025	.030	.084	.010	.046	.051	.056	.061	.066	
28.0	.006	.012	.018	.023	.030	.035	-041	.047	.054	.060	.066	.072	.078	
22.0	.007	.013	.020	.027	.084	.041	.047	.054	-062	.069	.076	.083	.090	
21.0 20.0	.008	.015	.023	.080	.038	.046	.053	.062	.070	.077	.085	.098	.101	
20.0	+.008	+.017	+.026	+.084	+.048	+.051	+.059	+.069	+.078	+.086	+.095	+.104	+.118	
		Wet B	ulb belo	w the		! 	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u>'</u>		<u> </u>	
			sing-Po			EXAMPLE OF CALCULATION.								
31.0	001	002	003	004	006		7	Wet Bull	above t	he Free	dng-Poir	at.		
80.5	.001	.001	.002	.003	.003	'£' .	= 62°	F. t-	- t' =	10°.	Barom	— 26 .	5 in.	
30.0	000	000	001	001	001	T	he larg	e table	s give f	ora me	an bar	0-		
29.5	+.000	+.000	+.000	+.001	+.001		rical he		•		Force	_	Inch.	
29.0	.001	.001	.002	.002	.003	Vap			. •	•			0.403	
28.5	.001	.002	.003	.004	.005						able, f			
						B-	26.5 i	nches,	ena 10º	•		=	0.014	
23.0	.001	.008	.004	.005	.007		Co	orrected	Force	of Va	or	. =	0.417	
27.5	.002	.008	.008	.007	.009					•				
27.0	.002		.006	.008	.011	•				•	re, at a	•	•	
26.5 26.0	.002	.005	.007	.010	.014						the abo			
25.5	.003	.007	.010	.013	.016						for the			
23.3			.3.0								able, a			
25.0	.003	.007	.011	.015	.018						nbers i This co			
24.0	.004	.009	.018	.018							or the			
23.0	.005	.010	.016	.021	.026	L .		•	~		resenti			
22.0	.006	.012	.018	.024	.030						rs arisi			
21.0	.006	.014	.020	.027	.084						l little			
20.0	+.007	l		+.080	1	1	uracy of					•		
I	11	l	1	l	l	1	•							

TABLE VIII.

FOR DEDUCING THE RELATIVE HUMIDITY OF THE AIR FROM THE INDICATIONS, IN ENGLISH MEASURES, OF THE DEW-POINT INSTRUMENTS.

THE object of every Dew-Point instrument is to ascertain, by causing a part of the apparatus to cool, the temperature at which the vapor contained in the air begins to condense, in the shape of light dew, on the cooled portion of the instrument. It is obvious that this is the temperature at which the atmosphere itself, if cooled likewise, would be fully saturated by the amount of vapor present in the air at the time of the observation.

The temperature of the dew-point being known, all the hygrometrical conditions of the air can be easily deduced from it.

The Absolute Humidity, or the total amount of vapor in the atmosphere, is expressed by the number, in the Tables of Elastic Forces of Vapor, due to that temperature.

The Relative Humidity, or the degree of moisture, being the ratio of the quantity of vapor actually contained in the air to the quantity it could contain if fully saturated, is expressed by the proportion

Relative Humidity: 1:: Force of Vapor at Dew-Point: Maximum Force of Vapor.

Calling the

Force of Vapor at the Temperature of the Dew-Point, f; Force of Vapor at the Temperature of the Air, F;

then

Relative Humidity =
$$f$$
.

It is thus found by dividing the force of vapor due, in the Table of Elastic Forces, to the temperature of the dew-point, by the maximum of the force of vapor due, in the same table, to the temperature of the air at the time of the observation. F being always greater than f, when the air is not saturated, the Relative Humidity is expressed by a fraction, which is termed the *fraction of saturation*. Making the point of saturation = 100, in order to obtain this fraction in hundredths, we have

Relative Humidity =
$$\frac{f \times 100}{7}$$
.

Example.

Suppose the

Temperature of the Air, or t, to be $= 43^{\circ}$ F. Temperature of the Dew-Point, or t', to be $= 35^{\circ}$ F. Difference between the two, or t-t', to be $= 8^{\circ}$ F.

Taking in Table VI. the Elastic Forces due to t and t', we have

Force of Vapor at $t' = \frac{.3067 \times 100}{.2775} = 73.4$, Relative Humidity in Hundredths.

The following Table VIII. gives, in hundredths, the fraction of saturation, or Relative Humidity, corresponding to each degree of t', or of the temperature of the air, from 0° to 104°; and for every half degree of t—t', or of the difference between the temperature of the air and of the dew-point, from 0.°5 to 24.°5. Regnault's Table of Elastic Forces of Vapor, reduced to English measures, has been used in the computation.

Though the fraction of saturation expressed in hundredths indicates the Relative Humidity with sufficient accuracy, the thousandths have been added to facilitate, as remarked above in the preface to the Psychrometrical Tables, the interpolations for any number falling between those given in the table.

USE OF THE TABLE.

Example.

Temperature of Air, or t, being $= 62^{\circ}$ F. Temperature of the Dew-Point, or t', $= 53^{\circ}$ F. Difference, or t-t', $= 9^{\circ}$ F.

Find out the Relative Humidity.

In the column of temperatures, the first on the left, find 62°; on the same horizontal line, in the column headed 9°, is found 72.4, which is the Relative Humidity required.

Should it seem desirable to compute the Relative Humidity for values of t—t' not contained in the table, the factors given below in Table IX. may be used. It may be seen, however, that an interpolation at sight will always suffice for meteorological purposes.

VIII.

FOR DEDUCING THE RELATIVE HUMIDITY OF THE AIR,

FROM THE INDICATIONS OF DEW-POINT INSTRUMENTS.

Relative Humidity expressed in Hundredths, full Saturation being = 100.

Temper- ature of Air,		t-t'-1	Difference o	f Temperal	tures of the	Air and o	f the Dew-	Point. — Fr	hrenheit.	
Fahren- heit.	0.0	0.5	1.0	1.5	2.0	2.5	8.0	8.5	4.0	4.5
o°	100.	97.7	93.4	98.2	91.0	88.9	86.8	84.8	82.8	80.9
1	100.	97.7	93.5	98.8	91.1	89.0	86.9	84.9	82.9	81.0
2	100.	97.7	95.5	98.8	91.2	89.1	87.0	85.0	88.0	81.1
8	100.	97.8	95.5	98.4	91.2	89.2	87.1	85.1	88.1	81.2
4	100.	97.8	95.6	93.1	91.8	89.2	87.2	85.2	88.2	81.8
5	100.	97.8	95.6	93.5	91.4	89.8	87.8	85.3	83.3	81.4
6	100.	97.8	93.8	93.5	91.4	89.8	87.3	85.3	83.3	81.5
7	100.	97.8	95.6	98.5	91.4	89.8	87.3	85.8	83.4	81.5
8	100.	97.8	93.6	93.5	91.8	89.3	87.8	85.8	88.4	81.5
9	100.	97.8	95.6	93.5	91.8	89.3	87.3	85.8	83.4	81.5
10	100.	97.8	95.6	93.4	91.8	89.8	87.8	85.8	83.4	81.5
31	100.	97.8	95.6	93.4	91.3	89.3	87.3	85.3	88.4	81.6
12	100.	97-8	95.5	93.4	91.8	89.8	87.8	85.4	83.4	81.6
13	100.	97.8	93.5	93.4	91.8	89.3	87.8	85.4	88.5	81.6
14	100.	97.7	95.5	93.4	91.8	89.3	87.8	85.4	88.5	81.7
15	100.	97.7	95.5	93.4	91.3	89.4	87.4	85.5	88.5	81.7
16	100.	97.7	95.5	98.4	91.8	89.3	87.3	85.4	88.5	81.6
17	100.	97.7	95.5	93.4	91.8	89.3	87.8	85.8	88.4	81.6
18	100.	97.7	95.5	98.4	91.3	89.8	87.8	85.8	88.4	81.5
19	100.	97.8	95.5	98.4	91.8	89.8	87.2	85.2	88.3	81.4
	0.0	0.5	1.0	1.5	2.0	2.5	3.0	8.5	4.0	4.5

	1	t-t'-1	Difference o	of Tempera	tures of th	e Air and c	of the Dew-	Point. — F	ahrenheit.	
Temper- ature of Air,						1		1	1	<u> </u>
Fahren- heit.	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5
0°	79.0	77.2	75.4	78.6	. 71.9	70.1	69.5	66.9	65.8	63.7
1	79.1	77.8	75.5	73.7	72.0	70.2	68.6	67.0	65.4	63.8
2	79.2	77.4	75.6	73.8	72.1	70.8	68.7	67.1	65.5	64.0
8	79.3	77.5	75.7	73.9	72.2	70.5	68.8	67.2	65.6	64.1
4	79.4	77.6	75.8	74.0	72.3	70.6	68.9	67.3	65.7	64.2
5	79.5	77.7	75.9	74.1	72.4	70.7	69.1	67.4	65.8	64.4
6	79.6	77.8	76.0	74.2	72.5	70.8	69.2	67.6	66.0	64.5
7	79.6	77.8	76.0	74.3	72.6	70.9	69.3	67.7	66.1	64.6
8	79.6	77.9	76.1	74.4	72.7	71.0	69.4	67.8	66.2	64.7
9	79.7	77.9	76.1	74.4	72.7	71.1	69.5	67.9	66.8	64.8
10	79.7	77.9	76.2	74.5	72.8	71.2	69.6	68.0	66.4	64.9
11	79.7	78.0	76.2	74.5	72.8	71.2	69.6	68.0	66.5	64.9
12	79.8	78.0	76.2	74.5	72.9	71.2	69.6	68.0	66.5	63.0
13	79.8	78.0	76.3	74.6	72.9	71.8	69.6	68.1	66.5	65.0
14	79.8	78.1	76.3	74.6	72.9	71.8	69.6	68.1	66.5	65.1
15	79.8	78.1	76.8	74.6	72.9	71.8	69.7	68.1	66.6	65.1
16	79.8	78.0	76.2	74.5	72.9	71.2	69.6	68.1	66.5	65.1
17	79.7	77.9	76.1	74.5	72.8	71.2	69.6	68.0	66.5	65.0
18	79.6	77.8	76.1	74.4	72.7	71.1	69.5	68.0	66.5	65.0
19	79.6	77.8	76.0	74.8	72.7	71.1	69.5	68.0	66.4	63.0
	10.0	10.5	11.0	11.5	19.0	19.5	13.0	13.5	14.0	14.5
0°	62.1	60.7	59.2	57.7	56.3	54.9	53.6	52.3	51.0	49.8
1	62.3	60.8	59.3	57.9	56.5	55.1	53.7	52.5	51.2	50.0
2	62.4	61.0	59.5	58.1	56.6	55.8	53.9	52.7	51.4	50.1
3	62.6	61.1	59.6	58.2	56.8	55.5	54.1	52.8	51.5	50.3
4	62.7	61.8	59.8	58.4	57.0	53.7	54.8	53.0	51.7	50.5
5	62.9	61.4	60.0	58.6	57.2	55.8	54.5	58.2	51.9	50.7
- 6	63.0	61.5	60.1	58.7	57.8	55.9	54.6	58.3	52.0	50.8
7	63.1	61.7	60.2	58.8	57.4	56.0	54.7	58.4	52.1	50.9
8	63.2	61.8	60.3	58.9	57.5	56.2	54.8	53.5	52.3	51.0
9	63.3	61.9	60.4	59.0	57.6	56.8	24-9	53.6	52.4	51.2
10	63.4	62.1	60.5	59.1	57.7	56.4	55.0	53.8	52.5	51.3
11	63.5	62.1	60.6	59.2	57.8	56.5	55.1	53.9	52.6	51.4
12	63.5	62.1	60.6	59.8	57.9	56.6	55.2	54.0	52.7	51.5
13	63.5	62 2	60.7	59.8	58.0	56.6	55.3	54.1	52.8	51.6
14	63.6	62.3	60.8	59.4	58.1	56.7	55.4	54.2	52. 9	51.7
15	63.6	62.3	60.8	59.5	58.1	56.8	55.5	54.3	58.0	51.9
16	68.6	62.3	60.8	59.5	58.1	56.8	55.5	54.8	58.0	61.8
17	63.6	62.2	60.8	59.4	58.1	56.7	55.5	54.2	53.0	51.8
18	63.5	62.2	60.7	59.4	58.0	56.7	55.4	54.2	53.0	51.8
19	68.5	62.1	60.7	59.8	58.0	56.6	55.4	54.2	52.9	51.8

Temper- ature of Air,		t — t' = I	Afference o	f Temperal	sures of the	Air and o	f the Dew-	Point. — F	abrenheit.	
Fahren- heit.	15.0	15.5	16.0	16,5	17.0	17.5	18.0	18.5	19.0	19.5
0°	48.5	47.8	46.1	45.0	43.9	42.8	41.6	40.6	89.5	88.5
1	48.7	47.5	46.3	45.2	44.0	42.9	41.8	40.8	39.7	88.7
2	48.9	47.7	46.5	45.4	44.2	48.1	42.0	41.0	89.9	88.9
8	49.1	47.9	46.7	45.5	44.4	48.8	42.2	41.2	40.2	89.2
4	49.8	48.1	46.9	45.7	41.6	48.5	42.4	41.4	40.4	89.4
5	49.4	48.2	47.1	45.9	44.8	43.7	42.6	41.6	40.6	89.6
6	49.6	48.4	47.2	46.1	44.9	48.9	42.8	41.8	40.7	89.8
7	49.7	48.5	47.8	46.2	45.1	44.0	42.9	41.9	40.9	89.9
8	49.8	48.7	47.5	46.4	45.8	44.2	48.1	42.1	41.1	40.1
9	50.0	48.8	47.6	46.5	45.4	44.8	48.3	42.2	41.2	40.2
10	50.1	48.9	47.8	46.7	45.6	44.5	48.4	42.4	41.4	40.4
11	50.2	49.0	47.9	46.8	45.7	44.6	48.5	42.5	41.5	40.5
12	50.3	49.1	48.0	46.9	45.8	44.7	48.6	42.6	41.6	40.6
13	50.4	49.2	48.1	47.0	45.9	44.8	43.7	42.7	41.7	40.7
14	50.5	49.3	48.2	47.1	46.0	44.9	48.8	42.8	41.8	40.8
15	50.6	49.4	48.8	47.2	46.1	45.0	43.9	42.9	41.9	40.9
16	50.6	49.5	48.8	47.2	46.1	45.0	44.0	43.0	41.9	41.0
17	50.6	49.5 -	48.8	47.2	46.1	45.0	44.0	48.0	42.0	41.0
18	50.6	49.5	48.8	47.2	46.2	45.0	44.1	43.1	42.0	41.1
19	50.6	49.5	48.3	47.8	46.2	45.1	44.1	48.1	42.1	41.1
	20.0	20.5	21.0	21.5	22.0	22.5	23.0	28.5	24.0	24.5
o°	37.5	86.5	35.5	84.6	88.7	82.8	81.9	81.0	80.2	29.3
1	87.7	86-8	35.8	84.8	83.9	38.0	32.1	81.8	80.4	29.6
2	87.9	87.0	86.0	85.1	84.2	33.8	82.4	31.5	80.7	29.9
8	38.2	37.2	86.2	35.8	84.4	33.5	82.6	81.8	80.9	30.1
4	88.4	87.4	86.5	85.6	34.6	88.8	82.9	82.0	31.2	80.4
5	88.6	87.7	86.7	35.8	34.9	84.0	83.1	82.3	81.4	30.6
6	38.8	87.8	86.9	86.0	85.0	84.2	83.3	82.5	81.6	80.8
7	88.9	38.0	87.0	86.1	85.2	84.8	88.5	82.6	31.8	81.0
8	39.1	38.1	87.2	36.3	85.4	84.5	88.6	32.8	82.1	81.2
9	89.2	88.8	87.8	86.4	85.5	84.7	83.8	88.0	82.3	81.4
10	39.4	38.4	87.5	36.6	85.7	34.8	84.0	83.1	82.5	31.6
11	89.5	38.6	37.6	86.7	35.8	85.0	84.1	88.8	82.6	81.7
12	89.6	89.7	87.8	36.9	86.0	85.1	84.2	88.4	82.7	31.8
13 14	39.8 39.9	88.8 39.0	37.9 88.0	87.0 87.1	86.1 36.2	85.2 85.4	84.4 84.5	33.6 33.7	32.8 32.9	82.0 82.1
										-3
15	40.0	89.1	38.2	87.8	36.4	85.5	84.7	83.9	33.0	32.2
16	40.0	89.1	88.2	87.8	26.4	85.6	84.7	88.9	88.1	82.8
17	40.1	39.2	88.2	87.4	86.5	85.6	84.8	84.0	33.1	82.4
18	40.1	39.2	38.3	87-4	86.5	85.7	34.8	34.0	88.2	82.4
19	40.2	39.3	38.3	37.5	86.6	85.7	84.9	84.1	38.2	82.5

Temper- ature		t-t'-1	Difference o	of Tempera	tures of th	• Air and o	of the Dew-	Point. — F	hrenbeit.	
of Air, Fahren- beit.	0.0	0.5	1.0	1.5	2.0	2.5	8.0	8.5	4.0	4.5
20°	100.	97.8	95.6	98.4	91.8	89.2	87.2	83.2	83.2	81.3
21	100.	97.8	95.6	93.4	91.3	89.8	87.8	85.3	83.3	81.5
22	100.	97.8	95.6	93.5	91.4	89.3	87.3	85.4	83.4	81.6
23	100.	97.8	95.6	93.5	91.4	89.4	87.4	85.5	83.5	81.7
24	100.	97.8	95.7	98.5	91.5	89.5	87.5	85.5	83.6	81.8
25	100.	97.8	. 95.7	98.6	91.5	89.5	87.6	85.6	83.7	81.9
26	100.	97.8	95.7	98.6	91.6	89.6	87.7	85.7	83.8	82.0
27	100.	97.9	95.8	93.7	91.7	89.7	87.8	85.9	84.0	82.1
28	100.	97.9	95.8	98.8	91.8	89.8	87.9	86.0	84.1	82.3
29	100.	97.9	95.9	93.8	91.8	89.9	88.0	86.1	84.2	82.4
80	100.	97.9	95.9	93.9	91.9	90.0	88.1	86.2	84.3	82.5
31	100.	98.0	96.0	94.0	92.0	90.1	88.2	86.4	84.5	82.7
82	100.	98.0	96.0	94.0	92.1	90.2	88.4	86.6	84.7	83.0
88	100.	98.0	96.1	94.1	92.2	90.4	88.6	86.7	84.9	88.2
84	100.	98.0	96.1	94.2	92.3	90.5	88.7	86.9	85.1	83.4
85	100.	98.0	96.1	94.8	92.4	90.6	88.9	87.1	85.8	83.6
36	100.	98.1	96.2	94.3	92.5	90.7	88.9	87.1	85.4	83.7
87	100.	98.1	96.2	94.8	92.5	90.7	88.9	87.2	85.4	83.7
88	100.	98.1	96.2	94.8	92.5	90.7	89.0	87.2	85.5	83.8
39	100.	98.1	96.2	94.8	92.5	90.7	89.0	87.2	85.5	88.9
40	100.	96.1	96.2	94.4	92.5	90.8	89.0	87.8	85.6	83.9
41	100.	98.1	96.2	94.4	92.6	90:8	89.1	87.8	85.7	84.0
42	100.	98.1	96.2	94.4	92.6	90.8	89.1	87.4	85.7	84.1
43	100.	98.1	96.3	91.4	92.6	90.9	89.2	87.5	85.8	84.2
44	100.	98.1	96.8	94.5	92.7	90.9	89.2	87.5	85.9	84.2
45	100.	98.1	96.8	94.5	92.7	91.0	89.8	87.6	85.9	84.8
46	100.	98.1	96.8	94.5	92.7	91.0	89.3	87.6	86.0	84.4
47	100.	98.1	96.3	94.5	92.8	91.0	89.3	87.7	86.0	84.4
48	100.	98.2	96.8	94.6	92.8	91.1	89.4	87.7	86.1	84.4
49	100.	98.2	96.4	94.6	92.8	91.1	89.4	87.7	86.1	84.5
50	100.	98.2	96.4	94.6	92.9	91.1	89.4	87.8	86.2	84.5
51	100.	98.2	96.4	94.6	92.9	91.2	89.5	87.8	86.2	84.6
52	100.	98.2	96.4	94.6	92.9	91.2	89.5	87.9	86.3	84.7
53	100.	98.2	96.4	94.7	92.9	91.2	89.6	87.9	86.3	84.7
54	100.	98.2	96.4	94.7	98.0	91.8	89.6	88.0	86.4	84.8
55	100.	98.2	96.5	94.7	98.0	91.8	89.7	88.0	86.4	84.8
56	100.	98.2	96.5	94.7	93.0	91.4	89.7	88-1	86.5	84.9
57	100.	98.2	96.5	94.8	93.1	91.4	89.7	88.1	86.5	95.0
58	100.	98.2	96.5	94.8	93.1	91.4	89.8	88.2	86.6	85.0
59	100.	98.2	96.5	94.8	93.1	91.5	89.8	88.2	86.6	85.1
60	100.	98.2	96.5	94.8	93.2	91.5	89.9	88.3	86.7	85.1
61	100.	98.3	96.5	94.9	98.2	91.5	89.9	88.8	86.7	85.2
62	100.	98.8	96.6	94.9	93.2	91.6	90.0	88.4	86.8	85.3
	0.0	0.5	1,0	1.5	. 2.0	2.5	3.0	3.5	4.0	4.5

lemper- ature of Air,		t — t' = 1	Afference o	f Tempera	tures of the	Air and o	the Dew-	Point. — T	ahrenheit.	
Pahren- heit.	0.0	0.5	1.0	1.5	2.0	2.5	8.0	2.5	4.0	4.5
62°	100.	98.8	96.6	94.9	93.2	91.6	90.0	88.4	86.8	85.3
63	100.	98.3	96.6	94.9	93.2	91.6	90.0	88.4	86.8	85.
64	100.	98.3	96.6	94.9	93.3	91.6	90.0	88.5	86.9	85.
65	100.	98.8	96.6	94.9	93.3	91.7	90.1	88.5	86.9	85.
66	100.	98.8	96.6	94.9	98.8	91.7	90.1	88.5	87.0	85.
67	100.	98.8	96.6	95.0	98.8	91.7	90.1	88.6	87.0	85.
63	100.	98.3	96.6	95.0	98.4	91.8	90.2	88.6	87.1	85.
69	100.	98.8	96.6	95.0	98.4	91.8	90.2	88.7	87.2	85.
70	100.	99.8	96.7	95.0	93.4	91.8	90.8	88.7	87.2	85.
71	100.	98.8	96.7	95.0	98.4	91.9	90.8	88.8	87.2	85.6
72	100.	98.3	96.7	93.1	98.5	91.9	90.8	88.8	87.8	85.6
73	100.	98.3	96.7	95.1	98.5	91.9	90.4	88.8	87.3	85.1
74	100.	98.3	96.7	95.1	98.5	91.9	90.4	88.9	87.4	85.9
75	100.	98.3	96.7	95.1	93.5	92.0	90.4	88.9	87.4	86.0
76	100.	98.3	96.7	95.1	93.6	92.0	90.5	89.0	87.5	86.0
77	100.	99.4	96.7	95.2	98.6	92.0	90-5	89.0	87.5	86.
79	100.	98.4	96.7	95.2	93.6	92.1	90.5	89.1	87.6	86.
79	100.	93.4	96.8	95.2	98.6	92.1	90.6	89.1	87.6	86.
80	100.	98.4	96.8	95.2	93.6	92.1	90.6	89.1	87.7	86 :
81	100.	98.4	96.8	95.2	98.7	92.1	90.6	89.2	87.7	86.
82	100.	99.4	96.8	93.2	93.7	92.2	90.7	89.2	87.8	86.
83	100.	98.4	96.8	95.8	98.7	92.2	90.7	89.3	87.8	86.
84	100.	98.4	96.8	95.3	98.7	92.2	90.8	89.8	87.8	86.
85	100.	98.4	96.8	93.8	93.8	92.3	90.8	89.8	87.9	86.
86	100.	98.4	96.8	95.8	93.8	92.3	90.8	89.4	87.9	86-1
87	100.	98.4	96.9	95.8	93.8	92.3	90.9	89.4	88.0	26.0
88	100.	98.4	96.9	95.8	98.8	92.3	90.9	89.4	88.0	86.6
89	100.	98.4	96.9	95.4	93.9	92.4	90.9	89.5	88.1	86.1
90	100.	98.4	96.9	95.4	93.9	92.4	91.0	89.5	88.1	86.1
91	100.	99.4	96.9	95.4	98.9	92.4	91.0	89.6	88.2	86.8
92	100.	98.5	96.9	95.4	93.9	92.5	91.0	89.6	88.2	86.8
93	100.	98.5	96.9	95.4	98.9	92.5	91.1	89.6	88.2	86.9
94	100.	98.5	96.9	95.4	94.0	92.5	91.1	89.7	88.3	86.9
93	100.	98.5	97.0	95.5	91.0	92.5	91.1	89.7	88.8	87.0
96	100.	98.5	97.0	95.5	94.0	92.6	91.2	89.7	88.4	87.0
97	100.	99.5	97.0	95.5	94.0	92.6	91.2	89.8	88.4	8%(
93	100.	98.5	97.0	95.5	94.1	92.6	91.2	89.8	88.4	87.1
99	100.	99.5	97.0	95.5	94.1	92.7	91:8	89.9	88.5	87.1
100	100.	98.5	97.0	95.6	94.1	92.7	91.3	89.9	88.5	87.5
101	100.	98.5	97.0	95.6	94.1	92.7	91.3	89.9	88.6	87.5
102	100.	98.5	97.0	95.6	94.2	92.7	91.4	90.0	83.6	87.3
103	100.	98.5	97.0	95.6	94.2	92.8	91.4	90.0	88.7	87.5
104	100.	99.5	97.0	95.6	94.2	92.8	91.4	90.0	88.7	87.
	0.0	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5

Temper-		t — t' — I	Difference o	f Temperat	tures of the	Air and o	f the Dew-	Point I	shrenheit.	
of Air, Fabren- beit.	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5
20°	79.5	77.7	75.9	74.2	72.6	71.0	69.4	67.9	66.4	61.9
21	79.6	77.8	76.0	74.8	72.7	71.1	69.5	68.0	66.4	65.0
22	79.7	77.9	76.1	74.4	72.8	71.2	69.6	68.0	66.5	65.0
28	79.8	78.0	76.2	74.6	72.9	71.8	69.6	68.1	66.5	65.0
21	79.9	78.1	76.4	74.7	78.0	71.4	69.7	68.1	66.6	65.1
25	80.0	78.2	76.5	74.8	78.1	71.5	69.8	68.2	66.6	65.1
26	80.2	78.4	76.6	74.9	78.2	71.7	70.0	68.4	66.8	65.8
27	80#	78.5	76.8	75.1	78.4	71.8	70.1	68.6	67:0	65.5
28	80.5	76.7	76.9	75.2	73.6	72.0	70.8	68.8	67.2	65.7
29	80.6	78.8	77.1	75.4	78.7	72.1	70.5	68.9	67.4	65.9
80	80.7	78.9	77.2	75.6	78.9	72.8	70.7	69.1	67.6	66.1
31	81.0	79.2	77.5	75.8	74.2	72.6	71.0	69.4	67.9	66.4
82	81.2	79.4	77.7	76.1	74.4	72.8	71.8	69.7	68.2	66.7
33	81.4	79.7	78.0	76.4	74.7	78.1	71.5	70.0	68.5	67.0
84	81.7	79.9	78.8	.76.6	75.0	78.4	71.8	70.8	68.8	67.8
85	81.9	80.2	78.5	76.9	75.8	78.7	72.1	70.6	69.1	67.6
36	82.0	80.8	78.6	77.0	75.4	78.9	72.8	70.8	69.8	67.8
37	82.0	80.4	78.8	77.2	75.6	74.0	72.5	71.0	69.5	68.1
38	82.1	80.5	78.9	77.8	75.8	74.2	72.7	71.2	69.8	68.3
39	82.2	80.6	79.0	77.4	75.9	74-4	72.9	71.5	70.0	68.6
40	82.8	80.7	79.1	77.6	76.1	74.6	78.2	71.7	70.2	68.8
41	82.4	80.8	79.2	77.7	76.2	74.7	73.2	71.8 ·	70.3	68.9
42	82.5	80.9	79.8	77.8	76.8	74.8	78.3	71.9	70.5	69.0
43	82.5	80.9.	79.4	77.9	76.4	74.9	78.4	72.0	70.6	69.2
44	82.6	81.0	79.5	78.0	76.5	75.0	78.5	72.1	70.7	69.8
45	82.7	81.1	79.6	78.0	76.5	75.1	78.6	72.2	70.8	69.4
46	82.8	81.2	79.6	78.1	76.6	75.1	78.7	72.3	70.9	69.5
47	82.8	81.2	79.7	78.2	76.7	75.2	73.8	72.4	71.0	69.6
48	82.9	81.8	79.8	78.2	76.8	75.8	73.9	72.5	7 b 1	69.7
49	82.9	81.8	79.8	78.3	76.8	75.4	74.0	72.6	71.2	69.8
50	88.0	81.4	79.9	78.4	76.9	75.5	74.0	72.7	71.3	69.9
51	83.0	81.5	80.0	78.5	77.0	75.5	74.1	72.8	71.4	70.0
52	83.1	81.5	80.0	78.5	77.1	75.6	74.2	72.8	71.5	70.1
53	83.2	81.6	80.1	78.6	77.2	75.7	74.8	72.9	71.6	70.2
54	83.2	81.7	80.2	78.7	77.2	75.8	74.4	78.0	71.7	70.8
55	83.3	81.8	80.3	78.8	77.8	75.9	74.5	78.1	71.8	70.4
56	83.4	81.8	80.3	78.9	77.4	76.0	74.6	73.2	71.9	70.5
57	83.4	81.9	80.4	78.9	77.5	76.1	74.7	73.3	72.0	70.6
58	83.5	82.0	80.5	79.0	77.6	76.2	74.8	78.4	72.1	70.7
59	83.6	82.0	80.6	79.1	77.7	76.2	74.9	78.5	72.2	70.9
60	83.6	82.1	80.6	79.2	77.7	76.8	75.0	78.6	72.3	71.0
61	83.7	82.2	80.7	79.2	77.8	76.4	75.0	73.7	72.4	71.0
62	83.7	82.2	80.8	79.3	77.9	76.5	75.1	73.8	72.4	71.1
	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5

Tumper- ature of Air,		t-v-1	Milerence o	f Temperat	cares of the	Air and o	f the Dew-	Point. — F	ahrenheit.	
Fahren- heit.	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5
62°	83.7	82.2	80.8	79.8	77.9	76.5	75.1	78.8	72.4	71.1
63	83.8	82.8	80.8	79.4	78.0	76.6	75.2	78.9	72.5	71.2
64	83.9	82.4	80.9	79.5	78.1	76.7	75.8	74.0	72.6	71.3
65	83.9	82.4	81.0	79.6	78.1	76.8	75.4	74.0	72.7	71.4
66	84.0	82.5	81.1	79.6	78.2	76.8	75.5	74.1	72.8	71.5
67	84.0	82.6	81.1	79.7	78.8	76.9	75.6	74.2	72.9	71.6
68	84.1	82.6	81.2	79.8	78.4	77.0	75.7	74.8	78.0	71.7
69	84.2	82.7	81.8	79.9	78.5	77.1	75.7	74.4	78.1	71.8
70	84.2	82.8	81.3	79.9	78.5	77.2	75.8	74.5	73.2	71.9
71	84.8	82.8	81.4	80.0	78.6	77.3	75.9	74.6	73.8	72.0
72	84.3	82.9	81.5	80.1	78.7	77.8	76.0	74.7	78.4	72.1
78	84.4	88.0	81.5	80.1	78.7	77.4	76.1	74.8	73.5	72.2
74	84.5	83.0	81.6	80.2	78.8	77.5	76.2	74.9	73.6	72.3
75	84.5	88.1	81.7	80.3	78.9	77.6	76.2	74.9	78.7	72.4
76	84.6	88.1	81.7	80.4	78.9	77.7	76.8	75.0	78.7	72.5
77	84.6	88.2	81.8	90.4	79.0	77.7	76.4	75.1	78.8	72.6
78	84.7	83.3	81.9	80.5	79.1	77.8	76.5	75.2	78.9	72.7
79	84.7	83.3	81.9	80.6	79.1	77.9	76.6	75.3	74.0	72.8
80	84.8	83.4	82.0	80.6	79.2	78.0	76.7	75.4	74.1	72.9
81	84.9	88.5	82.1	80.7	79.8	78.0	76.7	75.5	74.2	78.0
82	84.9	83.5	82.1	80.8	79.4	78.1	76.8	75.5	74.8	73.0
88	85.0	83.6	82.2	80.8	79.4	78.2	76.9	75.6	74.4	78.1
84	85.0	88.6	82.8	80.9	79.5	78.3	77.0	75.7	74.5	73.2
85	85.1	83.7	82.8	81.0	79.6	78.4	77.1	75.8	74.6	73.8
86	85.1	83.7	82.4	81.1	79.7	78.4	77.1	75.9	74.6	78.4
87	83.2	83.8	82.5	81.1	79.8	78.5	77.2	76.0	74.7	78.5
88	85.2	83.9	82.5	81.2	79.9	78.6	77.8	76.1	74.8	78.6
89	85.8	88.9	82.6	81.3	79.9	78.7	77.4	76.1	74.9	78.7
90	85.8	84.0	82.6 82.7	81.8	80.0 80.1	78.7	77.5	76.2 76.3	75.0 75.1	78.8
91 92	85.4 85.4	84.0 84.1	82.7 82.8	81.4 81.5	80.2	78.8 78.9	77.5 77.6	76.4	75.1	73.9 74.0
										, ·
93	85.5	84.2	82.8	81.5	80.2	79.0	77.7	76.5	75.2	74.0
94	85.6	84.2	82.9 83.0	81.6	80.8 80.4	79.0 79.1	77.8 77.9	76.6 76.6	75.3 75.4	74.1
95 96	85.6 85.7	84.8 84.8	88.0	81.7 81.7	80.4	79.1	77.9	76.7	75.5	74.2
97	85.7	84.4	88.1	81.8	80.5	79.8	78.0	76.8	75.6	74.4
98	85.8	84.4	88.1	81.9	80.6	79.8	78.1	76.9	75.7	74.5
99	85.8	84.5	88.2	81.9	80.7	79.4	78.2	77.0	75.8	74.6
100	85.9	84.6	83.3	82.0	80.7	79.4	78.3	77.0	75.8	74.7
101	85.9	84.6	88.8	82.0	80.8	79.6	78.8	77.1	75.9	74.8
102	86.0	84.7	83.4	82.1	80.9	79.6	78.4	77.2	76.0	74.9
103	86.0	84.7	83.4	82.2	80.9	79.7	78.5	77.8	76.1	74.9
104	86.1	84.8	88.5	82.2	81.0	79.8	78.6	77.4	76.2	75.0
	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5

ture of Air,		t — t' = I	Afference o	f Temperat	tures of the	Air and o	the Dew-	Pôlat. — Fe	hreabelt.	
Fahren- heit.	10.0	10.5	11.0	11.5	12.0	12.5	18.0	13.5	14.0	14.5
20°	63.5	62.1	60.6	59.8	58.0	56.6	55.4	54.1	52.9	51.7
21	68.5	62.1	60.7	59.8	58.0	56.6	55.4	54.2	53.0	51.8
22	63.5	62.1	60.7	59.4	58.0	56.7	55.5	54.2	58.0	51.8
28	68.6	62.1	60.7	59.4	58.0	56.7	55.5	54.8	53.0	51.9
24	68.6	62.1	60.7	59.4	58.1	56. 8	55.5	54.8	58.1	51.9
25	63.6	62.1	60.7	59.4	58.1	56.8	55.6	54.4	58.1	52.0
26	63.8	62.8	60.9	59.6	58.8	57.0	55.7	54.5	58.8	52.1
27	64.0	62.5	61.1	59.8	58.5	57.2	55.9	54.6	58.4	52.2
28	64.2	62.7	61.8	60.0	58.6	57.8	56.0	54.8	53.5	52.3
29	64.4	68.0	61.5	60.2	58.8	57.5	56.2	54.9	58.7	52.4
80	64.6	63.2	61.8	60.4	59.0	57.7	56.8	55.1	53. 8	52.6
31	64.9	63.5	62.1	60.7	59.3	58.0	56.6	55.4	54.1	52.9
82	65.2	63.8	62.4	61.0	59.6	58.3	57.0	55.7	54.4	58.2
83	63.5	64.1	62.7	61.3	59.9	58.6	57.8	56.0	54.7	53.5
84	65.8	64.4	68.0	61.6	60.2	58.9	57.6	56.3	55.0	53.8
82	66.1	64.7	68.8	61.9	60.5	59.2	57.9	56.6	55.4	54.1
36	66.4	64.9	63.5	62.1	60.8	59.5	58.2	56.9	55.6	51.4
37	66.6	65.2	63.8	62.4	61.1	59.8	58.5	57.2	55.9	54.7
89	66.9	65.5	64.1	62.7	61.4	60.1	58.8	57.5	56.2	55.0
39	67.1	65.7	64.4	63.0	61.7	60.8	59.1	57.8	56.5	55.3
40	67.4	66.0	64.6	63.8	62.0	60.6	59.4	58.1	56.8	55.6
41	67.5	66.1	61.8	63.5	62.1	60.9	59.6	58.8	57.1	55.9
42	67.7	66.8	63.0	63.6	62.3	61.1	59.8	58.6	57.3	56.1
43	67.8	66.4	65.1	63.8	62.5	61.8	60.0	58.8	57.6	56.4
44	67.9	66.6	65.3	64.0	62.7	61.5	60.3	59.0	57.8	56.6
45	68.1	66.7	65.4	64.2	62.9	61.7	60.5	59.8	58.1	56.9
46	63.2	66.9	65.6	64.8	63.0	61.8	60.6	59.4	58.2	57.0
47	68.3	67.0	88.7	64.4	63.2	61.9	60.7	59.5	58.3	57.2
48	68.4	67.1	65.8	64.5	63.8	6 2 .0	60.8	59.6	58.5	57.8
49	68.5	67.2	63.9	64.6	63.4	62.1	61.0	59.8	58.6	57.4
50	69.6	67.8	66.0	64.7	63.5	62.2	61.1	59.9	58.7	57.6
51	69.7	67.4	66.1	64.9	63.6	62.4	61.2	60.0	58.9	57.7
52	68.8	67.5	66.2	65.0	63.7	62.5	61.8	60.1	59.0	57.8
53	68.9	67.6	66.4	65.1	63.9	62.6	61.4	60.8	59.1	58.0
51	69.0	67.7	66.5	65.2	64.0	62.7	61.6	60.4	59.2	58.1
55	69.1	67.8	66.6	65.3	64.1	62.9	61.7	60.5	59.4	58.2
56	69.2	67.9	66.7	65.4	64.2	68.0	61.8	60.6	59.5	58.4
57	69.3	69.1	66.8	65.6	64.8	68.1	61.9	60.8	59.6	58.5
58	69.5	68.2	66.9	65.7	64.4	63.2	62.1	60.9	59.8	58.6
59	69.6	68.8	67.0	65.8	64.6	63.4	62.2	61.0	59.9	58 8
60	69.7	68.4	67.1	65.9	64.7	63.5	62.8	61.2	60.0	58.9
61	69.8	68.5	67.2	66.0	64.8	63.6	62.4	61.3	60.1	59.0
62	69.9	68.6	67.4	66.1	64.9	63.7	62.6	61.4	60.3	59.1
	10.0			11.5		12.5				

Temper- ature		t-#=I	Afficence of	l Temperat	eres of the	Air and o	f the Dew-	Point. — F	ahrenheit.	
of Air, Fahren- heit.	10.0	10.5	11.0	11.5	13.0	19.5	18.0	13.5	14.0	14.5
62°	69.9	68.6	67.4	66-1	64.9	68.7	62.6	61.4	60.8	59.1
63	70.0	68.7	67.5	66.2	65.0	68.8	62.7	61.5	60.4	59.3
64	70.1	68.8	67.6	66.8	65.1	64.0	62-8	61.6	. 60.5	59.4
65	70.2	68.9	67.7	66.5	65.8	64.1	62.9	61.8	60.6	59.5
66	70.3	69.0	67.8	66.6	65.4	64.2	62.0	61.9	60.8	59.7
67	70.4	69.1	67.9	66.7	65.5	64.8	68.2	62.0	60.9	59.8
68	70.5	69.2	68.0	66.8	65.6	64.4	63.8	62.1	61.0	59.9
69	70.6	69.8	68.1	66.9	65.7	64.5	63.4	62.3	61.1	60.0
70	70.7	69.4	68.2	67.0	65.8	64.7	63.5	62.4	61.3	60.2
71	70.8	69-5	68.8	67.1	65.9	64.8	63.6	62.5	61.4	60.3
72	70.9	69.6	68.4	67.2	66.0	64.9	63.7	62.6	61.5	€0.4
78	71.0	69.7	68.5	67.8	66.2	65.0	63.9	62.7	61.6	60.5
74	71.1	69.8	68.6	67.4	66.8	65.1	64.0	62.8	61.7	60.7
75	71.1	69.9	68.7	67.5	66-4	65.2	64.1	63.0	61.9	60.8
76	71.2	70.0	68.8	67.6	66.5	65.8	64.2	63.1	62.0	60.9
77	71.8	70.1	68.9	67.8	66.6	65.5	64.8	68.2	62.1	61.0
78	71.4	70.2	69.0	67.9	66.7	65.6	64.4	63.3	62.2	61.1
79	71.5	70.3	69.1	68.0	66.8	65.7	64.5	68.4	62.3	61.8
80	71.6	70.4	69.2	68.1	66.9	65.8	64.7	63.6	62.5	61.4
81	71.7	70.5	69.3	68.2	67.0	65.9	64.8	63.7	62.6	61.5
82	71.8	70.6	69.4	68.3	67.1	66.0	64.9	68.8	62.7	61.6
83	71.9	70.7	69.5	68.4	67.2	66.1	65.0	68.9	62.8	61.8
84	72.0	70.8	69.6	68.5	67.8	66.2	65.1	64.0	62.9	61.9
85	72.1	70.9	69.7	68.6	67.4	66.8	65.2	64.1	63.0	62.0
86	72.2	71.0	69.8	68.7	67.5	66.4	65.3	64.2	68.2	62.1
87	72.3	71.1	69.9	68.8	67.7	66.5	65.4	64.4	63.3	62.2
88	72.4	71.2	70.0	68.9	67.8	66.6	65.5	64.5	68.4	62.8
89	72.5	71.3	70.1	69.0	67.9	66.8	65.7	64.6	68.5	62.5
90	72.6	71.4 71.4	70.2 70.3	69.1 69.2	68.0 68.1	66.9 67.0	65.8	64.7 64.8	63.6 63.7	62.6
91 92	72.7 72.8	71.5	70.4	69.3	68.2	67.1	65.9 66.0	64.9	68.9	62.7 62.8
93	72.9	71.6	70.5	69.4	68.3	67.2	66.1	65.0	64.0	62.9
94	72.9 73.0	71.7 71.8	70.6 70.7	69.5 69 .6	68.4 68.5	67.3 67.4	66.2 66.8	65.1 65.2	64.1 64.2	68.0 63.2
95	73.0 78.1	71.9	70.7	69.7	68.6	67.5	66.4	65.4	64.3	63.8
96 97	78.2	72.0	70.9	69.8	68.7	67.6	66.5	65.5	64.4	63.4
96	78.3	72.1	71.0	69.9	68.8	67.7	66.6	65.6	64.5	63.5
	78.4	72.8	71.1	70.0	68.9	67.8	66.7	65.7	64.6	63.6
99 100	73.5	72.4	71.2	70.1	69.0	67.9	66.8	65.8	64.8	63.7
101	73.6	72.5	71.8	70.2	69.1	68.0	67.0	65.9	64.9	68.9
102	78.7	72.6	71.4	70.8	69.2	68.1	67.1	66.0	65.0	64.0
103	73.8	72.7	71.5	70.4	69.8	68.2	67.2	66.1	65.1	64.1
104	78.9	72.8	71.6	70.5	69.4	68.8	67.8	66.2	65.2	64.2
	10.0	10.5	11.0	11.5	19.0	19.5	18.0	13.5	14.0	14.

Temperature of Air,		t t' = I	difference of	f Temperat	ures of the	Air and o	f the Dew-	Point. — Fe	shrenheit.	
Fahren- heit.	15.0	15.5	16.0	16,5	17.0	17.5	18.0	18.5	19.0	19.5
20°	50.6	49.5	48.4	47.8	46.2	45.1	44.1	43.1	42.1	41.2
21	50.6	49.5	48.4	47.8	46.2	45.1	44.2	43.2	42.2	41.2
22	50.7	49.5	48.4	47.4	46.8	45.2	44.2	48.2	42.2	41.8
28	50.7	49.6	48.5	47.4	46.8	45.2	44.2	48.8	42.8	41.3
24	50.7	49.6	48.5	47.4	46.4	45.8	44.8	48.3	42.8	41.4
23	50.8	49.7	48.5	47.5	46.4	45.4	44.8	43.8	42.4	41.4
26	50.9	49.3	48.6	47.6	46.5	45.4	44.4	43.4	42.4	41.5
27	51.0	49.9	48.7	47.7	46.6	45.5	44.5	43.5	42.5	41.6
28	51.1	50.0	48.8	47.7	46.7	45.6	44.6	48.6	42.6	41.6
29	51.2	50.1	48.9	47.8	46.8	45.7	44.7	48.7	42.7	41.7
80	51.4	50.2	49.0	47.9	46.8	45.8	44.7	48.7	42.7	41.8
31	51.7	50.5	49.4	48.2	47.1	46.1	45.0	44.0	48.0	42.0
82	52.0	50.8	49.7	48.5	47.4	46.4	45.8	44.8	43.8	42.8
88	52.3	51.1	50.0	48.8	47.7	46.6	45.6	44.5	48.5	42.5
84	52.6	51.4	50.8	49.1	48.0	46.9	45.9	44.8	43.8	42.8
85	52.9	51.7	50.6	49.4	48.8	47.2	46.1	45.1	44.1	48.0
86	58.2	52.0	50.9	49.7	48.6	47.5	46.4	45.4	44.4	43.3
87	53.5	52.8	51.2	50.0	48.9	47.8	46.7	45.7	44.7	48.6
38	53.8	52.6	51.5	50.8	49.2	48.1	47.0	46.0	45.0	48.9
39	54.1	52.9	51.8	50.6	49.5	48.4	47.3	46.8	45.8	44.2
40	54.4	58.2	52.1	50.9	49.8	48.7	47.6	46.6	45.6	44.5
41	54.7	53.5	52.3	51.2	50.1	49.0	47.9	46.9	45.8	44.8
42	54.9	53.8	52.6	51.5	50.4	49.8	48.2	47.2	46.1	45.1
43	55.2	54.0	52.9	81.8	50.7	49.6	48.5	47.5	46.4	45.4
44	55.5	54.8	58.2	52.1	50.9	49.9	48.8	47.7	46.7	45.7
45	55.7	54.6	58.4	52.3	51.2	50.2	49.1	48.0	47.0	46.0
46	55.9	54.7	53.6	52.5	51.4	50.4	49.3	48.3	47.2	46.2
47	56.0	24.9	58.8	52.7	51.6	50.6	49.5	48.5	47.5	46.5
48	56.2	55.0	54.0	52.9	51.8	60.8	49.8	48.7	47.7	46.7
49	56.8	55.2	54.1	58.1	52.0	51.0	50.0	49.0	47.9	47.0
50	56.5	55.4	21.8	53.2	52.2	51.2	50.2	49.2	48.2	47.2
51	56.6	55.5	54.4	58.4	52.8	51.8	50.3	49.8	48.3	47.4
52	56.7	58.6	54.6	53.5	52.5	51.5	50.5	49.5	48.5	47.5
58	56.9	55.8	54.7	58.6	52.6	51.6	50.6	49.6	48.6	47.7
21	57.0	55.9	54.8	58.8	52.7	51.7	50.7	49.8	48,8	47,8
55	57.1	56.0	55.0	58.9	52.9	51.9	50.9	49.9	48.9	48.0
56	57.8	56.2	55.1	84.1	53.0	52.0	51.0	50.0	49.1	48.1
57	57.4	56.3	55.2	54.2	53.2	52.2	51.2	50.2	49.2	48.3
58	57.5	56.4	55.4	21.8	53.8	52.8	51.3	50.8	49.4	48.4
59	57.7	56.6	55.5	54.5	58.4	52.4	51.4	50.5	49.5	48.6
60	57.8	56.7	55.6	54.6	53.6	52.6	51.6	50.6	49.7	48.7
61	57.9	56.8	55.8	54.7	58.7	52.7	51.7	50.8	49.8	48.9
62	58.0	57.0	55.9	54.9	53.8	52.8	51.9	50.9	49.9	49.0
	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.5

Temper- ature		t-t-1	Afference o	f Temperat	ares of the	Air and o	f the Dow-	Point. — Fr	hrenheit.	
of Air, Fahren- beit.	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.
62°	58.0	57.0	55.9	54.9	53.8	52.8	51.9	80.9	49.9	49.0
63	58.2	57.1	56.0	55.0	54.0	58.0	52.0	51.0	60.1	49.1
64	58.8	57.2	56.2	55.1	54.1	58.1	52.1	51.2	50.2	49.8
65	58.4	57.4	56.8	55.8	54.8	53.8	52.3	51.8	50.4	49.4
66	58.6	57.5	56.4	55.4	54.4	58.4	52.4	51.5	50.5	49.6
67	58.7	57.6	56.6	55.5	54.5	58.5	52.6	51.6	50.6	49.7
68	58.8	57.8	56.7	55.7	54.7	53.7	52.7	51.7	50.8	49.9
69	59.0	57.9	56.8	55.8	54.8	53.8	52.8	51.9	50.9	50.0
70	59.1	58.0	57.0	55.9	54.9	53.9	58.0	52.0	51.1	50.1
71	59.2	58.2	57.1	56.1	55.1	54.1	53.1	52.1	51.2	50.5
72	59.3	58.3	57.2	56.2	55.2	54.2	58.2	52.3	51.8	50.4
73	59.5	58.4	57.4	56.3	55.3	54.8	58.4	52.4	51.5	50.6
74	59.6	58.5	57.5	56.5	55.5	54.5	53.5	52.6	51.6	50.7
75	59.7	58.7	57.6	56.6	55.6	54.6	58.6	52.7	51.7	50.8
76	59.8	58.8	57.8	56.7	55.7	54.7	58.8	52.8	51.9	51.0
77	60.0	58.9	57.9	56.9	55.9	54.9	58-9	58.0	52.0	51.1
78	60.1	59.1	58.0	57.0	56.0	55.0	54.0	58.1	52.2	51.2
79	60.2	59.2	58.1	57.1	56.1	55.1	54.2	53.2	52.8	51.4
80	60.3	59.8	58.3	57.8	56.8	55.8	54.3	58.4	52.4	51.5
81	60.5	59.4	58.4	57.4	56.4	55.4	54.5	53.5	52.6	51.7
82	60.6	59.6	58.5	57.5	56.5	55.5	54.6	53.6	52.7	51.8
83	60.7	59.7	58.6	57.6	56.6	55.7	54.7	58.8	52. 8	51.9
84	60.8	59.8	58.8	57.8	56.8	55.8	54.8	58.9	58.0	52.
85	60.9	59.9	58.9	57.9	56.9	55.9	55.0	54.0	58.1	52.2
86	61.1	60.0	59.0	58.0	57.0	56.1	55.1	54.2	58.2	52.8
87	61.2	60.2	59.1	58.1	57.2	56.2	55.2	54.8	58.4	52.0
88	61.3	60.3	59.3	58.3	57.8	56.3	55.4	54.4	53.5	52.6
89	61.4	60.4	59.4	58.4	57.4	56.5	55.5	54.6	58.7	52.7
90	61.6	60.5	59.5	58.5	57.6	56.6	55.6	54.7	58.8	52.9
91	61.7	60.7	59.6	58.7	57.7	56.7	55.8	54.8	53.9	58.0
92	61.8	60.8	59.8	58.8	57.8	56.9	55.9	55.0	54.1	53.2
93	61.9	60.9	59.9	58.9	57.9	57.0	56.0	55.1	54.2	58.8
94	62.0	61.0	60.0	59.0	58.1	57.1	56.2	55.2	54.8	58.4
95	62.1	61.1	60.1	59.2	58.2	57.2	56.3	55.4	54.5	58.€
96	62.3	61.3	60.8	59.8	58.8	67.4	56.4	55.5	54.6	58.7
97	62.4	61.4	60.4	59.4	58.4	57.5	56.5	55.6	54.7	58.8
98	62.5	61.5	60.5	59.5	58.6	57.6	56.7	\$5.8	54.9	54.0
99	62.6	61.6	60.6	59.6	58.7	67.7	56.8	55.9	55.0	54.1
100	62.7	61.7	60.7	59.8	58.8	57.9	56.9	56.0	55.1	54.2
101	62.8	61.9	60.9	59.9	58.9	58.0	57.1	56.2	55.8	54.4
102	63.0	62.0	61.0	60.0	59.1	58.1	57.2	56.3	55.4	54.5
103	63.1	62.1	61.1	60.1	59.2	58.3	57.8	56.4	55.5	54.6
104	68.2	62.2	61.2	60.8	59.8	58.4	57.5	56.6	55.7	54.8
	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.

Temper-		t-t'-1	Difference o	f Temperat	tures of the	Air and o	f the Dew-	Point.—F	sbrenheit.	
of Air, Fahren- heit.	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	24.0	24.5
20°	40.2	39.8	96.4	87.5	36.6	85.8	84.9	84.1	33.8	82.5
21	40.3	89.4	28.4	27.6	36.7	85.8	35.0	84.2	33.4	82.6
22	40.3	39.4	36.5	87.6	36.8	85.9	85.1	84.8	88.5	32.7
28	40.4	39.5	38.6	87.7	36.8	36.0	85.2	84.4	83.6	32.8
24	40.4	39.6	38.6	87.8	36.9	86.1	85.2	84.4	83.6	32.9
25	40.5	39.6	38.7	3 7.8	87.0	86.2	85.8	84.5	88.7	88.0
26	40.5	89.7	36.8	87.9	87.0	86.2	85.4	84.6	83.8	33.1
27	40.6	39.7	88.8	88.0	37.1	36.3	35.5	84.7	83.9	83.1
28	40.7	39.8	28.9	38.0	37.2	36.8	35.5	84.7	84.0	83.2
29	40.8	89.9	38.9	36.1	97.2	86.4	85.6	84.8	84.0	88.8
80	40.8	39.9	89.0	28.1	37.8	86.5	85.7	34.9	34.1	88.4
81	41.1	40.2	39.2	38.4	87.5	36.7	85.9	85.1	84.8	33.6
82	41.8	40.4	39.5	36.6	27.7	87.0	36.1	35.8	84.5	33.8
88	41.6	40.6	89.7	88. 8	88.0	87.2	86.8	85.5	34.7	84.0
84	41.8	40.9	3 9. 9	39.1	86.2	87.4	36.5	85.7	84.9	84.2
35	42.1	41.1	40.2	89.3	38.4	87.7	36.7	35.9	85.1	84.4
86	42.8	41.4	40.4	39.6	88.7	87.9	37.0	86.2	85.4	84.6
37	42.6	41.7	40.7	39.8	86.9	38.2	37.2	86.4	85.6	84-8
88	42.8	42.0	41.0	40.1	89.2	88.4	37.5	86.6	85.8	35.0
39	43.1	42.8	41.8	40.4	89.5	88.6	87.7	86.9	86.0	85.2
40	48.3	42.6	41.6	40.7	89.8	88.9	88.0	87.1	86.8	85.4
41	48.7	42.9	41.9	41.0	40.0	89.1	38.8	37.4	36.5	85.7
42	44.0	43.2	42.2	41.2	40.3	89.4	38.5	87.7	86.8	36.0
43	44.3	43.4	42.5	41.5	40.6	39.7	88.8	88.0	87.1	36.3
44	44.7	48.7	42.8	41.8	40.9	40.0	89.1	88.2	87-4	36.6
45	45.0	44.0	43.1	42.1	41.2	40.3	89.4	38.5	87.7	86.8
46	45.2	44.3	43.8	42.4	41.4	40.5	8 9.7	38.8	87.9	37.1
47	45.5	44.5	43.6	42.6	41.7	40.8	29.9	39.1	28.2	87.4
48	45.7	44.9	43.8	42.9	42.0	41.1	40.2	89.8	38.5	37.6
49	46.0	45.0	44.1	48.2	42.2	41.8	40.5	89.6	88.7	87.9
50	46.2	45.8	44.3	48.4	42.5	41.6	40.7	89.9	39.0	87.2
51	46.4	45.4	44.5	43.6	42.7	41.8	40.9	40.1	89.2	38.4
52	46.6	45.5	44.7	48.8	42.9	42.0	41.2	40.8	39.5	88.6
53	46.7	45.8	44.9	44.0	48.1	42.2	41.4	40.5	89.7	38.9
21	46.9	46.0	45.1	44.2	43.8	42.4	41.6	40.8	39.9	89.1
55	47.0	46.1	45.2	44.4	48.5	42.6	41.8	41.0	40.1	39.3
56	47.2	46.3	45.4	44.5	43.6	42.8	42.0	41.1	40.8	39.5
57	47.8	46.4	45.5	44.7	48.8	42.9	42.1	41.8	40.5	89.6
58	47.5	46.6	45.7	44.8	43.9	43.1	42.8	41.4	40.6	89.8
59	47.6	46.7	45.8	45.0	44.1	43.2	42.4	41.6	40.8	40.0
60	47.8	46.9	46.0	45.1	44.2	43.4	42.5	41.7	40.9	40.1
61 62	47.9 48.1	47.0 47.2	46.1 46.3	45.8 45.4	44.4 44.5	43.5 43.7	42.7 42.8	41.9 42.0	41.1 41.2	40.3 40.4
	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	24.0	94.5

Temper- ature		t — t' — I	Difference o	(Temperat	cures of the	Air and o	f the Dew-	Point. — Y	ahrenheit.	
of Air, Fahren- heit.	20.0	20.5	21.0	21.5	22.0	22.5	23.0	28.5	24.0	94.5
62°	48.1	47.2	46.3	45.4	44.5	43.7	42.8	42.0	41.2	40.4
63	48.2	47.8	46.4	45.5	44.7	48.8	43.0	42.2	41.4	40.6
64	48.4	47.5	46.6	45.7	44.8	44.0	43.1	42.8	41.5	40.7
65	48.6	47.6	46.7	45.8	45.0	44.1	48.3	42.5	41.7	40.9
66	48.7	47.8	46.9	46.0	45.1	44.8	43.4	42.6	41.8	41.0
67	48.8	47.9	47.0	46.1	45.8	44.4	43.6	42.8	42.0	41.2
68	48.9	48.0	47.2	46.3	45.4	44.6	48.7	42.9	42.1	41.3
69	49.1	48.2	47.8	46.4	45.6	44.7	48.9	48.1	42.8	41.5
70	49.2	48.3	47.4	46.6	45.7	44.9	44.0	48.2	42.4	41.6
71	49.4	48.5	47.6	46.7	45.9	45.0	44.2	48.4	42.6	41.8
72	49.5	48.6	47.7	46.9	46.0	45-2	44.8	43.5	42.7	41.9
73	49.6	48.8	47.9	47.0	46.1	45.3	44.5	48.7	42.9	42.1
74	49.8	48.9	48.0	47.1	46.8	45.4	44.6	43.8	48.0	42.2
75	49.9	49.0	48.2	47.3	46.4	45.6	44.8	44.0	43.1	42.4
76	50.1	49.2	48.8	47.4	46.6	45.7	44.9	44.1	48.8	42.5
77	50.2	49.8	48.5	47.6	46.7	45.9	45.1	44.2	43.4	42.6
78	50.8	49.5	48.6	47.7	46.9	46.0	45.2	44.4	43.6	42.8
79	50.5	49.6	48.7	47.8	47.0	46.2	45.8	44.5	48.7	48.0
80	50.6	49.7	48.9	48.0	47.2	46.3	45.5	44.7	48.9	48.1
81	50.8	49.9	49.0	48.1	47.8	46.5	45.6	44.8	44.0	48.2
82	50.9	50.0	49.2	48.3	47.4	46.6	45.8	45.0	44.2	48.4
83	51.0	50.1	49.3	48.4	47.6	46.8	45.9	45.1	44.8	43.5
84	51.2	50.3	49.4	48.6	47.7	46.9	46.1	45.8	41.5	48.7
85	51.8	50.4	49.6	48.7	47.9	47.0	46.2	45.4	44.6	43.8
86	51.4	50.6	49.7	48.8	48.0	47.2	46.4	45.6	44.8	44.0
87	51.6	50.7	49.8	49.0	48.1	47.8	46.5	45.7	44.9	44.1
88	51.7	50.8	50.0	49.1	48.3	47.5	46.6	45.8	45.0	44.8
89	51.9	51.0	50.1	49.8	48.4	47.6	46.8	46.0	45.2	44.4
90	52.0	51.1	50.8	49.4	48.6	47.7	46.9	46.1	45.8	44.6
91	52.1	51.8	50.4	49.5	48.7	47.9	47.1	46.8	45.5	44.7
92	52.8	51.4	50.5	49.7	48.8	48.0	47.2	46.4	45.6	44.8
93	52.4	51.5	50.7	49.8	49.0	48.2	47.4	46.6	45.8	45.0
94	52.5	51.7	50.8	50.0	49.1	48.3	47.5	46.7	45.9	45.1
95	52.7	51.8	50.9	50.1	49.8	48.4	47.6	46.8	46.1	45.8
96	52.8	51.9	51.1	50.2	49.4	48.6	47.8	47.0	46.2	45.4
97	52.9	52.1	51.2	50.4	49.5	48.7	47.9	47.1	46.8	45.6
96	53.1	52.2	51.4	50.5	49.7	48.9	48.1	47.8	46.5	45.7
99	58.2	52.8	51.5	50.6	49.8	49.0	48.2	47.4	46.6	45-9
100	58.4	52.5	51.6	50.8	50.0	49.1	48.3	47.5	46.8	46.0
101	53.5	52.6	51.8	50.9	50.1	49.8	48.5	47.7	46.9	46.2
102	53.6	52.8	51.9	51.1	50.2	49.4	48.6	47.8	47.1	46.3
103 104	53.8 53.9	52.9 53.0	52.0 52.2	51.2 51.3	50.4 50.5	49.6 49.7	48.9 48.9	48.0 48.1	47.2 47.8	46.4 46.6
	20.0	20.5	21.0	21.5	22.0	22.5	28.0	23.5	24.0	24.5

TABLE IX.

FACTOR $^{100}_{\ \ F}$, FOR COMPUTING THE BELATIVE HUMIDITY, OR THE DEGREE OF MOISTURE OF THE AIE, EXPRESSED IN HUNDREDTHS, FROM ITS ABSOLUTE HUMIDITY GIVEN IN ENGLISH MEASURES.

The Relative Humidity, or the degree of moisture of the air, is, as explained above, the ratio of the quantity of vapor contained in the air to the quantity it could contain at the temperature observed, if fully saturated.

If we call

The force of vapor contained in the air = f,

The maximum of the force of vapor at the temperature of the air = F,

The point of saturation = 100,

we have the proportion,

Relative Humidity: 100::f:F,

and

 $f \times \frac{100}{2}$ = Relative Humidity in Hundredths.

But as $\frac{f \times 100}{g} = f \times \frac{100}{g}$, it is obvious that the operation indicated by the former expression, viz. $\frac{f \times 100}{g}$, would be reduced to a simple multiplication, if we had a table of the factors $\frac{160}{g}$. Such a table is obtained by dividing the constant number 100 by each number in the Table of Elastic Forces of Vapor, and substituting the quotients for the tensions, or forces of vapor.

The following Table gives the factor $\frac{100}{F}$ for every tenth of a degree from 0° to 104° Fahrenheit, corresponding to the Forces of Vapor in Table VI., or Regnault's table reduced to English measures.

USE OF THE TABLE.

The force of vapor contained in the air, or its absolute humidity, being given in English measures, multiply the number expressing it by the factor in the table corresponding to the temperature of the air at the time of the observation; the result will be the *Relative Humidity in Hundredths*.

Examples.

1. Suppose the temperature of the air to be = 60° Fahrenheit.

" force of vapor in the air to be = .388 English inch.

Opposite 60° is found in the table the factor 193.1.

Then $0.388 \times 193.1 = 74.9$, Relative Humidity in Hundredths.

2. Suppose the temperature of the air to be = 74°.5 Fahrenheit.

" " force of vapor in the air to be = .650 English inch.
Table gives for 74°.5 the factor 117.2.

Then $0.650 \times 117.2 = 76.2$, Relative Humidity required.

IX. FACTOR $^{100}_{T}$, FOR COMPUTING THE RELATIVE HUMIDITY, OR THE DEGREE OF MOISTURE OF THE AIR,

EXPRESSED IN HUNDREDTHS, FROM ITS ABSOLUTE HUMIDITY GIVEN IN ENGLISH INCHES.

Temper- ature of Air,					Tenths o	f Degrees.				
Fahren- heit.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
0°	2806	2295	2285	2275	2264	2254	2248	2233	2222	2211
1	2201	2191	2181	2171	2162	2152	2142	2182	2122	2111
2	2101	2092	2068	2074	2064	2055	2045	2086	2026	2017
8	2007	1998	1990	1981	1972	1963	1954	1945	1986	1927
4	1918	1910	1901	1898	1885	1876	1868	1859	1851	1842
5	1834	1826	1818	1810	1802	1794	1786	1777	1769	1761
6	1753	1745	1788	1780	1722	1714	1707	1699	1691	1688
7	1675	1668	1660	1658	1646	1638	1681	1623	1616	1608
8	1600	1594	1587	1580	1572	1565	1558	1551	1544	1587
9	1529	1528	1516	1509	1508	1496	1489	1482 .	1475	1469
10	1462	1455	1449	1448	1486	1480	1423	1417	1410	1404
11	1397	1391	1895	1879	1373	1867	1361	1855	1848	1842
12	1336	1330	1324	1319	1813	1307	1301	1295	1289	1284
13	1278	1272	1267	1261	1255	1250	1244	1239	1238	1226
14	1222	1217	1211	1206	1200	1195	1189	1184	1178	1173
15	1167	1162	1157	1151	1146	1141	1136	1180	1125 -	1120
16	1114	1109	1104	1099	1094	1089	1084	1079	1074	1069
17	1064	1059	1055	1050	1045	1040	1035	1081	1026	1021
18	1016	1012	1007	1008	998.2	998.6	989.1	984.5	979.9	975.
19	970.6	966.4	962.2	957.9	958.7	949.4	945.0	• 940.7	986.8	931.
20	927.5	923.5	919.5	915.5	911.4	907.4	908.8	899.1	895.0	890.
21	886.7	882.9	879.1	875.3	871.4	867.6	863.7	859.8	855.8	851.
22	847.9	844.8	840.7	887.1	883.4	829.8	826.1	822.4	818.7	815.
28	811.2	807.8	804.8	800.8	797.8	793.8	790.2	786.7	783.1	779.
24	775.9	772.6	769.8	766.0	762.7	759.8	756.0	752.6	749.2	745.
25	742.4	789.8	786.2	783.0	729.9	726.7	728.5	720.8	717.1	713.
26	710.6	707.7	704.7	701.8	698.8	695.8	692.8	689.7	686.7	688.
27	680.5	677.8	675.0	672.1	669.8	666.5	663.6	660.7	657.8	654.
28	652.0	649.4	646.7	644.1	641.4	638.7	686.0	638.8	630.5	627.
29	625.0	622.5	620.0	617.5	614.9	612.4	609.8	607.2	604.6	602.
80	599.4	597.1	594.7	592.3	589.9	587.4	585.0	582.6	580.1	577.
3 1	575.1	572.9	570.7	568.4	566.2	568.9	561.6	559.2	556.9	854.
	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.

Temper-				<u>.</u>	Tenths (of Degrees.				
of Air, Fahren- heit.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
82°	552.2	550.0	547.8	545.7	543.6	541.4	589.3	587.2	585.1	533.
33	530.9	528.8	526.8	524.7	522.7	520.6	518.6	516.5	514.5	512.
84	510.5	508.5	506.5	504.5	502.5	500.5	498.6	496.6	494.7	492.
35	490.8	488.9	487.0	485.1	483.2	481.8	479.4	477.5	475.6	473.
8 6	471.9	470.1	468.2	466.4	461.6	462.8	461.0	459.2	457.4	455.
87	458.8	452.0	450.8	448.5	446.8	445.0	443.8	441.6	489.9	438.
88	436.4	434.7	438.1	481.4	429.7	428.0	426.4	424.7	428.1	421.
39	419.9	418.2	416.6	415.0	413.4	411.8	410.2	408.6	407.0	405.
40	403.9	402.4	400.8	399.8	397.8	396.2	894.7	893.2	891.7	290.
41	388.7	387.2	885.8	884.8	882.9	881.4	880.0	378.5	877.1	3 75.
42	874.8	372.9	871.5	870.0	36 8.6	867.8	865.9	864.5	863.1	361.
43	860.4	859.0	857.6	356.3	854.9	353.6	352.3	350.9	849.6	348.
44	847.0	845.6	844.8	848.0	841.7	840.4	889.2	887.9	886.6	235.
45	334.1	832.8	831.6	330.8	828.1	827.8	826.6	825.4	824.1	322.
46	321.7	820.5	819.8	\$18.1	316.9	815.7	814.5	313.8	812.2	311.
47	809.8	808.7	807.5	806.4	805.2	804.1	802.9	801.8	800.7	299.
49	298.5	297.8	296.2	295.1	294.0	292.9	291.9	290.8	289.7	288.
49	287.6	286.5	285.4	284.4	283.8	282.3	281.8	280.2	279.2	278.
50	277.1	276.1	275.1	274.1	278.1	272.1	271.1	270.1	269.1	268.
51	267.2	266.2	265.2	264.3	263.3	262.3	261.4	260.4	259.5	258.
52	257.6	256.6	255.7	254.8	253.8	252.9	252.0	251.1	250.2	249.
58	248.3	247.4	246.5	245.6	244.7	248.9	248.0	242.1	241.2	240.
54 55	239.5 230.9	238.6 230.1	237.7 229.2	286.9 228.4	236.0 227.6	235.1 226.8	234.8 225.9	233.4 225.1	232.6 224.8	231.
56	222.7	221.9	221.1	220.3	219.5	218.7	217.9	217.1	216.4	223. 215.
57	214.8	214.0	213.3	212.5	211.8	211.0	210.2	209.5	208.7	208.
58	207.3	206.5	205.8	205.0	204.3	203.6	202.9	202.2	201.4	200.
59	200.0	199.8	198.6	197.9	197.2	196.5	195.8	195.1	194.4	198.
60	198.1	192.4	191.7	191.0	190.4	189.7	189.0	188.4	187.7	187.
61	186.4	185.7	185.1	184.4	188.8	183.1	182.5	181.8	181.2	180.
62	179.9	179.8	178.7	178.0	177.4	176.8	176.2	175.6	174.9	174.
63	178.7	178.1	172.5	171.9	171.8	170.7	170.1	169.5	168.9	168.
64	167.7	167.1	166.6	166.0	165.4	164.8	164.3	168.7	163.1	162.
65	162.0	161.4	160.9	160.8	159.7	159.2	158.6	158.1	157.5	157.
66	156.5	155.9	185.4	154.8	154.8	153.8	158.2	152.7	152.2	151.
67	151.1	150.6	150.1	149.6	149.1	148.6	148.1	147.6	147.1	146.
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

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Tumper- ature of Air,					Tenths o	f Degrees.				
Fahren- heit.	0.	1.	9.	3.	4.	5.	6.	7.	8.	9.
68°	146.0	145.6	145.1	144.6	144.1	143.6	143.1	142.6	142.1	141.6
69	141.2	140.7	140.2	189.7	139.2	138.8	188.8	187.8	187.4	186.9
70	186.4	136.0	185.5	135.1	184.6	134.1	188.7	133.2	182.8	182.8
71	131.9	181.4	181.0	180.5	180.1	129.7	129.2	128.8	128.8	127.9
72	127.5	127.1	126.6	126.2	125.8	125.3	124.9	124.5	124.1	128.7
78	123.8	122.8	122.4	122.0	121.6	121.2	120.8	120.4	120.0	119.6
74	119.2	118.8	118.4	118.0	117.6	117.2	116.8	116.4	116.0	115.6
75	115.3	114.9	114.5	114.1	118.7	118.8	113.0	112.6	112.2	111.9
76	111.5	111.1	110.7	110.4	110.0	109.6	109.8	108.9	108.6	109.2
77	107.9	107.5	107.1	106.8	106.4	106.1	105.7	105.4	105.1	104.7
78	104.4	104.0	103.7	108.3	108.0	102.7	102.8	102.0	101.7	101.8
79	101.0	100.7	100.8	100.0	99.68	99.85	99.02	98.70	98.38	98.0
80	97.73	97.42	97.10	96.78	96.47	96.15	95.84	95.52	95.21	94.9
81	94.59	94.29	98.98	98.67	98.87	93.06	92.76	92.46	92.16	91.8
82	91.56	91.26	90.97	90.67	90.88	90.09	89.80	89.51	89.22	88.9
83	88.64	88.36	88.07	87.79	87.50	87.22	86.94	86.66	86.38	86.1
84	85.88	85.55	85.27	85.00	84.73	84.46	84.19	83.92	83.65	83.8
85	83.12	82.85	82.59	82.82	82.06	81.80	81.54	81.28	81.02	80.7
86	80.51	80.25	80.00	79.74	79.49	79.24	78.99	78.74	78.49	78.2
87	77.99	77.75	77.50	77.26	77.01	76.77	76.52	76.28	76.04	75.8
88	75.56	75.32	75.08	74.85	74.61	74.87	74.14	78.91	78.67	73.4
89	78.21	72.98	72.75	72.52	72.29	72.06	71.84	71.61	71.89	71.1
90	70.94	70.72	70.49	70.27	70.05	69.83	69.61	69.39	69.18	68.9
91	68.74	68.53	68.82	68.10	67.89	67.68	67.47	67.26	67.05	66.8
92	66.68	66.42	66.22	66.01	65.81	65.60	65.40	65.19	64.99	64.7
93	64.59	64.89	64.19	68.99	68.79	68.59	68.40	68.20	68.01	62.8
94	62.62	62.48	62.24	62.04	61.85	61.66	61.47	61.29	61.10	60.9
95	60.72	60.54	60.85	60.17	59.98	59.80	59.62	59.48	59.25	59.0
96	58.89	58.71	58.58	58.85	88.17	58.00	57.82	57.64	57.47	57.2
97	57.12	56.94	56.77	56.60	56.42	56.25	56.08	55.91	55.74	55.5
96	55.40	55.23	55.06	54.90	54.78	54.56	54.40	54.28	54.07	53.9
99	53.74	58.58	58.42	58.26	58:09	52.98	52.77	52.61	52.45	52.3
100	52.14	51.98	51.82	51.67	51.51	51.86	51.20	51.05	50.90	50.7
101	50.59	50.44	50.29	.50.14	49.99	49.84	49.69	49.54	49.39	49.2
102	49.10	48.95	48.80	48.66	48.61	48.87	48.22	48.08	47.94	47.7
103	47.65	47.51	47.87	47.28	47.09	46.95	46.81	46.67	46.58	46.4
104	46.26	46.12	45.99	45.85	45.72	45.58	45.45	45.81	45.18	45.0
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

TABLE X.

WEIGHT OF VAPOR, IN GRAINS TROY,

contained in a cubic foot of saturated air, under a barometric pressure of 80 english inches, at temperatures between 0° and 105° fahrenheit.

The weight of a litre of dry air at the temperature of zero Centigrade, or 32° Fahrenheit, and under a barometric pressure of 760 millimetres, as determined by the experiments of Regnault (*Mémoires de l'Institut*, Tom. XXI. p. 157), and corrected for a slight error of computation (see above, p. 38), is 1.293223 grammes. The coefficient of expansion of the air, according to the same physicist, is 0.00367 for 1° Centigrade; and the theoretic density of vapor is nearly 0.622, or §, of that of the air at the same temperature and pressure. From these elements the weight of the vapor contained in a determined volume of air, the temperature and humidity of which are known, can be deduced.

Reducing these values to English measures, 1 litre being = 61.02705 cubic inches, and 1 gramme = 15.43208 grains Troy, we have

$$1.293223$$
 grammes = 19.9571208 grains,

and

61.027051 cubic inches: 19.9571208 grains:: 1 cubic inch: 0.32702 grain.

Therefore, the weight of a cubic foot of dry air, at 32° Fahrenheit, under a pressure of 760 millimetres, or 29.922 English inches, is = 0.32702 grain $\times 1728 = 565.0923$ grains Troy. Under a barometric pressure of 30 inches, it becomes

$$\frac{80}{29.922} \times 565.0923 = 566.5654$$
 grains.

The coefficient for the expansion of the air becomes 0.0020361 of its bulk for 1° Fahrenheit.

Now, if we call

В

t =the temperature of the air;

W =the weight of vapor in a saturated air at the temperature t;

F = the maximum of the force of vapor due to the temperature t, as given in the tables;

then the weight of the vapor contained in a cubic foot of saturated air is given by the formula

$$W = 0.622 \frac{566.5654 \text{ grains}}{1 + 0.002036 \times (t - 32^{\circ})} \cdot \frac{F}{30};$$

from which the values in Table X. have been computed. The forces of vapor due to the temperatures in the first column are those of Regnault, as given in Table VI.

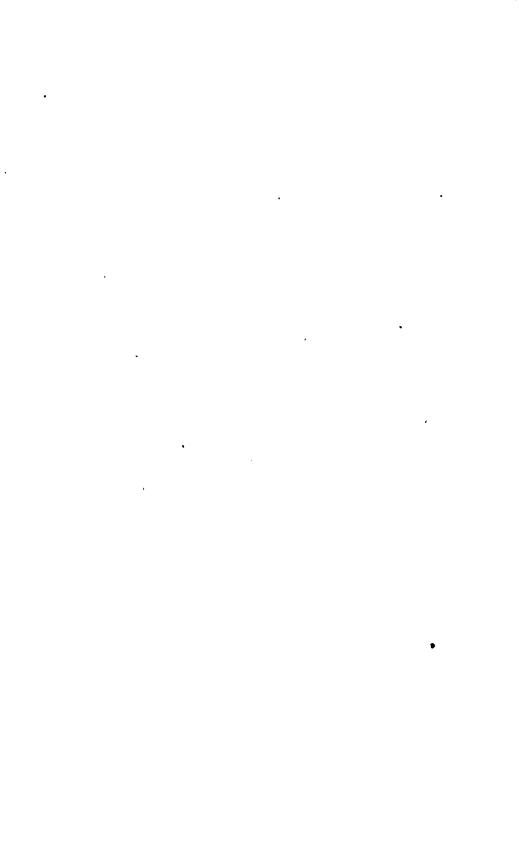
It is evident, that, in order to find the weight of the vapor contained in the air at any state of humidity and pressure, it suffices to substitute for the normal values of $\frac{\mathbf{F}}{30}$ the force of vapor and the barometric pressure given by the observation.

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X. WEIGHT OF VAPOR, IN GRAINS TROY,

CONTAINED IN A CUBIC FOOT OF SATURATED AIR, AT TEMPERATURES BETWEEN 0° AND 105° FAHRENHEIT.

						1	1	1		1	<u> </u>
Temperature of Air, Fahren.	Force of Vapor in Eng. Inches.	Weight of Vapor in Grains.	Differ- ence.	Temper- ature of Air, Fehren.	Force of Vapor in Eng. Inches.	Weight of Vapor in Grains.	Differ- ence.	Temper- ature of Air, Fahren.	Force of Vapor in Eng. Inches.	Weight of Vapor in Grains.	Differ- ence.
0°	0.043	0.545	0.024	85°	0.204	2.879	0.090	70°	0.788	7.992	
1	0.045	0.569	0.025	86	0.212	2.469	0.098	71	0.758	8.252	0.961
2	0.048	0.595	0.025	87	0.220	2.568	0.097	72	0.784	8.521	0.268
8	0.050	0.621	0.028	88	0.229	2.659	0.100	78	0.811	8.797	0.284
4	0.052	0.649	0.029	89	0.288	2.759	0.103	74	0.889	9.081	0.391
5	0.055	0.678	0-030	40	0.248	2.862	0.106	75	0.868	9.872	
6	0.057	0.708	0.030	41	0.257	2.967	0.100	76	0.897	9.670	0.228
7	0.060	0.739	0.031	42	0.267	8.076	0.109	77	0.927	9.977	0.307
8	0.062	0.772	0.084	48	0.277	3.189	0.116	78	0.958	10.292	0.315
9	0.065	0.806	0.035	44	0.288	8.806	0.110	79	0.990	10.616	0.894
10	0.068	0.841	0.037	45	0.299	3.426	0.194	80	1.023	10.949	0.342
11	0.072	0.878	0.028	46	0.811	8.550	0.129	81	1.057	11.291	
12	0.075	0.916	0.040	47	0.323	3.679	0.129	82	1.092	11.643	0.869
13	0.078	0.957	0.042	48	0.835	8.811	0.137	88	1.128	12.005	0.361
14	0.082	0.999	0.044	49	0.848	3.948	0.141	84	1.165	12.876	0.390
15	0.086	1.048	0.046	80	0.861	4.089	0.145	85	1.203	12.756	0.390
16	0.090	1.090	0.049	B1	0.874	4.284	0.149	86	1.242	13.146	0.400
17	0.094	1.188	0.041	52	0.888	4.388	0.154	87	1.282	13.546	0.411
18	0.098	1.190	0.062	58	0.408	4.587	0.159	88	1.823	18.957	0.421
19	0.108	1.248	0.058	54	0.418	4.696	0.168	89	1.866	14.878	0.432
20	0.108	1.298	0.087	55	0.433	4.860	0.168	90	1.410	14.810	0.448
21	0.113	1.855	0.059	56	0.449	5.028	0.174	91	1.455	15.254	0.455
22	0.118	1.415	0.062	57	0.466	5.202	0.179	92	1.501	15.709	0.467
28	0.128	1.476	0.064	58	0.482	5.381	0.185	93	1.548	16.176	0.479
24	0.129	1.540	0.066	59	0.500	5.566	0.190	94	1.597	16.654	0.491
25	0.185	1.606	0.000	60	0.518	5.756	0.100	95	1.647	17.145	
26	0.141	1.674	0.068	61	0.587	5.952	0.196	96	1.698	17.648	0.508
27	0.147	1.745	0.078	62	0.556	6.154	0.202	97	1.751	18.164	0.516
28	0.158	1.817	0.078	63	0.576	6.361	0.214	98	1.805	18.698	0.529
29	0.160	1.892	0.077	64	0.596	6.575	0.220	99	1.861	19.235	0.549
30	0.167	1.969	0.000	65	0.617	6.795	0.004	100	1.918	19.790	
81	0.174	2.046	0.077	66	0.689	7.021	0.226	101	1.977	20.357	0.567
32	0.181	2.126	0.080	67	0.662	7.258		102	2.037	20.988	0.589
33	0.188	2.208	0.082	68	0.685	7.493	0.289	103	2.099	21.535	0.896
34	0.196	2.292	0.087	69	0.708	7.789	0.240	104	2.162	22.146	0.611
35	0.204	2.879	0.087	70	0.788	7.992	0.253	105	2.227	22.771	0.625



PRACTICAL TABLES,

IN

ENGLISH MEASURES,

BASED ON THE HYGROMETRICAL CONSTANTS ADOPTED IN THE GREENWICH OBSERVATIONS.



TABLE

OF

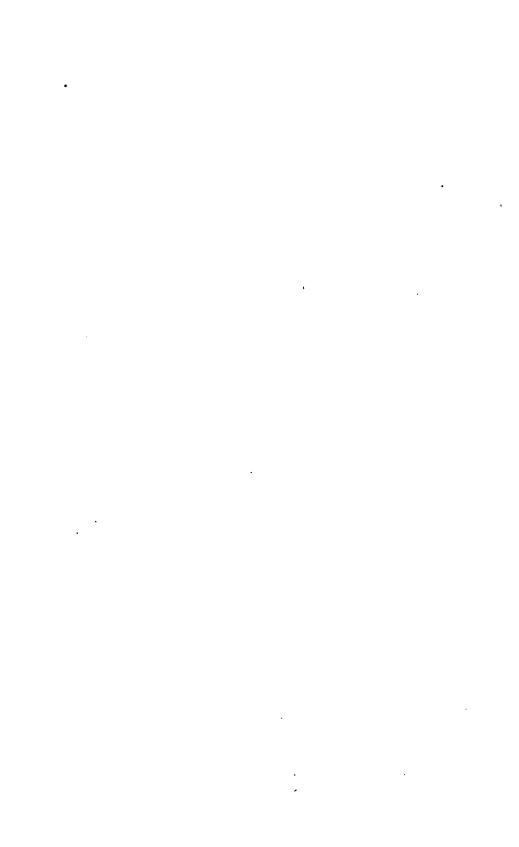
THE ELASTIC FORCES OF AQUEOUS VAPOR,

UNDER A PRESSURE OF 80 INCHES, EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHRENHEIT, ADOPTED IN THE GREENWICH OBSERVATIONS.

This table contains the values of the elastic force of vapor for temperatures from 0° to 90° Fahrenheit, derived from Dalton's experiments by Biot's formula, by Anderson, and published in *Edinburgh Encyclopædia*, Art. *Hygrometry*. It is republished, without the last decimal, in the volumes of the *Greenwich Magnetic and Meteorological Observations*, and on it are based the various hygrometrical tables published by Mr. Glaisher, either in the Greenwich volumes, or separately, most of which will be found below, Tables XII. to XVII.

Since Dalton published his experiments, numerous attempts have been made by various skilful physicists to determine with greater accuracy the elastic force of vapor. Dr. Ure in England, Regnault in France, and Magnus in Germany, deserve in this respect a special notice.

The last two experimenters having arrived simultaneously at results nearly identical, and their experiments having been conducted with all the care that modern science requires, and the means that it can secure, their determinations seem to command an especial confidence, and to deserve the preference over all others. It is, therefore, much to be regretted that the usefulness of the following otherwise so valuable tables, the formation of which involved so much labor, is in a measure impaired by the fact that they were computed from elements which cannot be regarded as the most reliable we now possess.



XI.

TABLE

OF THE

ELASTIC FORCE OF AQUEOUS VAPOR,

TWOER A BAROMETRIC PRESSURE OF 30 INCHES, EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHRENHEIT.

FROM THE GREENWICE OBSERVATIONS.

Temper-					Tenths of	Degrees.				
Fahren- heit.	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.
•	Ring. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.
0	0.061	0.061	0.062	0.062	0.062	0.062	0.068	0.068	0.068	0.068
1	0.064	0.064	0.064	0.064	0.065	0.065	0.065	0.065	0.066	0.066
2	0.066	0.066	0.067	0.067	0.067	0.067	0.068	0.068	0.068	0.068
8	0.069	0.089	0.069	0.069	0.070	0.070	0.070	0.071	0.071	0.071
4	0.071	0.072	0.072	0.072	0.072	0.078	0.078	0.078	0.078	0.074
5	0.074	0.074	0.075	0.075	0.075	0.075	0.076	0.076	0.076	0.077
6	0.077	0.077	0.077	0.078	0.078	0.078	0.079	0.079	0.079	0.080
7	0.080	0.080	0.080	0.081	0.081	0.081	0.082	0.082	0.082	0.088
8	0.083	0.083	0.088	0.084	0.084	0.084	0.085	0.085	0.085	0.086
9	0.086	0.086	0.087	0.087	0.087	0.088	0.088	0.088	0.089	0.089
10	0.089	0.090	0.090	0.090	0.091	0.091	0.091	0.092	0.092	0.092
11	0.098	0.093	0.093	0.094	0.094	0.094	0.095	0.095	0.096	0.096
12	0.096	0.097	0.097	0.097	0.098	0.098	0.098	0.099	0.099	0.099
18	0.100	0.100	0.101	0.101	0.101	0.102	0.102	0.102	0.108	0.108
14	0.104	0.104	0.104	0.105	0.105	0.106	0.106	0.106	0.107	0.107
15	0.108	0.108	0.108	0.109	0.109	0.110	0.110	0.110	0.111	0.111
16	0.112	0.112	0.112	0.118	0.118	0.114	0.114	0.115	0.115	0.115
17	0.116	0.116	0.117	0.117	0.118	0.118	0.118	0.119	0.119	0.120
18	0.120	0.121	0.121	0.121	0.122	0.122	0.123	0.128	0.124	0.124
19	0.125	0.125	0.126	0.126	0.126	0.127	0.127	0.128	0.128	0.129
20	0.129	0.180	0.180	0.131	0.131	0.132	0.182	0.183	0.188	0.184
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

ELASTIC FORCE OF AQUEOUS VAPOR.

From the Greenwich Observations.

Temper-					Teaths of	Degrees.				
Fahren- heit.	0.	1.	9.	8.	4.	5.	6.	7.	6.	9.
•	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In
21	0.134	0.135	0.185	0.186	0.186	0.137	0.137	0.138	0.138	0.139
22	0.189	0.140	0.140	0.141	0.141	0.142	0.142	0.143	0.143	0.144
23	0.144	0.145	0.145	0.146	0.146	0.147	0.147	0.148	0.148	0.149
24	0.150	0.150	0.151	0.152	0.152	0.152	0.153	0.153	0.154	0.155
23	0.155	0.156	0.156	0.157	0.157	0.158	0.158	0.159	0.160	0.160
26	0.161	0.161	0.162	0.168	0.168	0.164	0.164	0.165	0.165	0.166
27	0.167	0.167	0.168	0.168	0.169	0.170	0.170	0.171	0.172	0.172
28	0.178	0.178	0.174	0.175	0.175	0.176	0.177	0.177	0.178	0.178
29	0.179	0.180	0.180	0.181	0.182	0.182	0.183	0.184	0.184	0.185
80	0.186	0.186	0.187	0.188	0.188	0.189	0.190	0.190	0.191	0.192
•										
81	0.192	0.198	0.194	0.194	0.195	0.196	0.197	0.197	0.198	0.198
82	0.199	0.200	0.201	0.201	0.202	0.203	0.204	0.204	0.205	0.206
83	0.207	0.207	0.208	0.209	0.210	0.210	0.211	0.212	0.218	0.213
84	0.214	0.215	0.216	0.216	0.217	0.218	0.219	0.219	0.220	0.221
85	0.222	0.223	0.223	0.224	0.225	0.226	0.227	0.227	0.228	0.229
36	0.280	0.231	0.231	0.232	0.238	0.234	0.235	0.007	0.236	0.237
87	0.280	0.231	0.231	0.282	0.235	0.234	0.248	0.285	0.235	0.23
88	0.246	0.239	0.248	0.240	0.241	0.242	0.248	0.244	0.258	0.25
89	0.255	0.247	0.257	0.258	0.259	0.260	0.261	0.262	0.268	0.263
40	0.264	0.265	0.266	0.267	0.268	0.269	0.270	0.271	0.272	0.278
, 41	0.274	0.275	0.276	0.277	0.278	0.279	0.280	0.281	0.282	0.282
42	0.283	0.284	0.285	0.286	0.287	0.288	0.289	0.290	0.291	0.292
43	0.293	0.295	0.296	0.297	0.298	0.299	0.800	0.301	0.302	0.303
44	0.304	0.805	0.806	0.807	0.808	0.309	0.810	0.811	0.312	0.818
45	0.315	0.816	0.317	0.818	0.319	0.820	0.821	0.822	0.323	0.82
46	0.326	0.827	0.328	0.829	0.880	0.881	0.832	0.833	0.335	0.336
47	0.337	0.888	0.889	0.840	0.842	0.848	0.844	0.845	0.846	0.848
48	0.349	0.350	0.851	0.352	0.854	0.855	0.856	0.857	0.858	0.860
49	0.861	0.862	0.868	0.865	0.866	0.867	0.368	0.870	0.871	0.872
50	0.878	0.875	0.876	0.377	0.879	0.880	0.881	0.882	0.383	0.88
51	0.886	0.388	0.889	0.890	0.892	0.898	0.894	0.896	0.397	0.39
52	0.400	0.401	0.402	0.404	0.405	0.407	0.408	0.409	0.411	0.412
53	0.414	0.415	0.416	0.418	0.419	0.421	0.422	0.428	0.425	0.426
54 55	0.428 0.442	0.429 0.444	0.481 0.445	0.432 0.447	0.484	0.485 0.450	0.437 0.452	0.438 0.458	0.440 0.455	0.441
	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.

BLASTIC FORCE OF AQUEOUS VAPOR.

From the Greenwich Observations.

Temper-					Touths of	Degrees.				
Fahren- heit.	0.	1.	9.	3.	4.	5.	6.	7.	8.	9.
•	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eog. In.	Eng. In.
56	0.458	0.459	0.461	0.462	0.464	0.465	0.467	0.469	0.470	0.472
57	0.478	0.475	0.476	0.478	0.480	0.481	0.488	0.485	0.486	0.488
58	0.489	0.491	0.498	0.494	0.496	0.498	0.499	0.501	0.503	0.504
59	0.506	0.508	0.509	0.511	0.513	0.515	0.516	0.518	0.520	0.521
60	0.523	0.525	0.527	0.528	0.580	0.582	0.584	0.586	0.587	0.539
61	0.541	0.548	0.544	0.546	0.548	0.550	0.552	0.554	0.555	0.557
62	0.559	0.561	0.563	0.565	0.567	0.568	0.570	0:572	0.574	0.576
63	0.578	0.580	0.582	0.584	0.586	0.588	0.590	0.591	0.593	0.595
64	0.597	0.599	0.601	0.603	0.605	0.607	0.609	0.611	0.613	0.615
65	0.617	0.619	0.621	0.623	0.626	0.628	0.630	0.632	0.684	0.636
66	0.638	0.640	0.642	0.644	0.646	0.648	0.651	0.653	0.655	0.657
67	0.659	0.661	0.664	0.666	0.668	0.670	0.672	0.674	0.677	0.679
68	0.681	0.684	0.686	0.688	0.690	0.692	0.695	0.697	0.699	0.701
69	0.704	0.706	0.708	0.711	0.713	0.715	0.717	0.720	0.722	0.725
70	0.727	0.729	0.732	0.734	0.786	0.739	0.741	0.744	0.746	0.748
71	0.751	0.758	0.756	0.758	0.761	0.768	0.766	0.768	0.771	0.778
72	0.776	0.778	0.781	0.788	0.785	0.787	0.790	0.792	0.795	0.797
78	0.901	0.803	0.806	0.809	0.811	0.814	0.817	0.819	0.822	0.824
74	0.827	0.830	0.832	0.835	0.838	0.840	0.848	0.846	0.849	0.851
75	0.864	0.857	0.860	0.862	0.865	0.868	0.871	0.878	0.876	0.879
76	0.882	0.885	0.887	0.890	0.893	0.896	0.899	0.902	0.905	0.908
77	0.910	0.918	0.916	0.919	0.922	0.925	0.928	0.981	0.934	0.987
78	0.940	0.943	0.946	0.949	0.952	0.955	0.958	0.961	0.964	0.967
79	0.970	0.978	0.976	0.979	0.983	0.986	0.989	0.992	0.995	0.998
80	1.001	1.005	1.008	1.011	1.014	1.017	1.021	1.024	1.027	1.030
81	1.034	1.037	1.040	1.043	1.047	1.050	1.058	1.057	1.060	1.068
82	1.067	1.069	1.073	1.077	1.080	1.083	1.087	1.090	1.094	1.097
88	1.101	1.104	1.108	1.111	1.114	1.118	1.121	1.125	1.129	1.182
84	1.186	1.189	1.148	1.146	1.150	1.158	1.157	1.160	1.164	1.167
85	1.171	1.175	1.178	1.182	1.186	1.190	1.198	1.197	1.201	1.205
	1 600	1.610	1 010	1 000	1.224	1.000	1 600	1.005	1 600	1 040
86	1.209	1.212	1.216	1.220		1.228	1.232	1.235	1.239	1.248
87	1.247	1.251	1.255	1.258	1.262	1.266	1.270	1.274	1.278	1.282
88	1.286	1.290	1.294	1.298	1.802	1.806	1.810	1.814	1.318	1.822
89 90	1.326 1.368	1.830 1.872	1.335 1.876	1.339 1.381	1.348 1.385	1.347 1.389	1.851 1.898	1.855 1.897	1.859 1.402	1.364 1.406
	0.	1.	9.	8.	4.	5,	6.	7.	8.	9.

XII.

PSYCHROMETRICAL TABLE,

GIVING THE TEMPERATURE OF THE DEW-POINT, THE PORCE AND THE WEIGHT OF VAPOR IN THE ATMOSPHERE, AND ITS RELATIVE HUMIDITY, DEDUCED FROM THE INDICATIONS OF THE PSYCHEOMETER, OR DRY AND WET BULB THERMOMETERS.

By James Glaisher.

This elaborate table, first published in London, in 1847, in pamphlet form, by J. Glaisher, of the Royal Observatory at Greenwich, is based on the tables of elastic forces of vapor deduced from Dalton's experiments, and given above, Table XI.

The weight of a cubic foot of dry air at 32° Fahrenheit, and under the barometric pressure of 30 inches, which has been adopted by Glaisher, and from which the weight of vapor in a cubic foot of air is derived, is the mean of the determinations obtained by Shuckburgh and by Biot and Arago, which is 563.2154 grains Troy; 563 being the number actually used in the calculations. See Preface to the Table, p. 13, and also the *Greenwich Meteorological Observations* for 1842, p. xlvi.

The coefficient of the expansion of air which has been employed is that determined by the experiments of Gay-Lussac, according to which the air expands 0.00375 of its bulk for 1° Centigrade, or Thursday, or Thursd

All these values, as may be seen by comparing Tables VI. and XI. of the elastic forces, and also page 92, materially differ from those more recently determined with great care by Regnault, and on which are based the Psychrometrical Tables given above, page 50 et seq. This will account for the no inconsiderable differences often found between the results in the two tables derived from the same data. A few examples, taken from various parts of the tables, may be given here, in order to enable the meteorologist to judge of the amount of the discrepancies which may occur in the results when computed from different hygrometrical constants.

1. Suppose the temperature of the air indicated by the dry thermometer ter to be = 10° F.

The temperature of evaporation indicated by the wet thermometer = 9° F.

Difference 1° F.

Then, Glaisher's table gives,

The Force of Vapor = 0.065 inch. The Relative Humidity = 0.730

Guyot's table gives,

B

The Force of Vapor = 0.054 inch. The Relative Humidity = 0.791

PSYCHROMETRICAL TABLE.

2. By observation we have,

Dry Thermometer = 50° F. Wet Thermometer = 40° F. Difference = 10° F.

Then, by Glaisher's table, we find,

Force of Vapor = 0.186 inch.

Relative Humidity = 0.495

And by Guyot's table, we find,

Force of Vapor = 0.117 inch. Relative Humidity = 0.322

3. The reading of the

Dry Thermometer is = 90° F. Wet Thermometer is = 70° F. Difference = 20° F.

By Glaisher's table we have,

Force of Vapor = 0.523 inch.

Relative Humidity = 0.381

And by Guyot's table,

Force of Vapor = 0.464 inch.
Relative Humidity = 0.329

The temperatures of the Dew-Point, given in Glaisher's tables, have been computed by means of the empirical factors given below, page 140, and in the manner there described. See Preface to the Table, page 11.

ARRANGEMENT OF THE TABLE.

In the first two columns, at the left, are found the indications, in degrees of Fahrenheit, of the dry and wet bulb thermometers. In the following columns, in their order, and opposite to each of the temperatures of the wet thermometer, are given the temperature of the dew-point; the force of vapor, in English inches; the weight of vapor, in grains, contained in a cubic foot of air; the amount of the same required for saturation; and the relative humidity in thousandths, corresponding to the difference of temperature between the two thermometers. The second half of the page, at the right, furnishes, in seven columns, the weight, in grains, of a cubic foot of air, under various barometric pressures from 28 to 31 inches, and in the different hygrometric conditions indicated by the differences of the two thermometers. These numbers have been computed in the manner described below, page 142.

The range of the table extends from 10° to 90° of the dry thermometer, or of the temperature of the air. From 10° to 34° Fahrenheit the results are calculated for every second, third, and fifth of a degree of the wet thermometer, and for extreme differences of the temperature of evaporation ranging from 2° to 5° below the temperature of the air. From 34° to 90° the results are given only for every full degree of the wet thermometer, and for extreme differences gradually increasing

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B

PSYCHEOMETRICAL TABLE.

from 5° to 20°. This range falls short of the wants of the extreme climate of North America, where temperatures above 90° and far below 10° are of usual occurrence over a great portion of the continent. The same may be said of the range of the differences between the two thermometers in the first part of the table. The double interpolation for the fractions of degrees of both thermometers being rather too large to be neglected, its application becomes inconvenient.

USE OF THE TABLE.

Enter the table with the observed temperatures of the dry and wet bulb thermometers. On the same line as the last, and in their appropriate columns, the results deduced from these data will be found.

Example.

The observation has given,

Temperature of the air by the dry thermometer $= 62^{\circ}$ F. Temperature of evaporation by the wet-bulb thermometer $= 53^{\circ}$ F.

Page 129, find in the first column, headed Reading of the Dry Thermometer, the temperature of 62°, and in the second, that of the wet, 53°. On the line beginning with 53° are found, in their respective columns, the results deduced from these data, viz.:—

The temperature of the Dew-point = 46°.7 F.

The force of vapor in the air = 0.333 inch.

The weight of vapor in a cubic foot of air

The amount of vapor required for saturation = 2.53 grains.

The relative humidity in thousandths = 0.595

P.	ding	7	Force	We of V	ighs apor		ſ	Weigh	t in Grai	ns of a C	able Foot	of Air.	
2000	noter, ahr.	Temp. of Dew-	of Vapor in	In a	Reqd. for Sat'n.	Hu- midity, Satura-		Height o	of the Bar	rometer i	n English	Inches.	
Dry.	Wet.	Point, Fahr.	English Inches.	Foot of	of aCu- bic Ft. of Air.	tion == 1.000.	28.0	28.5	29.0	29.5	30.0	in. 30.5	in. 31.0
° 10	10.0	10.0	in. 0.089	gr.	gr. 0.00	1 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
	9.8	8.3	0.084	1.11	0.06	1.000 0.946	550.1 550.2	560.0	569.8	579.6	589.4	599.2	609.0
	9.6	6.6	0.079	0.98	0.18	0.888	550.2	560.1 560.1	569.9 569.9	579.7 579.7	589.5 589.5	599.3 599.8	609.1 609.1
	9.4	4.9	0.074	0.92	0.19	0.829	550.2	560.1	569.9	579.7	589.5	599.3	609.1
	9.2	3.2	0.069	0.86	0.25	0.775	550.8	560.2	570.0	579.8	589.6	599.4	609.2
	9.0	1.5	0.065	0.81	0.80	0.730	550.8	560.8	570.0	579.8	589.6	599.4	609.3
11	11.0	11.0	0.093	1.15	0.00	1.000	548.9	558.7	568.5	578.8	588.1	597.9	607.7
	10.8	9.8	0.087	1.08	0.07	0.989	548.9	558.7	568.5	578.8	588.1	597.9	607.7
	10.6	7.6	0.082	1.02	0.18	0.887	549.0	558.8	568.6	578.4	588.2	598.0	607.8
	10.4	5.9	0.077	0.96	0.19	0.835	549.0	558.8	568.6	578.4	588.2	598.0	607.8
	10.2	4.2	0.072	0.90	0.25	0.788	549.0	558.8	568.6	578.4	588.2	598.0	607.8
	10.0	2.5	0.067	0.84	0.81	0.781	549.1	558.9	568.7	578.6	588.8	598.1	607.9
	9.8	0.8	0.063	0.78	0.87	0.679	549.1	558.9	568.7	578.6	588.3	598.1	607.9
12	12.0	12.0	0.096	1.19	0.00	1.000	547.7	557.5	567.2	577.0	586.8	596.6	606.4
	11.8	10.8	0.090	1.12	0.07	0.942	547.7	557.5	567.2	577.0	586.8	596.6	606.4
	11.6	8.6	0.085	1.05	0.14	0.888	547.8	557.6	567.8	577.1	586.9	596.7	606.5
	11.4	6.9	0.080	0.99	0.20	0.882	547.8	557.6	567.8	577.1	586.9	596.7	606.5
	11.2	5.2	0.075	0.93	0.26	0.782	547.8	557.6	567.8	577.1	586.9	596.7	606.5
	11.0	8.5	0.070	0.87	0.32	0.781	547.9	557.7	567.4	577.2	587.0	596.8	606.6
	10.8	1.8	0.066	0.81	0.38	0.681	547.9	557.7	567.4	577.2	587.0	596.8	606.6
	10.6	0.1	0.061	0.76	0.43	0.689	547.9	557.7	567.4	577.2	587.0	596.8	606.6
18	18.0	13.0	0.100	1.24	0.00	1.000	546.5	556.8	566.0	575.8	585.5	595.3	605.0
	12.8	11.3	0.094	1.16	0.09	0.986	546.5	556.8	566.0	575.8	585.5	595.8	605.0
	12.6	9.6	0.088	1.08	0.16	0.871	546.6	556.4	566.1	575.9	585.6	595.4	605.1
	12.4	7.9	0.083	1.02	0.22	0.828	546.7	556.5	566.2	576.0	585.7	595.5	605.2
	12.2	6.2	0.077	0.97	0.27	0.788	546.7	556.5	566.2	576.0	585.7	595.5	605.2
	12.0	4.5	0.078	0.91	0.38	0.784	.546.7	556.5	566.2	576.0	585.7	595.5	605.2
	11.8	2.8	0.068	0.84	0.40	0.678	546.8	556.6	566.8	576.1	585.8	595.6	605.3
		1.1	0.064	0.79	0.45	0.687	546. 8	556.6	566.8	576.1	585.8	595.6	605.8
14	14.0	14.0	0.104	1.28	0.00	1.000	545.8	555.0	564.7	574.4	584.2	594.0	603.7
	18.8	12.8	0.097	1.20	0.08	0.988	545.8	555.0	564.7	574.4	584.2	594.0	603.7
	13.6 13.4	10.6 8.9	0.091	1.12	0.16	0.875	545.4	555.1	564.8	574.5	584.8	594.1	603.8
	13.4	7.2	0.080	1.00	0.22	0.828 0.782	545.4	555.1	564.8	574.5	584.3	594.1	608.8
	18.0	5.5	0.075	0.93	0.25	0.782	545.4 545.5	555.1 555.2	564.8	574.5	584.3	594.1	608.8
	12.8	3.8	0.071	0.87	0.41	0.680	545.5	555.2	564.9 564.9	574.6 574.6	584.4 584.4	594.2 594.2	608.9 608.9
	12.6		0.066	0.82	0.46	0.641	545.6	555.8	565.0	574.7	584.5	594.2	603.9
15	15.0	15.0	0.108	1.82	0.00	1.000	E44.0		F40 F				
"	14.8	13.3	0.101	1.82	0.08	0.940	544.0 544.0	553.8 553.8	568.5	578.2	582.9	592.6	602.8
	14.6	11.6	0.095	1.16	0.16	0.879	544.1	558.9	563.6	578.2 578.8	582.9 583.0	592.6	602.3 602.4
	14.4	•	0.089	1.10	0.22	0.883	544.1	558.9		573.3	583.0	592.7 592.7	602.4
	14.2	8.2	0.088	1.04	0.28	0.788	544.2			578.4	588.1	592.8	602.5
	14.0	6.5	0.078	0.97	0.35	0.785	544.2			578.4	583.1	592.8	602.5
	13.8	4.8	0.078	0.90	0.42	0.682	544.2		568.7	578.4	583.1	592.8	602.5
	13.6	8.1	0.069	0.85	0.47	0.644	544.8			578.5			

	ading Ther-	Temp.	Force	We of V	ight apor	Hu-		Weigh	t in Grai	ns of a Ci	abie Foot	of Alz.	
100.01	meter, ahr.	of Dew- Point,	Vapor in	In a Cubic		midity, Setura- tion ==		Height	of the Ba	rometer t	n Engliel	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bio Ft. of Air.	1.000.	98.0	28.5	ів. 29. 0	29.5	30.0	30.5	81.0
0			in.	gr.	gr.		gr.	gr.	gr.	gr.	gr.	gr.	gr.
16	16.0	16.0	0.112	1.37	0.00	1.000	542.8	552.5	56212	571.9	581.6	591.3	601.0
	15.8 15.6	14.3	0.105	1.29 1.21	0.08	0.942	542.9	552.6	562.8	572.0	561.7	591.4	601.1 601.1
	15.4	10.9	0.092	1.14	0.10	0.882	542.9 548.0	552.6 552.7	562.8 562.4	572.0 572.1	581.7 581.8	591.4 591.5	601.2
	15.2	9.2	0.087	1.07	0.80	0.781	548.0	552.7	562.4	572.1	581.8	591.5	601.2
	15.0	7.5	0.081	1.00	0.87	0.780	548.0	552.7	562.4	572.1	581.8	591.5	601.2
	14.8	5.8	0.076	0.94	0.48	0.686	548.1	552.8	562.5	572.1	581.9	591.6	601.3
	14.6	4.1	0.072	0.88	0.49	0.643	548.1	552.8	562.5	572.1	581.9	591.6	601.3
17	17.0	17.0	0.116	1.41	0.00	1.000	541.8	551.0	560.8	570.5	580.1	589.8	599.4
	16.8	15.8	0.109	1.33	0.08	0.943	541.8	551.0	560.8	570.5	580.1	589.8	599.4
	16.6	18.6	0.102	1.25	0.16	0.897	541.4	551.1	560.9	570.6	580.2	589.9	599.5
	16.4	11.9	0.096	1.17	0.24	0.830	541.4	551.1	560.9	570.6	580.2	589.9	599.5
	16.2	10.2	0.090	1.10	0.31	0.780	541.5	551.2	561.0	570.7	580.3	590.0	599.6
	16.0	8.5	0.064	1.03	0.38	0.780	541.5	551.2	561.0	570.7	580.8	590.0	599.€
	15.8	6.8	0.079	0.97	0.44	0.688	541.5	551.2	561.0	570.7	580.3	590.0	599.6
	15.6	5.1	0.074	0.91	0.50	0.646	541.6	551.8	561.1	570.8	580.4	590.1	599.7
18	18.0	18.0	0.120	1.47	0.00	1.000	540.5	550.2	559.8	569.5	579.1	588.8	598.4
	17.8	16.3	0.113	1.38	0.09	0.939	540.5	550.2	559.8	569.5	579.1	588.8	598.4
	17.6	14.6	0.106	1.29	0.18	0.878	540.6	550.3	559.9	569.6	579.2	588.9	598.5
	17.4	12.9	0.099	1.21	0.26	0.824	540.6	550.3	559.9	569.6	579.2	588.9	598.5
	17.2	11.2	0.093	1.14	0.83	0.776	540.7	550.4	560.0	569.7	579.3	589.0	598.6
	17.0	9.5	0.088	1.07	0.40	0.728	540.7	550.4	560.0	569.7	579.8	589.0	598.6
	16.8	7.8	0.082	1.01	0.46	0.688	540.7	550.5	560.1	569.8	579.8	589.0	598.6
	16.6	6.1	0.077	0.95	0.52	0.647	540.8	550.6	560.2	569.9	579.4	589.1	598.7
19	19.0	19.0	0.125	1.52	0.00	1.000	539.3	548.9	558.5	568.2	577.8	587.5	597-1
	18.8	17.3	0.117	1.43	0.09	0.941	589.3	548.9	558.5	568.2	577.8	587.5	597.1
	18.6	15.6	0.110	1.84	0.18	0.882	539.4	549.0	558.6	568.3	577.9	587.6	597.2
	18.4	13.9	0.103	1.26	0.26	0.829	539.4	549.0	558.6	568.3	577.9	587.6	597.2
	18.2	12.2	0.097	1.18	0.34	0.776	589.5	549.1	558.7	568.4	578.0	587.7	597.8
	18.0	10.5	0.091	1.11	0.41	0.730	539.5	549.1	558.7	568.4	578.0	587.7	597.8
	17.8	8.8	0.085	1.04	0.48	0.684	589.6	549.2	558.8	568.5	578.1	.587-8	597.4
	17.6	7.1	0.080	0.98	0.54	0.645	589.6	549.2	558.8	568.5	578.1	587.8	597-4
20	20.0	20.0	0.129	1.58	0.00	1.000	538.1	547.7	557.8	566.9	576.5	586.1	595.7
	19.8	18.3	0.121	1.48	0.10	0.987	538.2	547.8	557.4	567.0	576.6	586.2	595.8
	19.6	16.6	0.114	1.38	0.20	0.874	588.3	547.9	557.5	567.1	578.7	586.3	595.9
	19.4		0.107	1:80	0.28	0.828	588.3	ł	557.5	567.1	576.7	1	595.9
	19.2	13.2	0.101	1.23	0.85	0.779	588.3	547.9	557.5	567.1	576.7	586.8	595.9
1	19.0	11.5	0.094	1.15	0.43	0.728	538.4	ı	557.6	1	576.8	586.4	596.0
	18.8	9.8	0.089	1.08	0.50	0.684	538.4	548.0	557.6	567.2	576.8	586.4	596.0
	18.6	8.1	0.088	1.01	0.57	0.639	588.5	548.1	557.7	567.8	576.9	586.5	596.I
	18.4	6.4	0.078	0.95	0.63	0.601	538.5	548.1	557.7	567.8	576.9	586.5	5 96 .1
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	ding	Temp.	Force	We of V	ight apor	Hu-		Weigh	t in Grai	ns of a Cr	abie Foot	of Alr.	
2001	neter,	of Dew-	of Vapor in	In a	Reqd. for Sat'n.	midity,		Height o	of the Bar	rometer i	n Englist	Inches.	
!		Point, Fahr.	English	Foot of	ofaCu-	tion == 1.000.	in.	in.	in.	in.	in.	in.	fn.
Dry.	Wet		Inches.	Air.	ble Ft. of Air.		98.0	28.5	29.0	29.5	30.0	80.5	31.0
21	21.0	21.0	in. 0.134	gr. 1.63	gr. 0.00	1.000	gr. 587.0	gr. 546.6	gr. 556.1	gr. 565.7	gr. 575.8	gr. 584.9	gr. 594.5
	20.8	19.3	0.126	1.53	0.10	0.989	537.0	546.6	556.1	565.7	575.8	584.9	594.5
	20.6	17.6	0.118	1.44	0.19	0.884	587.1	546.7	556.2	565.8	575.4	585.0	594.6
	20.4	15.9	0.111	1.86	0.27	0.885	587.1	546.7	556.2	565.8	575.4	585.0	594.6
	20.2	14.2	0.104	1.28	0.85	0.785	587.2	546.8	556.3	565.9	575.5	585.1	594.7
1	20.0	12.5	0.098	1.20	0.48	0.786	587.2	546.8	556.8	565.9	575.5	585.1	594.7
	19.8	10.8	0.092	1.12	0.51	0.687	587.8	546.9	556.4	566.0	575.6	585.2	594.8
	19. 6 19.4	9.1 7.4	0.086	1.05 0.99	0.58	0.644	587.8	546.9	556.4	566.0	575.6	585.2	594.8
	15.3	1.4	0.001	0.55	0.04	0.607	537.3	546.9	556.4	566.0	575.6	585.2	594.8
22	22.0	22.0	0.139	1.69	0.00	1.000	535.7	545.3	554.9	564.5	574.0	583.6	598.1
	21.8	20.3	0.131	1.59	0.10	0.941	585.8	545.4	555.0	564.6	574.1	588.7	593.2
l .	21.6	18.6	0.123	1.49	0.20	0.882	535.8	545.4	555.0	564.6	574.1	588.7	593.2
l l	21.4	16.9	0.115	1.40	0.29	0.828	535.9	545.5	555.1	564.7	574.2	583.8	593.3
	21.2	15.2	0.108	1.31	0.88	0.775	585.9	545.5	555.1	564.7	574.2	583.8	593.3
1	21.0	13.5	0.102	1.28	0.46	0.728	586.0	545.6	555.2	564.8	574.3	583.9	598.4
1	20.8	11.8	0.096	1.16	0.53	0.686	536.0	545.6	555.2	564.8	574.8	588.9	593.4
1	20.6	10.1	0.090	1.09	0.60	0.645	586.1	545.7	555.3	564.9	574.4	584.0	593.5
1	20.4	8.4	0.084	1.02	0.67	0.604	586.1	545.7	555.8	564.9	574.4	584.0	593.5
	20.2	6.7	0.079	0.96	0.78	0.568	586.1	545.7	555.8	564.9	574.4	584.0	598.5
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23	23.0	28.0	0.144	1.75	0.00	1.000	534.6	544.2	558.7	568.8	572.8	582.4	591.9
1	22.8	21.8	0.136	1.65	0.10	0.948	584.6	544.2	558.7	568.3	572.8	582.4	591.9
1	22.6	19.6	0.127	1.55	0.20	0.886	534.7	544.3	553.8	563.4	572.9	582.5	592.0
l l	22.4	17.9	0.120	1.45	0.80	0.829	584.7	544.3	558.8	563.4	572.9	582.5	592.0
1	22.2	16.2	0.112	1.36	0.39	0.777	534.8	544.4	553.9	563.5	573.0	582.6	592.1
1	22.0	14.5	0.106	1.28	0.47	0.781	534.8	544.4	558.9	568.5	578.0	582.6	592.1
4	21.8	12.8	0.099	1.21	0.54	0.691	584.9	544.5	554.0	563.6	573.1	582.7	592.2
	21.6 21.4	11.1 9.4	0.098	1.18	0.62	0.646	584.9	544.5	554.0	563.6	573.1	582.7	592.2
il	21.2	7.7	0.087	1.06	0.69	0.606 0.571	585.0 585.0	544.6 544.6	554.1	568.7 563.7	578.2	582.8	592.8 592.8
		'''	0.002	1.00	0.75	0.071	000.0	044.0	554.1	003.7	578.2	582.8	002.5
24	24.0	24.0	0.150	1.81	0.00	1.000	583.4	542.9	552.4	562.0	571.5	581.1	590.6
1	28.8	22.5	0.142	1.72	0.09	0.951	583.5	543.0	552.5	562.1	571.6	581.2	590.7
	23.6	21.1	0.135	1.63	0.18	0.901	588.5	548.1		562.1	571.6		590.7
9	23.4	19.6	0.127				588.6						1
	23.2	18.2	0.121	1.46	0.85	0.807	583.6	548.2	552.6	562.2	571.7	581.3	590.8
ļ.	23.0	16.7	0.115	1.38	0.43	0.762	533.7	\$43.8	552.7	562.8	571.8	581.4	590.9
ľ	22.8		1				538.7					581.4	
	22.6	13.8		1.24		0.685	588.7	1					
1	22.4	U.	ı	1.18	0.63	0.652	583.8	548.4	552.8	562.4	571.9	581.5	591.0
1	22.2	10.8	0.091	1.12	0.69	0.684	583.8	543.4	552. 8	562.4	571.9	581.5	591.0
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Re	ding	Temp.	Force	We of V	ight apor	Hu-		Weigh	t in Grai	ne of a C	abie Foot	of Alz.	•
mor	neter, ahr.	of Dew-	of Vapor in	In a	Reqd. for Sat'n.	midity, Setura-		Height (of the Ba	rometer 1	n English	Inches.	
<u> </u>		Point, Fahr.	English Inches		ofaCu- ble Ft.	tion = 1.000.	ln.	in.	in.	in.	la.	in.	ta.
Dry.	Wot.		Inches.	AU .	of Air.		28.0	28.5	99.0	29.5	80.0	80. 5	81.0
, 0	0	0	in.	gr.	gr.		gr.	gr.	gr.	gr.	gr.	gr.	gr.
16	16.0 15.8	16.0 14.3	0.112	1.87	0.00	1.000	542.8 542.9	552.5	56212	571.9	581.6	591.3	601.0
H I	15.6	12.6	0.098	1.21	0.16	0.883	542.9	552.6 552.6	562.8 562.8	572.0 572.0	581.7 581.7	591.4 591.4	601.1 601.1
	15.4	10.9	0.092	1.14	0.28	0.882	548.0	552.7	562.4	572.1	581.8	591.5	601.2
// I	15.2	9.2	0.087	1.07	0.80	0.781	548.0	552.7	562.4	572.1	561.8	591.5	601.2
!!	15.0	7.5	0.081	1.00	0.87	0.780	548.0	552.7	562.4	572.1	561.8	591.5	601.2
1 1	14.8	5.8	0.076	0.94	0.48	0.686	548.1	552.8	562.5	572.1	581.9	591.6	601.3
	14.6	4.1	0.072	0.88	0.49	0.643	543.1	552.8	562.5	572.1	581.9	591.6	601.3
17	17.0	17.0	0.116	1.41	0.00	1.000	541.8	551.0	560.8	570.5	580.1	589.8	599.4
'	16.8	15.8	0.109	1.38	0.08	0.943	541.8	551.0	560.8	570.5	580.1	589.8	599.4
	16.6	18.6	0.102	1.25	0.16	0.897	541.4	551.1	560.9	570.6	580.2	589.9	599.5
	16.4	11.9	0.096	1.17	0.24	0.830	541.4	551.1	560.9	570.6	580.2	589.9	599.5
1	16.2	10.2	0.090	1.10	0.81	0.780	541.5	551.2	561.0	570.7	580.8	590.0	59 9 .6
1	16.0	8.5	0.084	1.03	0.88	0.780	541.5	551.2	561.0	570.7	580.3	590.0	599.6
	15.8	6.8	0.079	0.97	0.44	0.688	541.5	551.2	561.0	570.7	580.8	590.0	599.6
	15.6	5.1	0.074	0.91	0.50	0.646	541.6	551.8	561.1	570.8	580.4	590.1	599.7
10	10 0	10.0	0.100	7 400	0.00	1 000				WAG -	- 200	FOC 5	WOC .
18	18.0	18.0	0.120	1.47	0.00	1.000	540.5	550.2	559.8	569.5	579.1	588.8	598.4
	17.8 17.6	16.8	0.118	1.38	0.09	0.939	540.5	550.2	559.8	569.5	579.1	588.8	598.4
	17.6	14.6 12.9	0.106 0.0 99	1.29	0.18	0.878	540.6	550.3	559.9	569.6	579.2	588.9	598.5
1 1	17.4	11.2	0.098	1.21	0.26		540.6	550.8	559.9	569.6	579.2	588.9	598.5
	17.2	9.5	0.088	1.14	0.83	0.776 0.728	540.7	550.4	560.0	569.7	579.3	589.0	598.6
	16.8	7.8	0.082	1.01	0.46	0.728	540.7 540.7	550.4 550.5	560.0 560.1	569.7 569.8	579.3 579.3	589.0 589.0	598.6 598.6
	16.6	6.1	0.002	0.95	0.52	0.647	540.7	550.6	560.2	569.9	579.8 579.4	589.1	598.7
	10.0	""	0.011	V.50	U.UZ	0.047	0.040	200.0	JUU-2	993.B	015.4	908.1	990.7
19	19.0	19.0	0.125	1.52	0.00	1.000	539.3	548.9	558.5	568.2	577.8	587.5	597.1
	18.8	17.8	0.117	1.48	0.09	0.941	589.8	548.9	558.5	568.2	577.8	587.5	597.1
{	18.6	15.6	0.110	1.84	0.18	0.882	589.4	549.0	558.6	568.8	577.9	587.6	597.2
1 1	18.4	18.9	0.108	1.26	0.26	0.829	539.4	549.0	558.6	568.3	577.9	587.6	597.2
j l	18.2	12.2	0.097	1.18	0.34	0.776	589.5	549.1	558.7	568.4	578.0	587.7	597.3
	18.0	10.5	0.091	1.11	0.41	0.780	589.5	549.1	558.7	568.4	578.0	587.7	597.3
	17.8	8.8	0.085	1.04	0.48	0.684	589.6	549.2	558.8	568.5	578.1	587.8	597.4
	17.6	7.1	0.080	0.98	0.54	0.645	539.6	549.2	558.8	568.5	578.1	587.8	597.4
20	20.0	20.0	0.129	1.58	0.00	1.000	538.1	547.7	557.8	566.9	576.5	586.1	595.7
	19.8	18.3	0.121	1.48	0.10	0.987	588.2	547.8	557.4	567.0	576.6	586.2	595.8
	19.6	16.6	0.114	1.38	0.20	0.874	538.8	547.9	557.5	567.1	576.7	586.3	595.9
	19.4	14.9	0.107	1.80	0.28	0.828	588.3		557.5	567.1	576.7	586.3	595.9
	19.2	18.2	0.101	1.23	0.85	0.779	588.8		557.5		576.7		595.9
	19.0	11.5	0.094	1.15	0.43	0.728	538.4	548.0	557.6	567.2	576.8	586.4	596.0
	18.8	9.8	0.089	1.08	0.50	0.684	588.4	548.0	557.6		576.8	586.4	596.0
	18.6	8.1	0.088	1.01	0.57	0.689	538. 5	548.1	557.7		576.9	586.5	596.1
	18.4	6.4	0.078	0.95	0.63	0.601	588.5	548.1	557.7	567.8	576.9	586.5	596.1
			<u> </u>						•				

Re	ding		_	We	ight apor			Weigh	t in Grat	as of a Cr	able Foot	of Alr.	
, mor	Ther- neter, ahr.	Temp. of Dew-	Force of Vapor	In a	Reqd.	Hu- midity, Satura-	ļ			ometer i			
		Point,	in English	Cubic	Sat'n. of aCu-	tion =	l			OLD OLD I	. sugar	I IIIUU.	
Dey.	Wet.	Fahr.	Inches.	Air.	bie Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	in. 80. 5	31.0
21	21.0	21.0	in. 0.134	gr. 1.63	gr. 0.00	1.000	gr. 587.0	gr. 546.6	gr. 556.1	gr. 565.7	gr. 575.8	gr. 584.9	gr. 594.5
	20.8	19.3	0.126	1.58	0.10	0.929	537.0	546.6	556.1	565.7	575.3	584.9	594.5
!	20.6	17.6	0.118	1.44	0.19	0.884	537.1	546.7	556.2	565.8	575.4	555.0	594.6
	20.4	15.9	0.111	1.86	0.27	0.885	587.1	546.7	556.2	565.8	575.4	585.0	594.6
		-0.5	0.222	1.00	V.2.	0.000	557.1	540.7	500.2	0.00	010.4	505.0	074.0
	20.2	14.2	0.104	1.28	0.35	0.785	587.2	546.8	556.3	565.9	575.5	585.1	594.7
	20.0	12.5	0.098	1.20	0.48	0.786	587.2	546.8	556.8	565.9	575.5	585.1	594.7
	19.8	10.8	0.092	1.12	0.51	0.687	587.8	546.9	556.4	566.0	575.6	585.2	594.8
	19.6	9.1	0.086	1.05	0.58	0.644	587.8	546.9	556.4	566.0	575.6	585.2	594.8
	19.4	7.4	0.081	0.99	0.64	0.607	587.8	546.9	556.4	566.0	575.6	585.2	594.8
							1						
22	99.0	22.0	0.100	7 00	0.00	* 600	F0					#AC -	
	22.0 21.8	20.3	0.1 39 0.181	1.69	0.00	1.000	585.7	545.8	554.9	564.5	574.0	583.6	598.1
	21.6	18.6		1.59	0.10	0.941	535.8	545.4	555.0	564.6	574.1	588.7	593.2
1	21.4	16.9	0.128	1.49	0.20	0.882	585.8	545.4	555.0	564.6	574.1	583.7	598.2
	21.2	15.2	0.118	1.40		0.828	535.9	545.5	555.1	564.7	574.2	588.8	598.8
1	21.2	10.2	0.108	1.31	0.88	0.775	585.9	545.5	555.1	564.7	574.2	583.8	598.3
	21.0	13.5	0.102	1.28	0.46	0.728	536.0	545.6	555.2	564.8	574.8	583.9	598.4
	20.8	11.8	0.096	1.16	0.58	0.686	536.0	545.6	555.2	564.8	574.8	588.9	598.4
	20.6	10.1	0.090	1.09	0.60	0.645	536.1	545.7	555.3	564.9	574.4	584.0	598.5
H	20.4	8.4	0.084	1.02	0.67	0.604	686.1	545.7	555.8	564.9	574.4	584.0	593.5
	20.2	6.7	0.079	0.96	0.78	0.568	536.1	545.7	555.3	564.9	574.4	584.0	598.5
1				0.00		0.000	000.1	040.1	000.5	504.5	512.2	004.0	030.0
1							•	ľ	1		- 1		
23	23.0	28.0	0.144	1.75	0.00	1.000	534.6	544.2	558.7	568.8	572.8	582.4	591.9
ı	22.8	21.8	0.136	1.65	0.10	0.948	584.6	544.2	558.7	563.8	572.8	582.4	591.9
	22.6	19.6	0.127	1.55	0.20	0.886	584.7	544.3	553.8	563.4	572.9	582.5	592.0
1	22.4	17.9	0.120	1.45	0.30	0.829	584.7	544.8	558.8	568.4	572.9	582.5	592.0
1	22.2	16.2	0.112	1.36	0.39	0.777	584.8	544.4	558.9	563.5	578.0	582.6	592.1
1											1		
	22.0	14.5	0.106	1.28	0.47	0.781	584.8	544.4	558.9	568.5	578.0	582.6	592.1
	21.8	12.8	0.099	1.21	0.54	0.691	534.9	544.5	554.0	563.6	578.1	582.7	592.2
	21.6	11.1	0.093	1.18	0.62	0.646	534.9	544.5	554.0	568.6	578.1	582.7	592.2
l	21.4	9.4	0.087	1.06	0.69	0.606	585.0	544.6	554.1	563.7	573.2	582.8	592.8
A	21.2	7.7	0.082	1.00	0.75	0.571	585.0	544.6	554.1	568.7	578.2	582.8	592.8
		[
24	24.0	24.0	0.150	1.81	0.00	1.000	zoe 4	E 40 0		K00 0		FO1 4	KOC 4
	23.8	22.5	0.142	1.72	0.09	0.951	583.4	542.9	552.4	562.0	571.5	581.1	590.6
	22.6	21.1	0.142	1.63	0.18	0.901	588.5 533.5	548.0	552.5	582.1	571.6	581.2	590.7
		19.6				0.856	533.6	548.1 548.2	552.5	562.1	571.6		590.7
	23.2	18.2	0.121		0.35	0.807	583.6		552.6		571.7		,
i		10.2		1.40	0.00	0.007	000.0	045.2	552.6	562.2	571.7	581.3	590.8
	23.0	16.7	0.115	1.88	0.48	0.762	583.7	548.8	552.7	562.8	571.8	581.4	590.9
		15.2	0.108				588.7			562.8			
Ĭ.		13.8	0.108			0.685	538.7				571.8		
		12.3				0.652	583.8			562.4	571.9		
	22.2	10.8	0.091	1.12	0.69	0.634	583.8		552.8		571.9	581.5	591.0
]		1											
<u> </u>		·			<u> </u>		<u> </u>	<u>. </u>					

Re	ading	Temp.	Force	We of V	ight apor	Hu-	-	Weigh	t in Grai	ns of a Cr	nbic Foot	of Alz.	
moi	neter, ahr.	of Dew- Point,	of Vapor in	In a	for Sat'n.	midity, Setura- tion =		Height (of the Ba	rometer i	n Tinglis)	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- ble Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.e	30.5	31.0
25	25.0	25.0	ha. 0.155	gr. 1.87	gr. 0.00	1.000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
	24.8	23.7	6.148	1.78	0.09	0.952	582.8 582.8	541.8 541.8	551.8 551.8	560.8 560.8	570.3 570.3	579.8 579.8	589.8 589.3
	24.6	22.4	0.141	1.70	0.17	0.909	582.4	541.9	551.4	560.9	570.4	579.9	589.4
	24.4	21.2	0.185	1.62	0.25	0.867	582.4	541.9	551.4	560.9	570.4	579.9	589.4
1	24.2	19.9	0.129	1.55	0.32	0.829	582.4	541.9	551.4	560.9	570.4	579.9	589.4
	24.0	18.6	0.128	1.48	0.49	0.791	582.5	542.0	551.5	561.0	570.5	580.0	589.5
1	23.8	17.8	0.117	1.41	0.46	0.754	582.5	542.0	.551.5	561.0	570.5	580.0	589.5
	23.6	16.0	0.112	1.84	0.58	0.717	582.6	542.1	551.6	561.1	570.6	580.1	589.6
	28.4	14.8	0.107	1.28	0.59	0.685	582.6	542.1	551.6	561.1	570.6	580.1	589.6
	23.2	13.5	0.102	1.22	0.65	0.653	582.6	542.1	551.6	561.1	570.6	580.1	589.6
26	26.0	26.0	0.161	1.98	0.00	1.000	581.1	540.6	550.0	559.5	569.0	578.5	588.0
	25.8	24.8	0.154	1.85	0.08	0.959	581.2	540.7	550.1	559.6	569.1	578.6	588.1
	25.6	28.6	0.147	1.78	0.15	0.923	531.2	540.7	550.1	559.6	569.1	578.6	588.1
	25.4	22.8	0.141	1.70	0.28	0.881	581.2	540.7	550.1	559.6	569.1	578.6	588.1
	25.2	21.2	0.185	1.62	0.81	0.889	581.3	540.8	550.2	559.7	569.2	578.7	588.2
	25.0	19.9	0.129	1.55	0.38	0.804	531.8	540.8	550.2	559.7	569.2	578.7	588.2
	24.8	18.7	0.128	1.48	0.45	0.767	581.4	540.9	550.8	559.8	569.8	578.8	588.3
li l	24.6	17.5	0.118	1.41	0.52	0.781	581.4	540.9	550.8	559.8	569.8	578.8	588.8
	24.4	16.2	0.112	1.85	0.58	0.700	581.4	540.9	550.3	559.8	569.8	578.8	588.8
	24.2	15.0	0.108	1.29	0.64	0.668	531.5	541.0	550.4	559.9	569.4	578.9	588.4
27	27.0	27.0	0.167	2.00	0.00	1.000	529.9	589.4	548.9	558.4	567.8	577.8	586.7
	26.7	25.2	0.156	1.88	0.12	0.940	529.9	539.4	548.9	558.4	567.8	577.4	586.8
	26.4 26.1	23.8	0.146	1.76	0.24	0.880	530.0	589.5	549.0	558.5	567.9	677.5	586.9
	25.8	19.7	0.128	1.53	0.47	0.765	580.1 530.1	539.6 539.6	549.1 549.1	558.6 558.6	568.0 568.0	577.6 577.6	587.0 587.0
								000.0	04011		20010	211.0	
	25.5	17.8	0.119	1.48	0.57	0.715	580.2	539.7	549.2	558.7	568.1	577.7	587.1
	25.2 24.9	16.0	0.112	1.84	0.66	0.670	530.8	539.8	549.8	558.8	568.2	577.8	597.2
	24.6	14.2	0.104	1.26	0.74	0.630 0.585	530.8 530.4	589.8 539.9	549.3 549.4	558.8 559.0	568.2 568.3	577.8 577.9	587.2 587.8
	24.8	10.5	0.091	1.09	0.91	0.545	580.5	540.0	549.5	558.9 559.0	568.3	577.9	587.8
							255.0	22010	22510	203.0		2.1.0	
28	28.0	28.0	0.178	2.07	0.00	1.000	528.7	588.1	547.6	557.0	566.5	575.9	585.4
	27.7	26.8	0.168	1.95	0.12	0.942	528.8	538.2		557.1	566.6	576.0	585.5
	27.4	24.6	0.158	1.84	0.28	0.889	528.9		547.8	557.2		576.1	585.6
	27.1	22.9	0.144	1.78	0.84	0.836	528.9	538.3	547.8	557.2	566.7	576.1	585.6
	26.8	21.2	0.135	1.62	0.45	0.783	529.0	588.4	547.9	557.8	566.8	576.2	585.7
	26.5	19.4	0.126	1.52	0.55	0.784	529.1	538.5	548.0	557.4	566.9	576.8	585.8
	26.2	17.7	0.119	1.42	0.65	0.686	529.1				566.9	576.8	
	25.9	16.0	0.112	1.84	0.78	0.648	529.2	588.6	548.1	557.5	567.0	576.4	585.9
	25.6	14.8	0.105	1.26	0.82	0.604	529.2		548.1	557.5		576.4	. ,
	25.8	12.6	0.098	1.18	0.89	0.571	529.2	588.6	548.1	557.5	567.0	576.4	585.9

Re	ding			We	ight		1	Walah	t in Grah	ne of a Ch	nhia Yasi	of Altr.	
of '	Ther-	Temp.	Force of		Beqd.	Hu- midity,							
3 71	ahr.	Dew- Point,	Vapor	In a Cubic		Satura- tion =		Height	of the Ba	rometer 1	n Englis)	Inches.	
Day.	Wet.	Fahr.	English Inches.	Air.	of aCu- ble Ft. of Air.	1.000.	28.0	28.5	n. 99.0	99.5	30.0	in. 80.5	ь 81.0
٥		. 0	in.	gr.	gr.		gr.	F .	gr.	gr.	gr.	gr.	gr.
29	29.0 28.7	29.0	0.179	2.14	0.00	1.000	527.6	587.0	546.5	555.9	565.8	574.7	584.1
	28.4	27.5 26.0	0.170 0.161	2.03 1.92	0.11	0.949	527.7 527.7	537.1	546.6	556.0 556.0	565.4 565.4	574.8 574.8	584.2 584.2
	28.1	24.5	0.152	1.82	0.22	0.851	527.8	587.1 587.2	546.6 546.7	556.1	565.5	574.9	584.3
	27.8	23.0	0.144	1.78	0.41	0.809	527.8	587.2	546.7	556.1	565.5	574.9	584.3
			3122			0.000	02110	007.2	020	000.1	000.0	0.4.0	504.5
	27.5	21.5	0.137	1.64	0.50	0.766	527.9	587.8	546.7	556.2	565.6	575.0	584.5
	27.2	20.0	0.129	1.55	0.59	0.725	528. 0	587.4	546.8	556.2	565.7	575.1	584.6
	26.9	18.5	0.122	1.47	0.67	0.687	528.0	537.4	546.8	556.3	565.7	575. 2	584.6
	26.6	17.0	0.116	1.38	0.76	0.845	528.1	587.5	546.9	556.4	565.8	575.8	584.7
	26.8	15.5	0.110	1.30	0.84	0.617	528.1	587.5	546.9	556.4	565.8	575.8	584.7
30	30.0	30.0	0.186	2.21	0.00	1.000	526. 5	585.9	545.8	554.7	564.1	578.5	582.9
} '	29.7	28.6	0.177	2.10	0.11	0.951	526. 5	585.9	545.8	554.7	564.1	573.5	582.9
	29.4	27.2	0.168	2.00	0.21	0.905	526.6	536.0	545.4	554.8	564.2	573.6	588.0
	29.1	25.9	0.160	1.91	0.80	0.864	526.7	586.1	545.5	554.9	564.8	578.7	583.1
	28.8	24.5	0.152	1.82	0.89	0.824	526.7	536.1	545.5	554.9	564.8	578.7	588.1
	28.5	23.1	0.145	1.78	0.48	0.788	526.8	586.2	545.6	555.0	564.4	578.8	588.2
	28.2	21.7	0.188	1.64	0.57	0.742	526.8	536.2	545.6	555.0	564.4	578.8	583.2
	27.9	20.3	0.181	1.56	0.65	0.706	526.9	536.3	545.7	555.1	564.5	578.9	588.8
	27.6	19.0	0.125	1.49	0.72	0.674	526. 9	536.8	545.7	555.1	564.5	573.9	588.8
	27.8	17.6	0.118	1.42	0.79	0.643	527.0	586.4	545.8	555.2	564.6	574.0	583.4
31	81.0	31.0	0.192	2.29	0.00	1.000	525.4	584.7	544.1	552.5	562.9	572.8	581.7
	80.7	29.9	0.135	2.20	0.09	0.961	525.4	584.7	544.1	558.5	562.9	572.8	581.7
l I	80.4	28.8	0.178	2.12	0.17	0.926	525.5	584.8	544.2	558.6	568.0	572.4	581.8
	80.1	27.7	0.171	2.04	0.25	0.891	525.5	584.8	544.2	558.6	568.0	572.4	581.8
	29.8	26.6	0.164	1.95	0.84	0.852	525.6	584.9	544.8	558.7	563.1	572.5	581.9
	90.5	25.5	0.150	1 00	0.40	A 61#	E0	E6. C		##C =	E00 -	200 "	#01 A
H	29.5 29.2	24.4	0.158 0.152	1.87 1.80	0.42	0.817 0.786	525.6 525.6	584.9 584.9	544.8 544.8	558.7 558.7	568.1 563.1	572.5 572.5	581.9 581.9
1	28.9	28.4	0.146	1.78	0.56	0.756	525.7	585.0	544.4	558.8	563.2	572.6	582.0
1	28.6	22.8	0.141	1.67	0.62	0.729	525.7	585.0	544.4	558.8	563.2	572.6	582.0
[]	28.3	21.2	0.185	1.60	0.69	0.699	525.7	585.0	544.4	558.8	568.2	572.6	582.0
[
													HAC -
32	82.0	32.0 30.8	0.199	2.37	0.00	1.000 0.958	524.2	588.5	542.9	552.3	561.6	570.9	580.8
	31.6 31.2	29.5	0.191		0.10		524.8	588.6	548.0	552.4	561.7	571.0	580.4 580.5
1	80.8	28.3	0.152	2.17 2.07	0.20	0.916 0.874	524.4 524.4		548.1 548.1		561.8 561.8	571.1 571.1	580.6
 	80.4	27.0	0.167	1.98	0.89	0.836	524.5				561.9	571.2	580.6
] :						3	322.0	500.0	J-20.2	302.0	301.5	3,1,5	500.0
	80.0	25.8	0.160	1.90	0.47	0.802	524 .5					571.2	580.6
	29.6	24.6	0.158	1	0.55		524.6			552.7			
H	29.2	23.8	0.146	1.74	0.63	0.785	524.6						
	28.8	22.1	0.140	1.67	0.70	0.705	524.6		548.8				
	Z5.4	20.8	0.133	1.00	0.77	0.675	DZ4.7	D34.0	048.4	002.8	562.1	571.4	8,080

of '	ding Ther-	Temp.	Force of	We of V	ight apor Read.	Hu-		Weigh	t in Grai	os of a C	able Foot	of Air.	
	abr.	Dow- Point.	Vapor	In a	for Sat'n.	midity, Seture- tion ==		Height	of the Ba	rometer i	a English	Inches.	
Dry.	Wet.	Fahr.	English Inches.		of aCu- blo Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	in. 31.0
. 0	0	33.0	in.	gr.	gr.	* 000	gr.	gt.	gr.	gr.	gt.	gr.	gr.
83	33.0 32.5	81.6	0.207	2.45 2.33	0.00	1.000 0.951	528.0 528.1	582.8 582.5	541.7 541.8	551.1 551.2	560.4 560.5	569.7 569.8	579.1 579.2
1 1	32.0	80.2	0.187	2.22	0.28	0.906	528.2	582.6	541.9	551.3	560.6	569.9	579.8
	31.5	28.8	0.178	2.11	0.84	0.862	528.3	582.7	542.0	551.4	560.7	570.0	579.4
	81.0	27.4	0.169	2.01	0.44	0.821	528.8	582.7	542.0	551.4	560.7	570.0	579.4
1													
	80.5	26.0	0.161	1.91	0.54	0.780	528.4	582.8	542.1	551.5	560.8	570.1	579.5
	80.0	24.6	0.158	1.82	0.68	0.748	528.4	532.8	542.1	551.5	560.8	570.1	579.5
	29.5	28.2	0.145	1.74	0.71	0.711	523.5	582.9	542.2	551.6	560.9	570.2	579.6
li 1	29.0	21.8	0.188	1.65	0.80	0.674	523 .5	582.9	542.2	551.6	560.9	570.2	579.6
	28.5	20.4	0.131	1.57	0.88	0.641	523.6	588.0	542.3	551.7	561.0	570.8	579.7
			.										
84	34.0	34.0	0.214	2.58	0.00	1.000	521.9	581.2	540.6	549.9	559.2	568.5	577-8
^	88.5	82.7	0.204	2.42	0.11	0.957	522.0	581.4	540.7	550.0	559.8	568.6	577.9
	38.0	31.4	0.195	2.31	0.22	0.918	522.0	581.4	540.7	550.0	559.3	568.6	577.9
	82.5	80.1	0.186	2.21	0.82	0.874	522.1	581.5	540.8	550.1	559.4	568.7	578.0
	82.0	28.8	0.178	2.11	0.42	0.884	522.1	581.5	540.8	550.1	559.4	568.7	578.0
	31.5	27.5	0.170	2.01	0.52	0.795	522.2	581.6	540.9	550.2	559.5	568.8	578.1
	81.0	26.2	0.162	1.91	0.62	0.755	522.8	581.7	541.0	550.8	559.6	568.9	578.2
	80.5	24.9	0.155	1.88	0.70	0.724	522.8	581.7	541.0	550.8	559.6	568.9	578.2
	80.0	23.6	0.147	1.75	0.78	0.692	522.4	581.8	541.1	550.4	559.7	569.0	578.8
	29.5	22.8	0.141	1.67	0.86	0.660	522.4	581.8	541.1	550.4	559.7	569.0 569.1	578.8 578.4
	29.0	21.0	0.184	1.59	0.94	0.629	522.5	581.9	541.2	550.5	559.8	509.1	010.4
11									'		İ		
85	- 85	85.0	0.222	2.62	0.00	1.000	520.8	580.1	539.4	548.7	558.0	567.8	576.6
	34	32.5	0.208	2.40	0.22	0.916	520.9	580.2	539.5	548.8	558.1	567.4	576.7
	38	30.0	0.186	2.19	0.43	0.886	521.0	580.8	589.6	548.9	558.3	567.5	576.8
	82	27.5	0.170	2.00	0.62	0.764	521.1	580.4	539.7	549.0	558.4	567.6	576.9
	81	25.0	0.155	1.88	0.79	0.698	521.2	580.5	539.8	549.1	558.5	567.7	577.0
				1.00			-		F00 0	F 40 =	***	E0= 0	Egp 1
	80	22.5	0.142	1.68	0.94	0.641	521.8 521.8	580.6 580.7	589.9	549.2	558.6 558.6	567.8 567.9	577.1 577.2
	29	20.0	0.129	1.58	1.09	0.584			540.0	549.8 549.4	558.7	568.0	577.Z
	28 27	17.5 15.0	0.117	1.39	1.28	0.581 0.485	521.4 521.5	530.8 580.9	540.1 540.2	549.5	558.7	568.1	577.4
	21	10.0	0.108	1.56	1.50	0.400	921.0	000.3	040.2	045.0	000.7	000.1	0.7.4
													<u>'</u>
36	86	86.0	0.280	2.73	0.60	1.000	519.7	529.0	588.8	547.5	556.8	566.1	575.4
	85	33.5	0.210	2.48	0.28	0.915	519.8	529.1	538.4	547.6	556.9	566.2	575.5
	84	81.0	0.192	2.27	0.44	0.888	519.9	529.2	588.5	547.7	557.0	566.3	575.6
	88	28.5	0.176	2.07	0.64		520. 0	529.8	588.6	547.8	557.1	566.4	575.7
	82	26.0	0.161	1.89	0.82	0.698	520.1	529.4	588.7	547.9	557.2	566.5	575.8
				,	0.00	0.010	28A C	E00 -	E00 C	E40 A	557.8	566.6	575.9
11	81	28.5	0.147	1.74	0.97	0.642	520.2		588.8	548.0		~~~	576.0
	80 29	21.0	0.184 0.122	1.58	1.18	0.588	520.3 520.4	529.6 529.7	588.9 589.0	548.1 548.2	557.4 557.5	1	576.1
	28	18.5 16.0	0.122	1.45 1.82	1.26	0.585	520.4 520.5	529.7	589.1	548.3	557.6		576.2
H I	""	10.0	V-112	1.02	1.00	V-407	UEU-0	VAB-0	J-5-1		007.0	0000	
<u> </u>		1	1	<u></u>					<u>' </u>	<u> </u>		<u> </u>	

of '	ding	Temp.	Force of	We of V	ight aper Read.	Hu-		Weigh	t in Grai	as of a Ct	able Foot	of Air.	
P	neter, shr.	Dew- Point,	Vapor	In a Cubic	for Sat'n.	midity, Satura-		Height o	of the Bes	rometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.		1.000.	28.0	28.5	99.0	29.5	80.0	30.5	31.0
87	37	37.0	in. 0.288	gr. 2.80	gr. 0.00	1.000	gr.	gr.	gr.	gt.	gr.	gr.	gr.
"	36	84.5	0.218	2.56	0.24	0.914	518.6 518.7	527.8 527.9	587.1 587.2	546.3 546.4	555.6 555.7	564.8 564.9	574.1 574.2
i	85	32.0	0.199	2.35	0.45	0:889	518.8	528.0	587.8	546.5	555.8	565.0	574.8
	84	29.5	9.182	2.14	0.66	0.764	518.9	528.1	587.4	546.6	555.9	565.1	574.4
	83	27.0	0.167	1.96	0.84	0.700	519.0	528.2	587.5	546.7	556.0	565.2	574.5
	32	24.5	0.152	1.79	1.01	0.640	519.1	528.3	537.6	546.8	556.1	565.8	574.6
	81	22.0	0.139	1.64	1.16	0.586	519.2	528.4	587.7	546.9	556.2	565.4	574.7
	30	19.5	0.127	1.50	1.30	0.536	519.8	528.5	587.8	547.1	556.8	565.5	574.8
	29	17.0	0.116	1.37	1.43	0.489	519.4	528.6	587.9	547.2	556.4	565.6	574.9
38	88	88.0	0.246	2.89	0.00	1.000	517.4	526.6	585.9	545.1	554.4	568.6	572.9
	87	85.5	0.226	2.65	0.24	0.917	517.5	526.7	586.0	545.2	554.5	568.7	573.0
	36	83.0	0.207	2.48	0.46	0.841	517.6	526. 8	586.1	545.8	554.6	568.8	578.1
	85	30.5	0.189	2.22	0.67	0.768	517.7	526.9	536.2	545.4	554.7	563.9	573.2
	84	28.0	0.178	2.08	0.86	0.703	517.8	527.0	536.3	545.5	554.8	564.0	578.8
	88	25.5	0.158	1.85	1.04	0.640	517.9	527.1	536.4	545.6	554.9	564.1	578.4
	82	23.0	0.144	1.70	1.19	0.588	518.0	527.2	586.5	545.7	555.0	564.2	578.5
	81	20.5	0.132	1.54	1.85	0.588	518.1	527.3	586.6	545.8	555.1	564.8	578.6
	80	18.0	0.120	1.89	1.50	0.481	518.2	527.4	536.7	545.9	555.2	564.4	578.7
		l											
39	89	39.0	0.255	2.99	0.00	1.000	516.8	525.5	584.7	543.9	558.2	562.4	571.6
	38	36.5	0.234	2.74	0.25	0.917	516.4	525.6	584.8	544.0	558.8	562.5	571.7
	87	34.0	0.214	2.51	0.48	0.840	516.5	525.7	534.9	544.1	558.4	562.6	571.8
	86	31.5	0.196	2.30	0.69	0.769	516.6	525. 8	585.0	544.2	553.5	562.7	571.9
	85	29.0	0.179	2.10	0.89	0.708	516.7	525.9	585.1	544.8	553.6	562.8	572.1
	34	26.5	0.164	1.91	1.08	0.689	516.8	526.0	535.2	544.4	558.7	562.9	572.2
	33	24.0	0.150	1.76	1.28	0.589	516.9	526.1	585.8	544.5	558.8	563.0	572.8
	82	21.5	0.187	1.60	1.39	0.585	517.0	526.2	585.4	544.6	558.9	568.1	572.4
	81	19.0	0.125	1.46	1.58	0.488	517.1	526.3	585.6	544.8	554.1	563.8	572.6
	30	16.5	0.114	1.82	1.67	0.442	517.2	526.4	585.7	844.9	554.2	563.4	572.7
40	40	40.0	0.264	8.09	0.00	1.000	515.2	524.4	588.6	542.8	552.0	561.2	570.4
	89	87.8	0.245	2.86	0.23	0.926	515.8	524.5	588.7	542.9	552.1	561.8	570.5
	38	35.6	0.227	2.65	0.44	0.858	515.4	524.6	588.8	548.0	552.2	561.4	570.6
	87	88.4	0.210	2.45	0.64	0.798	515.5	524.7	533.9	548.1	552.8	561.5	570.7
	86	81.2	0.194	2.27	0.82	0.734	515.6	524.8	584.0	543.2	552.4	561.6	570.8
	85	29.0	0.179	2.09	1.00	0.676	515.7	524.9	584.1	548.8	552.5	561.7	570.9
	84	26.8	0.165	1.94	ı	0.628	515.8	525.0	584.2	543.4	1	l	571.0
1	88	24.6	0.153	1.79	1.80	0.579	515.9		1		552.7	561.9	571.1
1	32	22.4	0.141	1.65	ı	0.584	516.0	l .	•		552.8	1	571.2
	31 30	20.2 18.0	0.130 0.120	1.58 1.42	1.56	0.495	516.1 516.1	525.8 525.3	584.5 584.5	543.7 54 3. 8	552.9 558.0	562.1 562.2	571.8 571.4
	~	13.0	0.120	1.72	1.07	0.408	510.1	020.0	00.1.0	0.0	000.0	502.2	01114
Щ		'									************************************		

of ?	ding Ther-	Temp.	Force of	We of V	ight spor	Hu-		Weigh	t in Grai	as of a C	abic Foot	of Air.	
	beter,	of Dew-	Vapor	In a Cubic	for Bat'n.	midity, Seture-		Height	of the Ba	rouneter !	n Englis	h Inches	
Dry.	Wet.	Point, Fahr.	English Inches.		of aCu- bic Ft. of Air.	1.000.	98.0	28.5	29.0	29.5	30.0	in. 30.5	81.0
.0	0	410	in.	gr.	gt.	T 000	gr.	gr.	gr.	gr.	gT.	gr.	gr.
41	41	41.0 88.8	0.274	8.19 2.96	0.00	1.000 0.928	514.1 514.2	523.3 523.4	582.5 582.6	541.6 541.7	550.8 550.9	560.0 560.1	569.2 569.8
11	89	36.6	0.235	2.74	0.45	0.859	514.8	523.5	582.7	541.8	551.0	560.2	569.4
11 1	88	84.4	0.217	2.54	0.65	0.796	514.4	528.6	532.8	541.9	551.1	560.8	569.5
li l	87	82.2	0.201	2.85	0.84	0.787	514.5	523.7	532.9	542.0	551.2	560.4	569.6
	86	80.0	0.186	2.16	1.03	0.677	514.6	523.8	538.0	542.1	551.8	560.5	569.7
	35	27.8	0.172	2.01	1.18	0.630	514.7	528.9	533.1	542.2	551.4	560.6	569.8
	34	25.6	0.172	1.85	1.34	0.580	514.8	524.0	583.2	542.8	551.5	560.7	569.9
	83	23.4	0.146	1.71	1.48	0.586	514.9	524.1	533.3	542.4	551.6	560.8	570.0
	32	21.2	0.135	1.58	1.61	0.495	514.9	524.1	533.8	542.5	551.7	560.9	570.1
	31	19.0	0.125	1.46	1.78	0.458	515.0	524.2	588.4	542.6	551.8	561.0	570.2
1 1													
42	42	42.0	0.283	3.30	0.00	1.000	518.0	522.2	581.8	540.5	549.6	558.8	567 9
	41	89.8	0.263	3.06	0.24	0.927	518.1	522.8	531.4	540.6	549.7	558.9	568.0
	40	37.6	0.243	2.83	0.47	0.858	518.2	522.4	581.5	540.7	549.9	559.0	568-1
	89	85.4	0.225	2.68	0.67	0.797	518.8	522.5	581.6	540.8	550.0	559.1	568.2
1	88	88.2	0.208	2.43	0.87	0.786	518.4	522.6	581.7	540.9	550.1	559.2	568.3
	87	81.0	0.192	2.24	1.06	0.679	513.5	522.7	581.8	541.0	550.2	559.8	568.4
11 1	36	28.8	0.178	2.08	1.22	0.681	518.6	522.8	531.9	541.1	550.8	559.4	568.5
11	35	26.6	0.164	1.91	1.89	0.579	513.7	522.9	582.0	541.2	550.4	559.5	568.6
	34	24.4	0.152	1.77	1.58	0.586	513.8	528.0	582.1	541.3	550.5	559.6	568.7
11	38	22.2	0.140	1.63	1.67	0.494	513.9	523.1	532.2	541.4	550.6	559.7	568.8
ll i	82	20.0	0.129	1.51	1.79	0.458	518.9	528.1	582.3	541.5	550.6	559.8	569.0
48	43	43.0	0.293	3.41	0.00	1.000	511.8	520.9	530.1	539.8	548.4	557.5	566.7
-	42	40.8	0.272	3.16	0.25	0.927	511.9	521.0	530.2	589.4	548.6	557.7	566.9
11	41	38.6	0.252	2.93	0.48	0.859	512.0	521.1	530.3	539.5	548.7	557.8	567.0
	40	36.4	0.233	2.71	0.70	0.795	512.1	521.2	530.4	589.6	548.8	557.9	567.1
11	89	84.2	0.216	2.51	0.90	0.736	512.2	521.3	530.5	539.7	548.9	558.0	567.2
1 1	88	82.0	0.199	2.32	1.09	0.680	512.3	521.4	580.7	589.8	549.0	558.1	567.8
1 1	87	29.8	0.184	2.15	1.26	0.680	512.4	521.5	530.8	539.9	549.1	558.2	567.4
	36	27.6	0.170	1.98	1.48	0.581	512.5	521.6	580.9	540.0	549.2	558.8	567.5
	85	25.4	0.157	1.82	1.59	0.584	512.6	521.7	581.0	540.1	549.8	558.4	567.6
	84	28.2	0.145	1.69	1.72	0.495	512.7	521. 8	581.1	540.2	549.4	558.5	567.7
	33	21.0	0.184	1.56	1.85	0.458	512.9	522.0	581.2	540.8	549.5	558.6	567.8
44	44	44.0	0.804	8.52	0.00	1.000	510.8	519.9	529.0	588.1	547.8	556.4	565.5
	43	41.8	0.282	8.27	0.25	0.929	510.9	520. 0	529.1	588.2	547.5	556.5	565.7
	42	39.6	0.261	3.02	0.50	0.858	511.0	520.1	529.2	1	547.6	1	00000
	41	37.4	0.241	2.80	0.72	0.796	511.1		1	ı	!	i	1 1
	40	35.2	0.223	2.60	0.92	0.789	511.2		ł		547.8	1	1
	89	33.0	0.207	2.40	1.12	0.682	511.8	l	529.5	1	547.9	556.9	1
	38	30.8	0.191	2.22	1.80		511.4	1	529.6		1	557.0	i 1
	87	28.6	0.177	2.05	1.47	0.582	511.5	l	529.7	ľ	548.1	(1 1
	36	26.4	0.163	1.89	1.63	0.537		520.7	529.8	I .	548.2	1	i 1
	35	24.2	0.151	1.75	1.77	0.497		520.8				557.8	
	84	22.0	0.139	1.62	1.90	0.460	511.7	520.8	580.0	589.1	548.3	557.4	566.6

of 1	ding Ther-	Temp.	Force of		ight apor	Hu-		Weigh	t in Grain	as of a C	ibic Foot	of Air.	`
	ueter, uhr.	of Dew-	Vapor	In a Cubic	Reqd. for Sat'n.	midity, Satura-		Height	of the Ba	rozneter i	n Englisi	h Inches	•
Dry.	Wet.	Point, Fabr.	English Inches	Foot of Air.		tion == 1.000.	98.0	98.5	29.0	29.5	30.0	30.5	31.0
58	 53	o 53.0	in. 0.414	gr. 4.71	gr. 0.00	1.000	gr. 500.9	509.8	gr. 518.8	gr. 527.7	gr. 586.7	gr. 545.6	67. 554.6
i	52	51.0	0.386	4.40	0.81	0.934	501.1	510.0	519.0	527.9	536.9	545.8	554-8
	51	49.0	0.361	4.11	0.60	0.878	501.2	510.1	519.1	528.0	537.0	545.9	554.9
	50	47.0	0.337	8.84	0.87	0.815	501.4	510.8	519.8	528.2	587.2	546.1	555.1
il	49	45.0	0.815	8.58	1.13	0.760	501.5 501.6	510.4 510.5	519.4	528.3	537.8	546.2 546.3	555.2 555.3
	48	48.0	0.298	8.34	1.87	0.709			519.5	528.4	587.4	İ	1
1	47	41.0	0.274	8.12	1.59	0.662	501.7	510.6	519.6	528.5	587.5	546.4	555.4
	46	39.0	0.255	2.91	1.80	0.618	501.8	510.7	519.7	528.6	537.6	546.5 546.7	555.5 555.7
	45	37.0 35.0	0.238 0.222	2.71 2.58	2.00 2.18	0.575	502.0 502.1	510.9 511.0	519.9 520.0	528.8 528.9	587.8 587.9	546.8	555.8
.	44	33.0	0.207	2.85	2.36	0.499	502.1	511.0	520.0	528.9	588.0	546.9	555.9
¦	42	31.0	0.192	2.18	2.53	0.463	502.2	511.1	520.1	529.0	588.1	547.0	556.0
54	54	54.0	0.428	4.86	0.00	1.000	499.9	508.8	517.8	526.7	585.6	544.5	558.5
	53	52.0	0.400	4.54	0.82	0.984	500.0	508.9	517.9	526.8	585.7	544.6	558-6
1 1	52	50.0	0.378	4.25	0.61	0.875	500.2	509.1	518.1	527.0	535.9	544.8	558.8
	51	48.0	0.849	3.96	0.90	0.815	500.8	509.2	518.2	527.1	586.0 586.1	544.9 545.0	558.9 554.0
	50	46.0	0.826	3.70	1.16	0.761	500.4	509.8	518.8	527.2			1
H	49	44.0	0.304	3.45	1.41	0.709	500.6	509.5	518.5	527.4	586.8	545.2	554.2
	48	42.0	0.288	3.23	1.63	0.665	500.7	509.6	518.6	527.5	586.4	545.8 545.4	554.8 554.4
i i	47	40.0 88.0	0.264	3.01 2.80	1.85 2.06	0.619	500.8 500.9	509.7 509.8	518.7 518.8	527.6 527.7	586.5 586.7	545.6	554.6
.	46 45	36.0	0.230	2.61	2.25	0.587	501.0	509.9	518.9	527.8	586.8	545.7	554.7
. !		1	0.214	ł	2.48	0.500	ł	510.0	519.0	527.9	586.9	845.8	554.8
	44	34.0 32.0	0.199	2.43 2.27	2.59	0.467	501.1 501.2	510.1	519.1	528.0	587.0	545.9	554.9
۱	42	30.0	0.186	2.10	2.76	0.482	501.8	510.2	519.2	528.1	587.1	546.0	555.0
;	41	28.0	0.178	1.96	2.90	0.408	501.4	510.8	519-3	528.2	587.2	546.1	555.1
,]	40	26.0	0.161	1.82	8.04	0.875	501.5	510.4	519-4	528.3	587.3	546.2	555.2
: 1													
56	55	55.0	0.442	5.02	0.00	1.000	498.8	507.7	516.6	525.5	584.4	543.8	552.2 552.4
	54	53.8 51.6	0.418	4.74	0.28	0.944	499.0 499.1	507.9 508.0	516.8 516.9	525.7 525.8	584.6 584.7	543.5 543.6	552.5
, 1	58 52	49.9	0.372	4.46	0.56	0.848	499.8	508.2	517.1	526.0	584.9	548.8	552.7
۱ ۱	51	48.2	0.851	3.98	1.04	0.798	499.4	508.3	517.2	526.1	585.0	543.9	552.8
	50	46.5	0.331	3.76	1.26	0.749	499.5	508.4	517.3	526.2	535.1	544.0	552.9
- 1	49	44.8	0.812	8.55	1.47	0.707	499.7	508.6	517.5	526.8	535.8	544.2	553.1
	48	43.1	0.295	3.34	1.68	0.665	499.8	508.7	517.6	526.5	585.4	544.8	558.3
	47	41.4	0.278	8.14	1.88	0.626	499.8	508.7	517.6	526.6	585.5	541.4	553.4
	46	39.7	0.262	2.97	2.05	0.591	499.9	508.8	517.7	526.7	585.6	544.5	553.5
	45	38.0	0.246	2.79	2.28	0.556	500.0	508.9	1	526.8	585.7	544.6	553.6
	44	36.3	0.232	2.64	2.38	0.526	500.1	509.0	518.0	526.9	585. 8	544.7	553.7
	48	84.6	0.219	2.47	2.55	0.492	500.2	509.1	518.1	527.0	585.9	544.8	553.8
	42	82.9	0.206	2.82	2.70	0.462	500.3	509.2	518.2	1	586.0	544.9	553.9
	41	31.2	0.194	2.20	2.82	0.438	500.4	509.8			ı	544.9	554.0
	40	29.5	0.182	2.07	2.95	0.412	500.5	509.3	518.4	1	586.1	545.0	554.1
	29	27.8	0.172	1.95	3.07	0.388	500.6	509.4					554.2
1	38	26.1	0.161	J.88	8.19	0.365	500.7	509.5	518.6	527.4	536.2	045.1	554.2

Re	ading Ther-	Temp.	Force		ight apor	Hu-		Weigh	t in Grah	ns of a C	abie Foot	of Air.	
22001	meter, ahr.	of Dew- Point,	Vapor Vapor	In a Cubic	Reqd. for Set'n.	midity, Setura- tion =		Height o	of the Bes	rometer i	n Englist	Inches.	
Dry.	Wet.	Fahr.	Ringlish Inches.	Foot of Air.	ofaCu- bic Ft. of Air.	1.000.	98.0	1n. 98.5	99.0	29.5	30.0	in. 30. 5	81.0
49	o 49	49.0	ln. 0.361	gr. 4.14	0.00	1.000	gr. 505.3	gr. 514.3	gr. 523.8	gr. 532.3	gr. 541.4	gr. 550.4	gr. 55 9 .4
-	48	46.9	0.886	3.85	0.29	0.980	505.4	514.4	528.4	532.4	541.5	550.5	559.5
	47	44.8	0.812	8.59	0.55	0.867	505.6	514.6	523.6	582.6	541.7	550.7	559.7
	46	42.7	0.290	8.34	0.80	0.807	505.7	514.7	523.7	582.7	541.8	550.8	559.8
	45	40.6	0.270	8.10	1.04	0.749	505.9	514.9	528-8	582.9	542.0	551.0	560.0
	44	88.5	0.251	2.88	1.26	0.696	506.0	515.0	528.9	588.0	542.1	551.1	560.1
l	43	36.4	0.238	2.68	1.46	0.647	506.1	515.1	524.0	583.1	542.2	551.2	560.2
	42	84.8	0.216	2.49	1.65	0.601	506.2	515.2	524.1	533.2	642.3	551.3	560.8
	41	32.2	0.201	2.82	1.82	0.560	506.3	515.8	524.2	583.3	542.4	551.4	560.4
	40	80.1	0.186	2.14	2.00	0.517	506.3	515.8	524.8	583.4	542.5	551.5	560.5
	89	28.0	0.178	1.99	2.15	0.481	506.4	515.4	524.4	588.5	542.6	551.6	560.6
50	38 50	25.9 50.0	0.160 0.378	1.84 4.28	2.30 0.00	0.444	506.4	515.4	524.4	588.5	542.6	551.6	560.6
50	49	48.0	0.849	8.99	0.29	1.000	504.1 504.2	513.1	522.1	581.1	540.2	549.2	558.2
	48	46.0	0.326	8.78	0.55	0.871	504.4	518.2 518.4	522.2 522.4	531.2 581.4	540.8 540.5	549.8 549.5	558.8 558.5
1	47	44.0	0.804	3.48	0.80	0.818	504.5	518.5	522.5	581.5	540.6	549.6	558.6
	46	42.0	0.288	3.25	1.03	0.759	504.6	513.6	522.6	531.6	540.7	549.7	558.7
	45	40.0	0.264	3.03	1.25	0.708	504.8	518.8	522.8	581.8	540.9	549.9	558.9
	44	38.0	0.246	2.82	1.46	0.659	504.9	513.9	522.9	582.0	541.0	550.0	559.0
	48	36.0	0.280	2.68	1.65	0.614	505.1	514.1	528.1	532.1	541.2	550.2	559.2
	42	84.0	0.214	2.45	1.88	0.572	505.2	514.2	528.2	582.2	541.8	550.8	559.3
	41	32.0	0.199	2.28	2.00	0.583	505.3	514.8	523.3	582.3	541.4	550.4	559.4
	40	80.0	0.186	2.12	2.16	0.495	505.4	514.4	528.4	532.4	541.5	550.5	559.5
	89	28.0	0.178	1.97	2.81	0.460	505.5	514.5	523.5	582.5	541.6	550.6	559.6
51	51	51.0	0.886	4.42	0.00	1.000	508.1	512.1	521.1	580.0	589.0	548.0	557.0
	50	49.0	0.861	4.12	0.80	0.982	508.2	512.2	521.2	530.1	589.1	548.1	557.1
	49	47.0	0.337	8-85	0.57	0.871	508.8	512.8	521.8	580.8	539.8	548.3	557.8
'	48	45.0	0.315	8.60	0.82	0.814	508.4	512.4	521.4	580.4	589.4	548.4	557.4
	47 46	48.0 41.0	0.293 0.274	3.36	1.06 1.29	0.760	508.5	512.5	521.5	580.5	589.5	548-5	557.5
	45	39.0	0.255	3.13 2.92	1.50	0.708 0.661	508.7 508.8	512.7 512.8	521.7 521.8	530.7 530.8	589.7 589.8	548.7 548.8	557.7 557.8
1	44	87.0	0.238	2.72	1.70	0.615	503.9	512.9	521.9	580.9	589.9	548.9	557.9
	43	85.0	0.222	2.54	1.88	0.575	504.0	518.0	522.0	531.0	540.0	549.0	558.0
	42	33.0	0.207	2.86	2.06	0.534	504.1	518.1	522.1	531.1	540.1	549.1	558.1
	41	81.0	0.192	2.20	2.22	0.498	504.2	513.2	522.2	531.2	540.8	549.8	558.3
	40	29.0	0.179	2.05	2.87	0.464	504.8	513.3	522.8	581.8	540.4	549.4	558.4
52	52	52.0	0.400	4.56	0.00	1.000	502.1	511.0	520.0	528.9	537.9	546.8	555.8
	51	50.0	0.878	4.26	0.80	0.934	502.2	511.1	520.1	529.0	588.0	546.9	555.9
	50	48.0	0.349	3.98	0.58	0.878	502.4	511.8	520.8	529.2	53 8.2	547.1	556.1
	49	46.0	0.326	8.72	0.84	0.816	502.5	511.4	520.4	529.3	588.8	547.2	556.2
	48	44.0	0.304	8.47	1.09	0.761	502.6	511.5	520.5	529.4	588.4	547.8	556.3
	47	42.0	0.288	3.23	1.88	0.709	502.8	511.7		529.6	588.6	547.5	556.5
	46	40.0	0.264	3.02	1.54	0.662	502.9	511.8	l .	529.7		547.6	556.6
	45	38.0 36.0	0.246	2.81	1.75	0.616	502.9	511.9	•	529.8	588.8 Ken n	547.8 549.0	556.8
	43	34.0	0.230	2.63	1.93 2.12	0.577 0.585	508.1 508.2	512.0 512.1	521.1	529.9 530.0	539.0 539.1	548.0 548.1	557.0 557.1
	42	82.0	0.199	2.28	2.28	0.500	508.2	512.1	521.3	580.2	539.2	548.2	557.2
1	41	30.0		2.13		0.467	508.4		521.4			1	
<u></u>	l	Li	0.200	1		1 2.30		4.2.4		500.0	200.0	5.0.0	

	ding Ther-	Temp.	Force of		ight apor Regd.	Hu-		Weigh	t in Grain	as of a Cr	abic Foot	of Air.	`
	neter, abr.	Dew-	Vapor	In a	for Sat'n.	midity, Satura-		Height o	of the Ba	rometer i	n Englis	h Inches	•
Dry.	Wet.	Point, Fahr.	English Inches.			tion = 1.000.	98.e	98.5	29.0	29.5	30.0	30.5	81.0
	•	0	bn.	gr.	gr.		gr.	gr.	gr.	gr.	gr.	gr.	gr.
58	58	53.0	0.414	4.71	0.00	1.000	500.9	509.8 510.0	518.8	527.7	536.7	545.6 545.8	554.6 554.8
!]	52 51	51.0 49.0	0.386	4.40	0.81	0.984	501.1 501.2	510.1	519.0 519.1	527.9 528.0	536.9 587.0	545.9	554.9
<u> </u>	50	47.0	0.837	8.84	0.87	0.815	501.4	510.3	519.3	528.2	587.2	546.1	555.1
	49	45.0	0.315	8.58	1.13	0.760	501.5	510.4	519.4	528.8	587.8	546.2	555.2
<u>l</u> l 1	48	43.0	0.298	8.84	1.87	0.709	501.6	510.5	519.5	528.4	537.4	546.8	555.8
	47	41.0	0.274	8.12	1.59	0.662	501.7	510.6	519.6	528.5	587.5	546.4	555.4
	46	89.0	0.255	2.91	1.80	0.618	501.8	510.7	519.7	528.6	587.6	546.5	555.5
	45	87.0	0.238	2.71	2.00	0.575	502.0	510.9	519.9	528.8	537.8	546.7	555.7
	44	35.0	0.222	2.53	2.18	0.587	502.1	511.0	520.0	528.9	587.9	546.8	555.8
[]	43	33.0	0.207	2.35	2.36	0.499	502.1	511.0	520.0	528.9	588.0	546.9	555.9
	42	81.0	0.192	2.18	2.53	0.463	502.2	511.1	520.1	529.0	588.1	547.0	556.0
54	54	54.0	0.428	4.86	0.00	1.000	499.9	508.8	517.8	526.7	585.6	544.5	558.5
34	58	52.0	0.400	4.54	0.32	0.984	500.0	508.9	517.9	526.8	535.7	544.6	558.6
	52	50.0	0.373	4.25	0.61	0.875	500.2	509.1	518.1	527.0	585.9	544.8	558.8
	51	48.0	0.849	3.96	0.90	0.815	500.3	509.2	518.2	527.1	586.0	544.9	558.9
	50	46.0	0.826	3.70	1.16	0.761	500.4	509.8	518.8	527.2	536.1	545.0	554.0
	49	44.0	0.304	8.45	1.41	0.709	500.6	509.5	518.5	527.4	586.3	545.2	554.2
	48	42.0	0.288	3.23	1.63	0.665	500.7	509.6	518.6	527.5	586.4	545.8	554.8
	47	40.0	0.264	3.01	1.85	0.619	500.8	509.7	518.7	527.6	536.5	545.4	554.4
	46	38.0	0.246	2.80	2.06	0.576	500.9	509.8	518.8	527.7	586.7	545.6	554.6
	45	36.0	0.230	2.61	2.25	0.587	501.0	509.9	518.9	527.8	536.8	545.7	554.7
	44	84.0	0.214	2.43	2.48	0.500	501.1	510.0	519.0	527.9	586.9	545.8	554.8
}	48	82.0	0.199	2.27	2.59	0.467	501.2	510.1	519.1	528.0	587.0	545.9	554.9
	42	80.0	0.186	2.10	2.76	0.482	501.8	510.2	519.2	528.1	587.1	546.0	555.0
li i	41	28.0	0.178	1.96	2.90	0.408	501.4	510.8	519-8	528.2	537.2	546.1	555.1
	40	26.0	0.161	1.82	8.04	0.875	501.5	510.4	519.4	528.8	587.8	546.2	555.2
55	55	55.0	0.442	5.02	0.00	1.000	498.8	507.7	516.6	525.5	584.4	548.8	552.2
	54	53.3	0.418	4.74	0.28	0.944	499.0	507.9	516.8	525.7	584.6	548.5	552.4
	58	51.6	0.894	4.46	0.56	0.888	499.1	508.0	516.9	525.8	584.7	543.6	552. 5
	52	49.9	0.872	4.28	0.79	0.843	499.8	508.2	517.1	526.0	584.9	548.8	552.7
	51	48.2	0.351	8.98	1.04	0.793	499.4	508.8	517.2	526.1	585.0	548.9	552. 8
	50	46.5	0.381	3.76	1.26	0.749	499.5	508.4	517.8	526.2	585.1	544.0	552.9
	49	44.8	0.812	3.55	1.47	0.707	499.7	508.6	517.5	526.8	585.8	544.2	553.1
	48	43.1	0.295	8.84	1.68	0.665	499. 8	508.7	517.6	526.5	585.4	544.8	558.3
1	47	41.4	0.278	8.14	1.88	0.626	499.8	508.7	517.6	526.6	585.5	541.4	558.4
	46	89.7	0.262	2.97	2.05	0.591	499.9	508.8	517.7	526.7	585.6	544.5	558.5
·,	45	38.0	0.246	2.79	2.28	0.556	500.0	l				544.6	558.6
	44	36.3	0.232	2.64	2.38	0.526	500.1	509.0	518.0	526.9	1	544.7	1
	48	34.6	0.219	2.47	2.55	0.492		509.1	1	527.0	l .	544.8	553.8
1	42	32.9	0.206	2.32	2.70	0.462		509.2			1	1	558.9
	41	31.2	0.194	2.20	2.82	0.438	500.4			l .	l	544.9	554.0 554.1
.	40	29.5	0.182	2.07	2.95	0.412	500.5 500.6	•			1	1	554.2
	39 3 8	27.8 26.1	0.172 0.161	1.95	3.07 3.19	0.388 0.365			518.6		•		l .
	-00	20.1	0.101	1.00	0.19	0.000	500.7	1 000.0	010.0	027.4	000.2	1 040.1	

of :	ding Ther- neter.	Temp.	Force of	of V	ight apor Reqd.	Hu- midity,		Weigh	t in Grai	as of a Ci	abic Foot	of Air.	
	hr.	Dew- Point.	Vapor in	In a Cubic	for Sat'n.	Satura-		Height o	of the Bar	rometer i	n Rnglish	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- ble Ft. of Air.	1.000.	28.0	m. 98.5	99.0	in. 29. 5	80.0	39.5	31.0
56	56	56.0	in. 0.458	gr. 5.18	gr. 0.00	1.000	497.7	gr. 506.6	gr. 515.5	524.4	533.2	gr. 542.1	gr. 551.0
30	55	54.8	0.482	4.89	0.29	0.944	497.9	506.8	515.7	524.6	583.4	542.3	551.2
	54	52.6	0.408	4.61	0.57	0.890	498.0	506.9	515.8	524.7	588.5	542.4	551.8
	58	50.9	0.885	4.87	0.81	0.844	498.2	507.1	516.0	524.9	588.7	542.6	551.5
	52	49.2	0.863	4.11	1.07	0.798	498.3	507.2	516.1	525.0	533.8	542.7	551.6
	51	47.5	0.848	8.87	1.81	0.747	498.4	507.8	516.2	525.1	533.9	542.8	551.7
	50	45.8	0.328	3.66	1.42	0.706	498.6	507.5	516.4	525.3	584.1	548.0	551.9
	49	44.1	0.305	3.45	1.73	0.666	498.6	507.5	516.4	525.3	584.2	548.1	552.0
	48	42.4	0.287	8.25	1.93	0.627	498.7	507.6	516.5	525.4	584.3	548.2	552.1
	47	40.7	0.271	8.07	2.11	0.593	498.8	507.7	516.6	525.5	584.4	548.8	552.2
	46 45	89.0	0.255	2.89	2.29	0.558	498.9	507.8	516.7	525.6	534.5	548.4	552.8
	40	87.8	0.240	2.78	2.45	0.527	499.0	507.9	516.8	525.7	584.6	543.5	552.4
	44	35.6	0.227	2.56	2.62	0.494	499.1	508.0	516.9	525.8	584.7	548.6	552.5
	48	38.9	0.213	2.41	2.77	0.465	499.2	508.1	617.0	525.9	534.8	543.7	552.6
	42	32.2	0.201	2.27	2.91	0.438	499.3	508.2	517.1	526.0	584.9	543.8	552.7
	41	80.5	0.189	2.14	8.04	0.418	499.4	508.8	517.2	526.1	535.0	548.9	552.8
	40	28.8	0.178	2.01	8.17	0.388	499.5	508.4	517.8	526.2	535.1	544.1	552.9
	39	27.1	0.167	1.89	8.29	0.865	499.5	508.4	517.8	526.2	585.1	544.1	552.9
	İ												
57	57	57.0	0.478	5.84	0.00	1.000	496.6	505.5	514.4	528.2	532.1	540.9	549.8
11	56 55	55.8	0.447	5.05 4.76	0.29	0.946	496.8	505.7	514.6	528.4 523.5	532.8 532.4	541.1 541.2	550.0 550.1
	54	58.6 51.9	0.422	4.50	0.58	0.848	496.9 497.1	505.8 506.0	514.7 514.9	523.7	582.6	541.4	550.3
	58	50.2	0.376	4.25	1.09	0.796	497.2	506.1	515.0	523.8	532.7	541.5	550.4
	52	48.5	0.855	4.00	1.84	0.749	497.3	506.2	515.1	528.9	582.8	541.6	55 0.5
H '	51	40.0	0.335	3.78	1.56	0.709	497.5	506.4	515.3	524.1	533.0	541.8	550.7
11	50	46.8 45.1	0.816	3.56	1.78	0.667	497.6	506.5	515.4	524.2	588.1	541.9	550.8
	49	48.4	0.298	8.86	1.98	0.629	497.7	506.6	515.5	524.3	533.2	542.0	550.9
	48	41.7	0.281	3.17	2.17	0.594	497.8	506.7	615.6	524.4	583.3	542.1	551.0
	47	40.0	0.264	2.99	2.35	0.560	497.9	506.8	515.7	524.5	533.4	542.2	551.2
	46	38.3	0.249	2.81	2.58	0.526	498.0	506.9	515.8	524.6	533.5	542.8	551.3
	45	86.6	0.285	2.65	2.69	0.496	498.1	507.0	515.9	524.7	533.6	542.4	551.4
	44	84.9	0.221	2.50	2.84	0.468	498.2	507.1	516.0	524.8	538.7	542.5	551.5
ll i	43	88.2	0.208	2.85	2.99	0.440	498.3	507.2	516.1	524.9	533.8	542.6	551.6
	42	81.5	1		I .	I.		1	1	524.9			1
	41	29.8			1		498.4		1	525.1	1		
	40	28.1	0.178	1.96	8.38	0.867	498.5	507.4	516.8	525.2	584.0	542.8	551.8
	-												

	ding	Temp	Force		ight apor	Hu-		Weigh	t in Grai	as of a Cu	ıbic Foot	of Air.	
	neter, shr.	of Dew- Point,	of Vapor in	In a Cubic	keqd. for Sat'n.	midity,		Height o	of the Ba	rometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.		1.000.	98.0	28.5	29.0	in. 29.5	in. 30.0	in. 30.5	31.0
58	o 58	58.0	ъ. 0.489	5.51	0.00	1.000	gr. 495.5	gr. 504.3	gr. 513.2	gr. 522.0	gr. 530.9	gr. 589.7	gr. 548.6
	57	56.3	0.462	5.21	0.30	0.946	495.7	504.5	513.4	522.2	531.1	539.9	548.8
	56	54.6	0.437	4.92	0.59	0.893	495.8	504.6	513.5	522.3	531.2	540.0	548.9
1 1	55	52.9	0.412	4.64	0.87	0.842	496.0	504.8	518.7	522.5	531.4	540.2	549.1
1 1	54	51.2	0.889	4.39	1.12	0.797	496.1	504.9	513.8	522.7	531.6	540.4	549.8
	58	49.5	0.367	4.14	1.87	0.751	496.2	505.0	518.9	522.8	531.7	540.5	549.4
	52	47.8	0.846	8.90	1.61	0.708	496.4	505.2	514.1	523.0	531.9	540.7	549.6
1	51	46.1	0.827	3.68	1.88	0.668	496.5	505.8	514.2	528.1	532.0	540.8	549.7
	50	44.4	0.308	8.48	2.03	0.682	496.6	505.4	514.8	523.2	532.1	540.9	549.8
	49	42.7	0.290	8.28	2.23	0.595	496.7	505.5	514.4	523.3	532.2	541.0	549.9
	48	41.0	0.274	3.08	2.43	0.559	496.8	505.6	514.5	523.4	532.3	541.1	550.0
	47	89.3	0.258	2.91	2.60	0.528	496.9	505.7	514.6	523.5	532.4	541.2	550.1
	46	37.6	0.243	2.74	2.77	0.497	497.0	505.8	514.7	523.6	582.5	541.8	550.2
	45	85.9	0.229	2.58	2.93	0.469	497.1	505.9	514.8	523.7	532.6	541.4	550.8
	44	84.2	0.216	2.43	8.08	0.441	497.2	506.0	514.9	523.8	532.7	541.5	550.4
	48	82.5	0.203	2.29	8.22	0.416	497.3	506.1	515.1	523.9	532.8	541.6	550.5
!	42	80.8	0.191	2.15	3.86	0.390	497.4	506.2	515.2	524.1	532.9	541.7	550.6
İ	41	29.1	0.180	2.03	8.48	0.868	497.5	506.8	515.8	524.2	533.0	541.8	550.7
	40	27.4	0.169	1.91	8.60	0.347	497.5	506.8	515.8	524.2	583.0	541.8	550.7
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50	59	59.0	0.506	5.69	0.00	1.000	494.5	503.3	512.2	521.0	529.8	538.6	547.5
1 1	58	57.3	0.478	5.87	0.32	0.944	494.6	503.4	512.3	521.1	529.9	538.7	547.6
i I	57	55.6	0.452	5.08	0.61	0.893	494.7	503.5	512.4	521.2	530.0	53 8.8	547.7
	56	53.9	0.426	4.79	0.90	0.842	494.8	503.6	512.5	521.3	530.1	538.9	547.8
	55	52.2	0.402	4.53	1.16	0.796	494.9	503.7	512.6	521.4	530.8	589.1	548.0
	54	50.5	0.880	4.28	1.41	0.752	495.1	508.9	512.8	521.6	580.5	539.8	548.2
	58	48.8	0.358	4.03	1.66	0.708	495.3	504.1	513.0	521.8	530.7	589.5	548.4
	52	47.1	0.338	8.80	1.89	0.668	495.4	504.2	513.1	521.9	530.8	539.6	548.5
	51	45.4	0.819	3.60	2.09	0.633	495.5	504.3	513.2	522.0	530.9	539.7	548.6
	50	48.7	0.301	3.39	2.80	0.596	495.7	504.5	518.4	522.2	531.1	589.9	548.8
	49	42.0	0.288	8.19	2.50	0.561	495.8	504.6	513.4	522.3	531.2	540.0	548.9
	48 47	40.3 38.6	0.267 0.252	8.01 2.84	2.68 2.85	0.529	495.9 496.0	504.7 504.8	513.5 518.6	522.4 522.5	531.8 531.4	540.1 540.2	549.0 549.1
	~.	60.0	0.202	2.04	a.00	U-100	730.U	5041.0	010.0	U.A.A.U	001.4	0-20.2	040.1
	46	86.9	0.237	2.67	3.02	0.469	496.1	504.9	513.7	522.6	531.5	540.3	549.2
	45	85.2	0.223	2.51	8.18	0.441	496.2	505.0	518.8	522.7	531.6		549.3
	44	33.5	0.210	2.87	3.32	0.417	496.3		513.9	522.8	531.7	3	549.4
li I	43	31.8	0.198	2.28	8.46	0.392	496.1		514.1		531.8	1	549.5
	42	30.1	0.186	2.09	8.60	0.867	496.5	505.8	514.2	523.0	581.9	540.7	549.6
1	41	28.4 26.7	0.175	1.97	3.72 3.84	0.346	496.6 496.6	505.4 505.4	514.3 514.3	523.1 523.1	532.0 532.0	540.8 540.8	549.7 549.7
	-10	20.1	0.100	1.00	0.04	0.020	100.0	000.4	014.5	023.1	Doz.U	04010	U25.1
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	ding	Temp.	Force	We of V	ight apor	Hu-		Weigh	t in Grai	as of a C	abic Foot	of Air.	
Znorz	eter, hr.	of Dew- Point.	of Vapor in	In a Cubic	for Sat'n.	midity, Setura- tion =		Height	of the Ba	rometer	n Rogiis	h Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.		1.000.	2.8.0	28.5	29.0	29.5	3 6. 6	30.5	31.0
60	0	60.0	in. 0.523	gr. 5.87	gr. 0.00	1.000	gr. 493.4	gr. 502.2	gr. 511.0	519.8	528.6	gr. 587.4	gr. 546.2
80	60 59	58.3	0.494	5.54	0.83	0.944	493.4	502.4	511.2	520.0	528.8	587.6	546-4
	58	56.6	0.467	5.24	0.68	0.898	498.7	502.5	511.8	520.1	528.9	587.7	546.5
	57	54.9	0.441	4.95	0.92	0.843	498.8	502.6	511.4	520.2	529.0	587.8	546.6
	56	53.2	0.416	4.68	1.19	0.797	494.0	502.8	511.6	520.4	529.2	588.0	546.8
	55	51.5	0.398	4.41	1.46	0.751	494.2	508.0	511.8	520.6	529.4	588.2	547.0
	54	49.8	0.371	4.17	1.70	0.710	494.4	508.2	512.0	520.8	529.6	588.4	547.2
	58	48.1	0.850	3.92	1.95	0.668	494.5	508.8	512.1	520.9	529.7	588.5	547.4
	52	46.4	0.830	8.70	2.17	0.680	494.7	508.4	512.8	521.1	529.9	588.7	547.6
	51	44.7	0.811	8.49	2.88	0.595	494.8	508.5	512.4	521.2	580.0	538.8	547.7
	50	48.0	0.298	3.29	2.58	0.561	494.8	503.6	512.5	521.8	580.1	588.9	547.8
	49	41.8	0.277	3.10	2.77	0.528	494.9	508.7	512.6	521.4	530.2	589.0	547.9
	48	89.6	0.261	2.98	2.94	0.499	495.0	508.8	512.7	521.5	580.3	589.1	548.0
	47	37.9	0.246	2.75	3.12	0.468	495.1	508.9	512.8	521.6	580.4	589.2	548.1
	46	86.2	0.281	2.60	8.27	0.448	495.2	504.0	512.9	521.7	580.5	539.8	548.2
	45	84.5	0.218	2.45	8.42	0.417	495.3	504.1	518.0	521.8	580.6	539.4	548.8
	44	32.8	0.205	2.81	3.56	0.894	495.4	504.2	513.1	521.9	580.7	589.5	548.4
	48	81.1	0.198	2.17	8.70	0.870	495.5	504.8	518.2	522.0	580.8	539.6	548.5
	42	29.4	0.182	2.04	3.83	0.848	495.6	504.4	513.8	522.1	530.9	589.7	548.6
	41	27.7	0.171	1.92	3.98	0.827	495.6	504.4	513.8	522.1	580.9	589.7	548.7
				l				İ	ì				
61	61	61.0	0.541	6.06	0.00	1.000	492.3	501.1	509.9	518.7	527.5	586.8	545.1
	60	59.8	0.511	5.72	0.84	0.944	492.5	501.8	510.1	518.9	527.7	586.5	545.8
	59	57.6	0.488	5.40	0.66	0.891	492.6	501.4	510.2	519.0	527.8	586.6	545.4
	58	55.9	0.456	5.11	0.95	0.843	492.8	501.6	510.4	519.2	528.0	536.8	545.6
	57	54.2	0.481	4.83	1.23	0.797	493.0	501.8	510.6	519.4	528.2	587.0	545.8
	56	52.5	0.407	4.55	1.51	0.751	498.1	501.9	510.7	519.5	528.3	587.1	545.9
	55	50.8	0.383	4.80	1.76	0.710	493.3	502.1	510.9	519.7	528.5	587.8	546.1
	54	49.1	0.362	4.05	2.01	0.668	498.4	502.2	511.0	519.8	528.6	587.4	546.2
	58	47.4	0.842	8.88	2.23	0.632	498.5	502.8	511.1	519.9	528.7	587.5	546.8
	52	45.7	0.322	8.61	2.45	0.596	493.6	502.4	511.2	520.0	528.8	587.6	546.4
	51	44.0	0.304	8.40	2.66	0.561	493.8	502.6	511.4	520.2	529.0	587.8	546.6
	50	42.3	0.286	3.21	2.85	0.580	498.9	502.7	511.5	520.3	529.1	587.9	546.7
	49	40.6	0.270	8.02	8.04	0.498	494.0	1	1	I	529.2	538.0	546.8
	48	88.9	0.254			0.470			511.7	•	529.8	1	1 1
	47	87.2	0.240	2.69	8.37	0.444	494.2	508.0	511.8	520.6	529.4	588.2	547.0
	46	85.5	0.226	2.53	8.58	0.417	494.3	503.1	511.9	520.7	529.5	538.3	547.1
	45	33.8	0.213		8.68	0.393	494.4	508.2	512.0	520.8	529.6	538.4	4 1
	44	32.1	0.200	2.24	3.82	0.870		-503.3			529.7		
	43	30.4	0.188	2.11	8.95	0.848	1		512.2				
	42	28.7	0.177	1.99	I I	0.328	494.7		512.8				547.5
	41	27.0	0.167	1.87	4.19	0.809	494.7	503.5	512.3	521.1	529.9	558.7	547.5

of 1	ding ber-	Temp.	Force of		ight spor.	Hu- midity,		Weigh	in Grain	u of a O	abic Foot	of Air.	
	br.	Dew- Point,	Vapor	In a Cubic	for Set'n.	Satura- tion =		Height	of the Ba	rometer i	in Englis	h Inches	•
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- ble Ft. of Air.	1.000.	98.0	28.5	29.0	29.5	30.0	3 0 .5	31.0
62	62	62.0	in. 0.559	gr. 6.25	gr. 0.00	1.000	gr. 491.2	gr. 499.9	gr. 508.7	gr. 517.5	gr. 526.3	gr. 535.1	gr. 543.9
"	61	60.8	0.528	5.91	0.84	0.946	491.4	500.1	508.9	517.7	526.5	535.8	544.1
	60	58.6	0.499	5.58	0.67	0.898	491.5	500.2	509.0	517.8	526.6	585.4	544.2
1	59	56.9	0.472	5.27	0.98	0.848	491.7	500.4	509.2	518.0	526.8	585.6	544.4
	58	55.2	0.445	4.99	1.26	0.798	491.9	500.6	509.4	518.2	527.0	585.8	544.6
1 1	57	58.5	0.421	4.70	1.55	0.752	492.0	500.7	509.5	518.3	527.1	535.9	544.7
	56	51.8	0.897	4.44	1.81	0.710	492.1	500.7	509.5	518.4	527.8	586.1	544.9
	55	50.1	0.375	4.19	2.06	0.670	492.2	500.9	509.7	518.5	527.4	586.2	545.0
	54	48-4	0.854	8.95	2.30	0.632	492.4	501.1	509.9	518.7	527.6	586.4	545.2
	53	46.7	0.333	8.72	2.53	0.595	492.5	501.8	510.1	518.9	527.7	586.5	545.8
	52	45.0	0.315	8.52	2.78	0.563	492.7	501.5	510.8	519.1	527.9	586.7	545.5
	51	48.8	0.297	8.31	2.94	0.530	492.8	501.6	510.4	519.2	528.0	536.8	545.6
	50	41.6	0.280	8.18	3.12	0.501	492.9	501.7	510.5	519.8	528.1	586.9	545.7
1 1	49	39.9	0.268	2.95	3.80	0.472	498.0	501.8	510.6	519.4	528.2	537.0	545.8
	48	38.2	0.248	2.77	8.48	0.448	498.1	501.9	510.7	519.5	528.8	587.1	545.9
1	47	36.5	0.234	2.61	3.64	0.418	498.2	502.0	510.8	519.6	528.4	587.2	546.0
	46	84.8	0.220	2.47	8.78	0.895	493.3	502.1	510.9	519.7	528.5	537.8	546.1
	45	33.1	0.207	2.32	3.98	0.871	498.3	502.1	511.0	519.7	528.6	537.8	546.1
1 1	44	81.4	0.195	2.18	4.07	0.849	493.4	502.2	511.0	519.8	528.6	537.4	546.2
	43 42	29.7 28.0	0.184	2.06	4.19	0.830	493.4 493.5	502.2 502.8	511.1	519.8	528.6	537.4	546.2 546.8
	41	26.8	0.173	1.94	4.31	0.298	498.6	502.4	511.2 511.3	519.9 520.0	528.7 528.8	537.5 537.6	546.4
			0.100	1.50		0.200	200.0	002.4	011.0	020.0	020.0	501.0	040.4
								i					
63	63	63.0	0.578	6.45	0.00	1.000	490.2	498.9	507.7	516.4	525.2	583.9	542.7
	62	61.3	0.546	6.10	0.35	0.946	490.4	499.1	507.9	516.6	525.4	584.1	542.9
	.61	59.6	0.516	5.76	0.69	0.893	490.5	499.2	508.0	516.7	525.5	584.2	543.0
	60	57.9	0.488	5.44	1.01	0.848	490.7	499.4	508.2	516.9	525.7	584.4	548.2
	59	56.2	0.461	5.15	1.80	0.798,	490.9	499.6	508.4	517.1	525.9	584.6	548.4
	58	54.5	0.485	4.86	1.59	0.758	491.0	499.7	508.5	517.2	526.0	584.7	548.5
	57	52.8	0.411	4.59	1.86	0.712	491.1	499.8	508.6	517.8	526.2	584.9	548.7
	56 55	51.1 49.4	0.888	4.83	2.12	0.671 0.634	491.2 491.8	499.9	508.7 508.8	517.4	526.3	585.0 585.1	543.8 543.9
	54	47.7	0.866	4.09 8.85	2.36 2.60	0.597	491.5	500.0 500.2	509.0	517.5 517:7	526.4 526.6	535.8	544.1
					1					1		l	
	53 52	46.0	0.826	3.63	2.82	0.568	491.7	500.4	509.2	518.0	526.8	535.5	544.8
	51	44.8	0.307 0.289	3.43 3.24	8.02 8.21	0.582	491.8 491.9	500.5	509.8 509.4	518.1 518.2	526.9 527.0	585.6 585.7	544.4
	50	40.9	0.273	3.05	8.40	0.478	491.9	500.7	509.5	518.8	527.0		
	49	89.2	0.257	2.07	1	0.445	492.1	500.8	509.6	518.4	1	585.9	544.7
	48	87.5	0.242	2.71	3.74	0.420	492.2	500.9	509.7	518.5		586.0	544.8
	47	35.8	0.228	2.56	8.89	0.897	492.8	501.0	509.8	518.6	1	536.1	544.9
	46	34.1	0.215	2.41	4.04	0.874	492.4)	518.7	1		545.0
	45	32.4	0.202	2.26	4.19	0.851	492.5	501.2	l.	518.8	1		545.1
	44	80.7	0.190	2.18	4.82	0.380	492.5	501.2		518.8	l	536.3	545.1
	43	29.0	0.179	2.00	4.45	0.810	492.6	501.8					545.2
<u> </u>	42	27.8	0.168	1.87	4.58	0.290	492.7	501.4	510.2	519.0	527.8	586.5	545.8

Rec	ading Ther-	Temp.	Force		ight upor.	Hu-		Weigh	t in Grai	ns of a Cr	ibie Foot	of Air.	
100	neter, ahr.	Dew- Point,	Vapor in	In a	Reqd. for Sat'n.	midity, Satura-		Height o	of the Ba	rometer i	n Kuglish	Inches.	
		Fahr.	English Inches		of aCu-	tion = 1.000.	in.	in.	in.	fn.	ln.	In.	in.
Dry.	Wet.				of Air.		28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	64	0	in.	gr.	gr.	* 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
64	63	64.0 62.8	0.597 0.565	6.65	0.00	1.000 0.946	489.1 489.3	497.8 498.0	506.6 506.8	515.8 515.5	524.0 524.2	532.7 532.9	541.5 541.7
	62	60.6	0.534	5.94	0.71	0.898	489.5	498.2	507.0	515.7	524.4	583.1	541.9
	61	58.9	0.504	5.61	1.04	0.843	489.7	498.4	507.2	515.9	524.6	533.3	542.1
	60	57.2	0.476	5.31	1.84	0.798	489.9	498.6	507.4	516.1	524.8	533.5	542.3
	59	55.5	0.450	5.01	1.64	0.758	490.0	498.7	507.5	516.2	524.9	533.6	542.4
	58	53.8	0.425	4.78	1.92	0.711	490.1	498.8	507.6	516.3	525.1	533.8	542.6
	57	52.1	0.401	4.47	2.18	0.672	490.2	499.9	507.7	516.4	525.2	533.9	542.7
	56	50.4	0.379	4.23	2.42	0.636	490.4	499.1	507.9	516.6	525.4	534.1	542.9
	55	48.7	0.357	8.98	2.67	0.598	490.5	499.2	508.0	516.7	525.5	534.2	543.0
	54	47.0	0.837	3.75	2.90	0.564	490.7	499.4	508.2	516,9	525.7	584.4	548.2
	53	45.3	0.318	3.55	3.10	0.584	490.8	499.5	508.3	517.0	525.8	584.5	543.3
	52	43.6	0.300	3.84	3.81	0.502	490.9	499.6	508.4	517.1	525.9	534.6	548.4
	51	41.9	0.282	8.15	8.50	0.473	491.0	499.7	508.5	517.2	526.0	584.7	543.5
	50	40.2	0.266	2.96	3.69	0.445	491.2	499.9	508.7	517.4	526.1	534.9	543.7
	49	38.5	0.251	2.79	8.86	0.419	491.3	500.0	508.8	517.5	526.2	535.0	543.8
	48 47	86.8	0.286	2.63	4.02	0.396	491.4	500.1	508.9	517.6	526.3	535.1	543.9
	46	35.1 33.4	0.228	2.47	4.18	0.372	491.5	500.2	509.0	517.7	526.4	535.2	544.0
	45	31.7	0.210	2.19	4.46	0.851	491.6 491.7	500.8 500.4	509.1	517.8 517.9	526.5 526.6	535.3 535.4	544.1
1	44	80.0	0.186	2.06	4.59	0.310	491.7	500.4	509.2 509.2	517.9	526.6	535.4	544.2 544.2
	43	28.3	0.175	1.94	4.71	0.292	491.8	500.5	509.3	518.0	526.7	585.5	544.3
	42	26.6	0.164	1.83	4.82	0.275	491.9	500.6	509.4	518.1	526.8	535.6	544.4
									505.4			555.15	
65	65	65.0	0.617	6.87	0.00	1.000	488.1	496.8	505.5	514.2	522.9	531.6	540.3
00	64	63.4	0.586	6.51	0.36	0.947	488.8	497.0	505.7	514.4	523.1	531.8	540.5
	68	61.8	0.555	6.17	0.70	0.898	488.5	497.2	505.9	514.6	523.8	582.0	540.7
١,	62	60.2	0.527	5.85	1.02	0.851	488.7	497.4	506.1	514.8	523.5	582.2	540.9
	61	58.6	0.499	5.55	1.32	0.808	488.9	497.6	506.8	515.0	523.7	532.4	541.1
	60	57.0	0.473	5.25	1.62	0.765	489.0	497.7	506.5	515.2	523.9	532.6	541.3
	59	55.4	0.449	4.98	1.89	0.725	489.1	497.8	506.6	515.8	524.0	532.7	541.5
	58	53.8	0.425	4.72	2.15	0.687	489.8	498.0	506.8	515.5	524.2	582.9	541.7
	57	52.2	0.402	4.47	2.40	0.651	489.4	498.1	506.9	515.6	524.8	583.0	541.8
	56	50.6	0.381	4.23	2.64	0.616	489.6	498.3	507.1	515.8	524.5	583.2	542.0
	55	49.0	0.361	4.01	2.86	0.584	489.7	498.4	507.2	515.9	524.6	533.3	542.1
	54	47.4	0.342	8.79	3.08	0.552	489.8	498.5	507.3	516.0	524.7	538.4	542.2
	58	45.8	0.823	3.60	3.27	0.524	489.9	498.6	507.4	516.1	524.8	533.5	542.8
	52	44.2	0.806	3.39	8.48	0.498	490.0	198.7	507.5	516.2	524.9	538.6	542.4
	51	42.6	0.289	3.22	8.65	0.469	490.1	498.8	507.6	516.8	525.0	533.7	542.5
	50 49	41.0	0.274	8.04	I .	0.442			507.7		1	l	1
	49 48	39.4 37.8	0.259	2.87	4.00	0.418 0.396	490.3 490.8	499.0 499.0	507.8	516.5 516.5	1	588.9	1
	47	36.2	0.245	2.72	4.30	0.874	490.4	l	507.8	516.6	1	1	1
	46	34.6	0.219	2.43	4.44	0.354	490.4	499.1		516.7			ŀ
	45	33.0	0.207	2.31	4.56	0.336	490.6	ı	508.1	516.8		584.2	1
	44	31.4	0.195	2.17	4.70	0.316	490.7	ı	508.2	1	l .	1	l .
	48	29.8	0.184	2.03	L	0.299	490.7		508.2	516.9	1	1	ı
			0.174				490.8	1	ı	517.0	ı	1	548.2

of ?	ding	Temp.	Force of	We of V	ight apor Regd.	Hu-		Weigh	t in Grab	ns of a C	abic Foot	of Air.	
	neter, sbr.	of Dew- Point.	Vapor	In a Cubic	for Sat'n.	midity, Satura- tion =		Height	of the Ba	rometer	n Englis	h Inches	•
Dry.	Wet.	Fahr.	English Inches.	Foot of		1.000.	98.0	28.5	29.0	99.5	30.0	30.5	ь. 31.0
66	66	66.0	in. 0.688	gr. 7.08	gr. 0.00	1.000	gr. 487.0	gr. 495.7	gt. 504.4	gr. 518.1	gr. 521.8	gr. 530.5	gr. 589.2
55	65	64.4	0.605	6.72	0.36	0.949	487.2	495.9	504.6	518.8	522.0	580.7	589.4
	64	62.8	0.574	6.35	0.73	0.897	487.8	496.0	504.7	518.4	522.1	580.8	589.5
	68	61.2	0.544	6.04	1.04	0.858	487.5	496.2	504.9	513.6	522.8	531.0	589.7
	62	59.6	0.516	5.72	1.36	0.808	487.7	496.4	505.1	513.8	522.5	581.2	589.9
	61	58.0	0.489	5.42	1.66	0.766	487.9	496.6	505.8	514.0	522.7	581.4	540.1
	60	56.4	0.464	5.14	1.94	0.726	488.0	496.7	505.4	514.1	522.8	581.5	540.2
	59	54.8	0.440	4.88	2.20	0.689	488.1	496.8	505.5	514.2	528.0	581.7	540.4
	58	53.2	0.416	4.62	2.46	0.652	488.2	496.9	505.6	514.8	528.1	581.8	540.5
	57	51.6	0.894	4.87	2.71	0.619	488.4	497.1	505.8	514.5	528.8	582.0	540.7
	56	50.0	0.373	4.15	2.93	0.586	488.5	497.2	505.9	514.6	523.4	582.1	540.8
	55	48.4	0.354	8.92	3.16	0.558	488.6	497.8	506.1	514.8	528.5	582.2	541.0
	54	46.8	0.835	8.72	3.36	0.525	488.8	497.5	506.3	515.0	528.7	582.4	541.2
	58	45.2	0.817	8.51	8.57	0.496	488.9	497.6	506.4	515.1	523.8	582.5	541.8
i	52	43.6	0.300	3.38	3.75	0.470	489.0	497.7	506.5	515.2	528.9	532.6	541.4
1	51	42.0	0.283	8.14	8.94	0.443	489.1	497.8	506.6	515.8	524.0	582.7	541.5
1	50	40.4	0.268	2.97	4.11	0.419	489.2	497.9	506.7	515.4	524.1	532.8	541.6
	49	88.8	0.253	2.81	4.27	0.897	489.8	498.0	506.8	515.5	524.2	582.9	541.7
	48	87.2	0.240	2.66	4.42	0.376	489.4	498.1	506.9	515.6	524.3	533.0	541.8
	47	33.6	0.227	2.51	4.57	0.855	489.4	498.1	506.9	515.6	524.8	533.0	541.8
	46	34.0	0.214	2.37	4.71	0.883	489.5	498.2	507.0	515.7	524.4	533.1	541.9
	45	32.4	0.202	2.24	4.84	0.316	489.6	498.8	507.1	515.8	524.5	538.2	542.0
	44	30.8	0.191	2.12	4.96	0.299	489.7	498.4	507.2	515.9	524.6	588.3	542.1
	43	29.2	0.180	2.00	5.08	0.283	489.7	498.4	507.2	515.9	524.6	533.8	542.1
-		1 1		}									
67	67	67.0	0.659	7.80	0.00	1.000	483.9	494.6	503.3	E10.0	520.6	529.8	538.0
0,	66	65.4	0.626	6.98	0.37	0.949	486.1	494.8	503.5	512.0 512.2	520.8	529.5	538.2
	65	63.8	0.598	6.55	0.75	0.897	496.8	495.0	503.7	512.4	521.0	529.7	538.4
	64	62.2	0.563	6.28	1.07	0.858	486.5	495.2	508.9	512.6	521.2	529.9	538.6
	63	60.6	0.534	5.91	1.39	0.810	486.7	495.4	504.1	512.8	521.4	530.1	538.8
	62	59.0	0.506	5.60	1.70	0.767	486.8	495.5	504.2	512.9	521.6	530.8	539.0
	61	57.4	0.480	5.81	1.99	0.728	486.9	495.6	504.8	513.0	521.7	580.4	589.1
	60	55.8	0.455	5.04	2.26	0.691	487.1	495.8	504.5	513.2	521.9	530.6	589.8
	59	54.2	0.431	4.77	2.58	0.658	487.2	495.9	504.6	513.3	522.0	530.7	589.4
	58	52.6	0.408	4.52	2.78	0.619	487.3	496.0	504.7	518.4	522.1	530.8	589.5
	57	51.0	0.386	4.28	3.02	0.586	487.5	496.2	504.9	513.6	522.8	531.0	589.7
	56	49.4	0.366	4.05	3.25	0.555	487.6	496.8	505.0	518.7	522.4	531.1	589.8
	55	47.8	0.846	3.83	8.47	0.524	487.8		505.1	513.8	522.6		549.9
	54	46.2	0.328	3.62	3.68	0.496	487.9	496.6	1			l	540.0
	58	44.6	0.810	3.48	3.87	0.470	488.0	496.7		514.0	[ı	1
	52	43.0	0.293	3.25	4.03	0.445	488.1	496.9	504.4	514.1	522.9	531.5	540.2
	51	41.4	0.278	8.08	4.22	0.422	488.2	496.9	505.5	514.2	528.0	581.6	540.8
	50	39.5	0.263	2.91	4.39	0.899	488.4	1	1		523.1	F	1
	49	38.2	0.248	2.75	4.55	0.877			505.8				

В

of	iding Ther-	Temp.	Force	We of V	ight apor	Hu-		Weigh	t in Grai	ns of a Ci	abie Foot	of Air.	
2000 3	noter, abr.	of Dew-	Vapor in	In a Cubic	Reqd. for Set'n.	midity, Seture-		Height o	of the Ba	rometer i	n English	Inches.	
Dry.	Wet.	Point, Fahr.	English Inches.		of aCu- bio Ft. of Air.	tion = 1.000.	1n. 98.0	^{in.} 28.5	29.0	29.5	30.0	in. 30.5	31.0
D	0	0	in.	gr.	gr.		gr.	g.	gr.	gr.	gr.	gr.	gr.
67	49 48	88.2 86.6	0.248	2.75	4.55	0.877 0.856	488.5 488.6	497.2	505.8	514.5	528.2	581.9	540.6
	47	35.0	0.222	2.46	4.84	0.837	488.7	497.4	505.9 505.9	514.6	528.8 528.4	532.0	540.7
	46	83.4	0.210	2.32	4.98	0.818	488.7	497.4	506.0	514.7 514.7	528.4	532.1 532.1	540.8 540.8
	45	81.8	0.198	2.19	5.11	0.801	488.8	497.5	506.1	514.8	523.5	582.2	540.9
	44	80.2	0.187	2.07	5.28	0.284	488.9	497.6	506.2	514.9	528.6	582.3	541.0
										523.5		552.5	
68	68	68.0	0.681	7.58	0.00	1.000	484.9	493.5	502.2	510.8	519.5	528.1	536. 8
	67	66.4	0.646	7.15	0.38	0.949	485.1	493.8	502.5	511.1	519.7	528.4	587.1
	66	64.8	0.618	6.77	0.76	0.899	485.3	494.0	502.6	511.2	519.9	528.6	587.3
1 1	65	63.2	0.582	6.48	1.10	0.854	485.5	494.2	502 .8	511.4	520.1	528.8	587.5
	64	61.6	0.552	6.10	1.43	0.810	485.7	494.4	508.0	511.6	520.8	529.0	587.7
	63	60.0	0.523	5.78	1.75	0.768	485.8	494.5	503.1	511.8	520.5	529.2	587.9
	62	58.4	0.496	5.47	2.06	0.726	485.9	494.6	508.8	512.0	520.7	529.4	588.1
	61	56.8	0.470	5.20	2.83	0.691	486.0	494.7	503.4	512.1	520.8	529.5	588.8
	60	55.2	0.445	4.98	2.60	0.655	486.2	494.9	508.6	512.8	521.0	529.7	5 3 8.5
	59	58.6	0.422	4.67	2.86	0.620	486.8	495.0	503.7	512.4	521.1	529.9	588.6
	58 57	52.0	0.400	4.42	8.11	0.587	486.4	495.1	508.8	512.6	521.2	529.9	588.6
1	07	50.4	0.879	4.19	8.84	0.556	486.6	495.3	504.0	512.7	521.4	580.1	588.8
	56	48.8	0.358	3.96	8.57	0.526	486.7	495.4	504.1	512.8	521.5	580.2	588.9
	55	47.2	0.839	8.75	3.78	0.498	486.8	495.5	504.2	512.9	521.6	530.8	589.0
	54	45.6	0.321	3.54	3.99	0.470	486.9	495.6	504.3	513.0	521.7	530.4	589.1
	58	44.0	0.804	8.35	4.18	0.445	487\0	495.7	504.4	513.1	521.8	580.5	589.2
	52 51	42.4	0.287	8.17	4.36	0.421	487.1	495.8	504.5	513.2	521.9	580.6	589.3
			0.272	3.00	4.53	0.399	487.2	495.9	504.6	513.8	522.0	530.7	589.4
	50	89.2	0.257	2.84	4.69	0.377	487.3	496.0	504.7	513.4	522.1	530.8	539. 5
	49 48	87.6 36.0	0.248	2.68	4.85	0.856	487.4	496.1	504.8	513.5	522.2	530.9	539.6
	47	84.4	0.230	2.54 2.40	4.99 5.13	0.837 0.319	487.5 487.6	496.2	504.9	518.6	522.8	581.0	539.7
1 1	46	32.8	0.205	2.27	5.26	0.802	487.6	496.3	505.0 505.0	513.7 513.7	522.4 522.4	581.1 581.1	539. 8 539. 8
	45	31.2	0.194	2.15	5.38	0.286	487.7	496.4	505.0	513.8	522.5	531.2	589.9
	44	29.6	0.183	2.04	5.49	0.271	487.8	496.5	505.2	518.9	522.6	581.8	540.0
							10010	1.00.0		020.0	522.0	552.5	0.000
69	69	69.0	0.704	7.76	0.00	1.000	483.8	492.4	501.1	509.7	518.8	527.0	535.6
1 1	68	67.4	0.668	7.37	0.89	0.950	484.0	492.6	501.3	509.9	518.5	527.2	585.8
[]	67	65.8	0.634	7.00	0.76	0.902	484.2	492.8	501.5	510.1	518.7	527.4	586.0
	66	64.2	0.601	6.63	1.18	0.854	494.4	493.0	501.7	510.8	518.9	527.6	586.2
	65	62.6	0.570	6.29	1.47	0.810	484.6		501.9	510.5	519.1	527.8	536.4
	64	61.0	0.541	5.97	1.79	0.769	484.8	498.4	502.1	510.7	519.8	528.0	586.6
	63	59.4	0.518	5.65	2.11	0.728	485.0	498.6	502.8	510.9	519.5	528.2	586. 8
	62	57.8	0.486	5.87	2.89	0.693	485.1		502.4		519.6		586.9
	61	56.2	0.461	5.09	2.67	0.657	485.1	498.7	502.6	511.2	519.8	528.5	537.1
	60	54.6	0.487	4.82	2.94	0.621	485.2	498 .9	502.7	511.8	519.9	528.6	587.3
	59	58.0	0.414	4.57	8.19	0.589	485.4	494.1	502.8	511.5	520.1	528.8	587.5
	58	51.4	0.392	4.33	8.48	0.558	485.5	494.2	502.9	511.6	520.2	528.9	587.6

B.	eding	Tomp.	Force		ight apor	Hu-		Weigh	t in Grat	as of a Cu	ibie Foot	of Air.	
100	noter, abr.	of Dew- Point,	Vapor in	In a Cubic		midity, Setura- tion —		Height o	of the Ba	rometer l	a English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of	ofaCu- ble Ft. of Air.	1.000.	98. 0	in. 28.5	29.0	29.5	ь. 30. 0	in. 30. 5	in. 81.0
69	o 58	o 51.4	in. 0.392	gr. 4.88	gr. 3.43	0.558	gr. 485.5	gr. 494.2	gr. 502.9	gr. 511.6	520.2	gr. 528.9	gr. 537.6
-	57	49.8	0.871	4.09	8.67	0.527	485.7	494.4	503.1	511.8	520.4	529.1	587.8
	56	48.2	0.351	8.87	3.89	0.499	485.8	494.5	508.2	511.9	520.5	529.2	587.9
	55	46.6	0.882	3.66	4.10	0.472	485.9	494.6	508.3	512.0	520.6	529.3	588.0
	54	45.0	0.815	3.47	4.29	0.447	486.0	494.7	508.4	512.1	520.7	529.4	538.1
	53	48.4	0.298	3.29	4.47	0.424	486.1	494.8	508.5	512.2	520.8	529.5	538.2
	52	41.8	0.282	8.11	4.65	0.401	486.2	494.9	508.6	512.3	520.9	529.6	588.3
	51	40.2	0.266	2.94	4.82	0.879	496.3	495.0	508.7	512.4	521.0	529.7	588.4
	50 49	38.6 37.0	0.252	2.78	4.98 5.18	0.858 0.839	486.4	495.1 495.2	508.8 508.9	512.5 512.6	521.1	529.8 529.9	538.5 538.6
	48	85.4	0.225	2.49	5.27	0.821	486.6	495.2	504.0	512.7	521.2 521.8	530.0	588.7
	47	38.8	0.218	2.84	5.42	0.802	486.7	495.4	504.1	512.8	521.4	530.1	588.8
	46	32.2	0.201	2.20	5.56	0.284	486.8	495.5	504.2	512.9	521.5	580.2	588.9
	45	80.6	0.190	2.06	5.70	0.266	486.8	495.5	504.2	512.9	521.5	580.2	588.9
70	70	70.0	0.727	8.00	0.00	1.000	482.8	491.4	500.0	508.6	517.2	525.8	584.4
'	69	68.5	0.692	7.62	0.88	0.958	488.0	491.6	500.2	508.8	517.4	526.0	534.6
	68	67.0	0.659	7.26	0.74	0.907	488.2	491.8	500.4	509.0	517.6	526.2	584.8
	67	65.5	0.628	6.91	1.09	0.865	483.3	491.9	500.5	509.1	517.7	526.8	584.9
	66	64.0	0.597	6.57	1.48	0.822	488.5	492.1	500.7	509.8	517.9	526.5	585.1
	65	62.5	0.568	6.25	1.75	0.781	488.7	492.8	500.9	509.5	518.1	526.7	585.3
	64	61.0	0.541	5.95	2.05	0.744	483.8	492.4	501.0	509.6	518.3	526.9	585.5
	63	59.5	0.515	5.66	2.84	0.708	484.0	492.6	501.2	509.8	518.5	527.1	585.7
	62	58.0	0.489	5.38	2.62	0.672	484.2	492.8	501.4	510.0	518.7	527.3	535.9
	61	56.5	0.465	5.12	2.88	0.640	484.8	492.9	501.5	510.1	518.8	527.4	536.0
	60	55.0	0.442	4.87	8.18	0.609	484.4	498.0	501.6	510.2	518.9	527.5	536.1
	59	53.5	0.421	4.62	8.88	0.578	484.6	498.2	501.8	510.4	519.1	527.7	536.3
	58	52.0	0.400	4.40	3.60	0.550	484.7	498.8	501.9	510.5	519.2	527.8	536.4
	57	50.5	0.380	4.18	3.82	0.522	484.8	498.4	502.0	510.6	519.8	527.9	586.5
	56	49.0	0.361	3.96	4.04	0.495	484.9	498.5	502.1	510.7	519.4	528.0	586.6
	55	47.5	0.848	3.76	4.24	0.470	485.1	498.7	502.8	510.9	519.6	528.2	586.8
	54	46.0	0.826	3.57	4.48	0.446	485.2	498.8	502.4	511.0	519.7	528.8	536.9
	58	44.5	0.809	3.40	4.60	0.425	485.3	498.9	502.5	511.1	519.8	528.4	587.0
	52	48.0	0.292	8.28	4.77	0.404	485.4	494.0	502.6	511.2	519.9	528. 5	587.1
	61	41.5	0.279	8.07	4.93	0.884	485.5	494.1	502.7			528.6	587.2
	50	40.0	0.264	2.81	5.19	0.851	486.5	494.1	502.7	511.8	520.0	528. 6	587.2
	49	88.5	0.251	2.76		0.845	485.6				520.1	528.7	587.8
	48	87.0	0.238	2.68	l .	0.829	485.7		1		520.2		587.4
	47	35.5		2.50	l	0.313	485.8				520.8		587.5
	46	84.0	0.214	2.37	(0.296	485.8	ľ		511.6			587.5
	45 44	32.5 31.0	0.208	1		0.280 0.265	485.9 486.0		1		520.4 520.5		587.6 587.7
I		29.5				0.251	I .					529.1 529.2	
	1 43	25.0	V-102	2.01	0.00	0.201	450.1	484.7	008.8	011.9	02U.6	025.Z	001.0

Res	ding	Temp.	Force	We of V	ight apor	Hu-		Weigh	t in Grain	s of a Ct	ibic Foot	of Air.	
mon	ne ter, .hr.	of Dew- Point,	Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion ==	·	Height	of the Be	rometer i	n Hoglis	h Inches	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.		1.000.	28.0	28.5	^{in.} 29.0	29.5	in. 30.0	30.5	31.0
0 71	0	71.0	in.	gr. 8.25	gr. 0.00	1.000	gr.	490.2	gr.	gr. 507.4	gt.	gr ED L C	gr.
"	71 70	69.5	0.751 0.715	7.86	0.89	0.958	481.6 481.8	490.4	498.8 499.0	507.6	516.0 516.2	524.6 524.8	533-2 533-4
	69	68.0	0.681	7.48	0.77	0.907	482.0	490.6	499.2	507.8	516.4	525.0	533.6
Ì	68	66.5	0.648	7.13	1.12	0.865	482.2	490.8	499.4	508.0	516.6	525.2	588.8
	67	65.0	0.617	6.79	1.46	0.828	482.4	491.0	499.6	508:2	516.8	525.4	534.0
ł	66	63.5	0.588	6.45	1.80	0.782	482.6	491.2	499.8	508.4	517.0	525.6	534.2
	65	62.0	0.559	6.14	2.11	0.744	482.8	491.4	500.0	508.6	517.2	525.8	534.4
	64	60.5	0.582	5.85	2.40	0.709	483.0	491.6	500.2	508.8	517.4	526.0	584.6
	63	59.0	0.506	5.56	2.69	0.674	483.1	491.7	500.3	508.9	517.5	526.1	534.7
	62	57.5	0.481	5.28	2.97	0.640	483.2	491.8	500.4	509.0	517.7	526.3	584.9
	61	56.0	0.458	5.08	3.22	0.609	483.8	491.9	500.5	509.1	517.8	526.4	535.0
	60	54.5	0.435	4.78	8.47	0.579	483.5	492.1	500.7	509.8	518.0	526.6	535.1
	59	53.0	0.414	4.54	3.71	0.550	488.6	492.2	500.8	509.4	518.1	526.7	585-2
	58	51.5	0.393	4.31	8.94	0.522	483.8	492.4	501.0	509.6	518.3	526.9	535.4
	57	50.0	0.378	4.10	4.15	0.497	483.9	492.5	501.1	509.7	518.4	527:0	585.5
	56	48.5	0.355	8.89	4.36	0.471	484.0	492.6	501.2	509.9	518.5	527.1	585.6
	55	47.0	0.337	8.69	4.56	0.447	484.1	492.7	501.8	510.0	518.6	527.2	535.7
	54	45.5	0.320	3.51	4.74	0.425	484.2	492.8	501.4	510.1	518.7	527.3	535.8
	53	44.0	0.304	3.33	4.92	0.404	484.3	492.9	501.5	510.2	518.8	527.4	535.9
	52	42.5	0.288	8.16	5.09	0.383	484.4	493.0	501.6	510.3	518.9	527.5	536.0
	51	41.0	0.274	3.00	5.25	0.864	484.5	498.1	501.7	510.4	519.0	527.6	586.1
	50	39.5	0.260	2.85	5.40	0.345	484.6	493.2	501.8	510.5	519.1	527.7	536.2
	49	38.0	0.246	2.70	5.55	0.827	484.7	498.8	501.9	510.6	519.2	527.8	536.8
ı	48	36.5	0.234	2.57	5.68	0.312	484.7	493.8	501.9	510.6	519.2	527.8	536.8
- 1	47	35.0	0.222	2.44	5.81	0.296	484.8	498.4	502.0	510.7	519.8	527.9	536.4
	46	33.5	0.210	2.81	5.94	0.280	484.9	493.5	502.1	510.8	519.4	528.0	536.5
	45	32.0	0.199	2.19	6.06	0.265	485.0	493.6	502.2	510.9	519.5	528.1	536.6
	44	30.5	0.189	2.08	6.17	0.252	485.0	498.6	502.2	510.9	519.5	528.1	536.6
72	72	72.0	0.776	8.50	0.00	1.000	480.6	489.2	497.8	506.4	514.9	523.5	532.1
	71	70.5	0.789	8.10	0.40	0.953	480.8	489.4	498.0	506.5	515.1	523.7	532.3
	70	69.0	0.704	7.71	0.79	0.907	481.0	489.6	498.2	506.7	515.8	523.9	582.5
	69	67.5	0.670	7.35	1.15	0.865	481.2	489.8	498.4	506.9	515.5	524.1	532.7
	68	66.0	0.638	7.00	1.50	0.824	481.4	490.0	498.5	507.1	515.7	524.8	582.9
	67	64.5	0.607	6.66	1.84	0.784	481.6	490.2	498.7	507.3	515.9	524.5	533.1
	66	63.0	0.578	6.33	2.17	0.745	481.7	490.3	498.8	507.4	516.1	524.7	533.3
	65	61.5	0.550	6.03	2.47	0.710	481.8	490.4	499.0	L	516.2	l	533.4
	64	60.0	0.528	5.73	2.77	0.674	482.0	490.6	499.2		516.4	l .	583.6
	63	58.5	0.498	5.45	3.05	0.641	482.1	490.7	499.8	507.9	516.5		533.7
	62	57.0	0.478	5.18	8.82	0.610	482.3	490.9	499.5	508.1	516.7		533.9
	61	55.5	0.450	4.98	3.57	0.580	482.5	491.1		508.3	516.9	l	534.1 584.2
- 1	60	54.0	0.428	4.68	3.82	0.551	482.6 482.8	491.2	499.8	508.4	517.0	525.6	

of:	ding	Temp.	Force	We of V	ight apor	Hu-		Wolgh	t in Grai	as of a Cr	ıble Foot	of Air.	
	noter, shr.	Dew- Point.	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Seture- tion ==		Height o	of the Bu	rometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	ofaCu- bic Ft. of Air.	1.000.	98.0	28.5	29.0	29.5	30.0	in. 80.5	31.0
0	59	52.5	in. 0.407	g z.	gr.	A 800	gr.	gr.	gr.	gr.	gr.	gt.	gr.
72	58	51.0	0.386	4.45	4.05	0.528	482.8 482.9	491.4 491.5	500.0 500.1	508.6 508.7	517.2 517.8	525.8 525.9	534.4 534.5
1	57	49.5	0.367	4.02	4.48	0.478	483.0	491.6	500.1	508.8	517.4	526.0	534.6
	56	48.0	0.349	3.82	4.68	0.449	483.1	491.7	500.2	508.9	517.5	526.1	534.7
	55	46.5	0.831	3.63	4.87	0.427	483.2	491.8	500.4	509.0	517.6	526.2	534.8
	54	45.0	0.315	3.45	5.05	0.406	488.3	491.9	500.5	509.1	517.7	526.2	534.9
	58	43.5	0.299	8.28	5.22	0.286	483.3	492.0	500.6	509.2	517.8	526.3	535.0
	52	42.0	0.288	3.11	5.39	0.366	483.5	492.1	500.7	509.8	517.9	526.4	535.1
i i	51	40.5	0.269	2.95	5.55	0.847	483.6	492.2	500.8	509.4	518.0	526.5	535.2
1 1	50	39.0	0.255	2.80	5.70	0.829	483.7	492.3	500.9	509.5	518.1	526.6	535.8
	49	87.5	0.242	2.66	5.84	0.318	483.8	492.4	501.0	509.6	518.2	526.7	585.4
	48	86.0	0.230	2.52	5.98	0.296	488.8	492.4	501.0	509.6	518.2	526.7	585.4
	47	34.5	0.218	2.39	6.11	0.281	488.9	492.5	501.2	509.7	518.8	526.8	535.5
1 1	46	\$3.0	0.207	2.27	6.23	0.267	484.0	492.6	501.8	509.8	518.4	526.9	585.6
	45	81.5	0.196	2.16	6.84	0.254	484.1	492.7	501.3	509.9	518.5	527.1	535.7
73	73	73.0	0.801	8.76	0.00	1.000	479.6	488.1	496.7	505.2	513.8	522.3	580.9
1	72	71.5	0.736	8.35	0.41	0.958	479.8	488.8	496.9	505.4	514.0	522.5	581.1
	71	70.0	0.727	7.95	0.81	0.908	480.0	488.5	497.1	503.6	514.2	522.7	531.3
	70	68.5	0.692	7.57	1.19	0.864	480.2	488.7	497.8	505.8	514.4	522.9	531.5
	69	67.0	0.659	7.21	1.55	0.828	480.4	488.9	497.5	506.0	514.6	528.1	581.7
	68	65.5	0.628	6.87	1.89	0.784	480.5	489.0	497.6	506.1	514.8	523.3	531.9
	67	64.0	0.597	6.53	2.23	0.745	480.7	489.2	497.8	506.3	515.0	523.5	582.1
	66	62.5	0.568	6.22	2.54	0.710	480.8	489.8	497.9	506.4	515.1	528.6	582.2
	65 .	61.0	0.541	5.92	2.84	0.676	481.0	489.5	498.1	506.6	515.8	528.8	532.4
	64	59.5	0.515	5.63	3.13	0.648	481.1	489.6	498.2	506.8	515.4	524.0	582.6
	63	58.0	0.489	5.34	8.42	0.610	481.2	489.8	498.4	507.0	515.6	524.2	582.8
	62	56.5	0.465	5.09	8.67	0.581	481.4	490.0	498.6	507.2	515.8	524.4	588.0
	61	55.0	0.442	4.84	3.92	0.558	481.6	490.2	498.8	507.4	516.0	524.6	533.2
	60	53.5	0.421	4.59	4.17	0.524	481.7	490.8	498.9	507.5	516.1	524.7	533.8
	59	52.0	0.400	4.87	4.39	0.499	481.8	490.4	499.0	507.6	516.2	524.8	533.4
	58	50.5	0.380	4.16	4.60	0.475	482.0	490.6	499.2	507.8	516.4	525.0	588.6
	57	49.0	0.361	3.94	4.82	0.450	482.1	490.7	499.8	507.9	516.5	525.1	588.7
	56	47.5	0.348	3.74	5.02	0.427	482.2	490.8	499.4	508.0	516.6	525.2	538.8
	55	46.0	0.326	3.56	5.20	0.406	482.3	490.9	499.5	508.1	516.7	525.3	583.9
	54	44.5	0.309	3.88	5.38	0.386	492.4	491.0	499.6	508.2	516.8	525.4	584.0
	58	43.0	0.298	3.21	5.55	0.866	482.5	491.1	499.7	508.3	516.9	525.5	584.1
	52	41.5	0.279	8.05	5.71	0.848	482.6	491.2	499.8	508.4	517.0	525.6	534.2
	51	40.0	0.264	2.89	5.87	0.330	482.7	491.8	499.9	508.5)	534.8
	50	88.5	0.251	2.74	6.02	0.818	482.8	491.4	500.0	508.6	517:2	525.8	584.4
	49	87.0	0.288	2.60	6.16	0.297	482.9	491.5		508.6	517.2	525.8	534.4
	48	85.5	0.226	2.47	6.29	0.282	483.0	491.6		508.7	1 1	1	584.5
	47	84.0	0.214	2.34		0.267	483.1	491.7	•			526.0	584.6
	46	32.5	0.203	Z.22	6.54	0.253	433.3	491.9	500.4	509.1	517.6	526.2	584.8

of 7	ding	Temp.	Force		ight apor	Hu-		Weigh	in Grah	u of a Co	ıbic Foot	of Air.	
	neter, Lhr.	of Dew-	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Seture-		Height	of the Ba	rometer i	n Englis	h Inches	
Dry.	Wet.	Point, Fahr.	Buglish Inches.	Foot of		tion == 1.000.	98.0	28.5	29.0	29.5	30.0	30.5	31.0
74	74	74.0	in. 0.827	gt. 9.04	gr. 0.00	1.000	gr. 478.4	gr. 486.9	gr. 495.5	gr. 504.0	gr. 512.6	gr. 521.1	gr. 529-7
′*	78	72.5	0.787	8.60	0.44	0.951	478.6	487.1	495.7	504.2	512.8	521.8	529.9
- 1	72	71.0	0.751	8.20	0.84	0.907	478.8	487.8	495.9	504.4	513.0	521.5	580.1
	71	69.5	0.715	7.81	1.23	0.864	479.0	487.5	496.1	504.6	518.2	521.7	580.8
	70	68.0	0.681	7.44	1.60	0.823	479.2	487.7	496.3	504.8	518.4	521.9	580.5
ı	69	66.5	0.648	7.08	1.96	0.788	479.4	487.9	496.5	505.0	513.6	522.1	580.7
	68	65.0	0.617	6.75	2.29	0.747	479.6	488.1	496.7	505.2	513.8	522.8	580.9
	67	63.5	0.588	6.41	2.68	0.709	479.8	488.3	4 9 6.9	505.4	514.0	522.5	531.1
i	66	62.0	0.559	6.10	2.94	0.675	480.0	488.5	497.1	505.6	514.2	522.7	581.3
	65	60.5	0.532	5.81	8.23	0.643	480.1	488.7	497.3	505.9	514.4	522.9	581.5
	64	59.0	0.506	5.52	8.52	0.611	480.8	488.9	497.5	506.1	514.6	523.2	581.8
	68	57.5	0.481	5.24	8.60	0.580	480.5	489.1	497.7	506.8	514.8	528.4	582.0
	62	56.0 54.5	0.458	4.99	4.05	0.552	480.6	489.2	497.8	506.4	514.9	528.5	582-1
	61	54.5	0.435	4.75	4.29	0.525	480.7	489.8	497.9	506.5	515.0	528.6	582.2
	60	58.0	0.414	4.52	4.52	0.500	480.9	489.5	498.1	506.7	515.2	528. 8	582.4
	59	51.5	0.398	4.29	4.75	0.475	481.0	489.6	498.2	506.8	515.3	528.9	582.5
,	58	50.0	0.878	4.08	4.96	0.451	481.1	489.7	498.3	506.9	515.4	524.0	582.6
	57	48.5	0.355	3.86	5.18	0.427	481.2	489.8	498.4	507.0	515.5	524.1	582.7
İ	56	47.0	0.887	8.66	5.88	0.405	481.3	489.9	498.5	507.1	515.6	524.2	582.8
- 1	55	45.5	0.320	8.48	5.56	0.885	481.4	490.0	498.6	507.2	515.7	524.3	532.9
	24	44.0	0.304	8.32	5.72	0.367	481.5	490.1	498.7	507.8	515.8	524.4	583.0
	53	42.5	0.288	8.15	5.89	0.848	481.6	490.2	498.8	507.4	515.9	524.5	533.1
	52	41.0	0.274	2.99	6.05	0.881	481.7	490.3	498.9	507.5	516.0	524.6	588.2
	51	39.5	0.260	2.88	6.21	0.313	481.8	490.4	499.0	507.6	516.1	524.7	538.8
	50	38.0	0.246	2.69	6.85	0.298	481.9	490.5	499.1	507.7	516.2	524.8	588.4
- 1	49	86.5	0.284	2.55	6.49	0.282	481.9	490.5	499.1	507.7	516.2	524.8	583.4
ŀ	48	35.0	0.222	2.42	6.62	0.268	482.0	490.6	499.2	507.8	516.8	524.9	583.5
	47	33.5	0.210	2.80	6.74	0.254	482.1	490.7	499.2	507.9	516.4	525.0	583.6
75	75	75.0	0.854	9.81	0.00	1.000	477.4	485.9	494.4	502.9	511.5	520.0	528.5
	74	78.5	0.814	8.87	0.44	0.958	477.6	486.1	494.6	508.1	511.7	520.2	528.7
	73	72.0	0.776	8.45	0.86	0.908	477.8	486.3	494.8	508.8	511.9	520.4	528.9
	72	70.5	0.789	8.05	1.26	0.865	478.0	486.5	495.0	508.5	512.1	520.6	529.1
	71	69.0	0.704	7.67	1.64	0.824	478.2	486.7	495.2	503.7	512.8	520.8	529.3
	70	67.5	0.670	7.80	2.01	0.784	478.3	486.8	495.3	508.8	512.5	521.0	529.5
	69	66.0	0.638	6.95	2.36	0.746	478.5	487.0	495.5	504.0	512.7	521.2	529.7
	68	64.5	0.607	6.62	2.69	0.711	478.7	487.2	495.7	504.2		1	529.9
	67	63.0	0.578	6.80	3.01	0.677	478.9	487.4	495.9		618.1	1	530.1
	66	61.5	0.550	5.99	8.32	0.648	479.1	487.6	496.1	504.6	513.8	1	580.8
	65	60.0	0.528	5.69	3.62	0.611 0.582	479.8	487.8	496.4	504.9	513.5	1	580.6 530.8
	64 63	58.5 57.0	0.498	5.42 5.15	3.89 4.16	0.553	479.5 479.6	488.0 488.1	496.6 496.7	505.1 505.2	518.7 518.8	l	580.9
	62	55.5	0.450	4.90	4.41	0.526	4	484.2	ı	ľ	513.9	,	1

Re	eding Ther-	Temp.	Force		ight apor	Hu-		Weigh	t in Grab	ns of a Cu	ible Foot	of Air.	
mo	neter,	of Dew-	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Seture-		Height (of the Ba	rometer i	n English	Inches.	
Dry.	Wet.	Point, Fahr.	English Inches.	Foot of Air.		1.000.	in. 98.0	in. 29.5	29.0	in. 29.5	In. 80.0	in. 30.5	in. 31.0
—			b .	<u> </u>									
75	62	55.5	0.450	4.90	4.41	0.526	479.7	488.2	496.8	gr. 505.3	513.9	522.4	581.0
	61	54.0	0.428	4.66	4.65	0.501	479.9	488.4	497.0	505.5	514.1	522.6	581.2
	60	52.5	0.407	4.43	4.88	0.476	480.0	488.5	497.1	505.6	514.2	522.7	581.8
	59	51.0	0.886	4.21	5.10	0.452	480.1	488.6	497.2	505.7	514.B	522.8	581.4
	58	49.5	0.367	4.00	5.81	0.429	480.8	488.8	497.4	505.9	514.5	523.0	531.6
1	57	48.0	0.849	8.79	5.52	0.407	480.4	488.9	497.5	506.0	514.6	523.1	581.7
	56	46.5	0.881	8.60	5.71	0.887	480.5	489.0	497.6	506.1	514.7	523.2	531.8
	55	45.0	0.815	3.42	5.89	0.367	480.6	489.1	497.7	506.2	514.8	523.3	531.9
	54	43.5	0.299	8.25	6.06	0.349	480.7	489.2	497.8	506.8	514.9	523.4	532.0
	58	42.0	0.288	3.09	6.22	0.882	480.8	489.3	497.9	506.4	515.0	523.5	532.1
	52	40.5	0.269	2.93	6.88	0.815	480.8	489.8	497.9	506.4	515.0	523.5	582.1
	51	89.0	0.255	2.78	6.53	0.299	480.9	489.4	498.0	506.5	515.1	523.6	532.2
	50	37.5	0.242	2.64	6.67	0.284	481.0	489.5	498.1	506.6	515.2	523.7	532.3
	49	\$6.0	0.280	2.51	6.80	0.270	481.1	489.6	498.2	506.7	515.3	523.8	532.4
	48	84.5	0.218	2.39	6.92	0.257	481.2	489.7	496.3	506.8	515.4	523.9	582.5
			1		1	· .							
	76	76.0	0.882	0.00		1 000	4500	404.0					
76	75	74.5	0.840	9.60 9.14	0.00	1.000 0.952	476.8 476.6	484.8	498.3	501.8	510.8	518.8	527.3
	74	73.0	0.801	8.71	0.89	0.907	476.8	485.1 485.8	493.6 493.8	502.1 502.3	510.6 510.8	519.1 519.8	527.6 527.8
	73	71.5	0.763	8.30	1.80	0.865	477.0	485.5	494.0	502.6	511.1	519.6	528.1
	72	70.0	0.727	7.90	1.70	0.828	477.2	485.7	494.8	502.8	511.8	519.8	528.8
	71	68.5	0.692	7.53	2.07	0.784	477.4	485.9	494.5	508.0	511.5	520.0	528.5
	70	67.0	0.659	7.17	2.43	0.747	477.6	486.1	494.7	508.2	511.7	520.2	528.7
						_			1				
	69	65.5	0.628	6.88	2.77	0.711	477.8	486.3	494.9	503.4	511.9	520.4	528.9
	68	64.0	0.597	6.49	8.11	0.676	477.9	486.4	495.0	508.6	512.1	520.6	529.2
	67 66	62.5 61.0	0.568	6.16 5.88	8.44	0.642	478.1	486.6	465.2	503.8	512.8	520.8	529.4
	65	59.5	0.515	5.59	4.01	0.618	478.2 478.8	486.7 486.8	495.3 495.4	503.9 504.0	512.4 512.5	520.9 521.0	529.5 529.6
	64	58.0	0.489	5.81	4.29	0.558	478.5	487.0	495.6	504.2	512.7	521.2	529.8
	68	56.5	0.465	5.06	4.54	0.527	478.6	487.1	495.7	504.8	512.8	521.8	529.9
	62	55.0	0.442	4.81	4.79	0.501	478.8	487.3	495.9	504.5	513.0	521.5	580.1
	61	53.5	0.421	4.57	5.03	0.476	479.0	487.5	496.1	504.7	513.2	521.7	580.8
	€0	52.0	0.400	4.84	5.26	0.452	479.1	487.6	496.2	504.8	518.3	521.8	530.4
	59 58	50.5	0.880	4.13	5.47	0.480	499.2	487.7	496.3	504.9	518.4	521.9	580.5
1	57	49.0 47.5	0.861 0.843	3.92 3.78	5.68 5.87	0.408	499.3 499.4	487.8 487.9	496.4 496.5	505.0 505.1	518.5	522.0 522.1	530.6 530.7
1	56	46.0	0.848	3.78	6.06	0.869	499.4	487.9 488.0	496.6	505.1 505.2	518.6 513.7	522.1 522.2	580.7 580.8
li l		13.0	4.550	5.02	0.00	0.003	200.0	400.V	450.0	003.2	010.7	042.2	090.0
,	55	44.5	0.309	3.86	6.24	0.851	499.6	488.1	496.7	505.8	513.8	522.8	580.9
'	54	48.0	0.293	8.19	6.41	0.332	499.7	488.2	496.8	505.4	518.9	522.4	581.0
	58	41.5	0.279	8.03	6.57	0.316	499.8	488.3	496.9	505.5	514.0	522.5	531.1
	52	40.0	0.264	2.88	6.72	0.801	499.9	488.4		505.6	514.1	522.6	531.2
li i	51	38.5	0.251	2.73	6.87	0.284	500.0	488.5		505.7	514.2	522.7	531.8
	50	37.0	0.238	2.59	7.01	0.269	500.1	488.6	497.2	505.8	514.3	522.8	531.4
<u></u>	49	35.5	0.226	2.46	7.14	0.256	500.2	488.7	497.3	505.9	514.4	522.9	531.5

of '	ding	Temp.	Force	Wed of V	ght apor	Hu-		Weigh	t in Grab	as of a Ci	able Foot	of Air.	
	neter, hr.	Dew- Point,	of Vapor in	In a Cubic	for Sat'n	midity, Setura- tion —		Height o	of the Ba	rometer !	n Englis	h Inches	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	in. 28.5	29.0	in. 29. 5	in. 80.0	30.5	31.0
°	0	77.0	in. 0.910	gr. 9.89	gr. 0.00	1.000	gr. 475.8	gr. 483.8	gr. 492.8	gr. 500.8	gr. 509.2	517.7	gr. 526-2
"	77 76	75.5	0.868	9.42	0.47	0.953	475.5	484.0	492.5	501.0	509.4	517.9	526.4
	75	74.0	0.827	8.99	0.90	0.909	475.7	484.2	492.7	501.2	509.6	518.1	526.6
	74	72.5	0.787	8.57	1.32	0.867	475.9	484.4	492.9	501.4	509.9	518.4	526.9
	73	71.0	0.751	8.15	1.74	0.824	476.1	484.6	493.1	501.6	510.1	518.6	527.1
	72	69.5	0.715	7.77	2.12	0.786	476.3	484.8	498.8	501.8	510.8	518.8	527.
	71	68.0	0.681	7.40		0.748	476.5	485.0	493.5	502.0	510.5	519.0	527.
	70	66.5	0.648	7.04	2.85	0.712	476.7	485.2	493.7	502.2	510.7	519.2	527.7
	69	65.0	0.617	6.71	8.18	0.678	476.9	485.4	493.9	502.4	510.9	519.4	527.9
	68	63.5	0.588	6.37	3.52	0.644	477.0	485.6	494.1	502.6	511.1	519.6	528.
	67	62.0	0.559	6.06	8.88	0.613	477.2	485.8	494.8	502.8	511.3	519.8	528.
	66	60.5	0.582	5.77	4.12	0.583	477.4	486.0	494.5	508.0	511.5	520.0	528.
	65	59.0	0.506	5.49	4.40	0.556	477.5	486.1	494.6	503.1	511.6	520.1	528-
	64	57.5	0.481	5.21	4.68	0.527	477.7	486.8	494.8	503.3	511.8	520.3	528.
	63	56.0	0.458	4.96	4.93	0.501	477.9	486.5	495.0	508.5	512.0	520.5	529.0
	62	54.5	0.435	4.70	5.19	0.476	478.0	486.6	495.1	508.7	512.1	520.6	529.
	61	53.0	0.414	4.49	5.40	0.454	478.0	486.6	495.1	503.7	512.2	520.7	529.
	60	51.5	0.893	4.26	5.68	0.481	478.1	486.7	495.2	503.8	512.8	520.8	529.
	59	50.0	0.378	4.05	5.84	0.410	478.2	456.8	495.3	508.9	512.4	520.9	529.
	58	48.5	0.855	3.85	6.04	0.389	478.3	486.9	495.4	504.0	512.5	521.0	529.
	57	47.0	0.337	3.65	6.24	0.369	478.5	487.1	495.6	504.1	512.7	521.2	529.
	56	45.5	0.320	3.47	6.42	0.351	478.6	487.2	495.7	504.2	512.8	521.3	529.
	55	44.0	0.304	3.29	6.60	0.333	478.7	487.3	495.8	504.8	512.9	521.4	580.
	54	42.5	0.288	3.13	6.76	0.317	478.8	487.4	495.9	504.4	513.0	521.5	530.
	53	41.0	0.274	2.97	6.92	0.301	478.9	487.5	496.0	504.5	513.1	521.6	530.
	52	39.5	0.260	2.82	7.07	0.285	479.0	487.6	496.1	504.6	513.2	521.7	530.
	51	38.0	0.246	2.67	7.22	0.270	479.1	487.7	496.2	504.7	513.3	521.8	580.
	50	36.5	0.234	2.53	7.36	0.256	479.1	487.7	496.2	504.7	513.3	521.8	530.
78	78	78.0	0.940	10.19	0.00	1.000	474.1	482.5	491.0	499.4	508.0	516.4	524.
	77	76.5	0.896	9.72	0.47	0.954	474.4	482.9	491.4	499.9	508.3	516.7	525.
	76	75.0	0.854	9.25	0.94	0.908	474.7	483.2	491.6	500.1	508.6	517.1	525.
	75	73.5	0.814	8.82	1.87	0.865	474.9	488.4	491.8	500.3	608.8	517.3	525-8
	74	72.0	0.776	8.40	1.79	0.824	475.2	488.7	492.1	500.6	509.1	517.6	526.
	78	70.5	0.789	8.00	2.19	0.785	475.4	483.9	492.3	500.8	500.3	517.8	526.
	72	69.0	0.704	7.62	2.57	0.748	475.6	484.1	492.5	501.0	509.5	518.0	526.
	71	67.5	0.670	1	2.94	0.711	475.8		1		509.7	L .	1
	70	66.0	0.638	6.91		0.678	475.9	484.4	•		509.9	518.4	
	69	64.5	0.607	6.58	ı	0.646	476.1	484.6	493.1	501.6	510.1		527.
	68	68.0	0.578	6.26		0.614	476.8	484.8	493.3	501.8			ł .
	67	61.5	0.550	1	4.28	0.585	476.4	484.9	493.4	501.9	510.4		527.
	66	60.0	0.523		4.53	0.555	476.6	485.1	1	502.1			527.
	65	58.5	0.498	5.38	4.81	0.528	476.8	495.3	493.8	502.3	510.8	519.8	527.

Reg	ding	Temp.	Force		ght apor	His-		Weigh	t in Grad	na of a Cu	bic Foot	of Air.	
20000	noter,	Dov-	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Seture-		Height o	of the Ba	rometer i	n English	Inches.	
Dry.	Wet.	Point, Fahr.	English Inches.		of aCu- ble Ft. of Air.	tion == 1.000.	98.0	28.5	29.0	29.5	30.0	in. 30.5	31.0
78	65	o 58.5	in. 0.498	5.88	gr. 4.81	0.528	gr. 476.8	gr. 485.8	gr.	gr.	gr.	gr.	gr.
	61	57.0	0.473	5.12	5.07	0.502	476.8	485.8	493.8 493.9	502.8 502.4	510.8 510.9	519.8 519.4	527.8 527.9
!	63	55.5	0.450	4.88	5.81	0.479	476.9	485.4	494.0	502.5	511.0	519.5	528.0
	62	54.0	0.428	4.63	5.56	0.454	477.1	485.6	494.2	502.7	511.2	519.7	528.2
1 1	61	52.5	0.407	4.40	5.79	0.482	477.2	485.7	494.8	502.8	511.8	519.9	528.3
	60	51.0	0.386	4.18	6.01	0.409	477.8	485.8	494.4	502.9	511.4	519.9	528.4
	59	49.5	0.867	8.98	6.21	0.391	477.4	485.9	494.5	503.0	511.5	520.0	528.5
	58	48.0	0.849	3.78	6.41	0.871	477.5	486.0	494.6	503.1	511.6	520.1	528.6
N I	57	46.5	0.831	8.59	6.60	0.352	477.6	486.1	494.7	503.2	511.7	520.2	528.7
	56	45.0	0.815	8.41	6.78	0.885	477.8	486.8	494.8	503.3	511.9	520.4	528.9
	55	43.5	0.299	3.24	6.95	0.818	477.9	486.4	494.9	503.4	512.0	520.5	529.0
	54	12.0	0.283	8.07	7.12	0.801	478.0	486.5	495.0	503.5	512.1	520.6	529.1
	53	40.5	0.269	2.92	7.27	0.287	478.1	486.5	495.0	503.5	512.1	520.6	529.1
	52 51	39.0 37.5	0.255	2.77	7.42	0.272	478.2	486.6	495.1	503.6	512.2	520.7	529.2
	31	97.5	0.242	2.63	7.56	0.258	478.8	486.7	495.2	503.7	512.8	520.8	529.8
			•	1			ţ	·					
79	79	79.0	0.970	10.50	0.00	1.000	473.1	481.5	490.0	499.4	506.9	515.3	523.8
'	78	77.5	0.925	10.01	0.49	0.958	478.4	481.8	490.8	498.7	507.2	515.6	524.1
	77	76.0	0.882	9.54	0.96	0.909	478.7	482.1	490.6	499.0	507.5	515.9	524.4
	76	74.5	0.840	9.10	1.40	0.867	478.8	482.2	490.7	499.2	507.7	516.2	524.7
1	75	78.0	0.801	8.66	1.84	0.825	474.0	482.4	490.9	499.4	507.9	516.4	524.9
	74	71.5	0.763	8.25	2.25	0.786	474.8	482.7	491.2	499.7	508.2	516.7	525.2
	73	70.0	0.727	7.86	2.64	0.749	474.5	482.9	491.4	499.9	508.4	516.9	525.4
	72	68.5	0.692	7.48	3.02	0.712	474.7	483.1	491.6	500.1	508.6	517.1	525.6
11	71	67.0	0.659	7.12	8.88	0.678	474.9	488.4	491.9	500.4	508.8	517.8	525.8
	70	65.5	0.628	6.79	3.71	0.647	475.1	483.6	462.1	500.6	509.0	517.5	526.0
	69	64.0	0.597	6.45	4.05	0.614	475.3	483.8	492.3	500.8	509.2	517.7	526.2
	68	62.5	0.568	6.14	4.86	0.585	475.4	483.9	492.4	500.9	509.8	517.8	526.8
	67	61.0	Q.541	5.84	4.66	0.556	475.6	484.1	492.6	501.1	509.5	518.0	526.5
	66	59.5	0.515	5.55	4.95	0.529	475.7	484.2	492.7	501.2	509.6	518.1	526.6
	63	58.0	0.489	5.28	5.22	0.508	475.8	484.8	492.8	501.3	509.8	518.8	526.8
	64	56.5	0.465	5.02	5.48	0.478	476.0	484.5	493.0	501.5	510.0	518.5	527.0
	63	55.0	0.442	4.78	5.72	0.455	476.1	484.6	493.1	501.6	510.1	518.6	527.1
	62	53.5	0.421	4.54	5.96	0.432	476.8	484.8	493.3	501.8	510.8	518.8	527.3
	61	52.0	0.400	4.81	6.19	0.410	476.4	484.9	498.4	501.9	510.4	518.9	527.4
	60	50.5	0.880	4.10		0.390	476.5	485.0	493.5	502.0	510.5	519.0	527.5
	59	49.0	0.861	8.90	6.60	0.371	476.6	485.1	498.6	502.1	510.6	519.1	527.6
	58	47.5	0.343	8.71	6.79	0.358	476.7	485.2	498.7	502.9	510.7	519.2	527.7
	57	46.0	0.326	3.52	i	0.335	476.8	485.3			510.8		
	56	44.5	0.309	3.84	1	0.818	476.9	485.4			510.9		527.9
	55	43.0	0.298	3.17		0.801	477.0	485.5			511.0		528.0
	54	41.5	0.279	8.01	7.49	0.287	477.1	485.6			511.1	519.6	528.1
	53	40.0	0.264		7.64	0.272	477.2						
	52	38.5	0.251	2.72	7.78	0.260	477.8	485.8	494.8	502.8	511.8	519.8	528.8

of 1	ding Ther-	Temp.	Force of	of V	ight apor Reqd.	Hu-		Weigh	in Grad	s of a Cu	abic Foot	of Air.	
	neter, .hr.	Dew-	Vapor	In a Cubic	for Sat'n.	midity, Seture-		Height (of the Ba	rometer i	n Englis	h Inches	•
Dry.	Wet.	Point, Fahr.	Buglish Inches.	Foot of Air.	of aCu- bic Ft. of Air.	tion == 1.000.	^{in.} 28.0	28.5	29.0	29.5	30.0	30.5	31.0
80	 80	80.0	In. 1.001	gr. 10.81	gr. 0.00	1.000	57. 472.0	gt. 480.4	gr. 488.9	gr. 497.8	gr. 505.7	gr. 514.1	gr 522-6
30	79	78.5	0.955	10.81	0.50	0.954	472.8	480.7	489.1	497.5	506.0	514.4	522.9
	78	77.0	0.910	9.83	0.98	0.909	472.5	480.9	489.4	497.9	506.3	514.7	523.2
	77	75.5	0.868	9.37	1.44	0.867	472.7	481.1	489.6	498.1	506.5	514.9	528.4
	76	74.0	0.827	8.98	1.88	0.826	473.0	481.4	489.9	498.4	506.8	515.2	523.7
	75	72.5	0.787	8.50	2.31	0.786	478.2	481.6	490.1	498.6	507.0	515.4	528.9
	74	71.0	0.751	8.11	2.70	0.750	473.4	481.8	490.3	498.8	507.2	515.6	524.1
	78	69.5	0.715	7.71	3.10	0.718	473.6	482.1	490.6	499.1	507.5	515.9	524.4
	72	68.0	0.681	7.35	8.46	0.680	473.8	482.3	490.8	499.3	507.7	516.1	524.6
	71	66.5	0.648	6.99	1	0.647	474.0	482.5	491.0	499.5	507.9	516.3	524.8
	70	65.0	0.617	6.66	4.15	0.616	474.2	482.7	491.2	499.7	508.1	516.5	525.0
	69	63.5 62.0	0.588	6.83	4.48	0.586	474.4	482.9 483.0	491.4 491.5	499.9 500.0	508.3 508.4	516.7 516.8	525.2 525.3
- }	68 67	60.5	0.582	5.74	5.07	0.531	474.7	488.2	491.7	500.2	508.6	517.0	525.6
ı	00	59.0	0.506	5.45	5.86	0.504	474.9	483.4	491.9	500.4	508.8	517.2	525.7
	66 65	57.5	0.481	6.18	5.63	0.479	475.0	483.5	492.0	500.5	508.9	517.8	525.8
1	64	56.0	0.458	4.93	5.96	0.456	475.2	488.7	492.2	500.7	509.1	517.5	526.0
ļ	68	54.5	0.435	4.69	6.12	0.484	475.8	483.8	492.8	500.8	509.2	517.6	526.1
	62	53.0	0.414	4.46	6.35	0.413	475.4	483.9	492.4	500.9	509.3	517.7	526.2
1	61	51.5	0.898	4.23	6.58	0.391	475.5	484.0	492.5	501.0	509.4	517.8	526.1
	60	50.0	0.378	4.02	6.79	0.372	475.6	484.1	492.6	501.1	509.5	517.9	526.4
- 1	59	48.5	0.855	3.82	6.99	0.358	475.7	484.2	492.7	501.2	509.6	518.0	526.5
	58	47.0	0.887	3.63	7.18	0.336	475.9	484.4	492.9	501.4	509.8	518.2	526.7
1	57	45.5	0.320	3.45	7.36	0.819	476.0	484.5	493.1	501.5	509.9	518.8	526.8
1	56	44.0	0.804	8.27	7.54	0.802	476.1	484.6	493.2	501.6	810.0	518.4	526.9
	55	42.5	0.288	8.11	7.70	0.288	476.2	484.7	493.8	501.7	510.1	518.5	527.0
	54 53	41.0 39.5	0.274 0.260	2.96 2.82	7.85 7.99	0.274	476.8 476.8	484.8 484.8	498.4 498.4	501.8 501.8	510.2 510.2	518.6 518.6	527.1
								l			l		İ
81	81	81.0	1.034	11.14	0.00	1.000	471.0	479.4	487.8	496.2	504.6	513.0	521.4
	80	79.5	0.986	10.62	0.52	0.958	471.3	479.7	488.1	496.5	504.9	513.3	521.
	79	78.0	0.940	10.18	1.01	0.910	471.5	479.9	488.4	496.8	505.2	513.6	522.
	78	76.5	0.896	9.65	1.49	0.866	471.7	480.1	488.6	497.0	505.4	513.8	522.1
-	77	75.0	0.854	9.20	1.94	0.826	472.0	480.4	488.9	497.3	505.7	514.1	522.6
	76	73.5	0.814	8.77	1	0.787	472.2	480.6	489.1	497.5	505.9	514.8	522.8
.	75	72.0	0.776	8.35	2.79	0.750	472.5	450.9	489.4	497.8	506.2	514.6	525.
	74	70.5	0.739	7.95	8.19	0.713	472.6	481.0	489.5	497.9	506.4	514.8	528.5
	73	69.0	0.704	7.57		0.680	472.8	1		498.1		ł	523.
	72	67.5	0.670	7.21	1	0.647	478.0	481.4		498.3	506.8	1	1
	71	66.0	0.638	6.87		0.617	473.2	481.6	1	498.5	507.0	ì	
	70	64.5	0.607	6.54	ı	0.587	478.4	481.8	1	498.7	507.2	1	524.1
	69 68	63.0 61.5	0.578 0.550	6.22	4.92 5.22	0.558	478.6	482.0	490.5	498.9	507.4 507.6	1	524.3

Re	ding		Force	Wei of V	ight apor			Weigh	t in Grah	as of a Cr	able Foot	of Alr.	
2000	Ther- meter, whr.	Temp. of Dew-	of Vapor in	In a Cubic	Reqd.	Hu- midity, Seture-		Height o	the Bu	rometer l	a English	Inches.	
Dry.	Wot.	Point, Fahr.	English Inches.	Foot of Air.		tion — 1.000.	25.0	28.5	29.0	29.5	in. 30.0	in. 20.5	81.0
81	ø8	61.5	in. 0.550	5.92	gr. 5.22	0.531	gr.	gt.	gr.	gr.	gr.	gr.	gz.
31	67	60.0	0.528	5.62	5.52	0.505	478.7 478.8	482.2	490.7 490.8	499.1 499.2	507.6 507.7	516.0 516.1	524.5 524.6
	66	58.5	0.498	5.81	5.88	0.477	474.0	482.5	491.0	499.4	507.9	516.8	524.8
li I	65	57.0	0.478	5.08	6.06	0.456	474.1	482.6	491.1	499.5	508.0	516.4	524.9
!!	64	55.5	0.450	4.84	6.80	0.434	474.3	482.8	491.8	499.7	508.2	516.6	525.1
	68	54.0	0.428	4.60	6.54	0.418	474.4	482.9	491.4	499.8	508.8	516.7	525.2
	62	52.5	0.407	4.87	6.77	0.392	474.5	488.0	491.5	499.9	508.4	516.8	525.3
	61	51.0	0.886	4.15	6.99	0.873	474.6	488.1	491.6	500.0	508.5	516.9	525.4
H	60	49.5	0.367	3.95	7.19	0.855	474.7	488.2	491.7	500.1	508.6	517.0	525.5
11	59	48.0	0.349	8.75	7.89	0.837	474.9	488.4	491.9	500.8	508.8	517.2	525.7
	58	46.5	0.331	8.56	7.58	0.320	475.0	488.5	492.0	500.4	508.9	517.8	525.8
1	57	45.0	0.815	8.88	7.76	0.308	475.1	488.6	492.1	500.5	509.0	517.4	525.9
	56	43.5	0.299	8.21	7.98	0.289	475.2	488.7	492.2	500.6	509.1	517.5	526. 0
	55 54	42.0 40.5	0.288	3.05 2.90	8.09 8.24	0.274	475.8	488.8	492-8	500.7	509.2	517.6	526.1
	~	20.0	0.205	2.50	0.24	0.200	475.8	488.8	492.8	500.7	509.2	517.6	526.1
1													
82	82	82.0	1.067	11.47	0.00	1.000	470.0	478.4	486.8	495.2	508.5	511.9	520.8
	81	80.5	1.017	10.94	0.58	0.954	470.8	478.7	487.0	495.4	503.8	512.2	520.6
11	80	79.0	0.970	10.44	1.08	0.910	470.6	479.0	487.8	495.7	504.1	512.5	520.9
 	79	77.5	0.925	9.95	1.52	0.868	470.7	479.1	487.5	495.9	504.8	512.7	521.1
1	78	76.0	0.882	9.49	1.98	0.827	471.0	479.4	487.8	496.2	504.6	518.0	521.4
li i	77	74.5 73.0	0.840	9.08	2.44 2.87	0.787	471.2	479.6	488.0	496.4	504.8	518.2	521.6
	"		0.501	0.00	2.01	0.750	471.5	479.9	488.3	496.7	505.1	518.5	521.9
1	75	71.5	0.763	8.19	8.28	0.714	471.6	480.0	488.5	496.9	505.8	513.7	522.1
1	74	70.0	0.727	7.81	8.66	0.681	471.8	480.2	488.6	497.1	505.5	513.9	522.4
11	78	68.5	0.692	7.43	4.04	0.648	472.0	480.4	488.8	497.8	505.7	514.1	522.6
	72	67.0	0.659	7.08	4.89	0.618	472.2	480.6	489.0	497.5	505.9	514.8	522.8
1	71 70	65.5 64.0	0.628	6.75	4.72	0.588	472.4	480.8	489.2	497.7	506.1	514.5	528.0
ll .	69	62.5	0.568	6.41 6.10	5.06 5.37	0.559	472.5 472.6	480.8 481.0	489.4	497.9 498.0	506.3 506.4	514.7	528.2 528.3
1	~		2.560			V.302	7,2.0	401.0	-000.0	-60.0	500.4	514.8	U-0-0
	6 8	61.0	0.541	5.81	5.66	0.507	472.8	481.2	489.7	498.2	506.6	515.0	528.5
Į.	67	59.5	0.515	5.52	5.95	0.481	478.0	481.4	489.9	498.4	506.8	515.2	528.7
	66	58.0	0.489	5.25	6.22	0.458	473.1	481.5	490.0	498.5	506.9	515.8	528. 8
ll l	65 64	56.5 55.0	0.465	4.99	6.48	0.485	478.2	481.6	490.1	498.6	507.0	515.4	528.9
#	92 94	53.5	0.442	4.75		0.414	478.4	481.8 482.0	490.8	498.8	507.2 507.4	515.6 515.8	524.1 524.8
	62	52.0	0.400		7.18	0.874	478.6		490.5	499.0	507.5	515.9	524.4
	-						2.0.0		200.0	20011		01010	224.4
11	61	50.5	0.380	4.08		0.856	478.7	482.2	490.7	499.2	507.6	516.0	524.4
	. 60	49.0	0.861	3.87		0.337	473.8	482.8	490.8		507.7		524.5
	59	47.5	0.848	3.68		0.320	478.9	482.4	490.9	499.4	507.8	516.2	524.6
	58 57	46.0 44.5	0.326	8.50	7.97 8.15	0.805	474.0	482.5	491.0	499.5	507.9	516.8	524.7
	56	48.0	0.298	8.15		0.289	474.1 474.2	482.6 482.7	491.1 491.2	499.6 499.7	508.0 508.1	516.4 516.5	524.8 524.9
i i	55	41.5			8.48				491.8	1	508.2		525.1
<u> </u>				,	5.40	J.500	7,7.0	102.0	101.0		1000.2	010.0	V-0-1

of ?	ding	Temp.	Force of	We of V	ight spor Reqd.	Hu-		Weigh	in Grain	as of a Cr	able Foot	of Air.	
	neter, shr.	Dew- Point,	Vapor in	In a Cubic	for Sat'n.	midity, Setura- tion =		Height	of the Ba	rometer i	n Englis	h Inches	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- blo Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
83	o 88	83.0	ь. 1.101	gr. 11.82	gr. 0.00	1.000	468.8	gr. 477.2	gr. 485.5	gr. 498.9	gr. 502.8	510.6	gr. 519-0
33	82	81.5	1.050	11.27	0.55	0.953	469.1	477.5	485.8	494.2	502.6	511.0	519.4
1	81	80.0	1.001	10.75	1.07	0.909	469.4	477-8	486.1	494.5	502.9		519.7
1	80	78.5	0.955	10.25	1.57	0.868	469.7	478.1	486.4	494.8	503.2	511.6	520.0
1 1	79	77.0	0.910	9.78	2.04	0.828	470.0	478.4	486.7	495.1	503.5	511.9	520.3
1	78	75.5	0.868	9.31	2.51	0.786	470.8	478.7	487.0	495.4	503.8	512. 2	520.6
	77	74.0	0.827	8.88	2.94	0.751	470.5	478.9	487.2	495.6	504.0	512.4	520.8
}		70 E	0.808	0.48		A #1 #	480.0	4000.0	400 4	407.0	* 04.0		
	76 75	72.5 71.0	0.787 0.751	8.45 8.05	3.87 8.77	0.715	470.6 470.8	479.0 479.2	487.4 487.6	495.8 496.0	504.2 504.4	512.6 512.8	521.0 521.2
	74	69.5	0.715	7.66	4.16	0.647	471.0	479.4	487.8	496.2	504.6	513.0	521.4
	73	68.0	0.681	7.80	4.52	0.618	471.2	479.6	488.0	496.4	504.8	513.2	521.6
1 1	72	66.5	0.648	6.95	4.87	0.588	471.4	479.8	488.2	496.6	505.0	513.4	521.8
1 1	71	65.0	0.617	6.62	5.20	0.560	471.6	480.0	488.4	496.8	505.2	513.6	522-0
	70	68.5	0.588	6.29	5.58	0.588	471.7	480.1	488.5	497.0	505.4	513.8	522.8
1 1							•		·				
1 1	69	62.0	0.559	5.99	5.88	0.507	471.9	480.8	488.7	497.2	505.6	514.0	522.5
1 1	68	60.5	0.532	5.70	6.12	0.482	472.0	480.4	488.8	497.8	505.7	514.1	522.6
1 1	67	59.0 57.5	0.506	5.42	6.40	0.459	472.2	480.6 480.8	489.0	497.5	505.9 506.1	814.8	522.8 523.0
l I	66 65	56.0	0.481 0.458	5.15 4.90	6.67	0.485	472.4 472.4	480.8	489.2 489.3	497.7	506.2	514.5 514.6	523.1
1	64	54.5	0.435	4.66	7.18	0.894	472.5	490.9	489.4	497.9	506.3	514.7	523.2
	68	53.0	0.414	4.48	7.89	0.875	472.7	481.1	489.6	498.1	506.5	514.9	523.4
					,,,,,,,	.5.1515		12212					
1 1	62	51.5	0.898	4.21	7.61	0.856	472.8	481.2	489.7	498.2	506.6	515.0	523.5
1 1	61	50.0	0.878	4.00	7.82	0.389	472.9	481.8	499.8	498.3	506.7	515.1	528.6
	60	48.5	0.855	3.80	8.02	0.322	478.1	481.4	489.9	498.4	506.8	515.2	523.7
	59	47.0	0.837	8.60	8.22	0.805	478.2	481.5	490.0	498.5	506.9	515.8	522.8
	58	45.5	0.820	8.42	8.40	0.289	478.8	481.6	490.1	498.6	507.0	515.4	523.9
.	57 56	44.0 42.5	0.304	3.25 8.09	8.57 8.78	0.276 0.261	473.4 478.5	481.7 481.8	490.2	498.7 498.8	507.1 507.2	515.6 515.6	524.0 524.1
ΙI	90	42.0	0.200	0.05	0.78	0.201	410.0	401.0	480.3	490.0	007.2	010.0	524.1
								}					
84	84	84.0	1.136	12.17	0.00	1.000	467.8	476.2	484.5	492.7	501.2	509.6	517.9
~-	88	82.5	1.083	11.61	0.56	0.954	468.1	476.4	484.8	498.2	5 01.5	509.8	518.2
	82	81.0	1.084	11.07	1.10	0.910	468.4	476.7	485.1	498.5	501.8	510.1	518.5
	81	79.5	0.986	10.55	1.62	0.867	468.6	476.9	485.4	493.7	502.1	510.5	518.8
	80	78.0	0.940	10.07	2.10	0.827	468.9	477.8	485.7	494.0	502.4	510.8	519.1
	79	76.5	0.896	9.59	2.58	0.788	469.1	477.5	485.9	494.2	502.6	511.0	519.8
	78	75.0	0.854	9.14	8.08	0.751	469.4	477.8	486.1	494.5	502.9	511.8	519.7
	-	70 =	A 0	0 ==	0.10	A #14	100.0	140 A	400 P	404 =	KOP 1	K12 F	K10 0
	77	73.5	0.814	8.71 8.80		0.716	469.6 469.8	1	486.8 486.5	494.7 494.9	508.1 508.3		519.9 520.1
	76 75	72.0	0.776	7.90		0.682	470.1				503.6	512.0	
	74	69.0	0.704	7.58	4.64	0.619	470.8			495.4			520.6
	73	67.5	0.670	7.17		0.589	470.5		487.2				520.8
	72	66.0	0.628	6.88		0.561	470.6		487.4	495.8			521.0
	71	64.5	0.607		5.67	0.584			487.5				

Res of 1	ding	Temp.	Force	Wed V	ight apor	Hu-		Weigh	t in Grah	as of a Cr	able Foot	of Alr.	
2000	ater, ahr.	of Dow- Point,	of Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion —		Height o	the Bu	rometer i	a English	Inches.	
Dry.	Wet	Pakr.	Magtish Inches.	Foot of Air.	of aCu- bie Ft. of Air.	1.000.	in. 98.0	28.5	29.0	29.5	30.0	30.5	31.0
84	71	64.5	bs. 0.607	gr. 6.50	gt. 5.67	0.584	gr. 470.7	gr. 479.1	gr.	gr.	gr.	gr.	gr.
اتا	70	63.0	0.578	6.18	5.99	0.508	470.9	479.8	487.5 487.7	495.9 496.1	504.8 504.5	512.7 512.9	521.1 521.3
	69	61.5	0.550	5.87	6.80	0.482	471.1	479.5	487.9	496.8	504.7	518.1	521.5
	68	60.0	0.528	5.59	6.58	0.459	471.2	479.6	488.0	496.4	504.8	513.2	521.6
	67	58.5	0.498	5.31	6.86	0.486	471.4	479.8	488.2	49 6.6	505.0	513.4	521.8
	66	57.0	0.478	5.05	7.12	0.415	471.6	480.0	488.3	496.7	505.2	513.6	522.1
1	65	55.5	0.450	4.81	7.86	0.895	471.6	480.0	488.4	496.8	505.8	513.7	522.2
1	64	54.0	0.428	4.57	7.60	0.875	471.7	480.1	488.5	496.9	505.4	513.8	522.3
l	68	52.5	0.407	4.85	7.82	0.857	471.8	480.2	488.6	497.0	505.5	518.9	522.4
\	62	51.0	0.386	4.13	8.04	0.889	471.9	480.4	488.8	497.2	505.7	514.0	522.5
	61	49.5	0.867	3.98	8.24	0.323	472.1	480.5	488.9	497.8	505.8	514.1	522.6
{	60	48.0	0.849	8.78	8.44	0.806	472.2	480.6	489.0	497.4	505.9	514.2	522.7
	59	46.5	0.881	8.55	8.62	0.292	472.8	480.7	489.1	497.5	506.0	514.3	522. 8
!	58	45.0	0.815	8.87	8.80	0.277	472.4	480.8	489.2	497.6	506.1	514.4	522.9
1	57	43.5	0.299	8.20	8.97	0.268	472.5	480.9	499.8	497.7	506.2	514.5	523.0
1 1													
85	85	85.0	1.171	12.53	0.00	1.000	466.8	475.2	400 8	491.8	F00 1	508.5	516.8
-	84	83.5	1.118	11.95	0.58	0.954	467.1	475.4	488.5 483.7	492.1	500.1 500.4	508.7	517.1
	88	82.0	1.067	11.40	1.13	0.910	467.8	475.6	484.0	492.4	500.7	509.0	517.4
1 1	82	80.5	1.017	10.87	1.66	0.868	467.6	475.9	484.8	492.7	501.0	509.8	517.7
	81	79.0	0.970	10.38	2.15	0.829	467.8	476.1	484.5	492.9	501.2	509.5	517.9
1 1	80	77.5	0.925	9.89	2.64	0.789	468.1	476.4	484.8	493.2	501.5	509.8	518.2
	79	76.0	0.882	9.48	3.10	0.758	468.4	476.7	485.1	493.5	501.8	510.1	518.5
	78	74.5	0.840	8.98	8.55	0.717	400 0	450.0		***	700 O		
	77	73.0	0.801	8.55	3.98	0.682	468.6 468.7	476.9 477.1	485.8 485.5	493.7 498.9	502.0 502.2	510.8 510.5	518.7 518.9
	76	71.5	0.763	8.15	4.38	0.650	469.0	477.4	485.8	494.2	502.5	510.8	519.2
	75	70.0	0.727	7.76	4.77	0.619	469.2	477.6	486.0	494.4	502.7	511.0	519.4
]	74	68.5	0.692	7.39	5.14	0.589	469.4	477.8	486.2	494.6	502.9	511.2	519.6
1	78	67.0	0.659	7.04	5.49	0.562	469.7	478.1	486.5	494.9	503.2	511.5	519.9
	72	65.5	0.628	6.71	5.82	0.536	469.9	478.8	486.7	495.1	508.4	511.7	520.1
	71	64.0	0.597		# 10	0 400	400 -	4000 -	1000	402 -			
	70	62.5	0.568	6.37 6.07	6.16 6.46	0. 50 8 0.484	470.1 470.8	478.5	486.9	495.8	508.6 508.8	511.9	520.3 520.5
	69	61.0	0.541	5.77	6.76	0.460	470.5	478.7 478.9	487.1 487.2	495.5 495.6	504.0	512.1 512.4	520.8
	68	59.5	0.515	5.48	7.05	0.487	470.6	479.0	487.8	495.7	504.1	518.5	520.9
i l	67	58.0	0.489	5.21	7.32	0.415	470.6	479.0	487.4	495.8	504.2	512.6	521.0
	.66	56.5	0.465	4.96	7.57	0.896	470.7	479.1	487.5	495.9	504.3	512.7	
	65	65.0	0.442	4.72	7.81	0.877	470.8	479.2	487.6	496.0	504.4	512.8	521.2
				4 40	0.01		444						
	64 68	58.5	0.421	4.49		0.859	470.9	479.3	487.7	496.1	504.5		521.8
	62	52.0 50.5	0.400	4.26 4.05		0.840	471.1			496.8	504.7		521.5
	61	49.0	0.361	3.85		0.828	471.2 471.3			496.4 496.5	504.8 504.9	513.2 513.8	521.6 521.7
	60	47.5	0.848	8.66		0.292	471.4	479.7		496.6	505.0		521.7
	59	46.0	0.826		9.05	0.278	471.5	479.9	488.4	496.7	505.1	518.5	521.9
		44.5				0.264			488.5		505.2	1	

Ree	ding		Force	We of V	ight apor			Weigh	in Grain	us of a Ci	abic Foot	of Air.	
mon	Ther- neter, .hr.	Temp. of Dow-	of Vapor	In a	Reqd.	Hu- midity, Setura-		Height o	of the Ba	rometer i	n Englis	h Inches	
		Point,	in English	Cubic Foot of	Sat'n. of aCu-	tion -			r			r	
Dry.	Wet.	Fahr.	Inches.	Air.	bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
o 86	o 86	86.0	in. 1.209	gr. 12.91	gr. 0.00	1.000	gr. 465.7	gr. 474.0	gr. 482.3	gr. 490.6	gr. 498.9	gr. 507.2	gr. 515.5
00	85	84.5	1.158	12.31	0.60	0.954	466.0	474.8	482.6	490.9	499.2	507.5	515.8
	84	88.0	1.101	11.75	1.16	0.910	466.8	474.6	482.9	491.2	499.5	507.8	516.1
1 1	88	81.5	1.050	11.20	1.71	0.868	466.5	474.8	483.2	491.5	499.8	508.1	516.5
1 1	82	80.0	1.001	10.69	2.22	0.828	466.8	475.1	483.5	491.8	500.1	508.4	516.8
1	81	78.5	0.955	10.19	2.72	0.789	467.1	475.4	488.8	492.1	500.4	508.7	517.1
	80	77.0	0.910	9.71	3.20	0.752	467.8	475.6	484.0	492.3	500.7	509.0	517.4
	80		0.510	3	0.20	0	301.0	1		102.0		000.0	
	79	75.5	0.868	9.25	3.66	0.717	467.5	475.8	484.2	492.5	500.9	509.2	517.6
	78	74.0	0.827	8.82	4.09	0.683	467.8	476.1	484.5	492.8	501.2	509.5	517.9
	77	72.5	0.787	8.40	4.51	0.651	468.0	476.8	484.7	498.0	501.4	509.7	518.1
	76	71.0	0.751	8.00	4.91	0.619	468.2	476.5	484.9	498.2	501.6	509.9	518.3
1 1	75	69.5	0.715	7.62	5.29	0.590	468.3	476.6	485.0	493.4	501.8	510.2	518.6
	74	68.0	0.681	7.26	5.65	0.562	468.5	476.8	485.2	498.6	502.0	510.4	518.8
	78	66.5	0.648	6.91	6.00	0.535	468.8	477.1	485.5	493.9	502.2	510.6	519.0
1	72	65.0	0.617	6.58	6.33	0.509	468.9	477.2	485.6	494.0	502.4	510.8	519.2
	71	63.5	0.588	6.26	6.65	0.485	469.1	477.4	485.8	494.2	502.6	511.0	519.4
1 1	70	62.0	0.559	5.95	6.96	0.461	469.2	477.5	485.9	494.3	502.7	511.1	519.5
1 1	69	60.5	0.532	5.66	7.25	0.438	469.4	477.7	486.1	494.5	502.9	511.3	519.7
1 1	68	59.0	0.506	5.38	7.58	0.417	469.6	477.9	486.3	494.7	508.1	511.5	519.9
1 1	67	57.5	0.481	5.11	7.80	0.896	469.8	478.1	486.5	494.9	503.8	511.7	520.1
1	66	56.0	0.458	4.87	8.04	0.877	469.9	478.2	486.6	495.0	508-4	511.8	520.2
1 1	-]
1	65	54.5	0.435	4.68	8.28	0.859	470.0	478.8	486.7	495.1	503-5	511.9	520.3
	64	53.0	0.414	4.40	8.51	0.341	470.1	478.4	486.8	495.1	508.6	512.0	520.4
1	68	51.5	0.893	4.19	8.72	0.325	470.2	478.5	486.9	495.2	503.7	512.1	520.5
	62	50.0	0.878	3.98	8.93	0.308	470.4	478.7	487.1	495.4	503.9	512.2	520.7
	61	48.5	0.855	8.78	9.13	0.293	470.5	478.8	487.2	495.5	504.0	512.3	520.8
	60	47.0	0.387	3.59	9.82	0.278	470.6	478.9	487.8	495.6	504.1	512.4	520.9
1	59	45.5	0.820	8.40	9.51	0.263	470.7	479.0	487.4	495.7	504.2	512.5	521.0
										l		ļ	1 1
				1								l	1 1
87	87	87.0	1.247	18.29	0.00	1.000	464.5	472.8	481.1	489.4	497.7	506.0	514.8
''	86	85.5	1.190	12.68	0.61	0.954	464.8	478.1	481.4	489.7	498.0	506.3	514.6
	85	84.0	1.136	12.10	1.19	0.910	465.1	478.4	481.7	490.0	498.3	506.6	514.9
	84	92.5	1.083	11.54	1.75	0.868	465.4	478.7	482.0	490.8	498.6	506.9	515.2
	83	81.0	1.034	11.01	2.28	0.828	465.7	474.0	482.8	490.6	498.9	507.2	515.5
	82	79.5	0.986	10.49	2.80	0.789	466.0	474.8	482.6	490.9	499.2	507.5	515.8
	81	78.0	0.940	10.01		0.758	466.8		482.9	491.2			516.1
	80	76.5	0.896	9.54	3.75	0.718	466.5	474.8	488.1	491.4	499.8	508.1	516.5
	79	75.0	0.854	9.09	4.20	0.684	466.8	475.1	483.5	491.8	500.1	508.4	516.8
	78	78.5	0.814	8.66		0.652	467.0	475.8	483.7	492.0	500.8	508.6	517.0
	77	72.0	0.776	8.24	5.05	0.620	467.2	475.5	483.9	192.2	500.5	508.8	517.2
	76	70.5	0.789	7.85		0.591	467.8	475.6	484.0	492.3	500.7	509.0	517.4
	75	69.0	0.704	7.48		0.563	467.5	475.8	484.2	492.5	500.9	509.2	517.6
	74	67.5	0.670		6.17	0.536	467.7	1		492.7	I .	509.4	

of	ading Ther-	Temp.	Force	We of V	ight apor	Hu-	Height of the Barometer in English Inches. 10 10 10 10 10 10 10 1						
7	noter, bhr.	Dew-	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura-		Height o	of the Bu	rometer i	n English	Inches.	
Dry.	Wot.	Point, Fahr.	English Inches.		of aCu- bic Ft. of Air.	1.000.							31.0
87	0 74	67.5	in. 0.670	gr. 7.12	gr. 6.17	0.586					-		gr.
٠.	73	66.0	0.638	6.78	6.51	0.510	i .	I .					517.8 518.0
	72	64.5	0.607	6.46	6.88	0.486		1					518.2
1	71	63.0	0.578	6.14	7.15	0.462			1				518.5
1	70	61.5	0.550	5.85	7.44	0.440	468.4	476.7	485.1	493.5			518.7
	69	60.0	0.523	5.56	7.73	0.418	468.5	476.9	485.3	498.7	502.0	510.4	518.8
1	68	58.5	0.498	5.28	8.01	0.897	468.7	477.1	485.5	493.9	502.2	510.6	519.0
i i	67	57.0	0.478	5.02	8.27	0.878	4000	477.0	105.0	1010			
	66	55.5	0.450	1.77	8.52	0.878			1				519.1
	65	54.0	0.428	4.54	8.75	0.342		ļ.					519.2 519.4
	64	52.5	0.407	4.33	8.96	0.326							519.5
	63	51.0	0.386	4.12	9.17	0.310	1	1					519.6
	62	49.5	0.367	8.91	9.88	0.294		Į.			-	1	519.7
	61	48.0	0.849	3.71	9.58	0.279	469.6	1	ı				519.9
	60	46.5	0.331	3.51	9.78	0.264	469.7	478.1	486.6	494.9	503.2	511.5	520.0
						1	l						
88	88	88.0	1.286	13.68	0.00	1.000							513.1
{	87	86.5	1.228	13.06	0.62	0.954							513.4
	86	85.0	1.171	12.46	1.22	0.911			•				513.9
	85 84	88.5 82.0	1.118 1.067	11.88	1.80	0.868							514.2
	88	80.5	1.017	11.34 10.81	2.34 2.87	0.829	l					•	514.5
	82	79.0	0.970	10.31	3.37	0.754							514.8 515.0
	-		0.010	10.01		0.101	405.2	475.5	401.0	450.1	490.4	500.7	515.0
]	81	77.5	0.925	9.88	3.85	0.718	465.5	473.8	482.1	490.4	498.7	507.0	515.3
	80	76.0	0.882	9.87	4.31	0.685	465.8	474.1	482.4	490.7	499.0	507.3	515.6
	79	74.5	0.840	8.93	4.75	0.658	466.1	474.4	482.7	491.0	499.3	507.6	515.9
	78	78.0	0.801	8.50	5.18	0.621				491.2	499.5	507.8	516.2
	77	71.5	0.763	8.09	5.59	0.591			1				516.4
	76	70.0	0.727	7.71	5.97	0.563							516.6
	75	68.5	0.692	7.84	6.34	0.587	466.8	475.1	423.4	491.7	500.1	508.4	516.8
	74	<i>6</i> 7.0	0.659	6.99	6.69	0.511	467.0	475.9	483.6	491.9	500.9	508.6	517.0
	78	65.5	0.628	6.66	7.02	0.487		l		1			517.2
	72	64.0	0.597	6.83	7.35	0.468							517.4
	71	62.5	0.568	6.03	7.65	0.441	467.4	475.7	484.0	492.4	500.8	509.1	517.5
	70	61.0	0.541	5.74	7.94	0.420	467.6	475.9	484.2	492.6	501.0	509.8	517.7
	69	59.5	0.515	5.45	8.23	0.398	467.7	476.0	484.3	492.7	501.2	509.4	517.8
	68	58.0	0.489	5.18	8.50	0.878	467.9	476.2	484.5	492.9	501.3	509.6	518.0
	g-,	56.5	A 100	4.00	0 ==	0.070	100 1	180 -	40 1 -	400	-0	¥00 0	#10 C
	67 66	55.0	0.465 0.442	4.69		0.859	468.1				501.5		518.2
- 1	65	58.5	0.421	4.47	•	0.842 0.826	468.2 468.3		484.8 484.9		501.6		518.3 518.4
- 1	64	52.0	0.400	4.25			468.4			493.8 498.4	501.7 501.8		518.5
- 1	63	50.5	0.380	4.04	I		468.6	,		493.6	502.0		518.7
	62	49.0	0.361	8.83			468.7				502.1		518.8
-	61	47.5	0.343			0.265			485.5				518.9
	-												

of 7	ding Ther- neter.	Temp.	Force of	of V	ight apor Reqd.	Hu- midity,		Weigh	in Grain	s of a Cu	ıbic Foot	of Air.	
	shr.	Dew- Point,	Vapor	In a Cubic	for Sat'n.	Batura-	1	Height o	of the Bas	rometer i	n Englis	h Inches	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- ble Ft. of Air.	tion — 1.000.	28.0	28.5	29.0	29.5	30.0	80.5	31.0
89	o 89	89.0	in. 1.826	gr. 14.08	gr 0.00	1.000	gr. 462.4	gr. 470.6	gr. 478.9	gr. 487.1	gr. 495.4	508.6	gr. 511.9
	88	87.5	1.266	18.44	0.64	0.954	462.7	470.9	479.2	487.4	495.7	503.9	512.2
	87	96.0	1.209	12.84	1.24	0.912	468.0	471.2	479.5	487.8	496.1	504.4	512.7
1	86	84.5	1.158	12.24	1.84	0.869	463.8	471.5	479.8	488.1	496.4	504.7	518.0
	85	88.0	1.101	11.68	2.40	0.880	468.6	471.8	480.1	488.4	496.7	505.0	513.3
	84	81.5	1.050	11.18	2.95	0.791	464.0	472.2	480.5	488.8	497.1	505.4	513.7
	88	80.0	1.001	10.62	8.46	0.754	464.2	472.5	480.8	489.1	497.4	505.7	514.0
	82	78.5	0.955	10.13	3.96	0.719	464.4	472.7	481.0	489.8	497.6	505.9	514.2
	81	77.0	0.910	9.66	4.42	0.686	464.7	473.0	481.3	489.6	497.9	506.2	514.5
	80	75.5	0.868	9.20	4.88	0.653	464.9	473.2	481.5	489.8	498.1	506.4	514.7
	79	74.0 72.5	0.827 0.787	8.77 8.35	5.31 5.73	0.628	465.2 465.4	478.5 478.7	481.8 482.0	490.1 490.3	498.4	506.7 506.9	515.0
	78 77	71.0	0.751	7.96	6.12	0.565	465.6	478.9	482.2	490.5	498.6 498.8	507.1	515-2 515-4
	76	69.5	0.715	7.57	6.51	0.537	465.8	474.1	482.4	490.7	499.0	507.8	515.7
	75	68.0	0.681	7.21	6.87	0.512	466.0	474.8	482.6	490.9	499.2	507.5	515.8
	74	66.5	0.648	6.87	7.21	0.488	466.2	474.5	482.8	491.1	499.4	507.7	516.0
	73	65.0	0.617	6.54	7.54	0.465	466.8	474.6	482.9	491.2	499.6	507.9	516.8
1 1	72	63.5	0.588	6.22	7.86	0.442	466.5	474.8	488.1	491.4	499.8	508.1	516.5
li	71	62.0	0.559	5.91	8.17	0.420	466.7	475.0	488.3	491.7	500.0	508.3	516.7
	70	60.5	0.532	5.62	8.46	0.899	466.8	475.1	488.4	491.8	500.1	508.4	516.8
	69	59.0	0.506	5.35	8.73	0.880	467.0	475.8	488.6	492.0	500.8	508.6	517.0
	68	57.5	0.481	5.08	9.00	0.861	467.1	475.4	488.7	492.1	500.4	508.7	517.1
	67	56.0	0.458	4.84	9.24	0.348	467.2	475.5	483.8	492.2	500.5	508.8	517.2
1 1	66	54.5	0.435	4.61	9.47	0.827	467.4	475.7	483.9	492.4	500.7	509.1	517.4
	65	58.0	0.414	4.89	9.69	0.812	467.5	475.8	484.1	492.5	500.8	509.2	517.5
	64	51.5	0.893	4.17	9.91	0.296	467.6	475.9	484.2	492.6	500.9	509.3	517.6
	63 62	50.0 48.5	0.878 0.855	8.96 8.76	10.12 10.82	0.281 0.267	467.7	476.1 476.2	484.3 484.4	492.7 492.8	501.0 501.1	509.4 509.5	517.7 517.8
90	90	90.0	1.868	14.50	0.00	1.000	461.8	469.5	477.8	486.0	494.8	502.5	510.8
	89	88.5	1.306	13.84	0.66	0.954	461.6	469.8	478.1	486.3	494.6	502.8	511.1
1	88	87.0	1.247	18.22	1.28	0.910	462.0	470.2	478.5	486.7	495.0	503.2	511.5
	87	85.5	1.190	12.61	1.89	0.870	462.3	470.5	478.8	487.0	495.8	503.5	511.8
	86	94.0	1.136	12.03	2,47	0.880	462.7	470.9	479.2	487.4	495.7	503.9	512.1
	85	82.5	1.088	11.47	3.08	0.791	463.0	471.2	479.5	487.7	496.0	504.2	512.5
	84	81.0	1.084	10.94	8.56	0.755	468.2	471.5	479.8	488.0	496.8	504.5	512-8
	88	79.5	0.986	10.48	4.07		468.4	471.7	480.0	488.2	496.5	504.7	518.0
	82	78.0	0.940	9.95	4.55		468.7	472.0	480.8	488.5	496.8	505.0	518.8
	81	76.5	0.896	9.48	5.02		464.0	472.8	480.6	488.8	497.1	1	
	80 79	75.0	0.854	9.08 8.61	5.47 5.89		464.2 464.3	472.5 472.6	480.7 480.9	488.9 489.1	497.8	505.5 505.7	518.9 514.1
	79	78.5 72.0	0.776	8.20	6.80	0.565	464.5	472.8	481.1	489.3	497.7	ı	514.3
	77	70.5	0.789	7.80	1		l .		481.8		497.9	1	1

	ading Ther-	Temp.	Toros	Wed of V		Hu-		Weigh	in Grab	ns of a Co	ible Foot	of Air.	
	meter, ahr.	of Dew- Point.	of Vapor in	In a	Reqd. for Sat'n.	midity, Satura- tion =		Height o	f the Bu	ometer i	n English	Inches.	
Dry.	Wet.	Fahr.	Hnglish Inches.	Foot of Air.	ofaCu- bic Ft. of Air.	1.000.	28.0	in. 28.5	in. 29. 0	29.5	80.0	30.5	31.0
90	Ϋ́	70.5	in. 0.739	gr. 7.80	gr. 6.70	0.588	464.7	₽. 478.0	€7. 481.8	gr. 489.5	gt. 497.9	gr. 506.1	gr. 514.5
	76	69.0	0.704	7.48	7.07	0.512	465.0	478.8	481.6	489.8	498.2	506.4	514.8
1	75	67.5	0.670	7.08	7.42	0.488	465.2	478.5	481.8	490.0	498.4	506.6	515.0
1	74	66.0	0.638	6.74	7.76	0.465	465.4	478.7	482.0	490.2	498.6	506.8	515.2
	78	64.5	0.607	6.42	8.06	0.448	465.6	478.9	482.2	490.4	498.8	507.0	515.4
ļ .	72	63.0	0.578	6.10	8.40	0.421	465.7	474.0	482.8	490.5	498.9	507.1	515.5
	71	61.5	0.550	.789 7.80 .704 7.48 .670 7.08 .688 6.74 .607 6.42 .578 6.10	8.69	0.400	465.9	474.2	482.5	490.7	499.1	507.3	515.7
	70	60.0	0.523	5.52	8.98	0.881	466.1	474.4	482.8	491.0	499.8	507.5	515.9
	69	58.5	0.498	5.25	9.25	0.862	466.2	474.5	482.9	491.1	499.4	507.6	516.0
l	68	57.0	0.478	4.99	9.51	0.344	466.4	474.7	488.1	491.3	499.6	507.8	516.2
	67	55.5	0.450	4.74	9.76	0.827	466.5	474.8	488.2	491.4	499.7	507.9	516.8
l	66	54.0	0.428	4.52	9.98	0.312	466.6	474.9	488.3	491.5	499.8	508.0-	516.4
	65	52.5	0.407	4.80	10.20	0.297	466.7	475.0	488.4	491.6	499.9	508.1	516.5
1	64	51.0	0.886	4.09	10.41	0.282	466.9	475.2	488.6	491.8	500.1	508.8	516.6
K	68	49.5	0.867	8.90	10.60	0.269	467.0	475.8	488.7	491.9	500.2	508.4	516.7

TABLE XIII.

PACTORS FOR COMPUTING THE FORCE OF VAPOR, FROM THE BRADINGS OF THE PSYCHROMETER, BY APJOHN'S FORMULA.

Dr. APJOHN's formula for deducing the force of vapor, and the temperature of the dew-point, from the readings of the Psychrometer, as given in the Proceedings of the Royal Irish Academy for 1840, is

$$f'' = f' - \frac{d}{88} \times \frac{h}{80},$$

when the readings of the wet-bulb thermometer are above 32° Fahr., in which formula

f'' = the force of vapor at the temperature of the dew-point in degrees of Fahr.,

f' = the force of vapor at the temperature of evaporation given by the wet-bulb thermometer,

d = the difference between the readings of the dry and wet thermometers,

h = the height of the barometer in English inches at the time of the observation. When the readings of the wet-bulb thermometer are below 32° Fahr., and the bulb is covered with ice, the formula becomes

$$f'' = f' - \frac{d}{96} \times \frac{h}{80}.$$

The factors in the following table, which is taken from the Greenwich Observations for 1843, represent $\frac{d}{58} \times \frac{1}{50}$ and $\frac{d}{56} \times \frac{1}{50}$, computed for all differences between the wet and dry bulb thermometers, or values of d, from 0° to 21°.

USE OF THE TABLE.

To find out the force of vapor in the air, and the temperature of the dew-point, by means of these factors, let the factor corresponding to d, or the difference between the wet and dry thermometer in the first column, be multiplied into the observed height of the barometer, and subtract the result from the force of vapor, in Table XI., due to the temperature of evaporation, indicated by the wet-bulb thermometer; the rest is the force of vapor in the air at the time of the observation; and the temperature of the dew-point is that which is due to it in Table XI.

EXAMPLE.

The observation gives,

Dry-bulb thermometer = 79° Fahr., or the temperature of the air.

Wet-bulb " = 69° " or temperature of evaporation.

Difference 10°

Height of barometer 29.7 English inches.

In the Table, 2d part, is found, — factor for a difference of $10^{\circ} = 0.00379 \times 29.7$, or height of barometer = 0.113, which, subtracted from the force of vapor due to 69°, in Table XI., = 0.704 — 0.113, gives force of vapor in the air = 0.591 inches, and temperature of the dew-point 62°.5.

When the temperature of the wet bulb is below 32° Fahrenheit, the factors in the first part of the Table must be used.

xiii. Pactor $\frac{d}{2d} \times \frac{1}{2d}$, for computing the force of vapor by apjohn's formula.

Below 320 Fahrenheit; the Wet Bulb covered with a Film of Ice.

d, or Difference		Tenths of Degrees.									
of Wet and Dry Bulb Thorm.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.	
	-						0.0000	0.00004	0.0000	A 00000	
0	11	1		ı	0.00014						
1	.00084	.00037	.00041	.00044			.00054		1	.00064	
2	.00068	.00071	.00075	.00078	.00081	.00085	.00088	.00092	.00095	.00099	
3	.00102	.00105	.00109	.00112	.00116	.00119	.00122	.00126	.00129	.00188	
4	.00136	.00129	.00148	.00146	.00150	.00158	.00156	.00160	.00163	.00167	
5	.00170	.00178	.00177	.00180	.00184	.00187	.00190	.00194	.00198	.00201	
6	.00204	.00207	.00211	.00214	.00218	.00221	.00224	.00228	.00231	.00235	
7	.00238	.00241	.00245	.00248	.00252	.00255	.00258	.00262	.00265	.00269	
8	.00272	.00275	.00279	.00282	.00285	.00289	.00292	.00296	.00299	.00302	
9	.00206	.00309	.00218	.00316	.00319	.00323	.00326	.00380	.00833	.00887	
10	.00340	.00348	.00847		1	.00857	.00860		.00867	.00370	
~~				123000	1				,		

FACTOR $\frac{d}{80} \times \frac{1}{80}$.

Reading of Wet-Bulb Thermometer above 82º Fahrenheit.

d, or Difference					Tenths o	l Degrees.				
of Wet and Dry Bulb Therm.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
°	0.00000	0.00004	0.00008	0.00011	0.00015	0.00019	0.00028	0.00027	0.00080	0.00084
1	.00038	.00042		.00049	.00058	.00057	.00061	.00064	.00068	.00072
2	.00076	.00080	.00068	.00087	.00091	.00095	.00098	.00102	.00106	.00110
8	.00114	.00118			.00129	.00182	.00137	.00140		.00148
.4	.00151	.00185	.00159	.00168	.00167	.00171	.00174	.00178	.00182	.00186
5	.00189	-00193	.00197	.00201	.00205	.00209	.00212	.00216	.00220	.00224
6	.00228	.00231	.00235	.00289	.00242	.00246	.00250	.00254	.00258	.00261
7	.00265	.00269	.00278	.00277	.00280	.00284	.00288	.00292	.00295	.00299
8	.00808	.00307	.00211	.00315	.00318	.00822	.00826	.00830	.00338	.00887
9	.00841	.00845	.00349	.00852	.00356	.00860	.00364	.00868	.00871	.00875
10	.00379	.00898	.00386	.00390	.00394	.00398	.00401	.00405	.00409	.00412
11 .	.00416	.00420	.00424	.00428	.00482	.00486	.00489	.00448	.00447	.00451
12	.00454	.00458	.00462	.00466	.00470	.00474	.00477	.00481	.00485	.00489
18	.00498	.00496	.00500	.00504	.00508	.00511	.00515	.00519	.00522	.00526
14	.00580	.00584	.00538	.00541	.00545	.00549	.00558	.00556	.00560	.00564
15	.00568	.00572	.00576	.00580	.00584	.00587	.00591	.00595	.00598	.00602
16	.00606	.00610	.00614	.00618	.00622	.00625	.00629	.00633	.00636	.00640
17	.00644	.00648	.00652	.00655	.00659	.00663	.00666	.00670	.00674	.00678
18	.00682	.00686	.00690	.00693	.00697	.00701	.00704	.00708	.00712	.00716
19	.00720	.00724	.00728	.00781	.00785	.00789	.00742	.00746	.00750	.00754
20	.00758	.00761	.00765	.00769	.00778	.00777	.00780	.00781	.00788	.00792

TABLE XIV.

In the Greenwich Magnetic and Meteorological Observations for 1842 and 1843, Mr. Glaisher discussed the relation between the temperature of evaporation given by the Wet-bulb Thermometer and the temperature of the Dew-Point as given by Daniell's Hygrometer. Comparing the observations taken simultaneously every six hours with the Psychrometer, and with Daniell's Dew-Point Hygrometer, and dividing the average difference between the temperatures of the Wet and Dry bulb by the average difference of the temperature of the Dew-Point and of the Air, he obtained the empirical factors given in the following Table.

The observations from which they are deduced are those taken at the Observatory in the years 1841 to 1845, for the temperatures below 35° F., and in the years 1841 to 1843, for the temperatures above 35° F.

The observations made at Toronto Observatory, Canada West, in similar circumstances, in the years 1840 to 1842, were also compared in the same manner, and the factors derived from them showed a very close accordance for temperatures above 30° F., but were found smaller at temperatures below 30° F.

The errors in the temperature of the Dew-Point, which may result by using the Greenwich factors, though frequently within half a degree, often amount, however, to \pm 2 or 3 degrees, and, in extreme cases, to \pm 4 or 5 degrees, as shown in the volume of the *Greenwich Observations* for 1842, p. 60 of the *Abstracts*.

Use of the Table.

Multiply the difference between the Wet-bulb and Dry-bulb Thermometers by the factor standing in the Table opposite the reading of the Dry-bulb, and subtract the product from the reading of the Dry-bulb; the remainder will be the temperature of the Dew-Point.

Example. — Dry-bulb = 62° F.; Wet-bulb = 55°; Difference = 7°.

Opposite 62°, in the first column, stands the factor 1.7, which multiplied by 7°, the difference, gives 11°.9, to be subtracted from the Dry-bulb; or $62^{\circ} - 11^{\circ}.9 = 50^{\circ}.1$, temperature of the Dew-Point.

XIV. FACTORS TO FIND OUT THE TEMPERATURE OF THE DEW-POINT FROM THE READINGS OF THE PSYCHROMETER. — GLAISHER.

Dry-Bulb Therm. Fabren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.
21°	8.5	85°	2.6	49°	2.2	63°	1.7	77°	1.5
22	8.5	86	2.6	50	2.1	64	1.7	78	1.5
28	8.5	87	2.5	51	2.1	65	1.7	79	1.5
24	7.8	88	2.5	52	2.0	66	1.6	80	1.5
25	6.4	89	2.5	58	2.0	67	1.6	81	1.5
26	6.1	40	2.4	54	2.0	68	1.6	82	1.5
27	5.9	41	2.4	55	2.0	69	1.5	83	1.5
28	5.7	42	2.4	56	1.9	70	1.5	84	1.5
29	5.0	48	2.4	57	1.9	71	1.5	85	1.5
30	4.6	44	2.3	58	1.9	72	1.5	86	1.5
81	3.6	45	2.3	59	1.8	78	1.5	87	1.5
82	3.1	46	2.8	60	1.8	74	1.5	88	1.5
33	2.8	47	2.2	61	1.8	75	1.5	89	1.5
84	2.6	48	2.2	62	1.7	76	1.5	90	1.5

XV. WEIGHT OF VAPOR, IN GRAINS TROY, CONTAINED IN A CUBIC FOOT OF SATURATED AIR, AT TEMPERATURES BETWEEN 0° AND 94° FAHRENHEIT.

From the Greenwich Observations.

Temper- ature of Air, Fahren.	Weight of Vapor, in Grains.	Temper- ature of Air, Fahren.	Weight of Vapor, in Grains.	Temper- ature of Air, Fahren.	Weight of Vapor, in Grains.	Temper- ature of Air, Fahren.	Weight of Vapor, in Grains.	Temper- ature of Air, Fahren.	Weight of Vapor, in Grains.
00	0.78	19°	1.52	38°	2.89	57°	5.84	76°	9.60
1	0.78	20	1.58	39	2.99	58	5.51	77	9.89
_				40		59	5.69		
2	0.84	21	1.63		2.09			78	10.19
3	0.87	22	1.69	41	8.19	60	5.87	79	10.50
4	0.90	23	1.75	42	8.80	61	6.06	80	10.81
5	0.98	24	1.81	48	8.41	62	6.25	81	11.14
6	0.97	25	1.87	44	3.52	63	6.45	82	11.47
7	1.00	26	1.93	45	3.64	64	6.65	83	11.82
8	1.04	27	2.00	46	3.76	65	6.87	84	12.17
9	1.07	28	2.07	47	3.88	66	7.08	85	12.58
10	1.11	29	2.14	48	4.01	67	7.80	86	12.91
11	1.15	30	2.21	49	4.14	68	7.58	87	18.29
12	1.19	81	2.29	50	4.28	69	7.76	88	13.68
13	1.24	32	2.87	51	4.42	70	8.00	89	14.08
14	1.28	88	2.45	52	4.56	71	8.25	90	14.50
15	1.32	84	2.58	58	4.71	72	8.50	91	14.91
16	1.87	85	2.62	54	4.86	78	8.76	92	15.33
17	1.41	86	2.71	55	5.02	74	9.04	98	15.76
18	1.47	87	2.80	56	5.18	75	9.31	94	16.22

XVI. FACTORS TO DEDUCE THE WEIGHT OF VAPOR CONTAINED IN A CUBIC FOOT OF AIR, AT THE TIME OF A GIVEN OBSERVATION, FROM THE INDICATIONS OF DEW-POINT INSTRUMENTS. — GREENW. OBS.

t - Temperature of Air; t" - Temperature of Dew-Point.

Difference or t—t".	Factors.	Difference or t-t".	Factors.	Difference or t—t#.	Pactors.	Difference or t — t".	Factors.	Difference or t—t".	Factors.
1	0.999	9	0.982	17	0.966	25	0.951	88	0.985
2	0.996 '	10	0.980	18	0.964	26	0.949	84	0.984
8	0.994	11	0.978	19	0.962	27	0.947	35	0.982
4	0.992	12	0.976	20	0.960	28	0.945	36	0.980
5	0.990	13	0.974	21	0.958	29	0.948	37	0.929
6	0.988	14	0.972	22	0.956	80	0.942	88	0.927
7	0.986	15	0.970	23	0.954	31	0.939	39	0.925
8	0.984	16	0.968	24	0.952	82	0.937	40	0.923

Use of Table XVI. — The difference between the temperatures of the air and of the Dew-Point being known, multiply the factor in the Table corresponding to that difference into the weight of a cubic foot of vapor at the temperature of the Dew-Point, as given in Table XV., and the product will be the weight of vapor in a cubic foot of air at the time of the observation.

Example. — Temperature of air = 60° F.; Dew-Point = 52° ; Diff. = 8° .

Table gives for a difference of 8°, factor 0.984; Table XV. gives weight of a cubic foot of vapor at temperature $52^{\circ} = 4.5^{\circ}.56$.

Hence, $0.984 \times 4.56 = 4^{\circ}.49$, the weight of vapor required.

TABLE XVII.

FOR COMPARING THE WEIGHT OF A CUBIC POOT OF DRY AND OF SATURATED AIR.

This table is composed of two tables found in the Greenwich Meteorological Observations for 1842, pages xlvi. and li.; the first containing the weight of a cubic foot of dry air, under a barometric pressure of 30 inches, at temperatures between 0° and 90° F.; the other giving the weight of a cubic foot of saturated air under the same barometric pressure and temperature, together with the excess of the first above the last.

The weight of a cubic foot of dry air, on which the tables are based, is assumed to be 563 grains Troy, being a mean value, in round numbers, between the determinations of Shuckburgh, which is 557.7295 grains, and that of Biot and Arago, 568.7013. The true mean is 563.2154, but 563 is the number used in the calculations.

The coefficient of the expansion of the air is that of Gay-Lussac, viz. 0.00375 for 1° Centigrade, or 0.002083 of its bulk for 1° Fahrenheit.

Use of the Table.

This table shows the amount of buoyancy imparted to the air by the addition of moisture; and from it, the temperature and the relative humidity of the air being known, the weight of a cubic foot of air, in the actual condition of the atmosphere at the time of an observation, can be deduced.

It suffices to take in the fourth column, headed "Excess," the quantity corresponding to the temperature of the air in the first, multiply it into the given Relative Humidity, and subtract the product from the number in the second column. The result will be the weight of a cubic foot of air at the existing temperature and moisture, under a barometric pressure of 30 inches.

This result will be reduced to its true value, under the barometric pressure given by the observation, by multiplying it by $\frac{\text{Height of Barometer}}{30}$.

Example.

The temperature of the air is 60° F.; the relative humidity, 0.852; the barometer reads 29 inches.

The table gives, for temperature of air, 60° ; excess, $3.35 \times 0.852 = 2.85$, which, subtracted from 531.91 in the second column, = 529.12, weight of a cubic foot of air under 30 inches of pressure; and $529.12 \times \frac{29 \text{ inch}}{30} = 511.48$, the weight of a cubic foot of air in the given conditions of temperature, moisture, and barometric pressure.

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XVII. FOR COMPARING THE WEIGHT OF A CUBIC FOOT OF DRY AND OF SATURATED AIR,

AT TEMPERATURES BETWEEN 0° AND 90° FAHRENHEIT.

From the Greenwich Observations.

Status Of a cubble Depth	Graina 3.85 3.45 3.78 3.88 4.01 4.14 4.26 4.41	ofa cubic foot of Saturated Air. Grains. 528.62 527.48 526.82 525.17 524.08 522.90 521.75 520.61	Grains. 581.97 580.98 529.88 529.84 527.81	60 61 62 63	Grains. 1.27 1.81 1.86 1.42	of a cubic foot of Saturated Air. Grains. 564.08	of a cubic foot of Dry Air. Grains. 565.85	ature Fahren.	of Dry Air.	of a cubic foot of Saturat- ed Air.	of a cubic foot of Dry Air.	stare Pahren.
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11 593.75 588.07 0.68 41 552.65 550.80 1.84 71 520.70 516.02 4 12 537.43 586.78 0.70 42 551.52 549.68 1.89 72 519.69 514.87 4 13 586.21 585.49 0.72 43 550.39 548.44 1.95 73 518.70 513.75 4 14 584.94 584.18 0.75 44 549.27 547.26 2.01 74 517.70 512.61 5 15 593.67 582.89 0.78 45 548.16 546.06 2.10 75 516.71 511.46 5 16 532.41 581.61 0.80 46 547.05 544.88 2.17 76 515.78 510.32 5 17 581.15 580.38 0.82 47 545.97 548.75 2.22 77 514.74 509.18 5 18 579.91 579.06 0.85 48 544.85 542.55 2.30 78 513.77 508.04 5	4.00	E10 10	K07.00	-		770 OO			0.01	¥00.40	¥00 04	10
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15 593.67 582.89 0.78 45 548.16 546.06 2.10 75 516.71 511.46 5 16 592.41 581.61 0.80 46 547.05 544.88 2.17 76 515.78 510.32 5 17 581.15 580.38 0.82 47 545.97 548.76 2.22 77 514.74 509.18 5 18 579.91 579.06 0.85 48 544.85 542.55 2.30 78 513.77 508.04 5	5.09											
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17 581.15 580.38 0.82 47 545.97 548.75 2.22 77 514.74 509.18 5 18 579.91 579.06 0.85 48 544.85 542.55 2.30 78 518.77 508.04 5	5.25	511.46	516.71	75	2.10	546.06	548.16	45	0.78	582.89	593.67	15
18 579.91 579.06 0.85 48 544.85 542.55 2.30 78 513.77 508.04 5	5.41	510.82	515.78	76	2.17	544.88	547.05	46	0.80	581.61	532.41	16
	5.56	509.18	514.74	77	2.22	548.75	545.97	47	0.82	580.33	581.15	17
10 2 0 0 0 2 0 0 0 0 0 0 0 0 0 0 0 0	5.78	508.04	518.77	78	2.30	542.55	544.85	48	0.85	579.06	579.91	18
13 5/5.67 5/7.79 0.00 49 545.75 541.56 2.89 79 512.60 506.91 5	5.89	506.91	512.80	79	2.89	541.86	543.75	49	0.88	577.79	578.67	19
	6.08											
	6.26											
	6.44			1								
	6.61 6.81			1					1 .			
A1 072.00 071.00 1.00 04 080.00 080.00 Z.78 34 007.87 001.10 0	0.51	201.10	507.87	04	2.78	080.00	D95.98	04	1.00	371.00	072.00	44
25 571.33 570.26 1.07 55 537.27 534.39 2.88 85 507.03 500.05 6	6.98	500.05	507.03	85	2.88	584.89	537.27	55	1.07	570.28	571.88	23
	7.20											
	7.40			1	1 1			1	1			
	7.61											
	7.81	495.44		89	3.26	529.77	538.03	59	1.28	565.31	566.54	29
\$0 565.35 564.08 1.27 60 531.97 528.62 8.35 90 502.32 494.28 8	8.04	494.28	502.32	90	8.35	528.62	531.97	60	1.27	564.08	565.85	80
	0.04			1				1			1	1

TABLE XIV'.

Mr. Glaisher published in London, in 1856, another series of Hygrometrical Tables, which were unknown to the writer when the Second Edition of this volume was issued. They are based on Regnault's Table of Elastic Forces of Vapor, and on the coefficient of the expansion of the air as determined by the same physicist. Psychrometrical Table, however, is not computed from Regnault's formula, but by first finding out, in the manner described on page 140, the temperatures of the dewpoint from the readings of the Psychrometer, by means of the empirical factors given below, in Table XIV'., and then taking the corresponding values of the force of vapor from Regnault's table. These factors have been derived from the combination of all simultaneous observations of the dry and wet bulb thermometers with those of Daniell's hygrometer, taken at the Royal Observatory, Greenwich, from the year 1841 to 1854, with some observations taken at high temperatures in India, and others at low and medium temperatures at Toronto; they are, therefore, more correct than those given in Table XIV. page 140. The results in this new Psychrometrical Table, nevertheless, by no means entirely coincide with those given by the formula, as a comparison with those in Table VII. will show.

xiv'. Factors to find out the temperature of the dew-point from the readings of the psychrometer. — Glaisher.

Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.
, 10	8.78	° 28	7.10	o 46	2.14	64	1.88	82	1.67
11	8.78	29	5.12 4.68	47	2.14	65	1.82	88	1.67
12	8.78	80 BO	4.15	48	2.12	66	1.81	84	1.66
18	8.77	81	8.70 ·	49	2.10	67	1.80	85	1.65
		1 1		50		68		86	
14	8.76	82	8.82	50	2.06	68	1.79	86	1.65
15	8.75	83	8.01	51	2.04	69	1.78	87	1.64
16	8.70	84	2.77	52	2.02	70	1.77	88	1.64
17	8.62	85	2.60	58	2.00	71	1.76	89	1.63
18	8.50	36	2.50	54	1.98	72	1.75	90	1.63
19	8.84	37	2.42	55	1.96	78	1.74	91	1.62
						1			
20	8.14	38	2.36	56	1.94	74	1.78	92	1.62
21	7.88	89	2.32	57	1.92	75	1.72	98	1.61
22	7.60	40	2.29	58	1.90	76	1.71	94	1.60
28	7.28	41	2.26	59	1.89	77	1.70	95	1.60
24	6.92	42	2.28	60	1.88	78	1.69	96	1.59
25	6.52	48	2.20	61	1.87	79	1.69	97	1.59
26	6.08	41	2.18	62	1.86	80	1.68	98	1.58
27	5.61	45	2.16	68	1.85	81	1.68	99	1.58
28	5.12	46	2.14	64	1.88	82	1.67	100	1.57

MISCELLANEOUS TABLES, .

FOR

COMPARING THE HYGROMETRICAL RESULTS OBTAINED BY DIFFERENT AUTHORITIES.

В



MISCELLANEOUS TABLES.

THE object of these Tables is to afford the means of comparing the different determinations of the hygrometrical elements which have been obtained, or adopted, by various physicists, especially the values of the elastic forces of vapor given in other tables than those contained in the preceding pages.

Table XVIII., giving the elastic forces of vapor, expressed in millimetres of mercury, for Centigrade temperatures, was calculated by August from Dalton's experiments, and reduced to French measures in the translation of Kaemtz's *Meteorology*, by Chas. Martins, page 70, from which it has been taken. On these values are based the first psychrometrical tables published by August, in Berlin, 1825.

Table XIX. is the table computed by Kaemtz from his own experiments. It is found, reduced to French measures, in the same volume, page 68.

Table XX. furnishes the results of the experiments made by Professor Magnus, in Berlin, and published in Poggendorf's *Annalen*, Tom. LXI. p. 226, and also in the *Annales de Chimie et de Physique*, 3^{mo} série, Tom. XII. p. 88, from which this table was copied.

Table XXI. has been published by the Committee of Physics and Meteorology of the Royal Society, in their Report on the Objects of Scientific Inquiry in these Sciences, London, 1840, p. 89. The values which it contains are not derived from new experiments, but are probably computed from those existing at that time.

Table XXII. furnishes a synoptic view of the differences in the values of the force of vapor adopted by various authorities, prepared with the view of facilitating their comparison. A reference to their respective origin will be found below, page 152.

Table XXIII., showing the weight, in grammes, of the vapor contained in a cubic metre of saturated air, at different temperatures, is taken from Pouillet's *Eléments de Physique*, Tom. II. p. 707.

Table XXIV. gives the weights as derived from August's experiments, in Kaemtz's *Vorlesungen über Meteorologie*. The table is copied from the French translation, by Martins, page 73. The tensions have been added, opposite the weights, and are extracted from August's table.

Table XXV. is found in Biot's Traité de Physique, Tom. I. p. 583.

XVIII. ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN MILLIMETRES OF MERCURY FOR EVERY TENTH OF A CENTIGRADE DEGREE.

CALCULATED BY AUGUST.

Centigrade					Tenths o	Degrees.				
Degrees.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Milim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
-81	0.45	0.45	0.45	0.44	0.44	0.48	0.48	0.42	0.42	0.41
-30	0.50	0.49	0.49	0.48	0.48	0.47	0.47	0.46	0.46	0.45
-29	0.54	0.54	0.54	0.58	0.58	0.52	0.52	0.51	0.51	0.50
-26	0.59	0.58	0.58	0.57,	0.57	0.56	0.56	0.55	0.55	0.54
-27	0.68	0.68	0.63	0.62	0.62	0.61	0.61	0.60	0.60	0.59
-26	0.70	0.69	0.68	0.68	0.67	0.66	0.66	0.65	0.64	0.64
· -25	0.77	0.76	0.75	0.75	0.74	0.73	0.78	0.72	0.71	0.71
-24	0.88	0.83	0.82	0.82	0.81	0.80	0.80	0.79	0.78	0.78
-28	0.90	0.89	0.88	0.88	0.87	0.86	0.86	0.85	0.84	0.84
-22	0.99	0.96	0.97	0.96	0.95	0.95	0.94	0.98	0.92	0.91
	1.06	107								
-21 -20	1.15	1.05 1.14	1.04	1.04	1.03	1.02	1.02	1.01	1.00	1.00
	1.15		1.13	1.12	1.11	1.11	1.10	1.09	1.08	1.07
-19 -18	1.33	1.25 1.32	1.24 1.81	1.23 1.81	1.22	1.21 1.29	1.20 1.29	1.18 1.28	1.17 1.27	1.16
-16 -17	1.44	1.48	1.42	1.41	1.40	1.29	1.38	1.26	1.35	1.27 1.34
-1,	1.44	1.40	1.72	1.41	1.40	1.39	1.00	1.50	1.35	1.04
-16	1.56	1.54	1.58	1.52	1.51	1.50	1.49	1.47	1.46	1.45
-15	1.69	1.68	1.67	1.65	1.64	1.68	1.61	1.60	1.59	1.67
-14	1.80	1.79	1.78	1.77	1.76	1.75	1.74	1.72	1.71	1.70
-13	1.96	1.94	1.93	1.91	1.89	1.88	1.86	1.85	1.88	1.82
-12	2.12	2.10	2.09	2.07	2.05	2.04	2.02	2.01	1.99	1.98
			Ì	1		ł				
-11	2.80	2.28	2.26	2.25	2.28	2.21	2.19	2.17	2.16	2.14
-10	2.48	2.46	2.44	2.48	2.41	2.89	2.87	2.85	2.34	2.32
– 9	2.66	2.64	2.62	2.61	2.59	2.57	2.55	2.58	2.52	2.50
-8	2.86	2.84	2.82	2.80	2.78	2.76	2.74	2.72	2.70	2.68
-7	8.09	3.06	3.04	3.02	3.00	2.97	2.95	2.98	2.91	2.88
6	8.82	3.29	3.27	8.25	3.22	8.20	3.18	3.16	3.14	8.11
5	8.56	8.56	8.54	8.51	3.48	8.46	8.48	3.40	8.37	3.35
-4	2.88	3.80	8.78	3.75	8.72	8.70	3.67	8.64	8.61	3.59
-8	4.11	4.07	4.05	4.02	8.99	8.97	3.94	8.91	8.88	3.86
-2	4.40	4.87	4.84	4.83	4.29	4.26	4.28	4.20	4.17	4.14
						ł				
-1	4.71	4.68	4.65	4.62	4.59	4.56	4.58	4.49	4.46	4.43
-0	5.05	5.01	4.98	4.95	4.91	4.88	4.85	4.81	4.78	4.74
+0	5.05	5.09	5.12	5.16	5.19	5.28	5.27	5.80	5.84	5.37
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Contigrade					Tenths of	Degrees.				
Degroes.	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.
•	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
ĭ	5.41	5.45	5.49	5.52	5.56	5.60	5.64	5.68	5.72	5.75
2	5.80	5.84	5.88	5.92	5.96	6.00	6.04	6.08	6.13	6.17
8	6.20	6.24	6.29	6.33	6.87	6.41	6.46	6.50	6.54	6.59
4	6.63	6.68	6.72	6.77	6.81	6.86	6.90	6.95	6.99	7.04
5	7.08	7.18	7.18	7.23	7.28	7.38	7.88	7.43	7.48	7.58
6	7.58	7.63	7.68	7.74	7.79	7.84	7.89	7.94	7.99	8.05
7	8.10	8.15	8.21	8.26	8.82	8.87	8.43	8.48	8.53	8.59
8	8.64	8.70	8.76	8.82	8.87.	8.93	8.99	9.05	9.11	9.17
9	9.23	9.80	9.26	9.48	9.50	9.57	9.63	9.70	9.77	9.84
10	9.90	9.96	10.02	10.08	10.14	10.20	10.25	10.31	10.87	10.48
11	10.49	10.56	10.63	10.69	10.76	10.83	10.90	10.96	11.03	11.10
12	11.17	11.24	11.81	11.38	11.45	11.52	11.59	11.66	11.73	11.80
13	11.86	11.94	12.02	12.10	12.18	12.26	12.84	12.42	12.50	12.58
14	12.66	12.74	12.82	12.90	12.98	13.05	18.13	13.21	13.29	13.37
15	18.44	13.52	13.61	13.69	13.77	13.86	18.94	14.02	14.11	14.19
16	14.28	7.4.00	,,,,,,	14.56		14.54	7.0.	14.98	15.02	,,,,
17	15.20	14.87 15.29	14.47 15.38	15.46	14.65 15.55	14.74 15.64	14.84 15.78	15.82	15.02	15.11 15.99
18	16.08	16.17	16.27	16.86	16.45	16.54	16.64	16.78	16.82	16.91
19	17.01	17.18	17.25	17.87	17.49	17.61	17.78	17.85	17.97	18.09
20	18.20	18.81	18.43	18.54	18.65	18.76	18.88	18.99	19.10	19.21
21	10.00	70.45	30.50	10.00	10.00	***	00.00	00.15	00.00	00.00
22	19.88 20.51	19.45 20.63	19.56 20.76	19.68 20.88	19.80 21.01	19.92 21.13	20.08 21.25	20.15 21.38	20.27 21.50	20.39 21.63
23	21.75	21.88	22.00	22.13	22.26	22.88	21.25	22.63	22.76	21.63
24	23.01	23.18	28.24	23.86	28.48	23.60	28.71	28.83	23.95	24.07
25	24.18	24.34	24.50	24.67	24.83	24.99	25.15	25.32	25.48	25.64
26	25.81	25.97	26.18	26.28	26.44	26.60	26.76	26.92	27.07	27.23
27 28	27.39 28.96	27.55 29.18	27.71 29.29	27.86 29.46	28.02 29.63	28.18 29.79	28.34 29.96	28.50 30.13	28.65 30.30	28.81 30.46
29	20.63	30.81	20.98	81.16	81.88	81.51	31.69	81.86	82.04	82.21
80	82.89	82.57	32.76	82.94	38.13	33.31	83.50	83.68	33.87	34.05
81	84.24	34.48	\$4.63	34.82	85.02	85.21	85.40	35.60	35.79	85.99
82	86.18	86.38	36.59	36.79	86.99	37.20	87.40	87.60	37.80	38.01
83 34	38.21	28.43	28.64	88.86	39.08	39.29	39,51	89.78	89.94	40.16
34 35	40.38 42.59	40.60 42.82	40.82 43.05	41.04 43.28	41.26 48.51	41.49 43.74	41.71 48.97	41.98 44.20	42.15 44.48	42.37 44.66
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
D		<u> </u>			140				· · · · · · · · · · · · · · · · · · ·	

XIX. ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN MILLIMETRES OF MERCURY, FOR CENTIGRADE TEMPERATURES.

By KARMTZ.

Temper- ature Centi- Grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor,	Temper- ature Centi- grade.	Force of Vapor.
	Millim.		Millim.		Millim.		Millim.		Millim.
-25	0.68	-12	1.92	Ō	4.58	12	10.24	24	21.43
-24	0.72	-11	2.05	1	4.92	18	10.91	25	22.74
-23	0.79	-10	2.21	2	5.26	14	11.62	26	24.16
-22	0.86	- 9	2.39	8	5.64	15	12.88	27	25.56
l 1					•				
-21	0.92	-8	2.57	4	6.01	16	13.17	28	27.07
-20	1.01	-7	2.78	5	6.45	17	14.08	29	28.67
-19	1.10	- 6	2.98	6	6.90	18	14.98	80	80.36
-18	1.20	- 5	3.20	7	7.88	19	15.86	31	32.17
		i 1		li l		i		1	
-17	1.29	- 4	3.45	8	7.89	20	16.87	82	33.95
-16	1.40	- 8	8.70	9	8.41	21	17.91	. 33	85.95
-15	1.51	- 2	8.97	10	9.00	22	19.04	34	87.99
-14	1.62	- 1	4.26	11	9.58	28	20.21	35	40.15
-13	1.76	0	4.58	12	10.24	24	21.43	36	42.40
J		<u> </u>				1			

XX. ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN MILLIMETRES OF MERCURY, FOR CENTIGRADE TEMPERATURES.

By MAGNUS.

Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.
•	Millim.		Millim.		Millim.	•	Millim.		Millim.
-20	0.916	-7	2.671	6	6.939	19	16.345	32	85.419
-19	0.999	-6	2.886	7	7.436	20	17.396	33	87.473
-18	1.089	-5	8.115	8	7.964	21	18.505	84	39.630
-17	1.186	-4	3.361	9	8.523	22	19.675	35	41.893
-16	1.290	-3	8.624	10	9.126	23	20.909	36	44.268
-15	1.403	-2	8.905	11	9.751	24	22.211	37	46.758
-14	1.525	-1	4.205	12	10.421	25	23.582	38	49.368
-13	1.655	0	4.525	13	11.130	26	25.026	89	52.103
-12	1.796	+1	4.867	14	11.882	27	26.547	40	54.964
-11	1.947	2	5.231	13	12.677	28	28.148	41	57.969
				1					
-10	2.109	3	5.619	16	13.519	29	29.832	42	61.109
- 9	2.284	4	6.032	17	14.409	30	81.602	43	64.896
- 8	2.471	5	6.471	18	15.851	81	33.464	44	67.833
	l								

XXL ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN ENGLISH INCHES OF MERCURY, FOR TEMPERATURES OF FAHRENHEIT.

From the Royal Society's Report.

						1	i
Temperature of Air.	Force of Vapor.	Temperature of Air.	Force of Vapor.	Temperature of Air.	Force of Vapor.	Temperature of Air.	Force of Vapor.
Fahrenheit.	Eng. Inches.	Fahrenheit.	Eng Inches.	Fahrenheit.	Eng Inches	Fahrenheit.	Eng. Inches.
0°	0.051	81°	0.179	62°	0.551	93°	1.514
1	0.053	82	0.186	68	0.570	94	1.562
2	0.056	83	0.198	64	0.590	95	1 610
8	0.058	84	0.200	65	0.611	96	1.660
4	0.060	35	0.208	66	0.632	97	1.712
5	0.063	86	0.216	37	0.654	98	1.764
6	0.066	87	0.224	68	0.676	99	1.819
7	0.069	88	0.288	69	0.699	100	1.874
8	0.071	89	0.242	70	0.728	101	1.931
9	0.074	40	0.251	71	0.748	102	1.990
10	0.078	41	0.260	72	0.778	108	2.050
11	0.061	42	0.270	78	0.799	104	2.112
12	0.084	48	0.280	74	0.826	108	2.176
13	0.088	44	0.291	75	0.854	106	2.241
14	0.092	45	0.302	76	0.882	107	2.807
15	0.095	46	0.818	77	0.911	108	2.876
16	0.099	47	0.824	78	0.942	. 109	2.447
17	0.103	48	0.886	79	0.978	110	2.519
18	0.107	49	0.849	80	1.005	111	2.593
19	0.112	50	0.861	81	1.036	112	2.669
20	0.116	51	0.875	82	1.072	113	2.747
21	0.121	52	0.889	88	1.106	114	2.826
22	0.126	58	0.402	84	1.142	115	2.908
28	0.181	54	0.417	85	1.179	116	2.992
24	0.186	55	0.432	86	1.217	117	8.078
25	0.142	56	0.447	87	1.256	118	8.166
26	0.147	57	0.468	88	1.296	119	8.257
27	0.153	58	0.480	89	1.837	1 2 0	8.349
28	0.159	59	0.497	90	1.380	121	8.111
29	0.165	60	0.514	91	1.428	122	3.542
30	0.172	61	0.532	92	1.468	128	8.641
81	0.179	62	0.551	98	1.514	124	3.748

TABLE XXII.

FOR SHOWING THE DIFFERENCES IN THE VALUES OF THE ELASTIC FORCE OF AQUEOUS VAPOR ADOPTED BY DIFFERENT AUTHORITIES.

The following synoptic view of the values of the elastic force of vapor adopted by various authorities, furnishes the means of readily comparing them, and of appreciating the amount of the differences which they exhibit. The values are given both in English and in French measures.

Dalton's values are copied from the Edinburgh Encyclopædia, Art. Hygrometry. Those adopted in the Greenwich Observations are found in the same article, and also in the volumes published annually by that Observatory. Biot's table of tensions is, in fact, the same, computed by Pouillet from Dalton's results, by Biot's formula, and published in Biot's Traité de Physique, Tom. I. p. 531. Dr. Ure's results are taken from his Memoir in the Philosophical Transactions for 1818, p. 347. In the column headed "Daniell" are given the forces of vapor as found in the table published in his Meteorological Essays, 2d edition, p. 596, a table computed by Galbraith, from Dr. Ure's experiments, by the formula of Ivory.

For the columns headed Royal Society, August, Kaemtz, Magnus, and Regnault, see above, p. 147.

XXII. FOR SHOWING THE DIFFERENCES IN THE VALUES OF THE ELASTIC FORCE OF AQUEOUS VAPOR, ADOPTED BY DIFFERENT AUTHORITIES.

FORCE OF VAPOR EXPRESSED IN ENGLISH INCHES FOR TEMPERATURES OF FAHRENHEIT.

Temper-				Ferce of	Vaper acc	ording to				Temper
ature of Air, Fahren- heit.	Dalton.	Green- wich Observa- tions.	Ure.	Daniell.	Royal Society.	August.	Kaemts.	Magnus.	Regnault.	of Air, Fahren- heit.
•	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Mag. In.	Eng. In.	Eng. In.	Eng. In.	•
0	0.064	0.061	••••	0.068	0.051	0.058	0.048	0.044	0.048	0
10	0.090	0.089	••••	0.098	0.078	0.082	0.074	0.070	0.068	10
20	0.129	0.129	• • • •	0.140	0.116	0.124	0.112	0.108	0.108	20
80	0.186	0.186		0.200	0.172	0.184	0.166	0.164	0.167	80
82	0.200	0.1 9 9	0.200	0.216	0.186	0.199	0.180	0.178	0.181	82
40	0.268	0.264	0.230	0.280	0.231	0.269	0.244	0.245	0.248	40
50	0.375	0.378	0.360	0.400	0.861	0.390	0.854	0.359	0.861	50
60	0.524	0.523	0.516	0.560	0.516	0.547	0.505	0.517	0.518	60
70	0.721	0.727	0.726	0.770	0.728	0.766	0.710	0.788	0.783	70
80	1.000	1.001	1.010	1.060	1.005	1.058	0.968	1.025	1.028	80
90	1.360	1.368	1.360	1.430	1.380	1.442	1.854	1.412	1.410	90
95	1.380	1.594	1.640	1.636	1.562	1.677	1.581	1.649	1.647	95
100	1.860	1.852	1.860		1.874			1.921	1.918	100

FORCE OF VAPOR EXPRESSED IN MILLIMETRES FOR CENTIGRADE TEMPERATURES.

Temper-		Force of Vapor according to												
ature of Air, Centi- grade.	Dalton.	Green- wich Observa- tions.	Biot.	Daniell.	Royal Society.	August.	Kaemts.	Magnus.	Regnault.	of Air, Centi- grade.				
- 0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Mülim.	Millim.	Millim.	-				
-20			1.33			1.15	1.01	0.91	0.91	-20				
-15	1.93	1.88	1.88	2.11	1.60	1.69	1.51	1.40	1.38	-15				
-10	2.64	2.62	2.68	2.92	2.84	2.48	2.21	2.11	2.08	-10				
- 5	8.66	3.66	3.66	4.01	3.33	8.56	8.20	8.11	8.18	- 5				
0	5.08	5.06	5.06	5.49	4.72	5.05	4.58	4.52	4.60	0				
+ 5	6.93	6.95	6.95	7.42	6.60	7.08	6.45	6.47	6.58	+ 5				
10	9.52	9.48	9.47	10.16	9.17	9.90	9.00	9.13	9.16	10				
15	12.88	12.85	12.84	18.79	12.62	13.44	12.38	12.68	12.70	15				
20	17.17	17.80	17.81	18.84	17.17	18.20	16.87	17.40	17.89	20				
25	23.11	28.12	23.09	21.51	23.14	24.18	22.74	23.58	28.55	25				
80	80.78	80.70	30.64	82.83	30.91	\$2.39	30.36	31.60	81.55	80				
35	40.18	40.47	40.40	41.55	40.89	42.59	40.15	41.89	41.83	85				
40			53.00		53.64			54.96	54.91	40				

XXIII. WEIGHT OF VAPOR, IN GRANNES, CONTAINED IN A CUBIC METRE OF SATURATED AIR, AT TEMPERATURES BETWEEN —20° AND +40° CENTIGRADE.—POUILLET.

Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.	Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.	Temper- ature of Dew-Point.	Force of Vapor,	Weight of Vapor.
Centigrade.	Millim.	Grammes.	Centigrade.	Millim.	Grammes.	Centigrade.	Millim	Grammes.
-20°	1.8	1.5	11°	10.1	10.8	26°	24.4	23.8
-15	1.9	2.1	12	10.7	10.9	27	25.9	23.1
-10	2.6	2.9	18	11.4	11.6	28	27.4	26.4
- 5	8.7	4.0	14	12.1	12.2	29	29.0	27.9
٥	5.0	5.4	15	12.8	13.0	80	80.6	29.4
+1	5.4	5.7	16	13.6	18.7	81	82.4	81.0
2	5.7	6.1	17	14.5	14.5	32	84.3	32.6
8	6.1	6.5	18	15.4	15.3	38	36.2	84.3
4	6.5	6.9	19	16.3	16.2	84	38.3	86.2
5	6.9	7.8	20	17.3	17.1	85	40-4	28.1
6	7.4	7.7	21	18.8	18.1	86	42.7	40.2
7	7.9	8.2	22	19.4	19.1	87	45.0	42.2
8	8.4	8.7	28	20.6	20.2	\$8	47.6	44.4
9	8.9	9.2	24	21.8	21.3	89	50.1	46.7
10	9.5	9.7	25	28.1	22.5	40	58.0	49.2

EXIV. WEIGHT OF VAPOR, IN GRAMMES, CONTAINED IN A CUBIC METRE OF SATURATED AIR, AT TEMPERATURES BETWEEN -25° AND -36° CENTIGE. - KAEMTZ.

Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.	Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.	Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.
Centigrade.	Millim.	Grammes.	Centigrade.	Millim.	Grammes.	Contigrade.	Millim.	Grammes.
-25°	0.77	0.98	-4°	8.88	4.87	16°	14.28	14.97
-24	0.88	1.01	-8	4.11	4.70	17	15.20	15.84
-28	0.90	1.10	-2	4.40	5.01	18	16.08	16.76
-22	0.99	1.19	-1	4.71	5.82	19	17.01	17.75
-21	1.06	1.26	0	5.05	5.66	20	18.20	18.77
-20	1.15	1.88	+1	5.41	6.00	21	19.33	19.82
-19	1.26	1.47	2	5.80	6.42	22	20.51	20.91
-18	1.83	1.60	8	6.20	6.84	28	21.75	22.09
-17	1.44	1.74	4	6.63	7.32	24	23.01	23.36
-16	1.56	1.84	5	7.08	7.77	25	24.18	24.61
-15	1.69	2.00	6	7.58	8.25	26	25.81	25.96
-14	1.80	2.14	7	8.10	8.79	26	27.89	27.84
-13	1.96	2.88	8	8.64	9.80	28	28.96	28.81
-12	2.12	2.48	9	9.28	9.86	29	30.63	80.83
-11	2.30	2.63	10	9.90	10.57	80	32.39	31.93
-10	2.48	2.87	111	10.49	11.18	81	84.24	83.65
- 9	2.66	8.08	· 12	11.17	11.58	82	86.18	85.45
- 8	2.86	8.80	18	11.86	12.57	38	88.21	87.20
- 7	8.09	8.58	14	12.66	13.88	84	40.88	89.12
· - 6	8.82	8.80	15	13.44	14.17	35	42.59	41.13
- 5	8.56	4.08	16	14.28	14.97	86	44.96	43.17

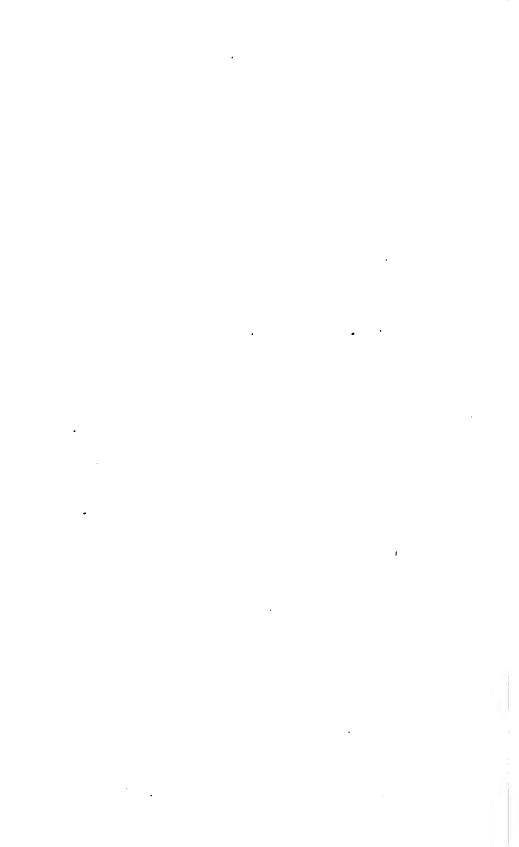
XXV. FORCES OF VAPOR AND RELATIVE HUMIDITY,

coerbsponding to the degrees of saussure's hair-hygrometer, at the temperature of 10° centigrade.

From the Experiments of Gay-Lussac.

The force of vapor is expressed in hundredths, the tension at full saturation being represented by 100.

	ŀ						
Force of Vapor.	Relative Humidity in Thou- sandths.	Degrees of Hur-Hy- grometer.	Force of Vapor.	Relative Humi-lity in Thou- sandths.	Degrees of Hair-Hy- grometer.	Force of Vapor.	Relative Humidity in Thou- sandths.
	0.000						
	0.000			0.177	1		İ
				0.177			
	1				1		0.472
1.80		38	19.54		71	48.51	0.4.2
2.25	0.022	89	20.16		72	49.82	0.500
2.71		40	20.78	0.208	78	51.14	
3. 18		41	21.45		74	52:45	
					1		0.588
4.10		48	22.79		76	55.25	
4.57	0.046	44	28.46		77	56.74	
5.05		45	24.18	0.241	73	58.24	
5.52	ł	46	24.86		79	59.73	
		47	25.59		80	61.22	0.612
6.48		48	26.82		81	62.89	
6.96	0.070	49	27.06		82	64.57	
				0.278	11		į
					11		0.696
	0.094				87		ĺ
				0.818			
	1			1	11		
	1						0.791
11.00	1	90	01.17		"	81.09	
12.03	0.120	59	85.87		92	83.08	
12.59		60	36.28	0.368	98	85.08	
18.14		61	87.81		94	87.07	
13.69	ł	62	86.84		95	89.06	0.991
14.28		68	89.86		96	91.25	
14.78	0.148	.61	40.39		97	93.44	
15.36		65	41.42	0.414	98	95.68	
15.94		66	42.58		99	97.81	
16.52		67	48.78		100	100.00	1.000
	0.00 0.45 0.90 1.35 1.80 2.25 2.71 3.18 3.64 4.10 4.57 5.05 5.52 6.00 6.48 6.96 7.46 7.95 8.45 8.95 9.45 9.97 10.49 11.01 11.58 12.03 12.39 14.28 14.28	Vapor. In Thotamandths. 0.00	Vapor. In Thousandths. grometer. 0.00 0.000 34 0.15 0.90 36 1.35 37 1.80 38 2.25 0.022 39 2.71 40 3.18 41 3.64 42 4.10 48 4.57 0.046 44 5.05 45 5.52 46 6.00 47 6.48 48 6.96 0.070 49 7.46 50 7.95 51 8.45 52 8.95 58 9.45 0.094 54 9.97 55 10.49 56 11.01 57 11.53 58 12.05 0.120 59 12.59 60 13.14 61 13.69 62 14.23 63	Vapor. In Thodamandths. grometer. Vapor. 0.00 0.000 34 17.10 0.45 36 18.80 0.90 36 18.80 1.35 18.92 18.92 1.80 20.16 20.78 2.71 40 20.78 3.18 41 21.45 3.64 42 22.12 4.10 48 22.79 4.57 0.046 44 23.46 5.05 45 24.13 5.52 46 24.36 6.00 47 25.59 6.48 26.32 6.96 0.070 49 27.06 7.46 50 27.79 7.95 51 28.58 8.95 53 30.17 9.45 0.094 54 30.97 9.97 55 31.76 10.19 56 32.66 11.01 57 33.57 <td>Vapor. In Tabodand Mand Mand Mand Mand Mand Mand Mand</td> <td>Vapor. Initial smidths. grometer. Vapor. Initial smidths. grometer. 0.00 0.000 34 17.10 67 0.45 0.90 36 18.30 69 1.35 18.92 70 71 1.80 38 19.54 72 2.25 0.022 39 20.16 72 2.71 40 20.78 0.208 73 3.18 41 21.45 74 3.64 42 22.12 75 4.10 43 22.79 76 4.57 0.048 44 23.46 77 5.52 46 24.13 0.241 78 5.52 46 24.86 79 6.00 47 25.59 80 6.48 26.32 81 6.96 0.070 49 27.06 82 7.95 51 28.58 84 8.95 53</td> <td>Vapor. Securities Vapor. Securities Page 17.10 Securities Page 17.10 Securities Page 17.10 Securities Page 17.10 Securities Page 17.10 Securities Page 17.10 Securities Page 17.10 Securities Page 17.10</td>	Vapor. In Tabodand Mand Mand Mand Mand Mand Mand Mand	Vapor. Initial smidths. grometer. Vapor. Initial smidths. grometer. 0.00 0.000 34 17.10 67 0.45 0.90 36 18.30 69 1.35 18.92 70 71 1.80 38 19.54 72 2.25 0.022 39 20.16 72 2.71 40 20.78 0.208 73 3.18 41 21.45 74 3.64 42 22.12 75 4.10 43 22.79 76 4.57 0.048 44 23.46 77 5.52 46 24.13 0.241 78 5.52 46 24.86 79 6.00 47 25.59 80 6.48 26.32 81 6.96 0.070 49 27.06 82 7.95 51 28.58 84 8.95 53	Vapor. Securities Vapor. Securities Page 17.10 Securities Page 17.10 Securities Page 17.10 Securities Page 17.10 Securities Page 17.10 Securities Page 17.10 Securities Page 17.10 Securities Page 17.10

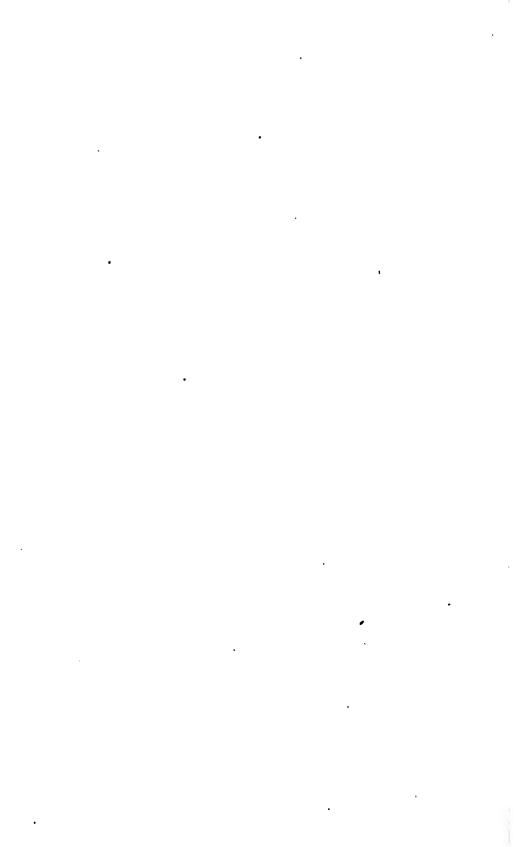


APPENDIX

10

THE HYGROMETRICAL TABLES.

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TABLES

FOR

COMPARING THE QUANTITIES OF RAIN-WATER.

THE three kinds of measures which are most in use for noting the quantities of rain and melted snow, are the Centimetres and Millimetres in France, the Paris or French inches and lines in Germany, and the English inches and decimals in England, America, and also in Russia, the Russian foot being the same as the English foot. The following tables will facilitate the comparison of these various measures with each other.

A glance at the tables will show that the first column on the left contains the numbers to be converted, and the heads of the following columns the fractions of these numbers, or units, each of which is one tenth of those in the first column. Shorter tables, at the bottom, give, when necessary, the value of proportional parts still smaller than those found in the larger tables.

Example.

Let 13 Centimetres be converted into French inches and lines.

Take, in Table II., the line beginning with 10 Centimetres in the first column, follow that line as far as the column headed 3 Centimetres, and there will be found the number of 4 inches 9.63 lines, which is the corresponding value in French inches of 10 + 3, or 13 Centimetres.

If the number is followed by a fraction, as for instance, 13.5 Centimetres, or 135 Millimetres, we find, -

French Inches, Lines. 13 Centimetres = 4.9,63In the larger table In the smaller table at the bottom 5 Millimetres = Or 13.5 Centimetres = 4.11.846

When the measures which are to be compared are both subdivided into decimal parts, the equivalents of the numbers greater than 9.9 may be found by moving the decimal point.

Example.

Let 346.7 Centimetres be converted into English inches.

In Table I., in the column headed 4, on the fourth line,

we find 3.4 Centimetres = 1.3386 English inches.

Moving the decimal point by two places we have

340 Centimetres = 133.86 English inches.

Then, in the column headed 7, on the

6.7 Centimetres = line beginning with 6, we find

Making together 346.7 Centimetres = 136.50 English inches. 161

B

I. CONVERSION OF CENTIMETRES INTO ENGLISH INCHES AND DECIMALS.

1 Centimetre == 0.3937079 English Inch.

_	1				Milli	metres.				
Centi- metres.	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.
0	Eng. Inch.	Eng. Inch. 0.0394	Eng.Inch 0.0787			Eng.lnch.	Eng.Inch. 0.2362	Eng.Inch. 0.2756	Eng.Inch 0.3150	Eng.Inch. 0.3543
1	0.3937	0.4831	0.4724	0.5118	0.5512	0.5906	0.6299	0.6693	0.7087	0.7480
2	0.7874	0.8268	0.8662	0.9055	0.9449	0.9843	1.0236	1.0630	1.1024	1.1418
8	1.1811	1.2205	1.2599	1.2992	1.3386	1.3780	1.4178	1.4567	1.4961	1.5355
4	1.5748	1.6142	1.6536	1.6929	1.7323	1.7717	1.8111	1.8504	1.8898	1.9292
5	1.9685	2.0079	2.0478	2.0867	2.1260		2.2048	2.2441	2.2835	2.3229
6	2.8622	2.4016	2.4410	2.4804	2.5197	2.5591	2.5985	2.6378	2.6772	2.7166
7	2.7560	2.7953	2.8347	2.8741	2.9134		2.9922	8.0816	8.0709	3.1103
8	3.1497	8.1890	3.2284	8.2678	8.3071	3.8465	8.8859	8.4258	3.4646	8.5040
9	3.5434	8.5827	8.6221	8.6615	8.7009	3.7402	8.7796	8.8190	3.8563	8.8977
fi. co	NVERSION	OF CE				CH INCE 4.43296 P		ES, AN	D DECIM	ĄLS.
					Uni	te.				
Centi- metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fr.In. Lin. F									
0										3. 3,90
10										7. 0,23
20		, ,	- 1							10. 8,56
80	11. 0,99 1									
40	14. 9,32 1									
	18. 5,65 1					- 1	•	•		
60 70	22. 1,98 2									
80	25.10,81 20 29. 6,64 20									
	38. 2,97 3		- 1	- 1	, ,	- 1	- 1	-	-	
		.ln. Lin.				Fr.In. Lin.				Fr.In. Lin.
		3.11,30		3.10.59		110.9,89		147.9,18	500	184.8,48
	CONVER	SION O	F CENT	METRES		PRENCH	LINES .	AND DE	CINALS.	
Centi-					U	nite.				
metres.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
~	Fr. Lines.		1	Fr. Lines.			Fr. Lines.			
0	0.00	4.48	8.87	13.30	17.78	22.16	26.60	31.03	35.46	39.90
10 20	44.38	48.76 98.09	53.20 97.53	57.63	62.06	66.49	70.93 115.26	75.36 119.69	79.79 124.12	84.23 128.56
80	88.66 132.99	137.42	141.85	101.96	106.89 150.72	110.82 155.15	159.59	164.02	168.45	172.89
40	177.32	181.75	186.18	190.62	195.05	199.48	203.92	208.85	212.78	217.22
50	221.65	226.08	230.51	234.95	239.38	243.81	248.25	252.68	257.11	261.54
60	265.98	270.41	274.84	279.28	283.71	288.14	292.58	297.01	301.44	305.87
70	310.81	814.74	819.17	823.61				341.34	345.77	350.20
80	854.64	859.07			1		1	385.67	390.10	
90	398.97	403.40	407.83	412.26	416.70	421.13	425.56	430.00	434.43	438.86
	CONVER	SION OI	F MILLI	METRES	INTO I	FRENCH	LINES .	AND DE	CIMALS.	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fr. Lines.			Fr. Lines.					Fr. Lines.	
	# 0.0	0.448	0.887	1.330	1.778	2.216	2.660	3.103	3.546	3.990

III. CONVERSION OF ENGLISH INCHES INTO CENTIMETRES.

I English Inch == 2.53995 Contimetres.

	1		-						Ŭ:	alte.				
English Inches.	1	0.		1.	2	,	8.	4	L	5.	6.	7.	8.	9.
	٦	Centir	- 1	Centin			Centim		tim.	Centim.	1			Centim.
0	H	0.0	- 1	2.5		08	7.62		.16	12.70				22.86
10	-	25.4		27.9			88.02	- 1	.56	38.10		1	1	48.26
20 30	- 11	50.8 76.2		53.8 78.7			58.42 88.82).96 3.36	68.50 88.90				73.66 99.06
40	-	101.6		104.1			109.22		.76	114.80	1			124.46
50	ı	127.0		129.5			184.62		.16	139.70	ł		1	149.86
60	ľ	152.4		154.9	1		160.02		.56					175.26
70	ı	177.8		180.3	4 182.	88	185.42	187	.96	190.50	198.04	195.58	198.12	200.66
80	ı	208.2	ю	205.7	4 206.	28	210.82	218	.36	215.90	218.44	220.98	223.52	226.06
90	H	228.6	10	281.1	4 283.	6 8	236.23	288	.76	241.80	248.84	246.38	248.92	251.46
100	H	254.0	00	256.5	4 259.	08	261.62	264	.16	266.70	269.24	271.78	274.82	276.85
i	1		-		- 1		1	1					ł	1
110	ŀ	279.3		281.9		_	287.01	- 1	.55	292.09			1	802.25
120	۱	804.7		307.8	- 1		312.41	- 1	1.95	1				827.65
130		880.1 855.5		332.7 358.1			363.21		.35 .75	342.89 368.29		· i		353.05
140 150	ŀ	880.9		888.5	_		388.61		.15	893.69	1			378.45 403.85
160		406.8		408.9			414.01	1	.55	419.09				429.25
170	ı	431.7		484.8	1		489.41		.95	444.49	1			454.65
180	-	457.1		459.7	_		464.81		.85	469.89		1	477.51	480.05
190	1	482-		485.1			490.21		.75	495.29	1	1		505.45
200	ı	507.9	- 1	510.5			515.61		.15					530.85
	7		_			_		Ten	the o	f an Inch.	1			
		0.		1.	2.	,	3.	4	l.	5.	6.	7.	8.	9.
		Centir 0.000		Centin 0.254			Centim 0.762		tim.)16	Centim. 1.270	Centim.	Centim. 1.778	Centim. 2.032	Centim. 2.286
1	ν.	CON	VE	RSION						NTO FR 1.2595 Pa		NCHES A	AND LIN	ES.
			_					•	۲ai	t u .	· · ·			
Eng. inches.		0.		1.	2.		8.	4.		5.	6.	7.	8.	9.
_	F	In. Lin	Fr	In Lin	Fr.In. L	n. F	r.In.Lin.	Fr.In. l	المنا	r.In. Lin.	Fr.In. Lin.	Fr.In. Lin	Fr.In. Lin.	Fr.In. Lin.
0													7. 6,08	
10 20														17. 9,98
30														27. 2,53 36. 7,12
11 . N														45.11,72
														55. 4.81
														64. 8.91
70														74. 1,50
80														83. 6,10
90														92.10,69
	En		Fr.		Eng.Inc	ı.F		Eng. In	ch.		Eng. Inch.		Eng.Inch.	
								Tenth	o of	an Inch.				
		0.		1.	2.	T	8.	4.	\neg	5.	6.	7.	8.	9.
		In. Lin.			Fr. In. Li 0.2,25		r.In. Lin. 0.8,38	Fr.In. I 0.4,		r.ln. Lin. 0.5,63	Fr.In. Lin. 0.6,76		Fr.In. Lin. 0.9,01	Fr.In. Lin. 0.10,18

V. CONVERSION OF FRENCH INCHES INTO CENTIMETRES.

I French Inch = 2.7070 Centimetres.

French					Un	ite.				
Inches.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.
0	0.00	2.71	5.41	8.12	10.88	13.53	16.24	18.95	21.66	24.36
10	27.07	29.78	32.48	35.19	87.90	40.60	48.31	46.02	48.78	51.43
20	54.14	56.85	59.55	62.26	64.97	67.67	70.38	73.09	75.80	78.50
80	81.21	83.92	86.62	89.33	92.04	94.74	97.45	100.16	102.87	105.57
40	108.28	110.99	113.69	116.40	119.11	121.81	124.52	127.28	129.94	132.64
50	135.85	188.06	140.76	148.47	146.18	148.88	151.59	154.80	157.01	159.71
'			1		ł			· ·	1	
60	162.42	165.18	167.83	170.54	172.25	175.95	178.66	181.87	184.08	186.78
70	189.49	192.20	194.90	197.61	200.82	203.02	205.78	208.44	211.15	213.85
80	216.56	219.27	221.97	224.68	227.39	280.09	232.80	235.51	238.22	240.92
90	243.63	246.34	249.04	251.75	254.46	257.16	259.87	262.58	265-29	2 67.99
100	270.70	273.41	276.11	278.82	281.53	284.28	286.94	289.65	292.36	295.06
ì	!									
110	297.77	300.48	803.18	305.89	308.60	311.30	814.01	316.72	319.42	322.13
120	324.84	327.55	380.25	332.96	335.67	338.37	341.08	343.79	846.49	349.20
130	351.91	354.62	357.32	360.03	862.74	865.44	368.15	370.86	373.56	376.27
140	378.98	381.69	384.39	887.10	389.81	392.51	395.22	397.98	400.68	403.34
150	406.05	408.76	411.46	414.17	416.88	419.58	422.29	425.00	427.70	430.41
1						1				
160	433.12	435.83	438.53	441.24	443.95	446.65	449.36	452.07	454.77	457.48
170	460.19	462.90	465.60	468.31	471.02	478.72	476.48	479.14	481.84	484.55
180	487.26	489.97	492.67	495.38	498.09	500.79	503.50	506.21	508.91	511.62
190	514.33	517.04	519.74	522.45	525.16	527.86	530.57	538.28	535.98	538.69
200	541.40	544.11	546.81	549.52	552.28	554.93	557.64	560.35	563.05	565.76

CONVERSION OF FRENCH LINES INTO CENTIMETRES.

1 French Line = 0.22558 Centimetre.

French					Tenths o	f a Line.				
Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.
0	0.000	0.023	0.045	0.068	0.090	0.113	0.135	0.158	0.180	0.203
1	0.226	0.248	0.271	0.293	0.316	0.338	0.861	0.388	0.406	0.429
2	0.451	0.474	0.496	0.519	0.541	0.564	0.587	0.609	0.632	0.654
3	0.677	0.699	0.722	0.744	0.767	0.790	0.812	0.835	0.857	0.880
4	0.902	0.925	0.947	0.970	0.993	1.015	1.038	1.060	1.083	1.195
5	1.128	1.150	1.178	1.196	1.218	1.241	1.263	1.286	1.308	1.331
6	1.853	1.376	1.399	1.421	1.444	1.466	1.489	1.511	1.534	1.557
. 7	1.579	1.602	1.624	1.647	1.669	1.692	1.714	1.787	1.760	1.782
8	1.805	1.827	1.850	1.872	1.895	1.917	1.940	1.963	1.985	2.008
9	2.030	2.053	2.075	2.098	2.120	2.143	2.166	2.188	2.211	2.233
10	2.256	2.278	2.301	2.324	2.346	2.369	2.891	2.414	2.436	2.459
11	2.481	2.504	2.527	2.549	2.572	2.594	2.617	2.639	2.662	2.684
12	2.707	2.730	2.752	2.775	2.797	2.820	2.842	2.865	2.887	2.910

VI. CONVERSION OF FRENCH INCHES INTO ENGLISH INCHES AND DECIMALS.

1 French Inch = 1.065765 English Inch.

French	1	Units.												
Inches.	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.				
						Eng.Inch.								
0	0.000	1.066			4.268	5.329	6.89 5	7.460						
10	10.658	11.723	12.789	13.855	14.921	15.986	17.052	18.118	19.184	20.250				
20	21.315	22.381	23.447	24.513	25.578	26.644	27.710	28.776	29.841	30.907				
80	81.973	33.039	84.104	85.170	86.286	87.302	88.868	39.483	40.499	41.565				
40	42.631	43.696	44.762	45.828	46.894	47.959	49.025	50.091	51.157	52.222				
50	58.2 88	54.854	55.420	56.486	57.551	58.617	59.688	60.749	61.814	62.880				
60	63.946	65.012	66.077	67.148	68.209	69.275	70.340	71.407	72.472	78.58				
70	74.604	75.669	76.735	77.801	78.867	79.982	80.998	82.064	88.130	84.198				
80	85.261	86.327	87.393	88.458	89.524	90.590	91.656	92.722	98.787	94.858				
90	95.919	96.985	98.050	99.116	100.182	101.248	102.814	108.379	104.445	105.51				
100	106.576	107.642	108.708	109.774	110.840	111.905	112.971	114.037	115.103	116.16				
110	117.284	118.800	119.366	120.481	121.497	122.563	128.629	124.695	125.760	126.82				
120	127.892	128.958	130.023	131.089	182.155	133.221	184.286	185.352	136.418	137.48				
130	138.549	139.615	140.681	141.747	142.813	148.878	144.944	146.010	147.076	148.14				
140	149.207	150.278	151.839	152,404	158.470	154.536	155.602	156.667	157.733	158.79				
150	159.865	160.931	161.996			165.194		167.825	168.391	169.45				
160	170.522	171.588	172.654	178.720	174.785	1 75. 851	176.917	177.983	179.049	180.11				
170			183.312		185.448		187.575	188.640		190.77				
180	1		198.969			197.167	198.282	199.298						
190	3		204.627			207.824			211.021					
200	0		215.285		217.416	i				222.74				

CONVERSION OF FRENCH LINES INTO ENGLISH INCHES.

1 French Line == 0.088814 English Inch.

D	Tenths of a Line.												
French Lines.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.			
	Eng.Inch.	Eng.Inch.	Eng.Inch.	Eng.Inch.	Eng. Inch.	Eng. Inch.	Eng.Inch.	Eng.Inch.	Eng. Inch.	Eng. Inch.			
0	0.0000	0.0089	0.0178	0.0266	0.0855	0.0444	0.0538	0.0622	0.0711	0.0799			
1	0.0888	0.0977	0.1066	0.1155	0.1243	0.1332	0.1421	0.1510	0.1599	0.1687			
2	0.1776	0.1865	0.1954	0.2048	0.2182	0.2220	0.2309	0.2398	0.2487	0.2576			
8	0.2664	0.2758	0.2842	0.2931	0.8020	0.8108	0.8197	0.3286	0.8375	0.8464			
4	0.8553	0.3641	0.3730	0.8819	0.3908	0.8997	0.4085	0.4174	0.4263	0.4852			
5	0.4441	0.4530	0.4618	0.4707	0.4796	0.4885	0.4974	0.5062	0.5151	0.5240			
6	0.5329	0.5418	0.5506	0.5595	0.5684	0.5778	0.5862	0.5951	0.6089	0.6128			
7	0.6217	0.6806	0.6395	0.6488	0.6572	0.6661	0.6750	0.6839	0.6927	0.7016			
8	0.7105	0.7194	0.7288	0.7872	0.7460	0.7549	0.7638	0.7727	0.7816	0.7904			
9	0.7998	0.8082	0.8171	0.8260	0.8349	0.8487	0.8526	0.8615	0.8704	0.8793			
10	0.8881	0.8970	0.9059	0.9148	0.9287	0.9325	0.9414	0.9503	0.9592	0.9681			
11	0.9770	0.9858	0.9947	1.0036	1.0125	1.0214	1.0802	1.0391	1.0480	1.0569			
12	1.0658	1.0746	1.0935	1.0924	1.1018	1.1102	1.1191	1.1279	1.1868	1.1457			

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METEOROLOGICAL TABLES.

III.

BAROMETRICAL TABLES.

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C



COMPARISON

OF

THE BAROMETRICAL SCALES,

OB

TABLES

FOR CONVERTING THE INDICATIONS OF THE ENGLISH, METRICAL, OLD FRENCH,
AND RUSSIAN BAROMETERS INTO EACH OTHER.

C



COMPARISON

OF

THE BAROMETRICAL SCALES.

The following tables are intended for converting into each other the four most important Barometrical Scales. They are sufficiently detailed to save the labor of any calculation or even of interpolation for the ordinary wants of Meteorology. But before making use of them, for comparing the observations taken with barometers of different scales, it is necessary to reduce the observed heights to the temperature of the freezing point, or to any other temperature, provided it be the same for all, by means of the tables calculated for this purpose, and which will be found below. The reason of it may be readily understood.

The length of the bars of metal, or of other substances, which represent the standard measures of length which obtain among different nations, varying with the temperature, it was necessary to determine a fixed point of temperature at which they really ought to have the length adopted as the standard unit of measure. This temperature is the *normal* temperature of the standard, and the length of the standard-bar, at this temperature, is the *true* length of it.

If the normal temperature of the various standards used for dividing Barometrical Scales were the same, the heights of the barometrical column, taken with these scales, could be compared directly, provided the scales be made of the same substance, brass, for instance, because their variations above or below this normal temperature would remain parallel with each other. But unfortunately it is not so. The English Yard is a standard at the temperature of 62° Fahrenheit; the Old French Toise, at 13° Reaumur; the Metre, at the freezing point, or zero Centigrade. Thus metallic rods intended to represent these various units of measure give the true or standard length only when at these respective temperatures; at any other temperature they are longer or shorter than the standard, and their subdivisions, inches, lines, or millimetres, partake of the error.

It is obvious, therefore, that the barometrical heights, taken with different scales, cannot be compared *directly* by means of the following tables, which give the relation between these scales at their respective *normal* temperatures. For suppose the temperature of the three barometers to be the freezing point, or 32° Fahrenheit,

COMPARISON OF THE BAROMETRICAL SCALES.

the scale of the Metrical Barometer alone will actually represent the standard length, and the millimeters will have the true length; while the inches and lines of the Old French and of the English Barometers will be too short, causing thus the barometrical column to appear too high. If the temperature of the instruments be 62° Fahrenheit, the divisions of the English Barometer will have the true standard length, and those of the Old French Barometer nearly so; but the millimeters of the Metrical Barometer will be too long, causing the barometrical column to appear too low. It is to neutralize the effect of those inequalities arising from the expansion of the scale that it is necessary, before comparing the observations taken with the three barometers, to reduce them to the same temperature. This is done by means of the tables above mentioned, for reducing the barometer to the freezing point, which suppose the scales to be of brass from top to bottom, and which take into account the expansion or contraction they undergo by the variations of temperature.

But in doing so, we must be aware that the accuracy of the comparison depends in part upon the correctness of the indications of the attached thermometers, which determine the amount of the correction to be applied for reducing the barometers to the freezing point. If the thermometers do not agree, an error is introduced which will affect the height of the reduced columns, and the final comparison. Therefore the correction of the attached thermometers ought to be ascertained and applied to them before the reduction is made; or if this correction is unknown, it will be well to place the instruments to be compared in the most favorable conditions for taking the same temperature, and then to take the temperature given by one of the thermometers to reduce both barometers. If the correction of the attached thermometer has not been applied before the reduction, it will be contained, after the reduction, in the total correction of the instrument. If it be so, this circumstance must be indicated.

In computing the following tables, the value of the Metre, as determined by Capt. Kater, (Philosoph. Transact. for 1818, p. 109, and Baily's Astronomical Tables, p. 192,) has been adopted, viz. 1 Metre, at 0° Centigrade = 39.37079 English inches, at 62° Fahrenheit. The relation of the Metre (legal) to the Old French system of measures is known to be 1 Metre = 443.296 French or Paris lines. From these equations are derived the elements used in the computations, which are found at the head of each table.

Besides the larger Tables I. – VIII., a set of smaller ones, Tables IX. – XVI., has been added, which will be found useful for comparing Barometrical differences, such as ranges, amount of variation in a given time, &c., expressed in measures of different scales, in which only small quantities occur that are not found in the large tables.

C 8

I. - II.

COMPARISON

OP

THE ENGLISH BAROMETER

WITH

THE METRICAL AND THE OLD FRENCH BAROMETERS,

OR

TABLES

FOR CONVERTING ENGLISH INCHES INTO MILLIMETRES, AND INTO FRENCH OR PARIS LINES AND DECIMALS;

GIVING THE VALUES CORRESPONDING TO EVERY TENTH OF AN INCH, FROM 9

TO 19 INCHES; AND TO EVERY HUNDREDTH, FROM

19 TO \$1.5 ENGLISH INCHES.

USE OF TABLE I.

Example.

THE English Barometer reads 20.657 inches. What would be the corresponding height in the Metrical Barometer?

In Table I., first column on the left, look out the line of 20 inches 6 tenths; on that line, in the sixth column, headed 5 hundredths, is found the value in millimetres for

At the bottom of the page, for
$$0.007$$
 " = 0.18 "

Or for 0.007 " = 524.68 "

which would be the reading of the Metrical Barometer.

This example may serve for all tables, throughout the volume, which are constructed on the same plan.

I. COMPARISON OF THE ENGLISH AND METRICAL BAROMETERS.

1 English Inch == 25.39954 Millimetres.

Facilish				BH IIICH	Tenths o	f an Inch	L			
English loches	0.	1.	2.	8.	4.	5.	6.	7.	s.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
9	228.60	231.14	233.68	236.22	238.76	241.30	248.84	246.38	248.92	251.46
10	254.00	256.54	259.08	261.62	264.16	266.70	269.24	271.78	274.32	276.85
11	279.39	281.93	284.47	287.01	289.55	292.09		297.17	299.71	802.25
12	304.79	307.33	309.87	812.41	314.95	817.49	1	322.57	825.11	827.65
13	330 19	332.78	335.27	337.81	840.85	342.89	345.48	847.97	850.51	853.05
14	355.5 9	858.13	360.67	363.21	865.75	368.29	870.88	373.37	375.91	878.45
15	380.99	383.58	386.07	388.61	391.15	393.69	396.23	898.77	401.31	403.85
16	406.39	408.93	411.47	414.01	416.55	419.09	421.63	424.17	426.71	429.25
17	431.79	434.38	436.87	439.41	441.95	444.49	447.03	449.57	452.11	454.65
18	457.19	459.73	462.27	464.81	467.35	469.89	472.48	474.97	477.51	480.05
English				1	Hundredthe	of an L	och.	'n	<u> </u>	
tepths.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim	Millim	Millim.	Millim	Millim.	Millim.
19.0	482.59	482.85	488.10	488.35	488.61	483.86	484.12	484.37	484.62	484.88
1	485.18	485.39	485.64	485.89	486.15	486.40	486.66	486.91	487.16	487.42
2	487.67	487.98	488.18	488.48	488.69	488.94	489.20	489.45	489.70	489.96
8	490.21	490.47	490.72	490.97	491.23	491.48	491.74	491.99	492.24	492.50
4	492.75	498.01	493.26	498.51	493.77	494.02	494.28	494.53	494.78	495.04
5	495.29	495.55	495.80	496.06	496.31	496.56	496.81	497.07	497.32	497.58
6	497.88	498.08	498.84	498.59	498.85	499.10		499.61	499.86	500.12
7	500.87	500.62	500.88	501.18	501.39	501.64	1	502.15	502.40	502.66
8	502.91	503.16	508.42	503.67	508.93	504.18	1	504.69	504.94	503.20
9	505.45	505.70	505.96	506.21	506.47	506.72	506.97	507.28	507.48	507.74
20 .0	507.99	508.24	508.50	508.75	509.01	509.26	509.51	509.77	510.02	510.28
1	510.58	510.78	511.04	511.29	511.55	511.80	1	512.81	512.56	512.82
2	518.07	518.82	518.58	513.88	514.09	514.84		514.85	515.10	515.36
8	515.61	515.86	516.12	516.37	516.63	516.88	1	517.89	517.64	
4	518.15	518.40	518.66	518.91	519.17	519.42	519.67	519.93	520.18	520.44
5	520.69	520.94	521.20	521.45	521.71	521.96	522.21	522.47	522.72	522.98
6	523.28	523.48	523.74	528.99	524.25	524.50	524.75	525.01	525.26	525.52
7	523.77	526.02	526.28	526.58	526.79	527.04	527.29	527.55	527.80	528.06
8	528.81	528.56	528.82	529.07	529.83	529.58	529.83	530.09	530.34	580.60
9	530.85	531.10	581.86	581.61	581.87	532.12	582.87	582.63	532.88	583.14
	•			Thousan	dthe of an	Inch.				
0.	1.	2.	8.	4		5.	6.	7.	8.	9.
0.0	0.08	0.05	0.00	в О.	10 0).13	0.15	0.18	0.20	0.23

English				I	lundredth	of an L	och.			
tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millin				Million
1.0	533.89	588.64	533.90	584.15	584.41	534.6				535.60
1	535.93	586. 18	586.44	586.69	586.95	587.2				538 2
2	538.47	538.72	53 8.98	539.23	589.49	589.7		1		540.70
8	541.01	541.26	541.52	541.77	542.08	542.2				543.30
4	548.55	548.80	544.06	544.81	544.57	544.8	2 545.0	7 545.88	545.58	545.84
5	546.09	546.84	546.60	546.85	547.11	547.8	_			548.88
6	548.63	548.88	549.14	549.89	549.65	549.9	0 550.1			550.92
7	551.17	551.42	551.68	551.98	552.19	552.4	4 552.6		1	558.46
8	553.71	558.96	554.22	554.47	554.73	554.9	8 555.21			556.00
9	556.25	556.50	556.76	557.01	557.27	557.5	557.77	558.08	558.28	558.54
2.0	558.79	559.04	559.30	559.55	559.81	560.0	560.8	560.57	560.82	561.08
1	561.38	561.58	561.84	562.09	562.85	562.6	0 562.8	563.11	568.36	563.62
2	568.87	564.12	564.38	564.68	564.89	565.1	4 565.39	565.65	565-90	566.16
8	566.41	566.66	566.92	567.17	567.48	567.6	567.91	568.19	568.44	568.70
4	568.95	569.20	569.46	549.71	569.97	570.2	2 570.47	570.73	570.96	571.24
5	571.49	571.74	572.00	572.25	572.51	572.7	6 573.0	573.27	578.52	573.78
6	574.08	574.28	574.54	574.79	575.05	575.8		_	576.06	576.82
7	576.57	576.82	577.08	577.88	577.59	577.8		1	1	578.86
8	579.11	579.86	579.62	579.87	580.18	580.8		580.89	581.14	581.40
9	581.65	581.90	562.16	562.41	582.67	582.9			583.68	583.94
3 .0	584-19	584-44	584.70	564.95	585.21	585.4	6 585.7	585.97	586.22	586.48
1	586.73	586.98	587.24	587.49	587.75	588.0		588-51	588.76	589.02
2	589.27	589.52	589.78	590.08	590.29	590.5	4 590.79	591.05	591.80	591.56
8	591.81	592.06	592.82	592.57	592.98	593.0				594.10
4	594.85	594.60	594.86	595.11	595.87	595.6		596.18	596.88	596.64
5	596.89	597.14	597.40	597.65	597.91	598.1	598.41	598-67	598.92	599.18
6	599.43	599.68	599.94	600.19	600.45	600.7				601.72
7	601.97	602.22	602.48	602.78	602.99	608.2	-			604-26
8	604.51	604.76	605.02	605.27	605.58	605.7				606.79
9	607.05	607.80	607.56	607.81	608.06	608.3			609.08	609.31
	609.59	609.84	610.10	610.85	610.60	610.8	8 611.11	611.37	611.62	611.87
4.0		612.38	612.64	612.89	618.14	618.4				614.4
1	612.18	614.92	615.18	615.43	615.68	615.9	1			616.9
2 3	614.67 617.21	617.46	617.72	617.97	618.22	618.4	_		1	619.49
4	619.75	620.00	620.26	620.51	620.76	621.0				622.0
			<u> </u>	. Thous	andthe of	an Inch	<u> </u>		<u> </u>	<u> </u>
0.	1.	2.	8.	4.		5.	6.	7.	8.	9.
0.0	0.08	0.05	0.08	0.1	0 0	.18	0.15	0.18	0.20	0.23

English					fundredthe	of an Inc	F			
inches and tenths.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Million.	Millim
24.5	622.29	622.54	622.80	623.05	623.30	623.56	623.81	624.07	624.32	624.5
6	624.83	625.08	625.84	625.59	625.84	626.10	626.35	626.61	626.86	627.11
7	627.87	627.62	627.88	628.13	628.38	628.64	628.89	629.15	629.40	629.63
8	629.91	630.16	630.42	630.67	680.92	631.18	631.43	631.69	631.94	632.19
9	632.45	632.70	632.96	633.21	683.46	633.72	633.97	634-23	634.48	684.7
25. 0	634.99	635.24	635.50	637.75	636.00	636.26	636.51	636.77	637.02	637.27
1	637.53	637.78	638.04	638.29	638.54	638.80	639.05	639.31	639.56	639.8
2	640.07	640.82	640.58	640.88	641.08	641.34	641.59	641.85	642.10	642.8
3	642.61	642.86	648.12	648.87	643.62	643.88	644.13	644.89	644.64	644.8
4	645.15	645-40	645.66	645.91	646.16	646.42	646.67	646.98	647.18	647.4
5	647.69	647.94	648.20	648.45	648.70	648.96	649.21	649.47	649.72	649.9
6	650.23	650.48	650.74	650.99	651.24	651.50	651.75	652.01	652.26	652.5
7	652.77	658.02	653.28	638.53	653.78	654.04	654.29	654-55	654.80	655.0
8	655.31	655.56	655.82	656.07	656.32	656.58	656.88	657.09	657.84	657.5
9	657.85	658.10	658.36	658.61	658.86	659.12	659. 37	659.68	659.88	660.1
26 .0	660.89	660.64	660.90	661.15	661.40	661.66	661.91	662.17	662.42	662.6
1	662.93	663.18	663.44	663.69	663.94	664.20	664.45	664.71	664.96	665.2
2	665.47	665.72	665.98	666.23	666.48	666.74	666.99	667.25	667-50	667.7
8	668.01	668.26	668.52	668.77	669.02	669.28	669.53	669.79	670.04	670.2
4	670.55	670.80	671.06	671.31	671.56	671.82	672.07	672.83	672.58	672.8
5	673.09	673.84	673.60	673.85	674.10	674.86	674.61	674.87	675-12	675.8
6	675.63	675.88	676.14	676.89	676.64	676.90	677.15	677.41	677.66	677.9
7	678.17	678.42	678.68	678.93	679.18	679.44	679.69	679.95	680.20	680.4
8	680.71	680.96	681.22	681.47	681.72	681.98	682.23	682.49	682.74	682.9
9	683.25	683.50	683.76	684.01	684.26	684.52	684.77	685.08	685.28	685.5
27 .0	685.79	686.04	686.80	686.55	686.80	687.06	687.81	687.57	687.82	688.0
1	688.33	688.58	688.84	689.09	689.84	689.60	689.85	690.11	690.36	690.6
2	690.87	691.12	691.38	691.63	691.88	692.14	692.39	692.65	692.90	698.1
3	693.41	693.66	693.92	694.17	694.42	694.68	694.93	695.19	695.44	695.6
4	695.95	696.20	696.46	696-71	696.96	697.22	697.47	697.78	697.98	698.2
5	698.49	698.74	699.00	699.25	699.50	699.76	700.01	700.27	700.52	700.7
6	701.03	701.28	701.54	701.79	702.04	702.30	702.55	702.81	703.06	703.3
7	703.57	703.82	704.08	704.88	704.58	704.84	705.09	705.35	705.60	705.8
8	706.11	706.36	706.62	706.87	707.12	707.38	707.63	707.89	708.14	706.3
9	708.65	708.90	709.16	709.41	709.66	709.92	710.17	710.43	710.68	710.9
	100.00	100.50	.03.10	100.11	703.00	103.32	/10.17	110.40	110.00	120.5
				Thou	andths of	an Inch.				
0.	1.	2.	3.	4		5.	6.	7.	8.	9.
0.0	0.08	0.05	0.08	0.1	0 0	.13	0.15	0.18	0.20	0.28

English				1	Hundredth	of an I	nch.			
Inches and tenths.	ll .	_			_	T -		1 _		
	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.
28 .0	Millim. 711-19	Millim. 711.44	Millim. 711.70	Millim. 711.95	Millim. 712.20	Millin 712.4			1	Millim 718.47
1	713.78	713.98	714.24	714.49	714.74	715.0				716.0
2	716.27	716.52	716.78	717.08	717.28	717.5				718.5
8	718.81	719.06	719.81	719.57	719.82	720.0	-	_ 1	1	721.0
4	721.85	721.60	721.85	722-11	722.86	722.6				723.6
5	723.89	724.14	724.89	724.65	724.90	725.1	6 725.4	725.66	725.92	726.17
6	726.48	726.68	726.98	727.19	727.44	727.7	0 727.9	728.20	728.46	728.7
7	728.97	729.22	729.47	729.78	729.98	780.2	4 780.4	780.74	731.00	731.2
8	781.51	731.76	782.01	732.27	782.52	732.7	8 783.0	733.28	733-54	732.7
9	734.05	734.30	734.55	734.81	785.06	785.8	2 785.51	785.82	736.08	736.33
29 .0	736.59	736.84	737.09	737.85	737.60	737.8	6 73 8.11	738.36	738.62	738.87
1	789.13	739.88	789.68	789.89	740.14	740.4	740.6	740.90	1	741.4
2	741.67	741.92	742.17	742.43	742.68	742.9	4 748.19	743.44	743.70	743.9
8	744.21	744.46	744.71	744.97	745.22	745.4	3 745.78	745.98	746.24	746.49
4	746.75	747.00	747.25	747.51	747.76	748.0	2 748.27	748.52	748.78	749.0
5	749.29	749.54	749 79	750.05	750.80	750.5	6 750.81	751.06	751.32	751.57
6	751.83	752.08	752.33	752.59	752.84	758.1	753.8	753.60	753.86	754.1
7	754.87	754.62	754.87	755.13	755.38	755.6	4 755.88	756.14	756-40	756.6
8	756.91	757.16	757.41	757.67	757.92	758.1	758.48	758.68	758.94	759.19
9	759.45	759.70	759.95	760.21	760.46	760.7	2 760.97	761.22	761.48	761.73
30 .0	761.99	762.24	762.49	762.75	763.00	763.2	6 763.51	763.76	764.02	764.27
1	764.53	764.78	765.03	765.29	765.54	765.8			766.56	766.81
2	767.07	767.82	767.57	767.83	768.08	768.3			769.10	769.35
3	769.61	769.86	770.11	770.37	770.62	770.8	1		771.64	771.89
4	772.15	772.40	772.65	772.91	773.16	778.4	2 773.67	773.92	774.18	774.43
5	774.69	774.94	775.19	775.45	775.70	775.9	6 776.21	776.46	776.72	776.97
6	777.23	777.48	777.78	777.99	778.24	778.5	778.78	779.00	779.26	779.51
7	779.77	780.02	780.27	780.58	780.78	781.0	4 781.29	781.54	781.80	782.03
8	782.31	782.56	782.81	783.07	783.82	783.5	783.83		784.34	784.59
9	784.85	785.10	785.35	785.61	785.86	786.1	786.37	786.62	786.88	787.18
31 .0	787.59	787.64	787.89	788.15	788.40	788.6		1	789.42	789.67
1	789.93	790.18	790.48	790.69	790.94	791.2	1			792.21
2	792.47	792.72	792.97	793.23	798.48	793.7	793.99	794.24		794.78
3	795.01	795.26	795.51	795.77	796.02	796.2				797.29
4	797.55	797.80	798.05	798.31	798.56	798.8	799.07	799.32	799.58	799.88
	·			Thou	sandths of	an Inch				
0.	1.	9.	3.	4.		s.	6.	7.	8.	9.

 \overline{c}

0.05

0.03

0.15

0.18

0.20

1 English Inch = 11.2595 French or Paris Lines.

	1				Tenths o	f an Inch				
English Inches.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Par lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par line	. Par.lines	Par.lines.	Par.lines	Par.lines.
11	123.85	124.93	126.11	127.23	128.36	129.48	130.61	131.74	132.86	133.99
12	135.11	136.24	137.37	138.49	139.62	140.74	141.87	143.00	144.12	145.25
13	146.37	147.50	148.63	149.75	150.88	152.00	153.18	154.26	155.88	156.51
14	157.63	158.76	159.88	161.01	162.14	163.26	164.89	165.51	166.64	167.77
15	168.89	170.02	171.14	172.27	173 40	174.52	175.65	176.77	177.90	179.03
16	180.15	181.28	182.40	183.53	184.66	185.78	186.91	188.03	189.16	190.29
				Hundre	dths of an	Inch.				
0.	1.	9.	8.	4.	, } ;	5.	6.	7.	8.	9.
0.000	0.113	0.225	0.338	0.45	0.	563	0.676	0.788	0.901	1.013
English Inches and				1	Iundreith	of an In	ch.			
Inches and Tenths.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines	Par lines.	Par.lines.	Par.lines	Par lines	Par.lines.	Par lines.	Par.lines.	Par.lines.
17.0	191.41	191.52	191.64	191.75	191.86	191.97	192.09	192.20	192.31	192.42
1	192.54	192.65	192.76	192.88	192.99	193.10	193.21	198.33	193.44	198.55
2	193.66	193.78	193.89	194.00	194.11	194-28		194.45	194.56	194.68
8	194.79	194.90	195.01	195.13	195.24	195.35	1	195.58	195.69	195.80
4	195.92	196.03	196.14	196.25	196.37	196.48	196.59	196.70	196.82	196.93
5	197.04	197.15	197.27	197.88	197.49	197.60	197.72	197.83	197.94	198.05
6	198.17	198.28	198.89	198.50	198.62	198.78	198.84	198.96	199.07	199.18
7	199.29	199.41	199.52	199.63	199.74	199.86	199.97	200.08	200.19	200.31
8	200.42	200.53	200.64	200.76	200.87	200.98	201.09	201.21	201.32	201.48
9	201.55	201.66	201.77	201.88	202.00	202.11	202.22	202.33	202.45	202.56
18.0	202.67	202.78	202.90	203.01	203.12	203.28	208.35	203.46	203.57	203.68
1	203.80	203.91	204.02	204.13	204.25	204.36	1	204.59	204.70	204.81
2	204.92	205.04	205.15	205.26	205.37	205.49	205.60	205.71	205.82	205.94
8	206.05	206.16	206.27	206.39	206.50	206.61	206.72	206.84	206.95	207.06
4	207.17	207.29	207.40	207.51	207.63	207.74	207.85	207.96	208.08	208.19
5	208.30	208.41	208.58	208.64	208.75	208.86	208.98	209.09	209.20	209.31
6	209.43	209.54	209.65	209.76	209.88	209.99	210.10	210.21	210.33	210.44
7	210.55	210.67	210.78	210.89	211.00	211.12	211.23	211.34	211.45	211.57
8	211.68	211.79	211.90	212.02	212.13	212.24	212.85	212.47	212.58	212.69
9	212.80	212.92	213.03	213.14	213.25	213.87	213.48	218.59	218.71	218.32
19.0	213.98	214.04	214.16	214.27	214.38	214.49	214.61	214.72	214.83	214.94
1	215.06	215.17	215.28	215.89	215.51	215.62	215.73	215.84	215.96	216.07
2	216.18	216.29	216.41	216.52		216.75		216.97	217.08	217.20
8	217.31			217.65	217.76	217.87	217.98			218.32
4	218.43	218.55	218.66	218.77	218.88	219.00	219.11	219.22	219.34	219.45
5	219.56	219.67	219.79	219.90	220.01	220.12	220.24	220.35	220.46	220.57
6	220.69	220.80	220.91	221.02	221.14		221.36			221.70
7	221.81	221.92	222.04		222.26	222.38	1 1		1	222.83
8	222.94	223.05	223.16		223.39	223.50	228.61	223.73	223.84	223.95
9	224.06	224.18	224.29	224.40	224.51		224.74			

1 English Inch = 11.2595 French or Paris Lines.

•			1 MORING	1100 = 1	1.2000 F 101	ach or Pari	, MUSOS.			
English Inches and				I	lundredthe	of an Inc	h.			
Tenths.	0.	1.	9.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Parlines.	Per.line
20.0	225.19	225.30	225.42	225.53	225.64	225.75	225.87	225.98		226.20
1	226.32	226.43	226.54	226.65	226.77	226.88	226.99	227.10	227.22	227.3
2	227.44	227.55	227.67	227.78	227.89	228.00	228.12	228.23	228.34	228.4
8	228.57	228.68	228.79	228.91	229.02	229.13	229.24	229.36	229.47	229.5
4	229.69	229.81	229.92	230.03	280.14	230.26	280.37	230.48	230.59	230.7
5	230.82	230.93	281.04	231.16	281.27	231.38	231.50	231.61	231.72	231.8
6	231.95	232.06	232.17	232.28	232.40	232.51	232.62	232.78	232.85	232.9
7	233.07	233.18	233.30	233.41	233.52	233.68	233.75	233.86	233.97	234.09
8	234.20	234.31	234.42	234.54	234.65	234.76	234.87	234.99	235.10	235.2
9	235.32	285.44	285.55	235.66	235.77	235.89	286.00	236.11	236.22	236.3
21.0	236.45	236.56	236.67	236.79	236.90	237.01	237.18	237.24	237.35	237.4
ų	237.58	237.69	237.80	287.91	238.03	238.14	238.25	238.36	238.48	238.5
2	23 8. 7 0	238.81	288.98	239.04	239.15	239.26	239.38	239.49	239.60	239.7
8	239.83	239.94	240.05	240.17	240.28	240.39	240.50	240.62	240.73	240.8
4	240.95	241.07	241.18	241.29	241.40	241.52	241.68	241.74	241.85	241.97
5	242.08	242.19	242.30	242.42	242.58	242.64	242.75	242.87	242.98	243.0
6	248.21	248.82	248.48	243.54	243.66	243.77	248.88	248.99	244.11	241.2
7	244.33	244.44	244.56	244.67	244.78	244.89	245.01	245.12	245.23	245.3
8	245.46	245.57	245.68	245.79	245.91	246.02	246.18	246.25	246.36	246.47
9	246.58	246.70	246.81	246.92	247.08	247.15	247.26	247.87	247.48	247.60
22.0	247.71	247.82	247.98	248.05	248.16	248.27	248.38	248.50	248.61	248.7
1	248.83	248.95	249.06	249.17	249.29	249.40	249.51	249.62	249.74	249.8
2	249.96	250.07	250.19	250.30	250.41	250.52	250.64	250.75	250.86	250.9
3	251.09	251.20	251.31	251.42	251.54	251.65	251.76	251.89	251.99	252.1
4	252.21	252.33	252.44	252.55	252.66	252.78	252.89	253.00	253.11	253.2
5	253-84	253.45	253.56	253.68	258.79	253.90	254.01	254.18	254.24	254.3
6	254.46	254.58	254.69	254.80	254.92	255.08	255.14	255.25	255.37	255.4
7	255.59	255.70	255.82	255.98	256.04	256.15	256.27	256.38	256.49	256.6
8	256.72	256.83	256.94	257.05	257.17	257.28	257.89	257.50	257.62	257.7
9	257.84	257.96	258.07	258.18	258.29	258.41	258.52	258.63	258.74	258.80
23.0	258.97	259.08	259.19	259.31	259.42	259.58	259.64	259.76	259.87	259.96
1	260.09	260.21	260.82	260.48	260.54	260.66	260.77	260.88	261.00	261.11
2	261.22	261.88	261.45	261.56	261.67	261.78	261.90	262.01	262.12	262.23
3	262.35	262.46	262.57	262.68	262.80	262.91	263.02	263.13	263.25	263.36
4	263.47	263.5 8	268.70	263.81	263.92	264.04	264.15	264.26	264.37	264.49
5	264.60	264.71	264.82	264.94	265.05	265.16	265.27	265.39	265.50	265.61
6	265.72	265.84	265.95	266.06	266.17	266.29	266.40	266.51	266.62	266.74
7	266.85	266.96	267.08	267.19	267.30	267.41	267.53	267.64	267.75	267.86
8	267.98	268.09	268.20	269.31	268.48	268.54	268.65	268.76	268.88	268.99
9	269.10	269.21	269.38	269.44	269.55	269.67	269.78	269.89	270.00	270.12
	0.	1.	2.	8.	4.			ı		9.

1 English Inch = 11.2595 French or Paris Lines.

English nches and				E	landredthe	of an Incl	h.			
Tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.		Par.lines.		Par.lines.		Par.lines.	l -	Par.lines.	Par.line
24.0	270.23	270.34	270.45	270.57	270.68	270.79	270.90	271.02	271.13	271.2
1	271.35	271.47	271.58	271.69	271.80	271.92	272.03	272.14	272.25	272.3
2	272.48	272.59	272.71	272.82	272.93	278.04	273.16	278.27	273.39	278.4
3	273.61	273.72	273.83	273.94	274.06	274.17	274.28	274.89	274.51	274.6
4	274.73	274.84	274.96	275.07	275.18	275.29	275.41	275.52	275.63	275.7
5	275.86	275.97	276.08	276.20	276.81	276.42	276.53	276.65	276.76	276.8
6	276.98	277.10	277.21	277.32	277.43	277.55	277.66	277.77	277.88	278.0
7	278.11	278.22	278.33	278.45	278.56	278.67	278.79	278.90	279.01	279.1
8	279.24	279.35	279.46	279.57	279.69	279.80	279.91	280.02	280.14	280.2
9	280.36	280.47	280.59	280.70	280.81	280.92	281.04	281.15	281.26	281.9
25 .0	281.49	281.60	281.71	281.83	281.94	282.05	282.16	282.28	282.39	282.5
1	282-61	282.73	282.84	282.95	283.06	283.18	283.29	283.40	283.51	283.6
2	288.74	288.85	283.96	284.08	284.19	284.30	284.41	284.53	284.64	284.7
3	284.87	284.98	285.09	285.20	285.32	285.43	285.54	285.65	285.77	285.8
4	285.99	286.10	286.22	286.83	286.44	286.55	286.67	286.78	286.89	287.0
5	287.12	287.23	287.84	287.46	287.57	287.68	287.79	287.91	288.02	288.1
6	288.24	288.36	288.47	288.58	288.69	288.81	288.92	289.03	289.14	289.2
7	289.87	289.48	289.59	289.71	289.82	289.93	290.04	290.16	290.27	290.8
8	290.50	290.61	290.72	290.83	290.95	291.06	291.17	291.28	291.40	291.5
9	291.62	291.78	291.85	291.96	292.07	292.18	292.30	292.41	292.52	292.6
26.0	292.75	292.86	292.97	293.08	293.20	293.31	293.42	293.54	293.65	293.7
1	293.87	293.99	294.10	294.21	294.82	294.44	294.55	294.66	294.77	294.8
2	295.00	295.11	295.22	295.34	295.45	295.56	295.67	295.79	295.90	296.0
3	296.12	296.24	296.35	296.46	296.58	296.69	296.80	296.91	297.08	297.1
4	297.25	297.86	297.48	297.59		297.81	297.98	298.04	298.15	298.2
•	291.20	251.00	291.40	287.38	297.70	297.51	251.50	290.04	250.10	200.2
5	296.3 3	298.49	298.60	298.71	298.88	298.94	299. 05	29 9.17	299.28	299.3
6	299.50	299.62	299.73	299.84	299.95	300.07	800.18	800.29	300.40	300.
7	800.63	800.74	800.85	800.97	301.08	301.19	301.30	801.42	801.53	801.6
8	301.75	301.87	801.98	802.09	802.20	302.82	802.43	802.54	802.66	302.7
9	302.88	802.99	803.11	303.22	803.38	303.44	803.56	803.67	803.78	303.8
27.0	804.01	804.12	804.23	804.84	304.46	304.57	304.68	804.79	304.91	805.0
1	305.13	305.25	805.36	305.47	305.58	805.70	305.81	805.92	306.03	306.1
2	306.26	806.37	306.48	806.60	306.71	306.82	306.93	807.05	307.16	307.2
3	307.38	807.50	807.61	307.72	307.83	807.95	808.06	808.17	808.29	308.4
4	308.51	808.62	808.74	308.85	308.96	309.07	309.19	809.30	809.41	809.5
5	309.64	309.75	809.86	309.97	810.09	810.20	810.81	810.42	810.54	810.6
6	310.76	310.87	310.99	311.10	811.21	311.88	811.44	811.55	811.66	311.7
7	311.89	312.00	812.11	312.23	812.84	812.45	812.56	312.68	812.79	812.9
8	813.01	313.13	813.24	\$13.85	813.46	313.58	318.69	313.80	318.91	314.0
9	814.14	314.25	814.37	314.48	814.59	814.70	814.82	814.98	815.04	315.1
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 English Inch = 11.2595 French or Paris Lines.

Inglish Inches and				I	Iandredth	of an Inc	b.			
Tenths.	6.	1.	2.	3.	4.	5.	6.	7.	8.	9.
20	Par.lines.	Par.lines.		Par.lines.	Par.lines.		Par.lines.			
28.0	815.27	315.38	315.49	315.60	815.72	815.83	315.94	316.05	T .	316.2
1	316.39	316.50	316.62	816.78	816.84	816.95	317.07	317.18	1	317.4
2	817.52	317.63	817.74	317.86	817.97	318.08	318.19	318.31	818.42	318.5
8 4	318.64 319.77	318.76 319.88	318.87 319.99	318.98 320.11	319.09 82 0.22	819.21 820.88	319.82 320.45	319.43 820.56	l	319.6 320.7

5	320.90	321.01	321.12	321.23	821.35	321.46	321.57	321.68		321.9
6	822.02	822.13	322.25	822.36	822.47	822.58	322.70	322.81		323.0 324.1
7	323.15	323.26	323.37	323.49	323.60	323.71	323.82	323.94		325.2
8 9	324.27 325.40	324.39 325.51	824.50 325.62	324.61 825.74	824.72 325.85	324.84 825.96	324.95 326.08	825.06 826.19	325.17 326.30	326.4
00 4		200.01	200 27	200.00	500 00	-0° 00	90* 90	007 01	997 19	327.5
29 .0	326.53	326.64	826.75	826.86	326.98	327.09	327.20 328.33	327.81 328.44	327-43 328-55	328.6
1	327.65 328.78	327.76 328.89	327.88 329.00	327.99 329.12	328.10 329.23	328.21 329.34	829.45	329.57	l .	329.7
2 8	329.90	330.02	830.18	330.24	380.35	830.47	330.58	330.69	1	330.9
4	331.08	331.14	331.25	831.87	331.48	831.59	831.70	331.82		332.0
	800.10	990 0*	000 00	600 40	020 61	200 00	000 00	999 04	333.06	333.1
5 6	332.16 333.28	332.27 338.39	332.38 338.51	832.49 838.62	332.61 333.78	382.72 333.84	332.83 333.96	832.94 834.07	334.18	334.2
-	1	334.52	834.68	834.74	334.86	884.97	335.08	335.20		835.4
7 8	834.41 335.53	335.65	835.76	835.87	885.98	336.10	336.21	336.32	1	336.5
9	336.66	336.77	336.88	887.00	387.11	837.22	337.33	837.45		337.6
30 .0	337.78	837.90	388.01	338.12	338.24	338.85	338.46	338.57	339.69	338.8
1	338.91	389.02	839.14	339.25	339.36	339.47	339.59	839.70	1	339.9
2	310.01	840.15	340.26	340.37	840.49	840.60	340.71	340.83	340.94	341.0
8	341.16	341.28	341.39	841.50	341.61	841.73	341.84	841.95	342.06	342.1
4	342.29	842.40	342.51	342.63	342.74	842.85	342.96	343.08	343.19	343.3
5	343.41	3 13.53	343.64	843.75	343.87	843.98	344.09	844.20	344.32	344.4
6	344.54	344.63	344.77	341.88	844.99	845.10	345.22	345.33	345.44	345.5
7	345.67	345.78	845.89	346.00	346.12	846.23	346.34	846.45	346.57	346.6
8	346.79	846.91	347 02	347.13	847.24	847.36	347.47	347.58	847.69	347.8
9	847.92	348.03	348.14	348.26	848.37	348.48	348.59	348.71	348.82	348.9
31.0	349.04	349.16	349.27	349.38	849.49	349.61	349.72	349.83	349.95	350.0
1	350.17	850.28	850.40	850.51	350.62	850.78	850.85	850.96	1	851.1
2	351.30	351.41	851.52	351.63	351.75	851.86	351.97	352.08		352.3
8	352.42	352.53	852.65	352.76	352.87	352.99	858.10	353.21	1	353.4
4	853.55	353.66	353.77	853.89	854.00	854.11	854.22	854.34		354.5
5	354.67	1	354.90				855.85		1	l
6	855.80	855.91	356.03	<u> </u>		356.36	300.45	300.39	850.70	1 390.0
				Thousar	dths of an	Inch.				
0.	1.	9.	8.	4.	_ _	5.	6.	7.	8.	9.
0.000	0.011	0.023	0.084	0.04	5 0.	056 0	.068	0.079	0.090	0.101

III.-IV.

COMPARISON

07

THE METRICAL BAROMETER

WITH

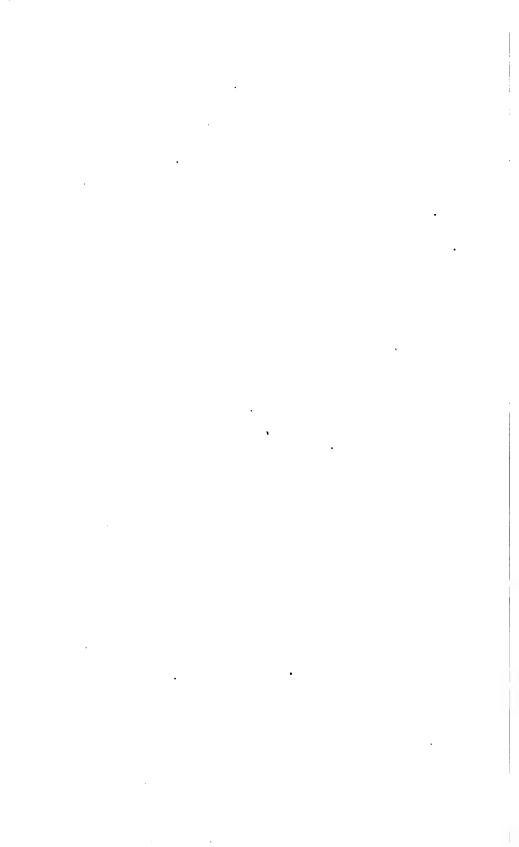
THE ENGLISH AND THE OLD FRENCH BAROMETERS,

OR

TABLES

FOR CONVERTING MILLIMETRES INTO ENGLISH INCHES AND DECIMALS,
AND INTO FRENCH OR PARIS LINES;

GIVING THE VALUES CORRESPONDING TO EVERY MILLIMETRE FROM 250 TO 600; AND TO EVERY TENTH OF A MILLIMETRE FROM 600 TO 800 MILLIMETRES.



1 Metre = 89.87079 English Inches.

Millimo- tres.					Millimetre	e. Units.	•			
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Ing. In.	Eng. In.		1 -	Eng. In.	
250	9.843	9.882	9.921	9.961	10.000	10.040	10.079	10.118	10.158	10.197
260	10.236	10.276	10.315	10.355	10.894	10.433	10.478	10.512	10.551	10.591
270	10.630	10.669	10.709	10.748	10.788	10.827	10.866	10.906	10.945	10.984
280	11.024	11.063	11.103	11.142	11.181		11.260	11.299	11.339	11.378
290	11.418	11.457	11.496	11.536	11.575	11.614	11.654	11.698	11.782	11.772
300	11.811	11.851	11.890	11.929	11.969	12.008	12.047	12.087	12.126	12.166
310	12.205	12.244	12.284	12.323	12.862	12.402	12.441	12.481	12.520	12.559
32 0	12.599	12.638	12.677	12.717	12.756	12.795	12.885	12.874	12.914	12.953
230	12.992	13.032	13.071	13.110	13.150	13.189	18.229	18.268	13.307	13.547
340	13-386	18.425	13.465	18.504	18.544	13.583	18.622	13.662	18.701	13.740
350	18.780	13.819	18.859	13.898	18.937	18.977	14.016	14.055	14.095	14.134
360	14.178	14.213	14.252	14.292	14.881	14.870	14.410	14.449	14.488	14.528
870	14.567	14.607	14.646	14.685	14.725	14.764	14.803	14.843	14.882	14.922
380	14.961	15.000	15.040	15.079	15.118	15.158	15.197	15.236	15.276	15.815
390	15.855	15.494	15.438	15.473	15.512	15.551	15.591	15.680	15.670	15.709
400	15.748	15.788	15.827	15.866	15.906	15.945	15.985	16.024	16.063	16.103
410	16.142	16.181	16.221	16.260	16.300	16.389	16.878	16.418	16.458	16.496
420	16.586	16.575	16.614	16.654	16.698	16.788	16.772	16.811	16.851	16.890
430	16.929	16.969	17.008	17.048	17.087	17.126	17.166	17.205	17.244	17.284
440	17.328	17.862	17.402	17.441	17.481	17.520	17.559	17.599	17.688	17.677
450	17.717	17.756	17.796	17.885	17.874	17.914	17.958	17.992	18.032	18.071
460	18.111	18.150	18.189	18.229	18.268	18.307	18.347	18.386	18.426	18.465
470	18.504	18.544	18.588	18.622	18.662	18.701	18.740	18,780	18.819	18.859
480	18.898	18.937	18.977	19.016	19.055	19.095	19.134	19.174	19.213	19.252
490	19.292	19.831	19.870	19.410	19.449	19.489	19.528	19.567	19.607	19.646
500	19.685	19.725	19.764	19.804	19.843	19.882	19.922	19.961	20.000	20.040
510	20.079	20.118	20.158	20.197	20.287	20.276	20.815	20.355	20.394	20.433
520	20.478	20.512	20.552	20.591	20.630	20.670	20.709	20.748	20.788	20.827
530	20.867	20.906	20.945	20.985	21.024	21.068	21.103	21.142	21.181	21.221
540	21.260	21.800	21.339	21.878	21.418	21.457	21.496	21.586	21.575	21.615
550	21.654	21.693	21.788	21.772	21.811	21.851	21.890	21.930	21.969	22.008
560	22.048	22.037	22.126	22.166	22.205	22.244	22.284	22.828	22.363	22.402
570	22.441	22.481	22.520	22.559	22.599	22.638	22.678	22.717	22.756	22.796
580	22.835	22.874	22.914	22.958	22.993	23.032	28.071	23.111	23.150	23.189
590	23.229	28.268	28.308	28.847	23.386	23.426	23.465	23.504	23.544	28.588
<u> </u>				Tenths	of Millime	otres.				
0.	1.	2.	3.	4.	0	5.	6.	7.	8.	9.
0.000	0.004	0.008	0.012	0.01	в 0.0	020 0	.024 (0.028	0.081	0.035

1 Metre = 89.87079 English Inches.

Millime-	Tenths of Millimetres. 0. 1. 2. 3. 4. 5. 6. 7. 8.									
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng In.	Eog. In.	Eng. In.	Eng. In.	Eng. In.	Rng. In.	Eng. In.		Eng. In.	Eng. I
600	28.622	23.626	23.680	23.684	23.638 23.678	23.642	23.646	23.650	23.654	23.69
601	23.662 23.701	23.666 23.705	23.670 28.709	28.713	23.717	23.682 23.721	28.685 28.725	23.689 23.729	23.783	23.7
602 603	23.741	28.745	23.748	23.752	25.717	23.721	28.764	28.768	23.772	23.7
604	23.780	23.784	28.788	28.792	28.796	23.800	28.804	28.808	23.811	23.8
ens.	23.819	23.823	23.827	23.831	23.885	23.839	28.843	23.847	23.851	23.8
605 606	23.859	23.863	28.867	23.871	23.574	23.878	23.882	23.886	23.890	23.8
607	23.898	23.902	28.906	23.910	28.914	23.918	28.922	28.926	23.930	23.9
608	23.937	23.941	23.945	28.949	23.958	28.957	28.961	23.965	23.969	23.9
609	23.977	23.981	28.985	23.989	23.998	23.996	24.000	24.004	24.008	24.0
610	24.016	24.020	24.024	24.028	24.032	24.036	24.040	24.044	24.048	24.0
611	24.056	24.059	24.063	24.028	24.071	24.075	24.079	24.083	24.067	24.0
612	24.095	24.099	24.103	24.107	24.111	24.115	24.119	24.122	24.126	24.13
613	24.134	24.138	24.142	24.146	24.150	24.154	24.158	24.162	24.166	24.17
614	24.174	24.178	24.182	24.185	24.189	24.198	24.197	24.201	24.205	24.20
615	24.213	24.217	24.221	2 4.225	24.229	24.233	24.237	24.241	24.245	24.2
616	24.252	24.256	24.260	24.264	24.268	24.272	24.276	24.280	24.284	24.28
617	24.292	24.296	24.300	24.304	24.308	24.811	24.315	24.819	24.323	24.32
618	24.331	24.835	24.389	24.843	24.347	24.351	24.355	24.359	24.363	24.36
619	24.371	24.874	24.878	24.382	24.886	24.890	24.894	24.398	24.402	24.40
620	24.410	24.414	24.418	24.422	24.426	24.480	24.484	24.487	24.441	24.4
621	24.449	24.453	24.457	24.461	24.465	24.469	24.478	24.477	24.481	24.48
622	24.489	24.493	24.497	24.500	24.504	24.508	24.512	24.516	24.520	24.52
623	24.528	24.532	24.536	24.540	24.544	24.548	24.552	24.556	24.559	24.50
624	24.567	24.571	24.575	24.579	24.583	24.587	24.591	24.595	24.599	24.60
625	24.607	24.611	24.615	24.619	24.622	24.626	24.630	24.634	24.638	24.64
626	24.646	24.650	24.654	24.658	24.662	24.666	24.670	24.671		24.68
627	24.685	24.689	24.693	24.697	24.701	24.705	24.709	24.713	24.717	24.72
628	24.725	24.729	24.733	24.787	24.741	24.745	24.748	24.752	24.756	24.70
629	24.764	24.768	24.772	24.776	24.780	24.784	24.788	24.792	24.796	24.80
630	24.804	24.808	24.811	24.815	24.819	24.828	24.827	24.831	24.835	24.8
631	24.843	24.847	24.851	24.855	24.859	24.863	24.867	24.871	24.874	24.87
632	24.882	24.886	24.890	24.894	24.898	24.902	24.906	24.910	24.914	24.91
633	24.922	24.926	24.930	24.984	24.937	24.941	24.945	24.949	24.953	24.90
634	24.961	24.965	24.969	24.973	24.977	24.981	24.985	24.989	24.993	24.99
635	25.000	25.004	25.008	25.012	25.016	25.020	25.024	25.028	25.032	25.03
686	25.040	25.044	25.048	25.052	25.056	25.060	25.068	25.067	25.071	25.07
637	25.079	25.083	25.087	25.091	25.095	25.099	25.103		25.111	25.11
638	25.119	25.128	25.126	25.130	25.134	25.188	1	25.146	I.	25.18
639	25.158	25.162	25.166	25.170	25.174	25.178	25.182	25.185	25.189	25.19
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Metre = 89.87079 English Inches

Millime-				!	Tenths of	Millimetres				
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. in.	Eng. In.	Eng. In.	Eng. In.	Eng In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In
640	25.197	25.201	25.205	25.209	25.213	25.217	25.221	25.225	25.229	25.238
641	23.237	25.241	25.245	25.248	25.252	25 256	25.260	25.264	25.268	25.272
642	25.276	25.280	25.284	25.288	25.292	25.296	25.300	25.304	25.308	25.311
643	25.315	25.319	25.323	25.327	25.331	25.335	25.889	25.343	25.347	25.35
644	25.355	25.359	25.363	25.367	25.371	25.874	25.878	25.382	25.386	25.390
645	25.394	25.398	25.402	25.406	25.410	25.414	25.418	25.422	25.426	25.480
646	25.434	25.437	25.441	25.445	25.449	25.458	25.457	25.461	25.465	25.469
647	25.473	25.477	25.481	25.485	25.489	25.493	25.497	25.500	25.504	25.508
648	25.512	25.516	25.520	25.524	25.528	25.532	25.536	25.540	25.544	25.548
649	25.552	25.556	25.560	25.563	25.567	25.571	25.575	25.579	25.588	25.587
650	25.591	25.595	25.599	25.603	25.607	25.611	25.615	25.619	25.623	25.626
651	25.630	25.634	25.638	25.642	25.646	25.630	25.654	25.658	25.662	25.66
652	25.670	25.674	25.678	25.682	25.686	25.689	25.693	25.697	25.701	25.70
653	25.709	25.713	25.717	25.721	25.725	25.729	25.738	25.737	25.741	25.74
654	25.748	25.752	25.756	25.760	25.764	25.768	25.772	25.776	25.780	25.78
655	25.788	25.792	25.796	25.800	25.804	25.808	25.811	25.815	25.819	25.82
656	25.827	25.831	25.935	25.839	25.843	25.847	25.851	25.855	25.859	25.86
657	25.867	25.871	25.874	25.878	25.882	25.886	25.890	25.894	25.898	25.902
656	25.906	25.910	25.914	25.918	25.922	25.926	25.930	25.984	25.937	25.94
659	25.945	25.949	25.953	25.957	25.961	25.965	25.969	25.973	25.977	25.981
660	25.985	25.989	25.993	25.997	26.000	26.004	26.008	26.012	26.016	26.020
661	26.024	26.028	26.032	26.036	26.040	26.044	26.048	26.052	26.056	26.060
662	26.063	26.067	26.071	26.075	26.079	26.088	26.087	26.091	26.095	26.099
663	26.103	26.107	26.111	26.115	26.119	26.123	26.126	26.130	26.184	26.188
664	26.142	26.146	26.150	26.154	26.158	26.162	26.166	26.170	26.174	26.178
665	26.182	26.186	26.189	26.193	26.197	26.201	26.205	26.209	26.213	26.21
666	26 221	26.225	26.229	26.233	26.237	26.241	26.245	26.249	26.252	26.25
667	26.260	26.264	26.268	26.272	26.276	26.280	26.284	26.288	26.292	26.29
668	26.300	26.304	26.308	26.311	26.815	26.319	26.328	26.327	26.831	26.33
669	26.339	26.343	26.347	26.351	26.855	26.859	26.863	26.867	26.871	26.37
670	26.378	26.382	26.386	26.390	26.894	26.898	26.402	26.406	26.410	26.41
671	26.418	26.422	26.426	26.480	26.484	26.437	26.441	26.445	26.449	26.45
672	26.457	26.461	26.465	26.469	26.473	26.477	26.481	26.485	26.489	26.49
673	26.497	26.500	26.504	26.508	26.512	26.516	26.520	26.524	26.528	26.582
674	26.536	26.540		26.548	26.552	26.556		26.563	26.567	26.57
675	26.575	26.579	26.583	26.587	26.591	26.595	26.599	26.603	26.607	26.61
676	26.615	26.619	26.623	26.626	26.630	26.634	26.688	26.642	26.646	26.650
677	26.654	26.658	26.662	26.666	26.670	26.674	26.678	26.682	26.686	26.689
678	26.693	26.697	26.701	26.705	26.709	26.713	26.717	26.721	26.725	26.729
679	26.733	26.737	26.741	26.745	26.749	26.752	26.756	26.760	26.764	26.76
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Metre = 89.87079 English Inches.

Millime-					Tenths of 1	Killimetres				
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.			Eng. In
680	26.772	26.776	26.780	26.784	26.788	26.792	26.796	26.800	26.804	26.80
681	26.812	26.815	26.819	26.823	26.827	26.831	26.885	26.839	26.843	26.84
682	26.851	26.855	26.859	26.863	26.867	26.871	26.875	26.878	26.882	26.88
683	26.890	26.894	26.898	26.902	26.906	26.910	26.914	26.918	26.922	26.92
684	26.930	26.934	26.937	26.941	26.945	26.919	26.958	26.957	26.961	26.96
685	26.969	26.978	26.977	26.981	26.985	26.989	26.993	26.997	27.000	27.00
686	27.008	27.012	27.016	27.020	27.024	27.028	27.082	27.036	27.040	27.04
687	27.048	27.052	27.056	27.060	27.063	27.067	27.071	27.075	27.079	27.08
688	27.087	27.091	27.095	27.099	27.108	27.107	27.111	27.115	27.119	27.12
689	27.126	27.130	27.134	27.188	27.142	27.146	27.150	27.154	27.158	27.16
690	27.166	27.170	27.174	27.178	27.182	27.186	27.189	27.193	27.197	27.20
691	27.205	27.209	27.213	27.217	27.221	27.225	27.229	27.233	27.287	27.24
692	27.245	27.249	27.252	27.256	27.260	27.264	27.268	27.272	27.276	27.28
693	27.284	27.288	27.292	27.296	27.800	27.304	27.808	27.812	27.815	27.81
694	27.323	27.827	27.331	27.835	27.839	27.843	27.847	27.851	27.355	27.35
695	27.363	27.367	27.371	27.875	27.378	27.382	27.886	27.390	27.894	27.39
696	27.402	27.406	27.410	27.414	27.418	27.422	27.426	27.430	27.484	27.43
697	27.441	27.445	27.419	27.458	27.457	27.461	27.465	27.469	27.473	27.47
698	27.481	27.485	27.489	27.498	27.497				27.512	1
699	27.520	27.524	27.528	27.532	27.536	27.500 27.540	27.504 27.544	27.508 27.548	27.512	27.51 27.55
700	27.560	27.563	27.567	27.571	00 505	07 570	07 500		04 501	
	27.599	1	l		27.575	27.579	27.583	27.587	27.591	27.59
701		27.603	27.607	27.611	27.615	27.619	27.628	27.626	27.630	27.63
702	27.638	27.642	27.646	27.650	27.654	27.658	27.662	27.666	27.670	27.67
703	27.678	27.682	27.686	27.689	27.693	27.697	27.701	27.705	27.709	27.71
704	27.717	27.721	27.725	27.729	27.733	27.787	27.741	27.745	27.749	27.75
705	27.756	27.760	27.764	27.768	27.772	27.776	27.780	27.784	27.788	27.79
706	27.796	27.800	27.804	27.808	27.812	27.815	27.819	27.823	27.827	27.83
707	27.835	27.839	27.848	27.847	27.851	27.855	27.859	27.868	27.867	27.87
708	27.875	27.878	27.882	27.886	27.890	27.894	27.898	27.902	27.906	27.91
709	27.914	27.918	27.922	27.926	27.930	27.934	27.938	27.941	27.945	27.94
710	27.953	27.957	27.961	27.965	27.969	27.973		27.981	27.985	27.98
711	27.993	27.997	28.001	28.004	28.008	28.012	28.016	28.020	28.024	28.02
712	28.032	28.086	28.040	28.044	28.048	28.052	28.056	28.060	28.063	28.06
713	28.071	28.075	28.079	28.083	28.087	28.091	28.095	28.099	28.103	28.10
714	28.111	28.115	28.119	28.123	28.126	28.130	28.134	28.138	28.142	28.14
715	28.150		1	28.162		28.170	1	1	28.182	28.18
716	28.189	28.193	29.197	28.201	28.205	28.209	28.218	28.217	28.221	28.22
717	28.229	28.288	28.237	28.241	28.245	28.249	28.252	28.256	28.260	28.26
718	28.268	28.272	28.276	28.280	28.284	29.288	28.292	28.296	28.300	28.30
719	28.308	28.312	28.315	28.319	28.323	28.327	28.831	28.835	28.339	28.84
	₽.	1.	2.	8.	4.	5.	6.	7.	8.	9.

1 Metre = 89.87079 English Inches.

Millime-				•	Countles of 1	Millimetres	•		,	
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. In.	Eng. In.		Eng. In.		Eng. In.	Eng. In.	, -	, -	Eng. In.
720	28.347	28.351	28.355	28.359	28.363	28.367	28.871	28.375	28.378	28.382
721	28.386	28.890	28.394	28.398	28.402	28.406	28.410	28.414	28.418	28.422
722	28.426	28.480	28.484	28.438	28.441	28.445	28.449	28.453	28.457	28.461
723	28.465	28.469	28.473	28.477	28.481	28.485	28.489	28.493	28.497	28.501
724	28.504	28.508	28.512	28.516	28.520	28.524	28.528	28.532	28.536	28.540
725	28.544	28.548	28.552	28.556	28.560	28.564	28.567	28.571	28.575	28.579
726	28.583	28.587	28.591	28.595	28.599	28.603	28.607	28.611	28.615	28.619
727	28.623	28.627	28.630	28.634	28.638	28.642	28.646	28.650	28.654	28.658
728	28.662	28.666	28.670	28.674	28.678	28.682	28.686	28.689	28.693	28.697
729	28.701	28.705	28.709	28.718	28.717	28.721	28.725	28.729	28.733	28.737
730	28.741	28.745	28.749	28.752	28.756	28.760	28.764	28.768	28.772	28.776
731	28.780	28.784	28.788	28.792	28.796	28.800	28.804	28.808	28.812	28.815
732	28.819	28.828	28.827	28.831	28.835	28.839	28.843	28.847	28.851	28.855
733	28.859	29.863	28.867	28.871	28.875	28.878	28.882	28.886	28.890	28.894
734	28.898	28.902	28.906	28.9 10	28.914	28.918	28.922	28.926	28.930	28.934
735	28.938	28.941	28.945	28.949	28.953	28.957	28.961	28.965	28.969	28.978
786	28.977	28.981	23.985	28.989	28.993	28.997	29.001	29.004	29.008	29.012
787	29.016	29.020	29.024	29.028	29.032	29.036	29.040	29.044	29.048	29.052
738	29.056	29.060	29.064	29.067	29.071	29.075	29.079	29.088	29.087	29.091
789	29.095	29.099	29.108	29.107	29.111	29.115	29.119	29.128	29.127	29.130
740	29.134	29.138	29.142	29.146	29.150	29.154	29.158	29.162	29.166	29.170
741	29.174	29.178	29.182	29.186	29.190	29.198	29.197	29.201	29.205	29.209
742	29.213	29.217	29.221	29.225	29.229	29.233	29.237	29.241	29.245	29.249
748	29.252	29.256	29.260	29.264	29.268	29.272	29.276	29.280	29.284	29.288
744	29.292	29.296	29.300	29.304	29.308	29.8 12	29.315	29.319	29.828	29.327
745	29.331	29.335	29.339	29.348	29.847	29.851	29.855	29.359	29.363	29.367
746	29.371	29.875	29.878	29.382	29.886	29.890	29.894	29.398	29.402	29.406
747	29.410	29.414	29.418	29.422	29.426	29.430	29.434	29.438	29.441	29.445
748	29.449	29.458	29.457	29.461	29.465	29.469	29.473	29.477	29.481	29.485
749	29.489	29.493	29.497	29.501	29.504	29.508	29.512	29.516	29.520	29.524
750	29.528	29.532	29.536	29.540	29.544	29.548	29.552	29.556	29.560	29.564
751	29.567	29.571	29.575	29.579	29.588	29.587	29.591	29.595	29.599	29.603
752	29.607	29.611	29.615	29.619	29.628	29.627	29.630	29.634	29.638	29.642
753	29.646	29.650	29.654	29.658	29.662	29.666	29.670	29.674	29.678	29.632
754	29.686	29.690	29.693	29.697	29.701	29.705	29.709	29.713	29.717	29.721
755	29.725	29.729	29.733	29.737	29.741	29.745	29.749	29.753	29.756	29.760
756	29.764	29.768	29.772	29.776	29.780	29.784	29.788	29.792	29.796	29.800
757	29.804	29.808	29.812	29.815	29.819	29.823	29.827	29.831	29.835	29.839
758	29.843	29.847	29.851	29.855	29.859	29.868	29.867	29.871	29.875	29.878
759	29.882	29.886	29.990	29.894	29.898	29.902	29.906	29.910	29.914	29.918
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Metre = 89.87079 English Inches.

Millime-					Tenths of	Millimetre				
tres.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Eng. In.	Eng. In.	Eng. In.	Eng In.	Eng. In.	Eng. In.	Eng. In.	Eng. In	Eng. In.	Eng. In.
760	29.922	29.926	29.930	29.934	29.988	29.941	29.945	29.949	29.953	29.957
761	29.961	29.965	29.969	29.973	29.977	29.9 81	29.985	29.989	29.993	29.997
762	30.001	30.004	30.008	30.012	80.016	30. 020	30.024	30.028	80.032	30.036
763	30.040	30.044	30.048	30.052	30.056	30.060	30.064	30.067	80.071	30 075
764	30.079	80.083	30.087	3 0.091	30.095	80.099	80.108	80.107	80.111	30.115
765	30.119	30.123	30.127	30.130	30.184	30.138	80.142	30.146	80.150	30.15
766	30.158	80.162	80.166	80.170	20.174	30.178	30.182	80.186	30.190	30.19
767	80.197	30.201	80.205	80.209	80.218	80.217	30.221	30.225	30.229	30.23
768	30.237	80.241	80.245	30.249	80.258	30.256	80.260	30.264	30.268	30.277
769	30.276	30.280	80.294	30.288	80.292	30.296	80.300	30.304	30.308	30.31
770	30.316	30.319	30.323	30.327	30.331	80.335	30.339	30.348	30.347	30.35
771	30.355	30.359	30.363	80.867	30.371	30.375	30.379	30.382	30.386	30.390
772	30.394	30.398	80.402	30.406	30.410	30.414	30.418	80.422	30.426	30.434
773	30.434	30.438	30.441	30.445	30.449	30.453	30.457	30.461	30.465	20.469
774	30.473	30.477	80.481	30.485	30.489	30.493	80.497	30.501	30.504	30.50
775	30.512	80.516	80.520	80.524	80.528	80.532	30.536	80.540	30.544	30.549
776	30.552	80.556	30.560	30.564	30.567	80.571	30.575	30.579	30.583	30.587
777	30.591	30.595	80.599	30.608	80.607	30.611	80.615	30.619	80.623	30.627
778	30.630	30.684	80.638	30.642	80.646	80.650	80.654	30.658	30.662	30.666
779	30.670	80.674	30.678	80.682	30.686	80.690	80.693	30.697	30.701	30.708
780	30.709	80.718	30.717	80.721	80.725	30.729	30.733	30.737	30.741	30.745
781	30.749	30.753	80.756	30.760	30.764	30.768	30.772	80.776	30.780	30.784
782	30.788	80.792	30.796	80.800	80.804	30.808	30.812	30.816	30.819	30.823
788	30.827	30.831	30.835	80.839	30.843	30.847	30.851	30.855	30.859	30.863
784	30.867	80.871	30.875	30.879	80.882	30.886	30.890	30.894	30.898	30.902
785	30.906	80.910	30.914	80.918	80.922	80.926	30.930	80.934	30.938	30.942
786	30.945	80.949	80.958	80.957	30.961	30.965	30.969	80.973	30.977	30.981
787	30.985	80.989	30.993	30.997	81.001	81.004	31.008	81.012	81.016	31.020
788	31.024	81.028	81.032	31.036	81.040	81.044	81.048	31.052	31.056	31.060
789	31.064	81.067	81.071	81.075	31.079	81.088	31.087	31.091	81.095	31.09
790	31.103	81.107	31.111	81.115	81.119	31.128	81.127	31.130	31.134	31.13
791	31.142	31.146	31.150	31.154	81.158	31.162	31.166	31.170	31.174	31.178
792	31.182	31.186	31.190	31.198	81.197	31.201	31.205	31.209	81.213	31.217
798	81.221	31.225	31.229	81.233	31.287	31.241	31.245	81.249	31.253	31.256
994	31.260	31.264	31.268	31.272	31.276	81.280	31.284	31.288	31.292	31.296
795	31.300	31.304	81.808	81.312	31.316	31.819	31.328	31.827	31.331	31.335
796	31.889	31.843	81.347	31.351	81.855	81.859	81.863	31.367	31.371	31.375
797	31.879	31.382	81.886	81.390	31.894	81.898	81.402	31.406	31.410	31.414
798	31.418	81.422	31.426	31.430		31.438	81.442	31.445	31.449	31.453
799	31.457	81.461	81.465	81.469	81.473	31.477	31.481	31.485	31.489	31.498
800	31.497	81.501	81.505	81.508	81.512		31.520	81.524	31.528	31.532
			,	napareau	s of Millis	metres.				
0.	1.	2.	3.	4.	_ _ 6	6. (5.	7.	8	9.
			1							

IV. COMPARISON OF THE METRICAL AND OLD FRENCH BAROMETERS.

1 Millimetre - 0.448296 French or Paris Line.

Milmetre					Millimetr	es. V	nits.				
Tens.	6.	1.	2.	3.	4.	5	•	6.	7.	8.	9.
1	Par.lines.	Par.lines	Par.lines	Par.lines	Par.lines.	Par.li	Des.	Par.lines	Par.line	Par.lines.	Par.lines.
300	182.99	133.43	133.88	134.82	134.76	135	.21	135.65	136.09	186.54	136.98
810	137.42	187.87	188.31	138.75	139.19	139.	.64	140.08	140.52	140.97	141.41
820	141.85	142.30	142.74	148.18	143.63	144.	.07	144.51	144.96	145.40	145.84
330	146.29	146.78	147.17	147.62	148.06	148.	.50	148.95	149.39	149.83	150.28
340	150.72	151.16	151.61	152.05	152.49	152	.94	158.38	153.82	154.27	154.71
350	155.15	155.60	156.04	156.48	156.93	157.	.37	157.81	158.26	158.70	159.14
360	159.59	160.03	160.47	160.92	161.36	161	.80	162.25	162.69	168.13	163.58
870	164.02	164.46	164.91	165.85	165.79	166	.24	166.68	167.12	167.57	168.01
380	168.45	169.90	169.34	169.78	170.23	170.	.67	171.11	171.56	172.00	172.44
890	172.89	173.33	178.77	174.22	174.66	175.	.10	175.55	175.99	176.48	176.88
400	177.32	177.76	178.20	178.65	179.09	179.	.53	179.98	180.42	180.86	181.31
410	181.75	182.19	182.64	183.08	183.52	183.	97	184.41	184.85	185.30	185.74
420	186.18	186.63	187.07	187.51	187.96	188.	.40	188.84	189.29	189.73	190.17
430	190.62	191.06	191.50	191.95	192.39	192	88	193.28	198.72	194.16	194.61
440	195.05	195.49	195.94	196.88	196.82	197.	.27	197.71	198.15	198.60	199.04
450	199.48	199.93	200.87	200.81	201.26	201.	70	202.14	202.59	203.03	208.47
460	203.92	204.86	204.80	205.25	205.69	206.	13	206.58	207.02	207.46	207.91
470	208.35	208.79	209.24	209.68	210.12	210.	.57	211.01	211.45	211.90	212.84
480	212.78	213.23	213.67	214.11	214.36	215.	.00	215.44	215.88	216.33	216.77
490	217.22	217.66	218.10	218.54	218.99	219	43	219.87	220.32	220.76	221.20
500	221.65	222.09	222.53	222.98	223.42	223.	86	224.31	224.75	225.19	225.64
510	226.08	226.52	226.97	227.41	227.85	228.	30	228.74	229.18	229.63	230.07
520	230.51	280.96	231.40	231.84	232.29	232	.78	283.17	283.62	284.06	284.50
530	234.95	235.39	235.83	236.28	236.72	287	16	287.61	238.05	238.49	288.94
540	239.38	239.82	240.27	240.71	241.15	241	.60	242.04	242.48	242.98	248.87
550	243.81	244.26	244.70	245.14	245.59	246	.03	246.47	246.92	247.36	247.80
560	248.25	248.69	249.13	249.57	250.01	250		250.91	251.35		252.24
570	252.68	253.12	258.57	254.01	254.45	254		255.34	255.78	1	256.67
580	257.11	257.55	258.00	258.44	258.88	259	.32	259.77	260.21	1	261.10
590	261.54	261.99	262.48	262.87	263.82	263	.76	264.20	264.65	265.09	265.58
	<u>"</u>			Tenths	of Millim	etres.				<u>-!</u>	
0.	1.	2.	3.	4.	5	.		в.	7.	8.	9.
0.000	0.044	0.089	0.188	0.177	-		0.5	266	0.310	0.355	0.899
				nundredi	hs of Milli	metres	•				
0.000	0.004	0.009	0.018	0.018	0.0	22	0.0	27	0.081	0.035	0.040

1 Millimetre = 0.448296 French Line.

Millime-					Cenths of 1	Gillimetres				
tres.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.Hnes.	Par.lines.	Par lines.	Par.line
600	265.98	266.02	266.07	266.11	266.15	266.20	266.24	266.29	266.33	266.3
601	266.42	266.47	266.51	266.55	266.60	266.64	266.69	266.73	266.78	266.8
602	266.86	266.91	266.95	267.00	267.04	267.09	267.13	267.17	267.22	267.2
603	267.81	267.35	267.40	267.44	267.48	267.58	267.57	267.62	267.66	267.7
604	267.75	267.80	267.84	267.88	267.93	267.97	268.02	268.06	268.11	26 8.1
605	268.19	269.24	268.28	268.38	268.87	268.42	268.46	268.50	268.55	268.5
606	268.64	268.68	268.78	268.77	268.81	268.86	268.90	268.95	268.99	269.0
607	269.08	269.13	269.17	269.21	269.26	269.80	269.85	269.39	269.44	269.4
608	269.52	269.57	269.61	269.66	269.70	269.75	269.79	269.83	269.88	269.9
609	269. 97	270.01	270.06	270.10	270.14	270.19	270.28	270.28	270.82	270.3
610	270.41	270.45	270.50	270.54	270.59	270.68	270.68	270.72	270.77	270.8
611	270.85	270.90	270.94	270.99	271.08	271.08	271.12	271.16	27 1.21	271.2
612	271.80	271.34	271.39	271.48	271.47	271.52	271.56	271.61	271.65	271.7
613	271.74	271.78	271.88	271.87	271.92	271.96	272.01	272.05		272.1
614	272.18	272.23	272.27	272.32	272.36	272.41	272.45	272.49	272.54	272.5
615	272.63	272.67	272.72	2 72.76	272.80	272.85	272.89	272.94	272.98	273.0
616	273.07	278.11	273.16	278.20	273.25	273.29	273.84	273.38	273.42	273.4
617	273.51	278.56	273.60	273.65	278.69	273.74	273.78	273.82	273.87	273.9
618	273.96	274.00	274.05	274.09	274.13	274.18	274.22	274.27	274.81	274.3
619	274.40	274.44	274.49	274.53	274.58	274.62	274.67	274.71	274.75	274.8
620	274.84	274.89	274.98	274.98	275.02	275.07	275.11	275.15	275.20	275.2
621	275.29	275.83	275.38	275.42	275.46	275.51	275.55	275.60	275.64	275.6
622	275.73	275.77	275.82	275.86	275.91	275.95	276.00	276.04	276.08	276.1
623	276.17	276.22	276.26	276.31	276.85	276.88	276.44	276.48	276.53	276.5
624	276.62	276.66	276.71	276.75	276.79	276.84	276.88	276.93	276.97	277.0
625	277.06	277.10	277.15	277.19	277.24	277.28	277.83	277.37	277.41	277.4
626	277.50	277.55	277.59	277.64	277.58	277.72	277.77	277.81	277.86	277.9
627	277.95	277.99	278.04	278.08	278.12	278.17	278.21	278.26	278.30	278.3
628	278.39	278.43	278.48	278.52	278.57	278.61	278.66	278.70	278.74	278.7
629	278.88	278.88	278.92	278.97	279.01	279.05	279.10	279.14	279.19	279.2
630	279.28	279.82	279.37	279.41	279.45	279.50	279.54	279.59	279.63	279.6
681	279.72	279.76	279.81	279.85	279.90	279.94	279.99	280.03	280.07	280.1
632	280.16	280.21	280.25	280.30	280.34	280.38	280.48	280.47	280.52	280.5
638	280.61	280.65	280.70	280.74	280.78	280.83	280.87	280.92	280.96	281.0
634	281.05	281.09	281.14	281.18	281.23	281.27	281.32	281.86	281.40	281.4
635	281.49	281.54	281.58	281.63	281.67	281.71	281.76	281.80	l .	281.8
636	281.94	281.98	282.02	282.07	282.11	282.16	282.20	282.25	282.29	282.3
687	292.38	282.42	282.47	282.51	282.56	282.60	282.65	282.69	282.78	282.7
638	282.82	282.87	282.91	282.96	283.00	283.04	283.09	283.13	283.18	283.2
689	283.27	283.31	288.35	283.40	283.44	283.49	283.53	283.58	288.62	283.6
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

28

C

1 Millimetre = 0.448296 French Line.

Millione-				1	Conths of 1	fillimetres	•			
tres.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Par.lines.		Par.lines.				Par.lines.	1	1	Par.lines.
640	283.71	283.75	283.80	283.84	283.89	283.93	283.98	284.02	284.06	284.11
641	284.15	284.20	284.24	284.29	284.83	284.87	284.42	284.46	284.51	284.55
642	284.60	284.64	284.68	284.78	284.77	284.82	284.86	284.91	284.95	284.99
613	285.04	285.08	285.13	285.17 285.62	285.22	285.26	285.81	285.85	285.89	285.44 285.88
614	285.48	285.53	285.57	280.02	285.66	285.70	285.75	285.79	285.84	200.08
645	285.93	295.97	286.01	286.06	286.10	286.15	286.19	286.24	286.28	286.32
646	286.37	286.41	286.46	286.50	286.55	286.59	286.64	286.68	286.72	286.77
647	286.81	286.86	286.90	286.95	286.99	287.03	287.08	287.12	287.17	287.21
648	287.26	287.30	287.34	287.39	287.43	287.48	287.52	287.57	287.61	287.65
649	287.70	287.74	287.79	287.83	287.88	287.92	267.96	288.01	288.05	288.10
650	288.14	289.19	289.23	288.28	288.32	288.36	288.41	288.45	288.50	288.54
651	288.59	288.63	238.67	288.72	288.76	288.81	288.85	288.90	288.94	288.98
652	299.03	289.07	289.12	289.16	289.21	289.25	289.29	289.34	289.89	289.43
653	289.47	289.52	289.56	289.61	289.65	289.69	289.74	289.78	289.88	289.87
654	289.92	289.96	290.00	290.05	290.09	290.14	290.18	290.28	290.27	290.31
655	290.36	290.40	290.45	290.49	290.54	290.58	290.62	290.67	290.71	290.76
656	290.80	290.85	290.89	290.94	290.98	291.02	291.07	291.11	291.16	291.20
657	291.25	291.29	291.33	291.38	291.42	291.47	291.51	291.56	291.60	291.64
658	291.69	291.73	291.78	291.82	291.87	291.91	291.95	292.00	292.04	292.09
659	292.13	292.18	292.22	292.26	292.31	292.85	292.40	292.44	292.49	292.58
669	292.58	292.62	292.66	292.71	292.75	292.80	292.84	292.89	292.98	292.97
661	293.02	293.06	293.11	293.15	293.20	293.24	298.28	293.33	293.87	293.42
662	293.46	293.51	293.55	293.59	293.64	293.68	293.73	293.77	293.82	293.86
663	293.91	293.95	293.99	294.04	294.08	294.13	294.17	294.22	294.26	294.80
664	294.85	294.39	294.44	294.48	294.58	294.57	294.61	294.66	294.70	294.75
665	294.79	294.84	294.88	294.92	294.97	29 5.01	295.06	295.10	295.15	295.19
666	295.24	295.28	295.82	295.37	295.41	295.46	295.50	295.55	295.59	295.63
667	295.6 8	295.72	295.77	295.81	295.86	295.90	295.94	295.99	296.08	296.08
668	296.12	296.17	296.21	296.25	296.30	296.34	296.39	296.48	296.48	296.52
689	296.56	296.61	296.65	296.70	296.74	296.79	296.83	296.88	296.92	296.96
670	297.01	297.05	297.10	297.14	297.19	297.23	297.27	297.32	297.36	297.41
671	297.45	297.50	297.54	297.58	297.68	297.67	297.72	297.76	297.81	297.85
672	297.89	297.94	297.98	298.03	298.07	298.12	298.16	298.21	298.25	298.29
673	298.34	298.38	298.43	298.47	298.52	298.56	298.60	298.65	298.69	298.74
674	298.78	298.83	298.87	298.91	298.96	299.00	299.05	299.09	299.14	299.18
675	299.22	299.27	299.31	299.36	299.40	299.45	299.49	299.54	299.58	299.62
676	299.67	299.71	299.76	299.80	299.85	299.89	299.93	299.98	800.02	800.07
677	300.11	300.16	300.20	800.24	800.29	800.83	800.38	300.42	800.47	800.51
678	300.55	800.60	800.64	300.69	300.78	800.78	800.82	800.86	800.91	300.95
679	301.00	301.04	301.09	801.13	801.18	801.22	301.26	301.31	801.35	301.40
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

C . 29

1 Millimetre = 0.448296 French line.

Millime-				•	Tenths of I	Millimotres				
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines,	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.		Par.lines.
680	301.44	301.49	801.53	801.57	801.62	801.66	801.71	301.75	801.80	301.84
681	301.88	301.93	301.97	302.02	802.06	302.11	802.15	802.19	302.24	302.28
682	302.83	302.37	302.42	302.46	302.51	802.55	802.59	302.64	802.68	302.73
683	302.77	302.82	302.86	802.90	802.95	302.99	303.04	303.08	303.13	303.17
684	303.21	303.26	303.30	308.35	808.39	803.44	303.48	303.52	803.57	303.61
685	303.66	803.70	303.75	303.79	803.88	303.88	803.92	303.97	804.01	804.06
686	804.10	304.15	304.19	304.23	804.28	304.32	804.87	304.41	304.46	304.50
687	804.54	304.59	304.63	304.68	804.72	304.77	804.81	804.85	804.90	304.94
688	304.99	805.03	805.08	805.12	305.16	805.21	805.25	305.80	305.34	305.39
689	305.43	305.48	305.52	305.56	805.61	805.65	805.70	305.74	805.79	805.83
690	305.87	305.92	805.96	306.01	806.05	806.10	806.14	306.18	806.23	306.27
691	806.82	806.36	806.41	806.45	306.49	806.54	306.58	806.63	306.67	306.72
692	306.76	306.81	306.85	806.89	806.94	806.98 807.48	807.03	307.07	807.12 307.56	307.16 307.60
693	307.20	807.25	807.29	307.34	307.38 307.82	807.48	307.47 307.91	307.51 307.96	308.00	308.05
694	307.65	807.69	307.74	307.78	507.02	501.61	507.91	507.50	200.00	300.00
695	308.09	309.13	308.18	808.22	308.27	808.81	808.36	308.40	308.45	308.49
696	308.53	809.59	808.62	808.67	808.71	808.76	808.80	308.84	808.89	308.98
697	308.98	809.02	809.07	809.11	809.15	809.20	309.24	309.29	809.33	309.38
698	809.42	309.46	809.51	809.55	309.60	809.64	809.69	309.78	809.78	309.82
699	809.86	80 9 .91	309.95	310.00	810.04	810.09	810.18	310.17	810.22	810.26
700	810.81	810.85	310.40	310.44	810.48	810.53	310.57	310.62	310.66	810.71
701	310.75	310.79	810.84	310.88	310.98	310.97	311.02	811.06	311.11	311.15
702	811.19	311.24	311.28	311.83	311.87	311.42	311.46	811.50	811.55	311.59
703	311.64	811.68	811.78	811.77	311.81	811.86	311.90	811.95	811.99	312.04
704	812.08	812.12	812.17	312.21	812.26	312.80	812.85	812.89	812.43	812.48
705	312.52	312.57	312.61	812.66	812.70	812.75	812.79	812.88	812.88	812.92
706	312.97	818.01	818.06	313.10	818.14	818.19	318.28	313.28	818.82	313.37
707	313.41	818.45	813.50	818.54	313.59	813.63	818.68	813.72	313.76	313.81
708	313.85	318.90	818.94	318.99	814.08	814.08	814.12	314.16	314.21	814.25
709	314.30	314.84	314.39	814.43	814.47	814.52	814.56	814.61	314.65	814.70
710	814.74	814.78	814.83	314.87	314.92	814.96	815.01	815.05	315.09	815.14
711	315.18	815.28	315.27	815.82	815.36	815.41	815.45	315.49	815.54	815.58
712	315.63	815.67	815.72	815.76	815.80	815.85	815.89	815.94	815.98	316.03
718	316.07	316.11	816.16	816.2 0	316.25	316. 29	316.34	816.88	816.42	816.47
714	316.51	816.56	316.60	816.65	816.69	316.78	816.78	816.82	816.87	816.91
715	316.96	817.00	317.05	317.09	817.18	817.18	817.22	817.27	817.81	317.36
716	817.40	817.44	817.49	817.58	317.58	317.62	317.67		317.75	817.80
717	317.84	817.89	317.98	817.98	318.02	318.06	818.11	318.15	318.20	318.24
718 719	318.29 318.73	\$18.33 \$18.77	318.88 318.82	818.42 818.86	318.46 318.91	818.51 818.95	318.55 319.00	318.60 319.04	318.64 319.08	818.69 319.13
				3.		5.	6.	7.	8.	9.
	0.	1.	2.	J.	4.	<u> </u>	υ.	••	.	.

1 Millimetre = 0.448396 French Line.

Millime-				,	Tenths of	Milimetres	-			
toss.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.line
720	319.17	319.22	319.26	319.31	319.35	319.39	819.44	319.48	319.53	319.57
721	319.62	319.66	819.70	819.75	819.79	319.84	819.88	819.93	319.97	320.02
722	820.06	820.10	320.15	820.19	820.24	320.28	820.33	\$20.37	320.41	820.4
723	320.50	320.55	320.59	820.64	320.68	820.72	820.77	320.81	320.86	320.9
724	820.93	820.99	321.03	821.08	821.12	821.17	821.21	321.26	321.30	321.3
725	321.39	321.43	321.48	821.52	821.57	821.61	321.66	821.70	821.74	821.7
726	321.83	321.88	321.92	821.97	822.01	822.05	822.10	322.14	322.19	322.2
727	322.28	322.32	322.36	822.41	322.45	822.50	322.54	822.59	322.63	822.6
728	322.72	822.76	322.81	822.85	822.90	322.94	322.99	323.03	823.07	323.1
729	323.16	323.21	323.25	828.80	323.34	323.88	823.48	823.47	323.52	328.5
730	323.61	823.65	823.69	823.74	823.78	323.63	823.87	323.92	323.96	824.0
731	324.05	324.09	824.14	324.18	824.23	824.27	324.32	824.36	824.40	824.4
732	324.49	824.54	324.58	824.63	324.67	824.71	324.76	824.80	824.85	324.8
733	324.94	324.9 8	325.02	825.07	325.11	325.16	825.20	825.25	825. 29	825.3
734	325.38	325.42	825.47	825.51	325.56	325.60	825.65	825.69	825.78	325.7
735	325.82	325.87	825.91	325.96	326.00	826.04	826.09	826.13	326. 18	826.2
786	826.27	326.31	326.35	826.40	326.44	326.49	826.58	3 26.58	826.62	826.6
737	326.71	326.75	326.80	326.84	826.89	326.93	826.98	827.02	327.06	827.1
738	327.15	\$27.20	827.24	327.29	327.33	827.87	827.42	827.46	827.51	827.5
739	327.60	327.61	327.68	827.78	327.77	327.82	327.86	827.91	327.95	827.9
740	828.04	828.08	328.13	328.17	328.22	828.26	828.30	828.85	328.39	329.4
741	328.48	329.53	828.57	328.62	328.66	828.70	828.75	328.79	828.84	328.8
742	328.93	328.97	829.01	329.06	329.10	829.15	829.19	829.24	329.28	829.3
743	329.37	329.41	329.46	829.50	829.55	329.59	329.63	329.68	829.72	329.7
744	829.81	329.86	829.90	329.93	829.99	830.08	880.08	880.12	330.17	830.2
745	330.26	880.80	330.34	830.89	830.43	830.48	830.52	880.57	330.61	330.6
746	830.70	330.74	330.79	330.83	830.88	330.92	830.96	881.01	331.05	331.1
747	331.14	331.19	881.28	831.28	331.32	381.86	881.41	831.45	331.50	331.5
748	331.59	331.63	331.67	831.72	331.76	331.81	331.85	831.90	331.94	331.9
749	832.03	832.07	832.12	332.16	882.21	332.25	332.29	332.34	382.38	882.4
750	832.47	332.52	332.56	832.60	882.65	332.69	882.74	832.78	832.83	832.8
751	832.92	332.96	333.00	833.05	833.09	383.14	833.18	833.23	333.27	333.3
752	888-86	883.40	888.45	883.49	333.54	333.58	833.62	333.67	833.71	838.7
753	333.80	333.85	333.89	888.98	838.98	834.02	384.07	334.11	334.16	334.2
754	834.25	384.29	834.88	384.88	884.42	384.47	884.51	334.56	334.60	334.6
755	884.69		384.78	884.82	334.87	884.91		885.00		885.0
756	835.13	385.18	835.22	335.26	335.31	835.85	835.40	885.44	335.49	885.5
757	335.58	385.62	335.66	385.71	335.75	335. 80	835.84	885.89	385.93	885.9
758 750	336.02	336.06	336.11	886.15	336.20	836.24	886.28	336.83	386.87	886.4
759	336.46	386.51	886.55	886.59	336.64	336.68	836.73	836.77	836.82	336.8
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Millimetre = 0.443296 French Line

Millime-					Cenths of I	Millimetres	•			
tres.	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Parlines.	Par.lines.	Par lines.	Par.line
760	336.90	386.95	886.99	887.04	337.08	837.13	837.17	337.22	337.26	337.30
761	337.35	337.39	387.44	887.48	337.58	337.57	337.61	337.66	337.70	837.75
762	387.79	387.84	337.88	887.92	837.97	838.01	\$38.06	33 8.10	338.15	338.19
768	338.23	339.28	388.32	338.37	838.41	888.46	338.50	33 8.55	838.59	338.6
764	338.68	888.72	388.77	33 6.81	338.56	888.90	888.94	338.99	339.08	\$39.06
765	339.12	389.17	339.21	839.25	889.30	389.84	839.89	389.43	339.48	389.52
766	339.56	339.61	339.65	889.70	889.74	889.79	839.83	839.87	\$39.92	339.96
767	340.01	840.05	840.10	840.14	840.19	840.28	340.27	340.32	340.86	840.41
768	340.45	840.50	840.54	840.58	340.68	840.67	840.72	340.76	340.81	340.8
769	340.89	340.94	840.98	341.08	841.07	341.12	841.16	841.20	341.25	341.25
770	341.84	341.38	341.43	341.47	841.52	841.56	841.60	841.65	841.69	841.74
771	341.78	841.83	841.87	841.91	841.96	342.00	842.05	842.09	342.14	842.18
772	3 (2.22	342.27	842.81	342.36	842.40	842.45	342.49	342.58	842.58	342.62
778	842.67	842.71	342.76	342.80	342.85	842.89	342.98	842.98	343.02	343.07
774	343.11	343.16	848.20	843.24	348.29	848.33	343.38	343.42	348.47	848.51
775	343.55	343.60	848.64	343.69	343.73	343.78	348.82	343.86	843.91	343.90
776	814.00	844.04	844.09	844.13	844.17	344.22	844.26	844.31	344.35	844.40
777	841.44	844.49	344.58	844.57	844.62	344.66	844.71	344.75	3 44.80	344.84
778	344.88	844.98	844.97	845.02	845.06	845.11	345.15	845.19	345.24	345.26
779	345.38	845.87	845.42	345.46	845.50	845.55	845.59	345.64	345.68	845.78
780	845.77	845.82	345.86	845.90	845.95	345.99	846.04	346.08	846.18	846.17
781	346.21	846.26	846.30	346.35	346.39	346.44	846.48	846.52	346.57	846.6
782	346.66	346.70	846.75	346.79	846.83	346.88	846.92	346.97	847.01	\$47.00
788	347.10	847.15	847.19	347.28	847.28	847.82	347.87	847.41	847.46	347.50
784	847.54	847.59	847.63	847.68	847.72	847.77	347.81	847.85	847.90	347.94
· 785	347.99	348.08	848.08	848.12	348.16	348.21	348.25	348.30	348.84	848.89
786	848.43	349.47	848.52	848.56	848.61	348.65	348.70	348.74	348.79	848.81
787	848.87	348.92	848.96	849.01	349.05	849.10	349.14	349.18	349.23	849.27
788	349.32	349.36	849.41	349.45	349.49	849.54	349.58	349.63	349.67	349.7
789	849.76	849.80	849.85	849.89	849.94	349.98	850.03	850.07	350.12	850.16
790	350.20	850.25	350.29	350.84	350.38	350.48	850.47	850.51	350.56	350.60
791	350.65	350.69	350.74	350.78	350.82	350.87	350.91	350.96	351.00	351.08
792	351.09	351.13	851.18	351.22	351.27	351.31	851.86	851.40	851.44	351.49
798	351.53	351.58	851.62	851.67	351.71	351.76	851.80	351.84	351.89	351.91
794	351.98	852.02	352.07	352.11	352.15	352.20	352.24	852.29	852.38	352.38
795	352.42	352.46	f	352.55		852.64	352.69	852.73	1	l .
796	352.86	852.91	1	1	1	353.09	353.18	1	i	353.26
797	358.81	353.35	ĭ	353.44		853.53	353.57	353.62	l.	358.71
798	358.75	858.79	353.84	858.88	358.98	853.97	854.02	354.06		354.15
799	854.19	854.24	854.28	854.88	1	854.42	354.46	854.50	354.55	354.59
800	354.64	354.68	354.78	854.77	354.81	354.86	354.90	854.95	354.99	855.0
	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.

V. - VI.

COMPARISON

OF

THE OLD FRENCH BAROMETER

WITH

THE ENGLISH AND THE METRICAL BAROMETERS,

OR

- TABLES

FOR CONVERTING FRENCH OR PARIS LINES INTO ENGLISH INCHES
AND DECIMALS, AND INTO MILLIMETRES;

GIVING THE VALUES CORRESPONDING TO EVERY PARIS LINE FROM 120 TO 216 LINES, OR FROM 10 TO 18 INCHES; AND TO EVERY TENTH OF A LINE FROM 216 TO 348 LINES, OR FROM 18 TO 29 FRENCH INCHES.

TABLE V.

MM. J. J. Pohl and J. Schabus have published, in the number for March, 1852, of the Proceedings of the Imperial Academy of Vienna, Class of Mathematics and Natural Philosophy, a set of short Thermometrical and Barometrical Reduction Tables, among which is found a table for the reduction of the Old French Barometrical Scale into the English. As this table shows slight discrepancies from the one given in the following pages, it may not be out of place to state that they arise from an accidental error in the equation used by MM. Pohl and Schabus in computing their table. Adopting, as they do, Bird's value of the metre, viz.

1 metre = 39.37062 English inches,

the value of the Paris line is

1 Paris line = 0.088813 English inches.

But the table seems to have been computed by using the equation

1 Paris line = 0.088823 English inches,

which gives, at the end of the table,

348 lines \times .088823 = 30.9104 English inches,

instead of

thus causing an error

which, of course, gradually diminishes in lower numbers.

1 Paris Line = 0.088814 English Inch.

French or Paris					U	ilte.				
Lines. Tens.	0.	1.	9.	8.	4.	5.	6.	7.	8.	.9.
10 Inch. 120	Eng. In. 10.658	Eng In. 10.746	Eng. In. 10.835	Eng. In. 10.924	Eng In 11.013	Eng. In. 11.102	Eng. In. 11.191	Eng. In. 11.279	1 -	Eng. In.
130	11.546	11.635	11.728	11.812	11.901	11.990	12.079	12.168	12.256	12.345
140	12.431	12.523	12.612	12.700	12.789	12.878	12.967	13.056	18.144	13.233
150	13.322	18.411	13.500	13.589	18.677		13.855	13.944	1	14.121
160	14.210	14.299	14.388	14.477	14.565	14.654	14.743	14.832	l	15.010
170	15.099	15.187	15.276	15.365	15.454	15.542	15.631	15.720	15.809	15.898
180	15.987	16.075	16.164	16.253	16.342	16.431	16.519	16.608	16.697	16.786
190	16.875	16.963	17.052	17.141	17.230	17.819	17.408	17.496	17.585	17.674
200	17.763	17.852	17.940	18.029	18.118	18.207	18.296	18.384	18.473	18.562
210	18.651	18.740	18.829	18.917	19.006	19.093	19.184	19.273	19.361	19.450
Paris					Ter	ths.				
Lines.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
18 Inch.	Eng. In.	Eng. In.	Eng. In.	Eng In	Eng. In.	Rng. In.	Eng. In.			Eng. In
216	19.184	19.193	19.202	19.210	19.219	19.228	19.237	19.246	1	19.264
217	19.273	19.282	19.290	19.299	19.308	19.317	19.326	19.835	1	19.853
218	19.861	19.370	19.879	19.388	19.897	19.406	19.415	19.424		19.441
219	19.450	19.459	19.468	19.477	19.486	19.495	19.504	19.512	19.521	19.530
220	19.539	19.548	19.557	19.566	19.575	19.583	19.592	19.601	19.610	19.619
221	19.628	19.637	19.646	19.655	19.663	19.672	19.681	19.690	19.699	19.708
223	19.717	19.726	19.734	19.748	19.752	19.761	19.770	19.779	19.788	19.797
223	19.806	19.814	19.823	19.832	19.840	19.850	19.859	19.868	19.877	19.885
224	19.894	19.903	19.912	19.921	19.930	19.939	19.948	19.957	19.965	19.974
225	19.983	19.992	20.001	20.010	20.019	20.028	20.086	20.045	20.054	20.063
226	20.072	20.081	20.090	20.099	20.107	20.116	20.125	20.134	20.143	20.152
227	20.161	20.170	20.179	20.187	20.196	20.205	20.214	20.223	20.232	20.241
19 Inch.										•
228	20.250	20.258	20.267	20.276	20.285	20.294	20.303	20.312	20.321	20.830
229	20.33 8	20.847	20.356	20.863	20.374	20.883	20.392	20.401	20.409	20.418
230	20.427	20.436	20.445	20.454	20.463	20.472	20.481	20.489	20.498	20.507
231	20.516	20.525	20.534	20.548	20.552	20.560	20.569	20.578	20.587	20.596
232	20.603	20.614	20.623	20.631	20.640	20.649	20.658	20.667	20.676	20.685
233	20.694	20.703	20.711	20.720	20.729	20.788	20.747	20.756	20.765	20.774
234	20.782	20.791	20.800	20.809	20.818	20.827	20.836	20.845	20.854	20.862
235	20.871	20.880	20.889	20.898	20.907	20.916	20.925	20.988	20.942	20.951
236	20.960	20.969	20.978	20.987	20.996	21.005	21.013	21.022	21.031	21.040
237	21.049	21.058	21.067	21.076	21.084	21.098	21.102	21.111	21.120	21.129
238	21.138	21.147	21.155	21.164	21.173	21.182	21.191	21.200	21.209	21.218
289	21.227	21.235	21.244	21.258	21.262	21.271	21.280	21.289	21.298	21.306
				Hundr	edths of a	Line.				
0.	1.	2.	3.	4.	5	•	6.	7.	8.	9.
.000	.001	.002	.003	.004	.00	04 .0	005	.006	.007	.008

1 Paris Line = 0.088814 English Inch.

Pounds or					Tenths-o	f a Line.				
French or ParisLines.	0.	1.	9.	8.	4.	5.	6,	7.	8.	9.
20 Inches.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In
240	21.315	21.824	21.383	21.842	21.331	21.360	21.369	21.378	21.386	21.39
241	21.404	21.413	21.422	21.481	21.440	21.449	21.457	21.466	21.475	21.48
242	21.493	21.502	21.511	21.520	21.529	21.537	21.546	21.555	21.564	21.57
243	21.582	21.591	21.600	21.608	21.617	21.626	21.635	21.644	21.653	21.66
244 245	21.671	21.679 21.768	21.688 21.777	21.697 21.786	21.706 21.795	21.715 21.904	21.724 21.813	21.733 21.822	21.742 21.830	21.75 21.83
							61 000	61 616	81 818	01.00
246	21.848	21.857	21.866	21.875	21.884	21.893	21.902	21.910	21.919	21.92 22.01
247 248	21.937	21.946	21.935	21.964	21.973	21.981 22.070	21.990 22.079	21.999 22.088	22.008 22.097	22.10
248	22.026 22.113	22.035 22.124	22.044 22.182	22.053 22.141	22.061 22.150	22.070	22.168	22.177	22 186	22.19
250	22.113	22.212	22.132	22.141	22.239	22.138	22.257	22.266	22.275	22.28
251	22.292	22.801	22.310	22.319		22.887	22.346	22.354	22.363	22.37
91 In. —	22.202	22.001	22.010	22.010	22.020	22.001	22.010	22.001		
252	22.381	22.390	22.399	22.408	22.417	22.426	22.484	22.443	22.452	22.46
253	22.470	22.479	22.488	22.497	22.505	22.514	22.523	22.532	22.541	22.55
254	22.559	22.568	22.577	22.585	22.594	22.603	22.612	22.621	22.630	22.63
255	22.648	22.656	22.665	22.674	22.683	22.692	22.701	22.710	22.719	22.72
256	22.736	22.745	22.754	22.763	22.772	22.781	22.790	22.799	22.807	22.81
257	22.825	22.884	22.848	22.852	22.861	22.870	22.878	22.887	22.596	22.90
258	22.914	22.923	22.982	22.941	22.950	22.958	22.967	22.976	22.985	22.99
259	23.003	28.012	28.021	23.029	23.038	23.047	23.056	23.065	23.074	23.08
260	23.092	28.101	23.109	23.118	23.127	23.136	23.145	23.154	23.163	23.17
26 1	23.180	23.189	23.198	23.207	23.216	23.125	28.234	28.243	23.252	23.26
262	23.269	23.278	23.287	23.296	28.305	23.814	23.323	23.331	23.340	23.34
263 33 In. —	23.358	23.367	28.876	23.3 85	23.394	23.402	23.411	23.420	23.429	23.43
264	23.447	23.456	23.465	23.474	23.482	23.491	23.500	23.509	23.518	23.52
265	23.536	23.545	23.553	23.562	28.571	28.580	23.589	23.598	23.607	23.61
266	23.625	23.633	23.642	28.651	23.660	28.669	23.678	23.687	23.696	23.70
267	23.713	28.722	28.731	23.740	23.749	23.758	23.767	23.776	23.784	23.79
268	23.802	23.811	23.820	23.829	23.888	23.847	28.855	23.964	23.873	23.88
269	23.891	28.900	23.909	23.918	28.926	28.935	28.944	23.953	28.962	23.97
270	23.980	23.989	23.998	24.006	24.015	24.024	24.088	24.042	24.051	24.06
271	24.069	24.077	24.086	24.095	24.104	24.118	24.122	24.131	24.140	24.14
272	24.157	24.166	24.175	24.184	24.198	24.202	24.211	24.220	24.228	24.23
273	24.246	24.255	24.264	24.273	24.282	24.291	24.300	24.308	24.317	24.32
274	24.835	24.344	24.353	24.362	24.871	24.879	24.388	24.397	24.406	24.41
275	24.424	24.433	24.442	24.450	24.459	24.468	24.477	24.486	24.495	24.50
				Hundr	edths of a	Line.				
0.	1.	2.	8.	4.	1 8	i. (5.	7.	8.	9.
			1							

1 Paris Line = 0.088814 English Inch.

French or					Tenths (of a Line.				
arisLines.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
3 Inches.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.		Eng. In
276	24.518	24.522	24.580	24.539	24.548	24.557	24.566	24.575	24.584	24.59
277	24.601	24.610	24.619	24.628	24.637	24.646	24.655	24.664	1	24.681
278	24.690	24.699	24.708	24.717	24.726	24.785	24.744	24.752	24.761	24.770
279	24.779	24.788	24.797	24.806	24.815	24.824	24.882	24.841	24.850 24.989	24.859
280 281	24.868 24.957	24.877 24.966	24.886 24.974	24.895 24.983	24.908 24.992	24.912 25.001	24.921 25.010	24.930 25.019		25.087
808	25.046	AF 074	0.E. 0.00	9E 000	96 001	85 000	05 000	25.108	25.117	25.12
282 283	25.134	25.034 25.143	25.063 25.152	25.072	25.081 25.170	25.090 25.179	25.099 25.188	25.197	1	25.214
284	25.181	25.232	25.241	25.161 25.250	25.259	25.268	25.276	23.285	25.294	25.30
285	25.213	25.321	25.830	25.889	25.348	25.356	25.365	25.874		25.89
286	25.401	25.410	25.419	25.427	25.486	25.445	25.454	25.463	25.472	25.48
287	25.490	25.498	25.507	25.516	25.525	25.584	25.543	25.552	25.561	25.57
14 In	20.450	20.420	20.007	20.010	20.020	20.004	20.040	20.002		
288	25.578	25.587	25.596	25.605	25.614	25.623	25.632	25.641	25.649	25.65
289	25.667	25.676	25.685	25.694	25.708	25.712	25.721	25.729	25.788	25.74
290	25.756	25.765	25.774	25.788	25.792	25.900	25.809	25.818	25.827	23.88
291	25.845	25.854	25.863	25.872	25.880	25.889	25.898	25.907		25.92
292	25.934	25.943	25.951	25.960	25.969	25.978	25.987	25.996	26.005	26.01
293	26.023	26.031	26.040	26.049	26.058	26.067	26.076	26.085	26.094	26.10
294	26.111	26.120	26.129	26.188	26.147	26.156	26.165	26.173	26.182	26.19
295	26.200	26.209	26.218	26.227	26.286	26.245	26.253	26.262	26.271	26.28
296	26.289	26.298	26.807	26.816	26.324	26.333	26.342	26.351	26.360	26.86
297	26.378	26.387	26.396	26.404	26.413	26.422	26.431	26.440	26.449	26.45
298	26.467	26.475	26.484	26.498	26.502	26.511	26.520	26.529	26.538	26.54
299	26.555	26.564	26.573	26.582	26.591	26.600	26.609	26.618	26.626	26.63
85 In	ļ					l				1
300 .	26.644	26.658	26.662	26.671	26.680	26.689	26.697	26.706	26.715	26.72
301	26.733	26.742	26.751	26.760	26.769	26.777	26.786	26.795	26 804	26.81
802	26.822	26.831	26.840	26.848	26.857	26.866	26.875	26.884	26.998	26.90
303	26.911	26.920	26.928	26.937	26.946	26.955	26.964	26.973	26.982	26.99
804	26.999	27.008	27.017	27.026	27.035	27.044	27.053	27.062	27.071	27.07
805	27.068	27.097	27.106	27.115	27.124	27.183	27.142	27.150	27.159	27.16
306	27.177	27.186	27.195	27.204	27.213	27.221	27.230	27.289	27.248	27.25
807	27.266	27.275	27.284	27.298	27.301	27.810	27.319	27.328	27.337	27.34
308	27.855	27.364	27.872	27.8 81	27.890	27.899	27.408	27.417	27.426	27.43
309	27.441	27.452	27.461	27.470	27.479	27.488	27.497	27.506	27.515	27.52
810	27.582	27.541	27.550	27.559	27.568	27.577	27.586	27.595	27.603	27.61
811	27.621	27.630	27.639	27.648	27.657	27.686	27.674	27.683	27.692	27.70
	·	·		Handr	edths of a	Line.				
9.	1.	2.	8.	4.	1 4	5. (6.	7.	8.	9.
				_	I	1	1			

1 Paris Line = 0.088814 English Inch.

French or					Tenths (f a Line.				
ParisLines.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
26 Inches.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.
812	27.710	27.719	27.728	27.737	27.745	27.754	27.763	27.772	27.781	27.790
313	27.799	27.808	27.817	27.825	27.834	27.843	27.852	27.861	27.870	27.879
814	27.888	27.896	27.905	27.914	27.928	27.932	27.941	27.950	27.959	27.968
815	27.976	27.985	27.994	28.008	28.012	28.021	28.030	28.039	28.047	28.056
816	28.063	28.074	28.083	28.092	28.101	28.110	28.119	28.127	28.136	28.145
817	28.154	28.163	28.172	28.181	28.190	28.198	28.207	28.216	28.225	28.234
818	28.243	28.252	28.261	28.269	28.278	28.287	28.296	28.305	28.314	28.323
319	29.882	28.341	28.349	29.858	28.367	28.876	28.385	28.394	28.403	28.412
820	28.420	28.429	28.438	28.447	28.456	28.465	28.474	28.483	28.492	28.500
821	28.509	28.518	28.527	28.536	28.545	28.554	28.563	28.571	28.580	28.589
322	28.598	28.607	28.616	28.625	28.634	28.643	28.651	28.660	2 9.669	28.678
828	28.687	28.696	28.705	28.714	28.722	28.781	28.740	28.749	28.758	28.767
27 In								00.000	00.04=	80 050
324	28.776	28.785	28.793	28.802	28.811	28.820	28.829	28.838	28.847	28.856 28.944
825	28.865	28.873	28.882	28.891	28.900	28.909	28.918	28.927 29.016	28.936 29.024	29.033
326	28.953	28.962	28.971	28.980	28.989	28.998	29.007		l	29.122
827	29.042	29.031	29.060	29.069	29.078	29.087	29.095	29.104	29.118	
828	29.181	29.140	29.149	29.158	29.167	29.175	29.184	29.193	29.202	29.211
829	29.220	29.229	29.238	29.246	29.255	29.264	29.278	29.282	29.291	29.300
880	29.809	29.818	29.326	29.335	29.344	29.358	29.862	29.371	29.380	29.389
831	29.397	29.406	29.415	29.424	29.488	29.442	29.451	29.460	29.468	29.477
882	29.486	29.495	29.504	29.513	29.522	29.531	29.540	29.548	29.557	29.566
833	29.575	29.584	29.593	29.602	29.611	29.619	29.628	29.637	29.646	29.655
834	29.664	29.673	29.682	29.691	29.699	29.708	29.717	29.726	29.735	29.744
835	29.753	29.762	29.770	29.779	29.788	29.797	29.806	29.815	29.824	29.833
28 In										'
836	29.842	29.850	29.859	29.868	29.877	29.386	29.895	29.904	29.913	29.921
837	29.930	29.939	29.948	29.957	29.966	29.975	29.984	29.992	30.001	80.010
838	80.019	30.028	80.037	80.046	30.055	80.064	30.072	30.081	30.090	30.099
839	30.108	30.117	30.126	30.135	30.143	80.152	30.161	30.170	30.179	80.188
840	30.197	80.206	80.215	30.223	30.232	30.241	30.250	30.259	30.268	30.277
341	30.286	80.294	30.303	30.312	80.321	30.330	30.339	30.348	30.357	30.366
842	30.374	80.383	30.892	30.401	30.410	80.419	30.428	30.437	30.445	30.454
843	30.463	30.472	80.481	30.490	80.499	30.508	80.516	80.525	30.534	30.543
844	80.552	80.561	80.570	80.579	30.588	80.596	30.605	80.614	30.623	30.632
845	80.641	80.650	30.659	30.667	80.676	80.685	30.694	30.703	30.712	30.721
346	30.730	80.789	80.747	30.756	30.765	80.774	80.783	80.792	30.801	39.810
847	80.818	30.827	80.836	80.845	30.854	80.863	30.872	80.881	80.990	30.898
39 In. —	30.907	80.916	30.925	30.994	30.948	80.959	30,961	30.969	30.978	30.987
	1 33.33	33.33			edths of a			<u> </u>	<u> </u>	i
								<u>~ 1</u>	<u> </u>	
0.	1.	<u>9.</u>	8.	4.	_ _	5.	6.	7.	8.	9.
.0000	.0009	.0018	.0027	.008	6 .00	0. 44	058	0062	.0071	.0090

1 Paris Line = 2.255829 Millimetres.

French or ParisLines.	Units.											
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
10 Inch.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.		
120	270.70	272.96	275.21	277.47	279.72	281.98	284.28	286.49	288.75	291.00		
130	293.26	295.51	297.77	300.03	302.28	804.54	806.79	309.05	311.30	318.56		
140	315.82	318.07	320.33	822.58	324.84	327.10	329.35	331.61	333.86	336.12		
150	388.37	840.68	842.89	345.14	347.40	349.65	351.91	854.17	356.42	358.68		
160	360.93	363.19	365.44	867.70	369.96	372.21	374.47	376.72	378.98	381.2		
170	383.49	385.75	388.00	390.26	392.51	394.77	397.03	399.28	401.54	403.79		
180	406.05	408.30	410.56	412.82	415.07	417.33	419.58	421.84	424.10	426.38		
190	428.61	430.86	433.12	435.87	487.63	439.89	442.14	444.40	446.65	448.91		
200	451.17	453.42	455.68	457.93	460.19	462.44	464.70	466.96	469.21	471.47		
210	478.72	475.98	478.24	480.49	482.75	485.00	487.26	489.51	491.77	194.08		
	Tenths of a Line.											
Paris Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
18 Inch.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.		
216	487.26	487.48	487.71	487.94	488.16	488.39	488.61	488.84	489.06	489.29		
217	489.51	489.74	489.97	490.19	490.42	490.64	490.87	491.09	491.32	491.55		
218	491.77	492.00	492.22	492.45	492.67	492.90	493.12	493.35	493.58	493.80		
219	494.03	494.25	494.48	494.70	494.98	495-15	495.38	495.61	495.83	496.06		
220	496.28	496.51	496.73	496.96	497.18	497.41	497.64	497.86	498.09	498.31		
221	498.54	498.76	498.99	499.21	499.44	499.67	499.89	500.12	500.84	500.57		
222	500.79	501.02	501.25	501.47	501.70	501.92	502.15	502.87	502.60	502.82		
223	503.03	503.28	503.50	503.73	503.93	504.18	504.40	504.63	504.85	505.08		
224	505.31	505.53	505.76	503.98	506.21	506.43	506.66	506.88	507.11	507.84		
225	507.56	507.79	508.01	508.24	508.46	508.69	508.91	509.14	509.37	509.58		
226	509.82	510.04	510.27	510.49	510.72	510.95	511.17	511.40	511.62	511.85		
227	512.07	512.30	512.52	512.75	512.98	513.20	513.43	513.65	513.88	514.10		
19 Inch.			1				١.			ł		
228	514.83	514.55	514.78	515.01	515.23	515.46	515.68	515.91	516.13	516.36		
229	516.58	516.81	517.04	517.26	517.49	517.71	517.94	518.16	518.39	518.61		
230	518.84	519.07	519.29	519.52	519.74	519.97	520.19	520.42	520.65	520.87		
231	521.10	521.82	521.55	521.77	522.00	522.22	522.45	522.68	522.90	523.13		
232	523.35	523.58	523.80	524.08	524.25	524.48	524.71	524.93	525.16	525.88		
233	525.61	525.83	526.06	526.28	526.51	526.74	526.96	527.19	527.41	527.64		
234	527.86	528.09	528.32	528,54	528.77	528.99	529.22	529.44	529.67	529.89		
235	530.12	530.35	530.57	530.80	531.02	531.25	531.47	531.70	531.92	532.15		
236	532.38	532.60	532.83	533.05	533.28	533.50	583.73	533.95	534.18	534.41		
237	534.63	534.86	585.08	585.31	535.58	535.76	585.98	586.21	536.44	536.66		
238	536.89	587.11	537.84	587.56	587.79	538.02	588.24	538.47	538.69	588.92		
239	589.14	539.87	589.59	589.82	540.05	540.27	540.50	540.72	540.95	541.17		
				Tent	hs of a Lin	30.						
0.	1.	2.	8.	4.	5	. (5.	7.	8.	9.		
0.00	0.23	0.45	0.68	0.90	1.1	3 1.	.35	1.58	1.80	2.03		

1 Paris Line = 2.255829 Millimetres.

Paris or	Tenths of a Line.												
French Lines.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.			
20 Inches.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.			
240	541.40	541.62	541.85	542.08	542.30	542.58	642.75	542.98	548.20	543.43			
241	548.65	543.88	544.11	544.33	544.56	544.78	545.01	545.23	545.46	545.69			
242	5 15.91	546.14	546.36	546.59	546.81	547.04	547-26	547.49	547.72	547.94			
243	548.17	548.39	548.62	548.54	549.C7	549.29	549.52	549.75	549.97	550.20			
244	530.42	550.65	550.87	551.10	551.82	551.55	551.78	552.00	552.23	552.45			
245	552.68	552.90	553.13	553.85	553.58	553.81	554.08	554.26	554.48	554.71			
246	554.93	555.16	555.39	555.61	555.84	556.06	556.29	556.51	556.74	556.96			
347	557.19	557.42	557.64	557.87	558.09	558.82	558.54	558.77	558.99	559.22			
248	559.45	559.67	559.90	560.12	560.85	560.57	560.80	561.02	561.25	561.48			
249	561.70	561.98	562.15	562.38	562.60	562.88	563.05	563.28	563.51	563.73			
250	563.96	564.18	564.41	561.63	564.86	565.09	565.31	563.54	565.76	565.99			
251	566.21	566.44	566.66	566.89	567.12	567.3			568.02	568.24			
31 Inches.													
252	568.47	568.69	568.92	569.15	569-87	569.60	569.82	570.05	570.27	570.50			
253	570.72	570.95	571.18	571.40	571.63	571.88			1	572.75			
254	572.98	578.21	573.43	573.66	573.88	574.11		1	1	575.01			
255	575.24	375.46	575.69	575.91	576.14	576.36			577.04	577.27			
256	577.49	577.72	577.94	578.17	578.89	578.62		1	579.30	579.52			
257	579.75	579.97	580.20	580.42	580.65	580.88			581.55	581.78			
258	582.00	582.23	582.46	582.68	582.91	583.18	583.36	583.58	533.81	584.03			
259	584.26	584.49	584.71	584.94	585.16	585.39	1	1	586.06	586.29			
260	586.52	586.74	586.97	587.19	587.42	587.64			588.32	588.55			
261	588.77	589.00	589.22	589.45	589.67	589.90			590.58	590.80			
262	591.03	591.25	591.48	591.70	591.98	592.16			592.83	593.06			
263	593.28	598.51	593.73	598.96	594.19	594.4			595.09	595.31			
22 Inches.							. 55 (100					
264	595.54	595.76	595.99	596.22	596.44	596.63	696.89	597.12	597.34	597.57			
265	597.79	598.02	598.25	598.47	598.70	598.92			599.60	599.82			
266	600.05	600.28	600.50	600.73	600.95	601.18			601.86	602.08			
267	602.31	602.53	602.76	602.98	603.21	608.48		1	604.11	604.34			
268	604.56	604.79	605.01	605.24	605.46	605.69		1 .	606.37	606.59			
269	606.82	607.04	607.27	607.49	607.72	607.9			608.62	608.85			
270	609.07	609.80	609.52	609.75	609.98	610.20	610.43	610.65	610.88	611.10			
271	611.33	611.56	614.78	612.01	612.23	612.46			613.13	613.36			
272	618.59	613.81	614.04	614.26	614.49	614.71			615.89	615.62			
273	615.84	616.07	616.29	616.52	616.74	616.97		1	617.65	617.87			
274	618.10	618.32	618.55	618.77	619.00	619.28		1	619.90	620.13			
275	620.35	620.58	620.80	621.03	621.26	621.48	1	1	622.16	622.38			
				Hundre	dths of a	Line.	· · · · ·		<u></u>	•			
0.	1.	2.	8.	. 4	. 4	5.	6.	7.	8.	9.			
0.000	0.023	0.045	0.068	3 0.0	90 O.	113	0.135	0.158	0.180	0.203			

1 Paris Line = 2.255829 Millimetres.

Paris or	. Tenths of a Line.											
French Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
23 Inches.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.		
276	622.61	622.88	623.06	623.29	623.51	623.74	623.96	624.19	624.41	624.64		
277	624.86	625.09	625.32	625.54	625.77	625.99	626.22	626.44	626.67	626.89		
278	627.12	627.35	627.57	627.80	628.02	628.25	628.47	628.70	628.93	629.15		
279	629.38	629.60	629.83	630.05	630.28	630.50	680.73	630.96	631.18	631.41		
280	631.68	631.86	632.08	632.31	632.58	632.76	632.99	633.21	633.44	633.66		
281	6 33. 89	684.11	634.34	634.56	634.79	635.02	635.24	635.47	685.69	685.92		
282	636.14	636.37	686.59	636.82	637.05	687.27	687.50	637.72	687.95	688.17		
283	638.40	638.68	638.85	689.08	689.30	639.58	639.75	639.98	640.20	640.43		
284	640.66	640.88	641.11	641.88	641.56	641.78	642.01	642.23	643.46	642.69		
285	642.91	643.14	643.36	643.59	643.81	644.04	644.26	644.49	644.72	644.94		
286	645.17	645.39	645.62	645.84	646.07	646.80		646.75	646.97	647.20		
297	617.42	647.65	647.87	648.10	648.88	648.55	648.78	649.00	649.23	649.45		
94 Inches.						1						
288	649.68	649.90	650.13	650.86	650.58	650.81	651.03	651.26	651.48	651.71		
289	651.98	652.16	652.89	652.61	652.84	658.06	658.29	653.51	658.74	653.96		
290	654.19	654.42	654.64	654.87	655.09	655.82		655.77	656.00	656.22		
291	656.45	656.67	656.90	657.12	657.85	1	657.90	658.03	658.25	658.48		
292	658.70	658.93	659.15	659.38	659.60	659.88	660.06	660.28	660.51	660.73		
293	660.96	661.18	661.41	661.68	661.86	662.09	662.31	662.54	662.76	662.99		
294	663.21	668.44	668.66	663.89	664.12	664.34	664.57	664.79	665.02	665.24		
295	665.47	665.70	665.92	666.15	666.37	666.60	1	667.08	667.27	667.50		
296	667.78	667.95	668.18	668.40	668.63	668.85	100000	669.30	669.53	669.76		
297	669.98	670.21	670.48	670.66	670.88	671.11	1	671.56	671.79	672.01		
296	672.24	672.46	672.69	672.91	678.14	673.36		673.82	674.04	674.27		
299	674.49	674.72	674.94	675.17	675.40	675.62	675.85	676.07	676.30	676.52		
25 Inches.	0.4.40	0.4	012102	075.27	070.40	075.02	070.00	676.07	070.30	070.52		
300	676.75	676.97	677.20	677.48	677.65	<i>099</i> 00	emp 10	070 90	000 EE	000 NO		
301	679.00	679.23	679.46				678.10	678.33	678.55	678.78		
302	681.26	681.49	681.71	679.68	679.91	680.13	680.36	680.58	680.81	681.08		
303	683.52	683.74	683.97	681.94	682.16		682.61	682.84	683.07	683.29		
304	685.77	686.00	686.22	684.19	684.42	684.64	684.87	685.10	685.32	685.55		
305	688.03	688.25	688.48	686.45 688.70	686.67 688.93	686.90 689.16		687.85 689.61	687.58 689.83	687.80		
				300.10	000.00	008.10	000.00	003.01	003.03	690.06		
306	690.28	690.51	690.78	690.96	691.19	691.41	691.64	691.86	692.09	692.31		
307	692.54	692.77	692.99	693.22	693.44	69 3.6 7	693.89	694.12	694.34	694.57		
808	694.80	695.02	695.25	695.47	695.70	695.92	696.15	696.37	696.60	696.83		
309	697.05	697.28	697.50	697.78	697.95	698.18	698.40	698.63	698.86	699.08		
810	699.31	699.58	699.76	699.98	700.21	700.48	700.66	700.89	701.11	701.84		
811	701.56	701.79	702.01	702.24	702.47	702.69	702.92	703.14	708.87	703.59		
				Hundr	dths of a	Line.						
0.	1.	2.	8.	4	. .	5.	6.	7.	8.	9.		
0.000	0.023	0.045	0.068	0.0	90 0.	113	0.135	0.158	0.180	0.203		

1 Paris Line = 2.255829 Millimetres.

Paris or	Tenths of a Line.												
French Lines.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.			
26 Inches.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Million.			
312	703.82	704.04	704.27	704.50	704.72	704.95	705.17	705.40	705.62	705.85			
813	706.07	706.80	706.53	706.75	706.98	707.20	707.43	707.65	707.88	708.10			
814	708.33	708.56	708.78	709.01	709.28	709.46	709.68	709.91	710.13	710.36			
815	710.59	710.81	711.04	711.26	711.49	711.71	711.94	712.17	712.39	712.62			
816	712.84	713.07	713.29	713.52	713.74	713.97	714.20	714.42	714.65	714.87			
817	715.10	715.82	715.55	715.77	716.00	716.23	716.45	716.68	716.90	717.18			
318	717.85	717.58	717.80	718.08	718.26	718.48	718.71	718.98	719.16	719.38			
819	719.61	719.84	720.06	720.29	720.51	720.74	720.96	721.19	721.41	721.64			
820	721.87	722.09	722.32	722.54	722.77	722.99	723.22	728.44	723.67	723.90			
821	724.12	724.85	724.57	724.80	725.02	725.25	725.47	725.70	725.93	726.15			
822	726.88	726.60	726.88	727.05	727.28	727.50	727.78	727.96	728.18	728.41			
328 27 Inches.	728.63	728.86	729.08	729.81	729.54	729.76	729.99	730.21	730.44	7 3 0.66			
824	730.89	731.11	731.34	731.57	731.79	732.02	732.24	732.47	782.69	782.92			
825	788.14	733.37	738.60	783.82	784.05	784.27	734.50	784.72	784.95	735.17			
826	785.40	735.63	735.85	786.08	786.80	736.53	786.75	736.98	787.20	737.43			
827	737.66	787.88	738.11	738.33	738.56	738.78	789.01	789.24	789.46	789.69			
328	739.91	740.14	740.86	740.59	740.81	741.04	741.27	741.49	741.72	741.94			
829	742.17	742.39	742.62	742.84	748.07	743.80	743.52	748.75	743.97	744.20			
830	744.42	744.65	744.87	745.10	745.88	745.55	745.78	746.00	746.23	746.45			
831	746.69	746.90	747.18	747.86	747.58	747.81	748.03	748.26	748.48	748.71			
332	748.94	749.16	749.39	749.61	749.84	750.06	750.29	750.51	750.74	750.97			
883	751.19	751.42	751.64	751.87	752.09	752.82	752.54	752.77	758.00	753.22			
884	753.45	753.67	758.90	754.12	754.85	754.57	754.80	755-03	755.25	755.48			
335 94 Inches.	755.70	755.93	756.15	756.38	756.61	756.88	757.06	757-28	757.51	757.73			
836	757.96	758.18	758.41	758.64	758.86	759.09	759.31	759.54	759.76	759.99			
837	760.21	760.44	760.67	760.89	761.12	761.84	761.57	761.79	762.02	762.24			
838	762.47	762.70	762.92	763.15	768.37	763.60	768.82	764.05	764.27	764.50			
339	764.73	764.95	765.18	765.40	765.68	765.85	766.08	766.31	766.53	766.76			
840	766.98	767.21	767.43	767.66	767.88	768.11	768.34	768.56	768.79	769.01			
841	769.24	769.46	769.69	769.91	770.14	770.87	770.59	770.82	771.04	771.27			
342	771.49	771.72	771.94	772.17	772.40	772.62	772.85	773.07	773.30	778.52			
843	773.75	773.97	774.20	774.48	774.65	774.89	775.10	775.83	775.55	775.78			
814	776,01	776.23	776.46	776.68	776.91	777.18	777.36	777.58	777.81	778.04			
845	778.26	778.49	778.71	778.94	779.16	779.39	779.61	779.84	780.07	780.29			
346	780.52	780.74	780.97	781.19	781.42	781.64	781.87	782.10	782.32	782.55			
817	782.77	783.00	783.22	788.45	783.67	788.90	784.13	784.35	784.58	784.80			
29 Inches.						1	ł						
348	785.03	785.25	785.48	785.71	785.93	786.16	786.38	786.61	786.83	787.06			
				Hundr	edths of a	Idne.							
9.	1.	9.	8.	4	. 4	5.	6.	7.	8.	9.			
0.000	0.023	0.045	0.06	8 0.0	90 0.	113).135	0.158	0.180	0.203			

VII. - VIII.

COMPARISON

OF

THE RUSSIAN BAROMETER

WITH

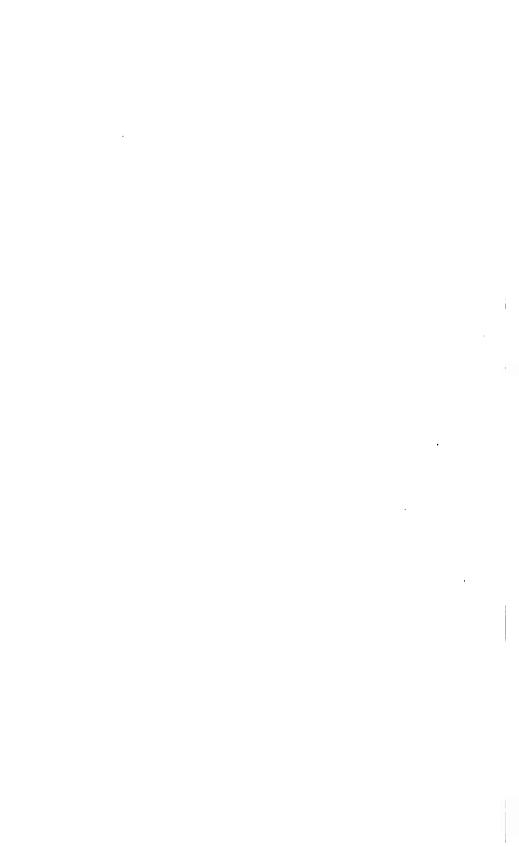
THE METRICAL AND THE OLD FRENCH BAROMETERS,

OR

TABLES

FOR CONVERTING RUSSIAN HALF-LINES INTO MILLIMETRES,
AND INTO FRENCH OR PARIS LINES;

GIVING THE VALUES CORRESPONDING TO EVERY HALF-LINE FROM 440 TO 540, OR FROM 22 TO 27 INCHES; AND TO EVERY TENTH, FROM 540 TO 610 HALF-LINES, OR FROM 27 TO 80.5 ENGLISH INCHES.



RUSSIAN BAROMETER.

A LEGULAR system of Meteorological Observations has been established by order of the Russian government throughout the extensive regions placed under its sway, and a vast amount of observations made in Europe, in Asia, and in North America have already been published. The scale of the barometer employed in this system is divided in units, each of which is equal to one half of a Russian, or English decimal line, that is, 1 = 0.05 of an inch, 600 half-lines of the Russian Barometer being = 30 inches of the English Barometer.

The conversion of this scale, which is the English scale, slightly modified in its form, is easy. It suffices to divide the Russian heights by two, and to put back, by one figure, the decimal point, in order to have them converted into English inches and decimals. This transformation is so easy to effect, that a peculiar table for it would seem superfluous.

The normal temperature of the standard being the same as that of the English, that is, 13°\frac{1}{3} Reaumur, or 62° Fahrenheit, the reduction of the Russian Barometer to the freezing point can be made by means of the table for reducing the English Barometers. But the attached thermometer being that of Reaumur, its indications must be first converted into degrees of Fahrenheit.

Tables VII. and VIII., which follow, have been computed in order to render more easy the comparison and the use of the Barometrical Observations recorded in the large collection, published annually by order of the Emperor of Russia, under the name of Annuaire Météorologique et Magnétique du Corps des Ingénieurs des Mines.

1 Russian Half-Line = 1.289977 Millimetres.

Russian	Units or Russian Half-Lines.											
Half-Lines.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.		
33 Inch.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim		
440	558.79	560.06	561.33	562.60	563.87	565.14	566.41	567.68	568.95	570.22		
450	571.49	572.76	574.08	575.30	576.57	577.84	579.11	560.38	581.65	582.93		
460	584.19	583.46	586.73	588.00	589.27	590.54	591.81	593.08	594.35	595.6		
470	596. 89	598.16	599.48	600.70	601.97	603.24	604.51	605.78	607.05	608.3		
480	609.59	610.86	612.13	613.40	614.67	615.94	617.21	618.48	619.75	621.0		
94.5 In.						l						
490	622.29	628.56	624.88	626.10	627.87	628.64	629.91	631.18	632.45	633.7		
500	634.99	636.26	687.53	688.80	640.07	641.34	642.61	643.88	645.15	646.4		
510	647,69	648.96	650.23	651.50	652.77	654.04	655.81	656.58	657.85	659.1		
520	660.89	661.66	662.93	664.20	665.47	666.74	668.01	669.28	670.55	671.8		
530	678.09	674.86	675.63	676.90	678.17	679.44	680.71	681.98	683.25	684.5		
Rossian					Ten	the.						
Half-Lines.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.		
97 Inch.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Million.	Militon		
540	685.79	685.91	686.04	686.17	686.80	686.42	686.55	686.68	686.80	686.9		
541	687.06	687.18	687.81	687.44	687.57	687.69	687.82	687.95	688.07	688.20		
542	688.33	688.45	688.58	688.71	688.84	688.96	689.09	689.22	689.34	689.4		
548	689.60	689.72	689.85	689.98	690.11	690.28	690.86	690.49	690.61	690.7		
544	690.87	690.99	691.12	691.25	691.88	691.50	691.63	691.76	691.88	692.0		
545	692.14	692.26	692.39	692.52	692.65	692.77	692.90	693.08	693.15	698.28		
546	693.41	698.53	693.66	698.79	693.91	694.04	694.17	694.80	694:42	694.5		
	694.68	694.80	694.93	695.06	695.19	695.81	695.44	695.57	695.69	695.8		
547 548	695.95	696.07				696.58				697.0		
549	697.22	697.34	696.20	696.33	696.46	697.85	696.71 697.98	696.84 698.11	696.96 698.28	698.3		
97.5 In.	081.22	087.04	697.47	697.60	697.78	097.00	091180	080.11	030.20	0 30.3		
550	698.49	698.61	698.74	698.87	699.00	699.12	699.25	699.38	699.50	699.6		
551	699.76	699.88	700.01	700.14	700.27	700.39	700.52	700.65	700.77	700.9		
552	701.03	701.15	701.28	701.41	701.54	701.66	701.79	701.92	702.04	702.1		
553	702.80	702.42	702.55	702.68	702.81	702.93	703.06	703.19	703.31	703.4		
554	708.57	703.69	708.82	703.95	704.08	704.20	704.88	704.46	704.58	704.7		
	#0.4 0.4	801.00	#A# A0	#A¥ 00	-04 04	***	#0# 00	-0" =0	****	#0# 0/		
555	704.84	704.96	705.09	705.22	705.35	705.47	705.60	705.73	705.85	705.9		
556	706.11	706.23	706.86	706.49	706.62	706.74	706.87	707.00	707.12	707.2		
557	707.88	707.50	707.63	707.76	707.89	708.01	708.14	708.27	708.89	708.5		
558	708.65	708.77	708.90	709.08	709.16	709.28	709.41	709.54	709.66	709.7		
559 28 Inch.	709.92	710.14	710.27	710.40	710.58	710.65	710.78	710.81	710.98	711.00		
560	711.19	711.31	711.44	711.57	711.70	711.82	711.95	712.08	712.20	712.85		
561	712.46	712.58	712.71	712.84	712.97	713.09	713.22	713.35	713.47	713.60		
562	718.78	713.85	713.98	714.11	714.24	714.36	714.49	714.62	714.74	714.8		
563	715.00	715.12	715.25	715.38	715.51	715.63	715.76	715.89	716.01	716.1		
564	716.27	716.89	716.52	716.65	716.78	716.90	717.08	717.16	717.28	717.4		
565	717.54	717.66	717.79	717.92	718.04	718.17	718.30	718.48	718-55	718.6		
566	718.81	718.93	719.06	719.19	719.31	719.44	719.57	719.70	719.82	719.9		
567	720.08	720.20	720.83	720.46	720.58	720.71	720.84	720.97	721.09	721.2		
- 10	721.85	721.47	721.60	720.46	721.85	721.98	722.11	722.24		721.4		
568			1						722.36			
569	722.62	122.74	722.87	723.00	728.12	723.25	723.88	728.51	728.63	723.7		

1 Russian Half-Line = 1.200977 Millimetre.

Romina	Tenths.										
Half-Lines.	0.	1.	2.	8.	.4.	5.	6.	7.	8.	9.	
96,5 Inch.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	
570	723.89	724.01	724.14	724.27	724.89	724.52	724.65	724.78	724.90	725.03	
571	725.16	725.2 8	725.41	725.54	725.66	725.79	725.92	726.05	726.17	726.80	
572	726.43	726.55	726.68	726.81	726.93	727.06	727.19	727.82	727.44	727.57	
573	727.70	727.82	727.95	728.08	728.20	728.88	728.46	728.59	728.71	728.84	
574 575	728.97	729.08	729.21	729.84	729.46	729.59	729.78	729.85	729.97	780.11	
	780.24	780.86	730.49	780.62	780.74	780.87	781.00	781.18	781.25	781.38	
576	731.51	781.63	781.76	781.89	732.01	732.14	732.27	782.40	782.52	782.65	
577	732.78	782.90	783.08	733.16	738.28	733.41	783.54	738.67	783.79	783.92	
578	734.05	784.17	734.80	784.48	734.55	784.68	734.81	784.94	735.06	785.19	
579	735.82	785.44	735.57	785.70	735.82	785.95	786.08	786.21	786.83	786.46	
39 Inch.											
580	736.59	786.71	736.84	786.97	737.09	787.22	787.85	787.48	787.60	787.78	
581	737.86	787.98	738.11	788.24	788.86	788.49	788.62	788.75	738.87	739.00	
582	789.13	789.25	739.38	789.51	789.63	789.76	739.89	740.02	740.14	740.27	
588	740.40	740.52	740.65	740.78	740.90	741.08	741.16	741.29	741.41	741.54	
584	741.67	741.79	741.92	742.08	742.17	742.80	742.48	742.56	742.68	742.81	
585	742.94	743.06	748.19	748.82	743.44	748.57	743.70	743.83	743.95	744.08	
586	744.21	744.83	744.46	744.59	744.71	744.84	744.97	745.10	745.22	745.85	
587	745.48	745.60	745.78	745.86	745.98	746.11	746.24	746.87	746.49	746.62	
588	746.75	746.87	747.00	747.18	747.25	747.38	747.51	747.64	747.76	747.89	
589 39. 5 In.	748.02	748.14	748.27	748.40	748.52	748.65	748.78	748.91	749.03	749.16	
590	749.29	749.41	749.54	749.67	749.79	749.92	750.05	750.18	750.80	750.43	
591	750.56	750.68	750.81	750.94	751.06	751.19	751.82	751.45	751.57	751.70	
592	751.88	751.95	752.08	752.21	752.88	752.46	752.59	752.72	752.84	752.97	
593	753.10	758.22	753.85	753.48	753.60	753.78	758.86	753.99	754.11	754.24	
594	754.87	754.49	754.62	754.75	754.87	755.00	755.13	755.26	755.88	755.51	
595	755.64	755.76	755.89	756.02	756.14	756.27	756.40	756.53	756.65	756.78	
596	756.91	757.03	757.16	757.29	757.41	757.54	757.67	757.80	757.92	758.05	
597	758.18	758.80	758.48	758.56	758.68	758.81	758.94	759.07	759.19	759.32	
598	759.45	759.57	759.70	759.84	759.96	760.09	760.21	760.84	760.46	760.59	
599 30 Inch.	760.72	760.84	760.97	761.10	761. 22	761.85	761.48	761.61	761.7 8	761.86	
600	761.99	762.11	762.24	762.87	762.49	762.62	762.75	762.88	768.00	763.13	
601	763.26	763.88	763.51	768.64	763.76	768.89	764.02	764.15	764.27	764.40	
602	764.53	764.65	764.78	764.91	765.08	765.16	765.29	765.42	765.54	765.67	
603	765.80	765.92	766.05	766.16	766.30	766.48	766.56	766.69	766.81	766.95	
604	767.07	767.19	767.82	767.45	767.57	767.70	767.88	767.96	768.08	768.21	
605	768.34	768.46	768.59	768.72	768.84	768.97	769.10	769.28	769.35	769.48	
606	769.61		769.85	769.99	770.11	770.24		770.50	770.62	770.75	
607											
608	772.15	772.27	772.40	772.58	772.65	772.78	772.91	778.08	778.16	778.29	
609	778.42	778.54	773.67			774.05		1	l .	774.56	
				H	undredths.						
0.000	0.018	0.025	0.088	0.05	1 0.0	68 0.	076	0.089	0.102	0.114	

1 Russian Half-Line - 0.562976 Paris Line.

Bussian		Units or Russian Half-Lines.											
Haif-Lines.	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.			
22 Inch.	Par. line.	Par. Mne.	-	Par. line.		Par line.			Par line.				
440	247.71	248.27	248.84	249.40	249.96	250.52	251.09	251.65	252.21	252.78			
450	253.34	253.90	254.47	255.03	255.59	256.15	256.72	257.28	257.84	258.41			
460	258.97	259.58	260.09	260.66	261.22	261.78	262.85	262.91	263.47	264.04			
470	264.60	265.16	265.72	266.29	266.85	267.41	267.98	268.54	269.10	269.67			
480	270.23	270.79	271.85	271.92	272.48	278.04	278.61	274.17	274.73	275.30			
94.5 In.													
490	275.86	276.42	276.98	277.55	278.11	278.67	279.24	279.80	280.36	280.93			
500	281.49	282.05	282.61	288.18	283.74	284.30	284.87	265.43	285.99	286.55			
510	287.12	287.68	288.24	268.81	289.87	289.93	290.50	291.06	291.62	292.18			
520	292.75	293.81	293.87	294.44	295.00	295.56	296.13	296.69	297.25	297.81			
580	296.38	298.94	299.50	800.07	300.63	801.19	301.76	802.32	302.88	303.44			
Russian					Ten	ths.	•						
Half-Lines.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.			
97 Inch.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line	Pur. line			
540	804.01	304.06	804.12	304.18	304.23	804.29	304.84	804.40	304.46	304.51			
541	304.57	304.63	304.68	804.74	304.80	304.85	804.91	304.96	305.02	305.08			
542	305.13	305.19	305.25	305.30	305.36	305.41	305.47	805.58	305.58	805.64			
548	805.70	805.75	305.81	305.86	805.92	805.98	306.03	306.09	806.15	306.20			
544	806.26	306.82	806.87	306.43	306.48	806.54	306.60	306.65	306.71	306.77			
545	806.82	306.88	806.98	806.99	307.05	807.10	307.16	307.22	307.27	307.33			
546	307.38	807.44	807.50	807.55	807.61	807.67	807.72	307.78	307.84	307.89			
547	807.95	308.00	308.06	308.12	808.17	808.23	308.29	308.34	808.40	308.45			
548	808.51	308.57	308.62	808.68	808.74	808.79	308.85	308.90	308.96	809.02			
549	809.07	309.13	809.19	309.24	309.30	809.36	809.41	309.47	309.52	309.58			
97.5 In.							İ	1	1	Ì			
550	809.64	309.69	809.75	309.81	309.86	309.92	309.97	310.03	310.09	310.14			
551	810.20	310.26	310.31	310.37	810.42	310.48	810.54	810.59	310.65	310.7			
552	810.76	810-82	310.88	810.93	310.99	311.04	811.10	311.16	311.21	311.27			
553	811.83	311.38	811.44	311.49	311.55	311.61	811.66	811.72	811.78	311.8			
554	311.89	311.95	812.00	812.06	812.11	312.17	312.23	312.28	312.34	312.40			
555	312.45	312.51	812.56	312.62	812.68	312.73	312.79	312.85	312.90	312.90			
556	818.01	813.07	818.13	313.18	818.24	813.30	813.35	818.41	813.47	318.5			
557	313.56	813.63	313.69	813.75	313.80	313.86	818.92	313.97	314.03	314.06			
558	814.14	814.20	814.25	814.81	814.87	314.42	814.48	814.53	314.59	814.6			
559	314.70	814.76	814.82	314.87	814.93	814.99	815.04	815.10	315.15	315.2			
96 Inch.		l	ŀ	ļ									
560	815.27	315.32	815.38	315.44	315.49	315.55	815.60	315.66	315.72	815.77			
561	315.83	815.89	815.94	816.00	816.05	316.11	816.17	816.22	316.28	816.3			
562	316.89	816.45	816.51	816.56	,	316.67		316.79	1	316.90			
568	816.96	817.01	317.07	817.12	317.18	817.24	817.29	817.85	317.41	817.40			
564	317.52	817.57	817.63	317.69	317.74	817-80	317.86	817.91	817.97	818.0			
565	318.08	1	318.19	318.25	318.31	318.86		318.48	818.53	318.59			
566	818.64	818.70	318.76	818.81	318.87	318.98		319.04	319.09	319.13			
567	819.21	319.26	819.32	319.39	•	319.49	819.55	819.60	319.66	819.7			
568	819.77	319.83	819.88	319.94	320.00	320.05	320.11	320.16	320.22	320.2			
569	820.88	320.89	820.45	320.50	820.56	B20.61	320.67	820.73	320.7 8	320.8			

COMPARISON OF THE RUSSIAN AND OLD FRENCH BAROMETERS.

1 Russian Half-Line = 0.562976 Paris Line.

Russian					Ten	the.				
Half-Lines.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
28.5 Incb.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	1		Par. line.	Par. line.
570	320.90	320.93	821.01	821.07	821.12	321.18	821.23	321.29	321.35	321.40
571	321.46	321.52	321.57	321.63	321.63	821.74	821.80	821.85	321.91	321.97
572	322.02	322.08	322.13	822.19	322.25	822.80	322.36	822.42	322.47	322.58
573	322.59	322.64	322.70	822.75	822.81	322.87	322.92	322.98	323.04	328.09
574	323.15	823.20	323.26	323.82	823.37	823.43	323.49	823.54	323.60	323.65
575	323.71	828.77	828.82	323.89	323.94	323.99	824.05	824.11	324.16	824.22
576	324.27	824.33	324.39	824.44	824.50	824.56	824.61	824.67	324.72	324.78
577	324.84	324.89	324.95	825.01	325.06	825.12	825.17	823.23	325.29	825.84
578	325.40	325.46	325.51	325.57	325.63	325.68	325.74	825.79	825.85	825.91
579	325.96	326.02	326.08	326.13	826.19	326.24	826.80	826.36	826.41	326.47
29 Inch.										
530	326.53	326.58	826.64	326.69	826.75	326.81	326.86	326.92	326.9 8	827.08
591	327.09	327.15	327.20	327.26	827.81	827.37	327.43	327.48	327.54	327.60
582	327.65	827.71	327.76	327.82	327.88	827.98	827.99	328.05	828.10	328.16
583	328.22	328.27	328.33	328.38	828.44	328.50	B28.55	328.61	328.67	828.72
584	328.78	328.83	828.89	329.95	329.00	829.06	329.12	829.17	329.23	329.28
585	329.34	329.40	329.45	329.51	329.57	329.62	329.68	329.74	329.79	329.85
586	329.90	329.96	330.02	830.07	330.13	330.19	830.24	330.30	830.85	330.41
587	330.47	330.52	380.58	380.64	830.69	330.75	830.80	330.86	380.92	380.97
588	331.03	331.09	331.14	881.20	331.26	331.31	331.37	331.42	881.48	831.54
589	831.59	331.65	381.71	831.76	831.82	881.87	331.93	881.99	332.04	882.10
29.5 In.									l	l
590	332.16	332.21	332.27	382.82	332.88	332.44	882.49	832.55	832.61	382.66
591	332.72	332.78	332.83	332.89	882.94	883.00	833.06	883.11	833.17	333.28
592	333.28	333.54	333.39	383.45	333 .51	883.56	333.62	383.68	383.78	833.79
593	333.84	333.90	333.96	884.01	884.07	884.18	284.18	384.24	834.80	834.35
594	834.41	884.46	334.52	884.58	834.63	384.69	884.75	834.80	384.86	884.91
595	334.97	335.03	335.08	885.14	835.20	835.25	835.31	335.36	835.42	835.48
596	335.53	335.59	335.65	885.70	885.76	885.82	835.87	335.93	835.98	336.04
597	336.10	336.15	336.21	336.27	836.82	886.38	336.43	836.49	336.55	836.60
598	836.66	336.72	886.77	336.88	886. 88	336.94	887.00	387.05	887.11	837.17
599	837.22	837.28	837.34	887.89	887.45	337.50	887.56	837.62	887.67	337.73
30 Inch.										200 00
600	337.79	887.84	337.90	387.95	238.01	838.07	338.12	838.18	888.24	338.29
601	338.35	338.40	888.46	338.52	838.57	838.63	338.69	338.74	338.80	838.86
602	338.91	338.97	339.02	339.08	839.14	389.19	839.25	339.31	839.86	839.42
603	339.47	839.53	389.59	889.64	889.70	889.76	889.81	839.87	889.92	339.98
601	340.04	840.09	840.15	840.21	340.26	340.82	840.88	340.43	840.49	340.54
605	340.60	340.66	340.71	340.77	840.83	340.88	840.94	840.99	341.05	841.11
606	341.16	841.22	841.28	341.88	841.89	841.44	341.50	341.56	841.61	841.67
607	341.73	341.78	841.84	341.90	841.95	342.01	842.06	842.12	342.18	842.28
609	342.29	342.35	842.40	842.46	842.51	342.57	342.68	842.68	842.74	342.80
609	342.85	842.91	842.96	843.02	843.08	343.13	343.19	343.25	348.30	343.36
				H	undredths.					
I		0.01	1 0 0				084 4) 000 I	0.045	0.051
0.000	0.006	0.011	0.017	0.02	2 0.0	28 0.	034 (0.039	0.045	0.051



IX.-XVI.

COMPARISON

OF

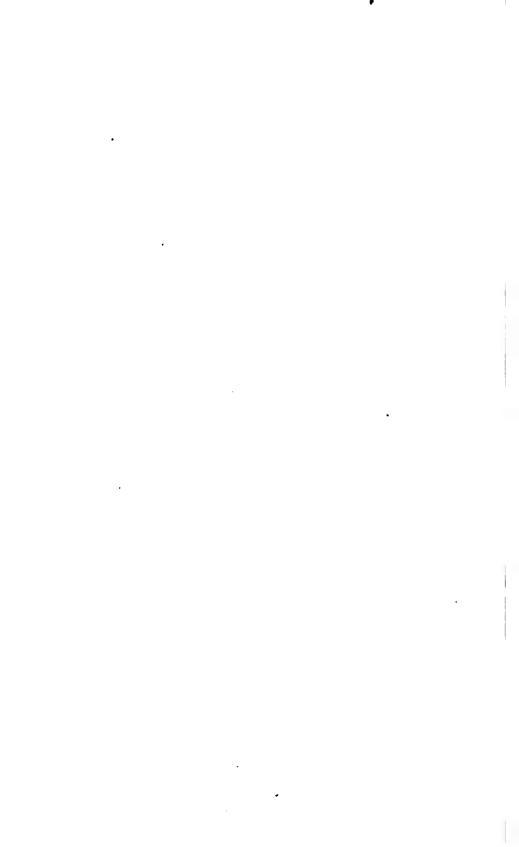
BAROMETRICAL DIFFERENCES

EXPRESSED IN MEASURES OF DIFFERENT SCALES,

OR

TABLES

FOR CONVERTING ENGLIST/ INCHES, MILLIMETRES, PARIS LINES, AND RUSSIAN HALF-LINES INTO EACH OTHER.



IX. CONVERSION OF ENGLISH INCHES INTO MILLIMETERS.

1 English Inch = 25.89954 Millimetres.

Roglish										
Inches and Tunths.	0.	1.	2.	8.	4.	5.	6,	7.	8.	9.
	Millim.	Millian.	Millim.	Millim.	Million.	Millim.	Millim.	Millim.	Millim.	Millim.
0.0	0.000	0.254	0.508	0.762	1.016	1.270	1.524	1.778	2.032	2.286
0.1	2.540	2.794	8.048	8.802	8.556	8.810	4.064	4.318	4.572	4.826
0.2	5.080	5.834	5.588	5.842	6.096	6.850	6.604	6.858	7.112	7.366
0.3	7.620	7.874	8.128	8.882	8.636	8.890	9.144	9.398	9.652	9.906
0.4	10.160	10.414	10.668	10.922	11.176	11.480	11.684	11.988	12.192	12.446
2.5	12.700	12.954	13.206	13.462	18.716	18.970	14.224	14.478	14.782	14.986
		ŀ								1
0.6	15.240	15.494	15.748	16.002	16.256	16.510	16.764	17.018	17.272	17.526
0.7	17.780	18.084	18.288	18.542	18.796	19.050	19.804	19.558	19.812	20.066
0.8	20.820	20.574	20.828	21.082	21.336	21.590	21.844	22.098	22.852	22.606
0.9	22.860	23.114	28.868	23.622	28.876	24.180	24.884	24.688	24.892	25.146
1.0	25.400	25.654	25.908	26.162	26.416	26.670	26.924	27.178	27.432	27.685
1.1	27.939	28.193	28.447	28.701	28.955	29.209	29.463	29.717	29.971	30.225
	l	}		1					l	
1.2	80.479	30.783	80.987	81.241	31.495	31.749	82.008	32.257	32.511	32.765
1.3	83.019	33.278	33.527	88.781	84.035	34.289	34.548	84.797	35.051	35.305
1.4	35.559	35.818	86.067	86.821	86.575	86.829	37.083	37.337	37.591	37.845
1.5	88.099	38.353	38.607	38.861	89.115	39.369	39.628	89.877	40.181	40.885
1.6	40.639	40.893	41.147	41.401	41.655	41.909	42.163	42.417	42.671	42.925
1.7	43.179	43.438	48.687	48.941	44.195	44.449	44.708	44.957	45.211	45.465
1.8	45.719	45.973	46.227	46.481	46.785	46.989	47.248	47.497	47.751	48.005

X. CONVERSION OF ENGLISH INCHES INTO FRENCH OR PARIS LINES. 1 English Inch = 11.259515 Paris Lines.

Bortish	Hundredths of an Inch.										
Inches and Tenths.	0.	1,	2.	8.	4.	5.	6.	7.	8.	9.	
	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	
0.0	0.000	0.118	0.225	0.338	0.450	0.563	0.676	0.788	0.901	1.013	
0.1	1.126	1.239	1.851	1.464	1.576	1.689	1.802	1.914	2.027	2.139	
0.2	2.252	2.864	2.477	2.590	2.702	2.815	2.927	8.010	3.158	3.265	
0.3	8.378	8.490	8.603	3.716	8.828	3.941	4.053	4.166	4.279	4.891	
0.4	4.504	4.616	4.729	4.842	4.954	5.067	5.179	5.292	5.405	5.517	
0.5	5.630	5.742	5.855	5.968	6.080	6.198	6.805	6.418	6.581	6.643	
0.6	6.756	6.868	6.981	7.098	7.206	7.819	7.431	7.544	7.656	7.769	
0.7	7.882	7.994	8.107	8.219	8.832	8.445	8.557	8.670	8.782	8.895	
0.8	9.009	9.120	9.238	9.345	9.458	9.571	9.688	9.796	9.908	10.021	
0.9	10.184	10.246	10.359	10.471	10.584	10.697	10.809	10.922	11.034	11.147	
1.0	11.260	11.372	11.485	11.597	11.710	11.822	11.985	12.048	12.160	12.273	
1.1	12.385	12.498	12.611	12.728	12.836	12.948	18.061	13.174	13.286	13.399	
1.2	18.511	13.624	13.787	13.849	13.962	14.074	14.187	14.800	14.412	14.525	
1.3	14.637	14.750	14.863	14.975	15.088	15.200	15.818	15.426	15.538	15.651	
1.4	15.763	15.876	15.988	16.101	16.214	16.826	16.489	16.551	16.664	16.777	
1.5	16.889	17.002	17.114	17.227	17.840	17.452	17.565	17.677	17.790	17.903	
1.6	18.015	18.128	18.240	18.858	18.466	18.578	18.691	18.803	18.916	19.029	
1.7	19.141	19.254	19.866	19.479	19.592	19.704	19.817	19.929	20.042	20.155	
1.8	20.267	20.380	20.492	20.605	20.717	20.880	20.948	21.055	21.168	21.280	

XI. CONVERSION OF MILLIMETRES INTO ENGLISH INCHES.

1 Metre = 89.57079 English Inches.

Millime-	Tenths of a Millimetre.										
tres.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.	
	Hng. In.	Hng. In.	Hng. In.		Bng. In.	Eng. In.		Eng. In.		Bog. In	
0	0.0000	0.0039	0.0079	0.0118	0.0157	0.0197	0.0236	0.0276	0.0815	0.035	
1	0.0394	0.0488	0.0472	0.0512	0.0551	0.0591	0.0630	0.0669	0.0709	0.0748	
2	0.0787	0.0827	0.0866	0.0906	0.0945	0.0984	0.1024	0.1068	0.1102	0.1142	
8	0.1181	0.1220	0.1260	0.1299	0.1389	0.1878	0.1417	0.1457	0.1496	0.153	
4	0.1575	0.1614	0.1654	0.1693	0.1782	0.1772	0.1811	0.1850	0.1890	0.1929	
5	0.1969	0.2008	0.2047	0.2087		0.2165	1	0.2244	0.2283	0.2321	
6	0.2362	0.2402	0.2441	0.2480	0.2520	0.2559	0.2598	0.2688	0.2677	0,2717	
7	0.2756	0.2795	0.2835	0.2974	0.2913	0.2953	0.2992	0.3032	0.3071	0.8110	
8	0.8150	0.3189	0.3228	0.8268	0.3307	0.3347	0.3386	0.8425	0.8465	0.350	
9	0.8548	0.3588	0.8622	0.3661	0.3701	0.8740	0.8780	0.8819	0.8858	0.8898	
10	0.3937	0.8976	0.4016	0.4055	0.4095	0.4134	0.4178	0.4218	0.4252	0.4291	
11	0.4331	0.4370	0.4410	0.4449	0.4488	0.4528	0.4567	0.4606	0.4646	0.4685	
12	0.4724	0.4764	0.4803	0.4843	0.4882	0.4921	0.4961	0.5000	0.5039	0.5079	
13	0.5118	0.5158	0.5197	0.5236	0.5276	0.5315	0.5854	0.5894	0.5433	0.5478	
14	0.5512	0.5551	0.5591	0.5630	0.5669	0.5709	0.5748	0.5788	0.5827	0.5866	
15	0.5906	0.5945	0.5984	0.6024		0.6102		0.6181	0.6221	0.6260	
16	0.6299	0.6839	0.6378	0.6417	0.6457	0.6496	0.6586	0.6575	0.6614	0.6654	
17	0.6693	0.6732	0.6772	0.6811	0.6851	0.6890	0.6929	0.6969	0.7008	0.7047	
18	0.7087	0.7126	0.7165	0.7205	0.7244	0.7284	0.7828	0.7362	0.7402	0.7441	
19	0.7480	0.7520	0.7559	0.7599	0.7638	0.7677	0.7717	0.7756	0.7795	0.7835	
20	0.7874	0.7914	0.7953	0.7992	0.8032	0.8071	0.8110	0.8150	0.8189	0.8228	
21	0.8268	0.8307	0.8847	0.8386	0.8425	0.8465	0.8504	0.8543	0.8583	0.8622	
22	0.8662	0.8701	0.8740	0.8780	0.8819	0.8858	0.8898	0.8987	0.8977	0.9016	
28	0.9055	0.9095	0.9134	0.9178	0.9213	0.9252	0.9292	0.9381	0.9870	0.9410	
24	0.9449	0.9488	0.9528	0.9567	0.9606	0.9646	0.9685	0.9725	0.9764	0.9801	
25	0.9843	0.9882	0.9921	0.9961	1.0000	1.0040	1.0079	1.0118	1.0158	1.0197	
26	1.0286	1.0276	1.0315	1.0355	1.0394	1.0438	1.0478	1.0512	1.0551	1.059	
27	1.0630	1.0669	1.0709	1.0748	1.0788	1.0827	1.0866	1.0906	1.0945	1.098	
28	1.1024	1.1068	1.1108	1.1142	1.1181	1.1221	1.1260	1.1299	1.1339	1.1878	
29	1.1418	1.1457	1.1496	1.1536	1.1575	1.1614	1.1654	1.1698	1.1732	1.177	
80	1.1811	1.1851	1.1890	1.1929	1.1969	1.2008	1.2047	1.2087	1.2126	1.216	
81	1.2205	1.2244	1.2284	1.2323	1.2362	1.2402	1.2441	1.2481	1.2520	1.2559	
82	1.2599	1.2638	1.2677	1.2717	1.2756	1.2796	1.2835	1.2874	1.2914	1.295	
88	1.2992	1.8082	1.8071	1.3110	1.8150	1.3189	1.8229	1.3268	1.3307	1.334	
84	1.8386	1.3425	1.3465	1.8504	1.3544	1.8588	1.3622	1.3662	1.3701	1.374	
35	1.3780	1.8819	1.3859	1.8898	1.3937	1.3977		1.4055	t .	1.413	
36	1.4178	1.4218	1.4252	1.4292	1.4831	1.4870	1.4410	1.4449	1.4488	1.452	
87	1.4567	1.4607	1.4646	1.4685	1.4725	1.4764	1.4803	1.4843	1.4882	1.492	
88	1.4961	1.5000	1.5040	1.5079	1.5118	1.5158	1.5197	1.5236	1.5276	1.531	
89	1.5355	1.5894	1.5488	1.5478	1.5512	1.5551	1.5591	1.5630	1.5670	1.570	
40	1.5748	1.5788	1.5827	1.5866	1.5906	1.5945	1.5985	1.6024	1.6063	1.610	
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.	

XII. CONVERSION OF MILLIMETRES INTO FRENCH OR PARIS LINES.

1 Millimetre = 0.448296 Paris Line.

Millime-		Tenths of a Millimetre.													
tres.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.					
	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. lin					
0	0.000	0.044	0.089	0.133	0.177	0.222	0.266	Ø.310	0.355	0.39					
1	0.448	0.488	0.532	0.576	0.621	0.665	0.709	0.754	0.798	0.84					
2	0.887	0.981	0.975	1.020	1.064	1.108	1.153	1.197	1.241	1.28					
8	1.380	1.374	1.419	1.463	1.507	1.552	1.596	1.640	1.685	1.72					
4	1.778	1.818	1.862	1.906	1.950	1.995	2.039	2.083	2.128	2.17					
5	2.216	2.261	2.305	2.849	2.894	2.488	2.482	2.527	2.571	2.61					
6	2.660	2.704	2.748	2.793	2.837	2.881	2.926	2.970	8.014	8.05					
7	8.103	8.147	3.192	3.236	3.280	3.325	8.369	8.418	8.458	3.50					
8	3.546	3.591	3.635	3.679	3.724	3.768	3.812	3.857	8.901	8.94					
9	8.990	4.084	4.078	4.128	4.167	4.211	4.256	4.800	4.844	4.38					
10	4.483	4.477	4.522	4.566	4.610	4.655	4.699	4.748	4.788	4.83					
11	4.876	4.921	4.965	5.009	5.054	5.098	5.142	5.187	5.231	5.27					
12	5.820	5.364	5.408	5.453	5.497	5.541	5.586	5.680	5.674	5.71					
13	5.763	5.807	5.851	5.896	5.940	5.984	6.029	6.078	6.117	6.16					
14	6.206	6.250	6.295	6.339	6.383	6.428	6.472	6.516	6.561	6.60					
15	6.649	6.694	6.738	6.782	6.827	6.871	6.915	6.960	7.004	7.04					
16	7.093	7.187	7.181	7.226	7.270	7.814	7.359	7.403	7.447	7.49					
17	7.586	7.580	7.625	7.669	7.713	7.758	7.802	7.846	7.891	7.98					
18	7.979	8.024	8.068	8.112	8.157	8.201	8.245	8.290	8.334	8.37					
19	8.423	8.467	8.511	8.556	8.600	8.644	8.689	8.783	8.777	8.82					
20	8.866	8.910	8.955	8.999	9.048	9.088	9.182	9.176	9.221	9.26					
21	9.809	9.354	9.398	9.442	9.487	9.581	9.575	9.620	9.664	9.70					
22	9.753	9.797	9.841	9.886	9.930	9.974	10.018	10.063	10.107	10.15					
23	10.196	10.240	10.284	10.329	10.873	10.417	10.462	10.506	10.550	10.59					
24	10.639	10.688	10.728	10.772	10.816	10.861	10.905	10.949	10.994	11.02					
25	11.082	11.127	11.171	11.215	11.260	11.804	11.848	11.893	11.437	11.48					
26	11.526	11.570	11.614	11.659	11.703	11.747	11.792	11.836	11.880	11.92					
27	11.969	12.013	12.058	12.102	12.146	12.191	12.285	12.279	12.824	12.86					
28	12.412	12.457	12.501	12.545	12.590	12.684	12.678	12.728	12.767	12.81					
29	12.856	12.900	12.944	12.989	18.033	18.077	13.122	18.166	18.210	13.20					
80	18.299	13.843	13.888	18.482	18.476	18.521	13.565	18.609	18.654	18.69					
31	13.742	13.786	13.881	13.875	18.919	18.964	14.008	14.052	14.097	14.14					
82	14.185	14.230	14.274	14.818	14.363	14.407	14.451	14.496	14.540	14.58					
83	14.629	14.678	14.717	14.762	14.806	14.850	14.895	14.939	14.983	15.02					
84	15.072	15.116	15.161	15.205	15.249	15.294	15.388	15.882	15.427	15.47					
85	15.515		15.604	1	1	15.787			1	15.91					
36	15.959	16.003	16.047	16.092		16.180	16.225	16.269	16.818	16.85					
87	16.402	16.446	16.491	16.535	ł	16.624	16.668	16.712	16.757	16.80					
88	16.845	16.890	16.934	16.978	17.028	17.067	17.111	17.156	17.200	17.24					
39	17.289	17.838	17.877	17.422	17.466	17.510	17.555	17.5 9 9	17.643	17.68					
40	17.732	17.776	17.820	17.865	17.909	17.953	17.998	18.042	18.066	18.13					
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.					

XIII. CONVERSION OF THE FRENCH OR PARIS LINES INTO MILLIMETRES.

1 Paris Line = 2.255829 Millimetres.

Paris					Tenths o	ć a Line.				
Lines.	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.000	0.226	0.451	0.677	0.902	1.128	1.358	1.579	1.805	2.030
1	2.256	2.481	2.707	2.933	8.158	3.384	8.609	8.835	4.060	4.286
2	4.512	4.787	4.963	5.188	5.414	5.640	5.865	6.091	6.816	6.542
8	6.767	6.993	7.219	7.444	7.670	7.895	8.121	8.847	8.572	8.798
4	9.023	9.249	9.474	9.700	9.926	10.151	10.877	10.602	10.828	11.054
5	11.279	11.505	11.780	11.956	12.181	12.407	12.633	12.858	18.084	13.309
j							1	1		
6	18.585	13.761	18.98€	14.212	14.437	14.663	14.888	15.114	15.340	15.565
7	15.791	16.016	16.242	16.468	16.693	16.919	17.144	17.870	17.595	17.821
8	18.047	18.272	18.498	18.723	18.949	19.175	19.400	19.626	19.851	20.077
9	20.302	20.528	20.754	20.979	21.205	21.480	21.656	21.882	22.107	22.333
10	22.558	22.784	23.009	23.235	23.461	23.686	23.912	24.137	24.363	24.589
11	24.814	25.040	25.265	25.491	25.716	25.942	26.168	26.393	26.619	26.544
ľ	1	ł								
12	27.070	27.296	27.521	27.747	27.972	28.198	28.423	28.649	28.875	29.100
13	29.826	29.551	29.777	30.003	30.228	30.454	30.679	80.905	31.130	21.356
- 14	31.582	81.807	32.033	32.258	32.485	32.711	32.986	83.162	88.387	33.613
15	38.837	84.063	34.289	34.514	84.740	84.965	35.191	35.417	85.642	35.868
16	86.098	36.319	86.514	86.770	36.996	87.221	87.447	87.672	37.898	38.124
17	38.349	38.575	38.800	89.026	89.251	89.477	39.703	89.928	40.154	40.379
18	40.605	40.881	41.056	41.282	41.507	41.788	41.958	42.184	42.410	42.635

XIV. CONVERSION OF FRENCH OR PARIS LINES INTO ENGLISH INCHES. 1 Paris Line = 0.088814 English Inch.

Paris	Tenths of a Line.											
Lines.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.		
	Eng. In.	Eng In.	Eng. In.	Eng. In.	Eng. In	Bog. In.	Eng. In.	Eng. In.	Hng. In.	Rog. In		
0	0.0000	0.0089	0.0178	0.0266	0.0355	0.0444	0.0583	0.0622	0.0711	0.0799		
1	0.0888	0.0977	0.1066	0.1155	0.1243	0.1332	0.1421	0.1510	0.1599	0.1687		
2	0.1776	0.1865	0.1954	0.2043	0.2132	0.2220	0.2809	0.2398	0.2487	0.2576		
8	0.2664	0.2753	0.2842	0.2931	0.8020	0.8108	0.8197	0.8286	0.3375	0.346		
4	0.3553	0.3641	0.3730	0.8819	0.8908	0.8997	0.4085	0.4174	0.4263	0.4352		
5	0.4441	0.4580	0.4618	0.4707	0.4796	0.4885	0.4974	0.5062	0.5151	0.5240		
6	0.5829	0.5418	0.5506	0.5595	0.5684	0.5773	0.5862	0.5951	0.6039	0.6129		
.7	0.6217	0.6306	0.6395	0.6483	0.6572	0.6661	0.6750	0.6839	0.6927	0.701		
8	0.7105	0.7194	0.7283	0.7872	0.7460	0.7549	0.7638	0.7727	0.7816	0.790		
9	0.7993	0.8082	0.8171	0.8260	0.8349	0.8437	0.8526	0.8615	0.8704	0.879		
40	0.8881	0.8970	0.9059	0.9148	0.9237	0.9325	0.9414	0.9503	0.9592	0.968		
ā. 1	0.9770	0.9858	0.9947	1.0036	1.0125	1.0214	1.0302	1.0391	1.0480	1.056		
12	1.0658	1.0746	1.0835	1.0924	1.1013	1.1102	1.1191	1.1279	1.1368	1.145		
13	1.1546	1.1635	1.1723	1.1812	1.1901	1.1990	1.2079	1.2168	1.2256	1.234		
14	1.2434	1.2523	1.2612	1.2700	1.2789	1.2878	1.2967	1.3036	1.3144	1.328		
15	1.3322	1.3411	1.3500	1.8589	1.8677	1.3766	1.3855	1.3944	1.4033	1.412		
16	1.4210	1.4299	1.4388	1.4477	1.4565	1.4654	1.4743	1.4832	1.4921	1.5010		
17	1.5098	1.5187	1.5276	1.5865	1.5454	1.5542	1.5631	1.5720	1.5809	1.5898		
18	1.5987	1.6075	1.6164	1.6253	1.6342	1.6431	1.6519	1.6608	1.6697	1.678		

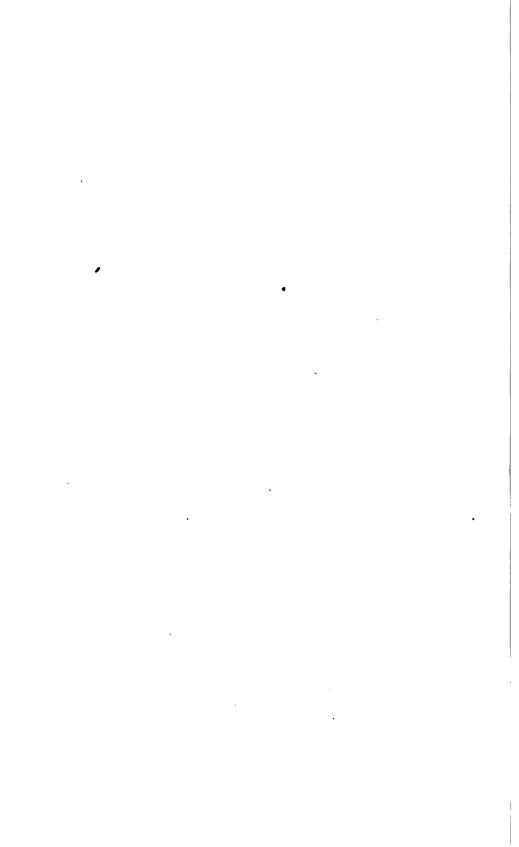
XV. CONVERSION OF RUSSIAN HALF-LINES INTO MILLIMETRES.

1 Russian Half-Line = 1.269977 Millimetres.

Rossian		Tenths.											
Half-Lines.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.			
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.			
0	0.000	0.127	0.254	0.361	0.508	0.635	0.762	0.889	1.016	1.143			
1	1.270	1.897	1.524	1.651	1.778	1.903	2.032	2.159	2.286	2.413			
2	2.540	2.667	2.794	2.921	3.048	8.175	8.302	8.429	8.556	3.688			
	3.810	8.937	4.064	4.191	4.818	4.445	4.572	4.699	4.826	4.953			
4	5.080	5.207	5.334	5.461	5.588	5.715	5.842	5.969	6.096	6.223			
5	6.350	6.477	6.604	6.731	6.858	6.985	7.112	7.239	7.866	7.493			
i	1												
6	7.620	7.747	7.874	8.001	8.128	8.255	8.382	8.509	8.636	8.768			
7	8.890	9.017	9.144	9.271	9.898	9.525	9.652	9.779	9,906	10.033			
8	10.160	10.287	10.414	10.541	10.668	10.795	10.922	11.049	11.176	11.303			
9	11.480	11-557	11.684	11.811	11.938	12.065	12.192	12.319	12.446	12.578			
10	12.700	12.827	12.954	13.081	13.208	18.335	18.462	13.589	13.716	18.843			
11	18.970	14.097	14.224	14.351	14.478	14.605	14.732	14.859	14.986	15.118			
12	15.240	15.367	15.494	15.621	15.748	15.875	16.002	16.129	16.256	16.383			
13	16.510	16.637	16.764	16.891	17.018	17.145	17.272	17.899	17.526	17.653			
14	17.780	17.907	18.084	18.161	18.288	18.415	18.542	18.669	18.796	18.923			
15	19.050	19.177	19.804	19.481	19.558	19.685	19.812	19.939	20.066	20.193			
16	20.320	20.447	20.574	20.701	20.828	20.955	21.082	21.209	21.336	21.468			
17	21.590	21.717	21.844	21.971	22.098	22.225	22.352	22.479	22.606	22.733			
18	22.860	22.987	28.114	28.241	23.868	28.495	23.622	28.749	23.876	24.003			

XVI. CONVERSION OF RUSSIAN HALF-LINES INTO PARIS LINES. 1 Russian Half-Line — 0.562976 Paris Line.

Russian	Tenths.											
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
	Par. line	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.			
0	0.000	0.056	0.113	0.169	0.225	0.281	0.338	0.894	0.450	0.507		
1	0.563	0.619	0.676	0.732	0.788	0.844	0.901	0.957	1.013	1.070		
2	1.126	1.182	1.289	1.295	1.851	1.407	1.464	1.520	1.576	1.683		
8	1.689	1.745	1.802	1.858	1.914	1.970	2.027	2.083	2.139	2.196		
4	2.252	2.308	2.864	2.421	2.477	2.533	2.590	2.646	2.702	2.759		
5	2.815	2.871	2.927	2.984	8.040	8.096	3.153	8.209	8.265	8.322		
6	3.378	8.484	8.490	3.547	8.608	8.659	8.716	3.772	3.829	3.885		
7	3.941	8.997	4.053	4.110	4.166	4.222	4.279	4.335	4.391	4.448		
8	4.504	4.560	4.616	4.673	4.729	4.785	4.842	4.898	4.954	5.010		
9	5.067	5.123	5.179	5.236	5.292	5.349	5.405	5.461	5.517	5.578		
10	5.630	5.686	5.742	5.799	5.855	5.911	5.968	6.024	6.080	6.136		
11	6.193	6.249	6.305	6.862	6.418	6.474	6.581	6.587	6.648	6.699		
12	6.756	6.812	6.868	6.925	6.981	7.037	7.093	7.150	7.206	7.262		
18	7.319	7.875	7.481	7.488	7.544	7.600	7.656	7.713	7.769	7.825		
14	7.882	7.938	7.994	8.051	8.107	8.163	8.219	8,276	8.332	8.388		
15	8.445	8.501	8.557	8.614	8.670	8.726	8.782	8.839	8.895	8.951		
16	9.008	9.064	9.120	9.177	9.233	9.289	9.345	9.402	9.458	9.514		
17	9.571	9.627	9.683	9.739	9.796	9.852	9.908	9.965	10.021	10.077		
18	10.184	10.190	10.246	10.302	10.859	10.415		10.528	10.584	10.640		



TABLES

FOR

REDUCING BAROMETRICAL OBSERVATIONS,

TAKEN AT ANY TEMPERATURE,

TO THE TEMPERATURE OF THE FREEZING POINT.

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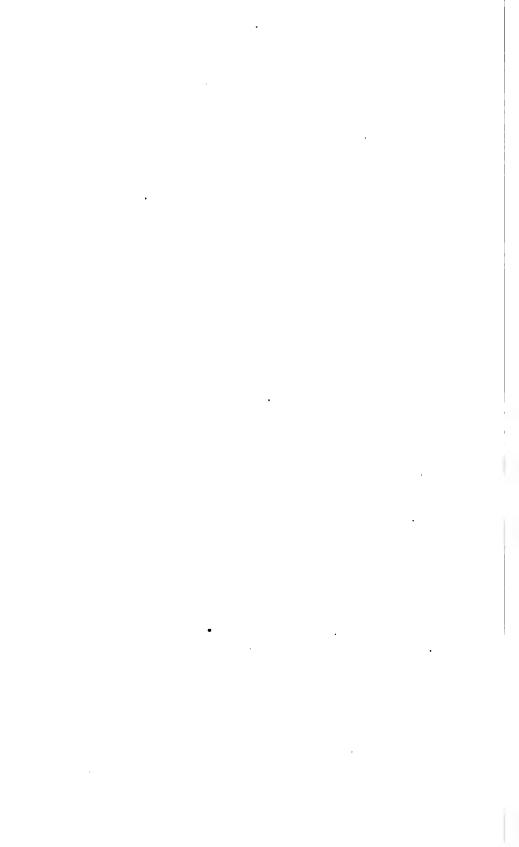
TABLES

FOR

REDUCING BAROMETRICAL OBSERVATIONS,

TAKEN AT ANY TEMPERATURE,

TO THE TEMPERATURE OF THE FREEZING POINT.



TABLES

FOR

REDUCING THE BAROMETRICAL OBSERVATIONS TAKEN AT ANY TEMPERATURE TO THE TEMPERATURE OF THE FREEZING POINT.

THE variations of the mercurial column in a stationary barometer are due to two causes, the changes of atmospheric pressure and the variations of temperature of the mercury, which affect the length of the column by changing its density. The variations of atmospheric pressure, which alone the barometer is destined to ascertain, are therefore hidden, and their observation falsified by the expansion or contraction of the mercury due to changes of temperature. For, supposing that, while the atmospheric pressure remains the same, the temperature of the instrument becomes lower, the mercurial column will become shorter, and the barometer will appear to fall; if the pressure becomes less, but the temperature increases, the expansion of the mercury will tend to compensate the diminution of pressure, and the barometer may remain stationary, or even may rise, while it ought to be falling; in other cases the action of temperature will tend to increase the amount of the changes of the barometrical height. It is therefore evident that successive observations, with the same barometer, do not give directly the actual changes of atmospheric pressure, unless they have been taken exactly at the same temperature, a case which, in practice, seldom occurs. Likewise simultaneous observations, taken with various barometers, do not give directly the actual differences of the absolute pressure of the atmosphere above the instruments. To obtain the true barometrical heights, that is, the action of the atmospheric pressure alone, the influence of the temperature must first be eliminated from the observed heights. This is done by reducing, by means of the following Tables, the various barometrical columns to the length they would have at a given temperature, which is the same for all. For the sake of convenient comparison, the freezing point has been almost universally adopted as the standard temperature to which all observations are to be reduced.

CONSTRUCTION OF THE TABLES.

In all the following Tables the barometers are supposed to be furnished with brass scales, extending from the surface of the mercury in the cistern to the top of the mercurial column. The correction to be applied is therefore composed of two elements: the correction for the expansion of the mercury, and that for the expansion of the scale; both of which ought to be, and have been, taken into account.

Indeed, the correction for the expansion of mercury is not sufficient to reduce the readings to the height which the barometer would indicate, under the same pressure, at the temperature of the freezing point. For when the temperature rises the mercurial column expands; but then the scale also grows longer, and this will tend to lower the reading of the height. The correction for the expansion of the mercury

TABLES FOR REDUCING BAROMETRICAL OBSERVATIONS.

must thus be diminished by the amount of that of the scale, that is, by nearly $\frac{1}{10}$, this being the proportion between the expansion of brass and that of mercury.

It is also the expansion of the scale which causes an apparent anomaly in the Tables for the Reduction of the English and Old French Barometers. It can be seen, that, though the observations are to be reduced to the freezing point, or to 32° Fahrenheit and zero Reaumur, the Tables give still a correction for observations taken at that temperature. The reason of it is, that the normal length of the English and Old French standards has not been determined at the temperature of the freezing point, as is the case with the metre, but respectively at the temperatures of 62° Fahrenheit and 13° Reaumur. It is thus only at these temperatures that the scales graduated with these standards have their true length. Above and below, the inches of the scales are longer or shorter than the inches of the standards. At the freezing point, therefore, the correction for the expansion of the mercury is null, but that for the expansion of the scale is not. The scale being too short, the reading will be too high, and a subtractive correction must still be applied, which will be gradually compensated at lower temperatures by the now additive correction of the mercurial column. Thus the point of no correction will occur at 28°.5 Fahrenheit, instead of 32°, in the English Barometer, and at -1°.5 Reaumur, instead of zero, in the Old French.

Schumacher has calculated and published in his Collection of Tables, &c., and in his Jahrbuch for 1836, 1837, and 1838, extensive tables for the reduction of the English, Old French, and Metrical Barometers, using the following general formula:—

Let h =observed height.

" t = temperature of the attached thermometer.

" T = temperature to which the observed height is to be reduced.

" m = expansion, in volume, of mercury.

" l = linear expansion of brass.

" 3 = normal temperature of the standard scale.

The reduction to the freezing point will be given by the formula, -

$$h \cdot \frac{m(l-T)-l(l-5)}{1+m(l-T)}$$

The following tables, which may be found more convenient for ordinary use, have been calculated from the same formula. Table XVII., published in the Instructions of the Royal Society of London, is mostly abstracted from the table of Schumacher. It gives the reduction of the English Barometer, adopting the following values:—

Let h =observed height in English inches.

" t = temperature of attached thermometer in degrees of Fahrenheit.

" m = expansion, in volume, of mercury for one degree Fahrenheit = 0.0001001.

" l = linear expansion of brass for one degree Fahrenheit = 0.0000104344.

The normal temperature of standard being $= 62^{\circ}$.

The reduction to 32° Fahrenheit will be given then by the formula,

$$-h \cdot \frac{m(t-82)-l(t-62)}{1+m(t-82)}.$$

The elements for the other tables are found at the head of each.

XVII.

ENGLISH BAROMETER.

TABLE

GIVING THE CORRECTION TO BE APPLIED TO ENGLISH BAROMETERS,

WITH BRASS SCALES EXTENDING FROM THE CISTERN TO THE TOP OF THE MERCURIAL COLUMN, FOR REDUCING THE OBSERVATIONS TO THIRTY-TWO DEGREES FAHRENHEIT.



TABLE XVII.

The following Table, calculated after that of Schumacher, has been adopted by the Committee of Physics and Meteorology of the Royal Society of London. It gives immediately the correction for every degree of Fahrenheit, and for every half-inch from 20 up to 31 inches. The scale of the barometer is supposed to be of brass, extending from the cistern to the top of the mercurial column. The difference of expansion of brass and mercury is taken into account. The standard temperature of the yard being 62° Fahr., and not 32° Fahr., the difference of expansion of the scale and of the mercurial column carries the point of no correction down to 29° Fahr. Therefore, from 29° up the correction must be subtracted from, from 29° down it must be added to, the observed height.

Examples of Calculation.

Barometer, observed height, 30.231
Attached thermometer 82° Fahr.

See in the last page the column of 30 inches; go down as far as the horizontal line corresponding with 82° in the first vertical column, which contains the temperatures; you will find there the correction —.143. We have thus:—

Barometer, observed height,	•	•	•	•	•	3 0.231
Subtractive correction for 82°	Fahr	٠,	•	•	•	—0.143
Barometer at 32°	Fahr	٠,	•	•	•	30.088
Barometer, observed height,	•	•		. •	•	29.743
Attached thermometer 25° Fa	ahr.					
The column of 29.5 inches opposit	e to	25°	Fahr.	gives	an	
additive correction of,	•	•	•	•	•	+0.009
Barometer at 32°	Fahr	٠.,	•		•	29.752

It will be easy to apply also the correction for fractions of a degree Fahrenheit; for example: —

Barometer, observed height,	•	•	•	•	•	28.358
Attached thermometer 71.3						

In the column of 28.5 inches, we find that the difference between the correction for 71° and that for 72° is .003; dividing this difference proportionally to the fraction, we have for three tenths of a degree a correction of —.001, which added to —.108, the correction for 71°, makes a total correction of.

 correction or,	•	•	•	•	103
And hammeter at 32°	Pahr				98 940

Degrees of Fabrenheit.	+.051 .049 .048 .046 .044	+.053 .051 .049 .047 .045	+.054 .052 .050	91.5 +.055	22	99.5	98	98.5	Degrees of Fab- renheit.
1 2 8 4 5	.049 .048 .046 .044	.051 .049 .047 .045	.052 .050						/I l
9 8 4 5	.048 .046 .044 .042	.049 .047 .045	:050	.053	+.056	+-058	+.059	+.060	°
8 4 5	.046 .044 .042	.047 .045			.054	.056	.057	.058	1
5	.044 .042	.045		.051	.052	.054	.055	.056	2
5	.042		-048	.049	.050	.052	.053	.054	8
1 11		.043	.046 .044	.047 .045	.048 .046	.050 .048	.051 .049	.052 .050	5
6	+.040	+.042	+:042	+.044	+.044	+.046	+.047	+.048	6
7 8	.039	.040	.041	.042	.042	.044	.044	.046	7
9	.037 .035	.038 .036	.039 .037	.040 .038	.041	.041 .039	.042 .040	.043 .041	8
10	.033	.034	.085	.036	.037	.037	.038	.039	10
11	+.031	+.032	+.033	+.034	+.085	+.035	+.086	+.037	11
12	.030	.030	.031	.032	.033	.083	.034	.035	12
13 14	.028 .026	.029 .027	.029 .027	.030 .028	.031	.031 .029	.032	.033	18 14
15	.024	.027	.027	.026	.029	.029	.028	.029	15
16	+.022	+.023	+.024	+.024	+.025	+.025	+.026	+.026	16
17	.021	.021	.022	.022	.023	.023	.024	.024	17
18 19	.019	.019	.020	.020	.021	.021	.022	.022	18 19
20	.017 .015	.018 .016	.018 .016	.018 .016	.019 .017	.019	.018	.020 .018	20
21	+.014	+.014	+.014	+.015	+.015	+.015	+.015	+.016	21
22	.012	.012	.012	.018	.013	.013	.013	.014	22
28	.010	.010	.010	.011	.011	.011	.011	.012	23 24
24 25	.008 .006	.008 .007	.009 .007	.009 .007	.009	.009 .007	.009 .007	.010 .007	25
26	+.005	+.005	+.005	+.005	+.005	+.005	+.005	+.005	26
27	.003	.003	.003	.003	.003	.003	.003	.003	27
28	.001	.001	.001	.001	.001	.001	.001	.001	28
29 30	001 .003	001 .003	001 .003	001 .003	001 .008	001 .003	001 003	001 003	29 80
81	005	005	005	005	005	005	005	005	81
32	.006	.006	.007	.007	.007	.007	.007	.007	32
88	.008	.008	.008	.009	.009	.009	.009	.010	33
34 35	.010 .012	.010 .01 2	.010 .012	.011 .013	.011 .018	.011 .013	.011 .013	.012 .014	34 35
36	013	014	014	014	015	015	016	016	36
37	.015	.016	.016	.016	.017	.017	.018	.018	37
38	.017	.017	.018	-018	.019	.019	.020	.020	38
39 40	.019 .021	.019 .021	.020 .022	.020 .022	.021 .023	.021 .023	.022 .024	.022 .024	39 40
40	022	023	024	024	025	025	026	026	41
41 42	.024	.025	.025	.026	.027	.027	.028	.028	42
43	.026	.027	.027	.028	.029	.029	.030	.081	43
44 45	.028 .030	.029 .030	.029 .031	.030 .032	.031 .038	.031 .038	.032 .034	.033 .035	44 45
46	031	032	033	<i>⊢</i> .034	035	035	036	037	46
47	.033	.034	.035	.036	.036	.037	.038	.039	47
48	.035	.086	.037	.038	.038	.039	.040	.041	48
49 50	.037 .038	.038 .039	.039 .040	.040 .041	.040 .042	.041 .043	.042 .044	.043 .045	49 50

Degrees of Fuh-	English Inches.												
of Fuh- renheit.	90	20.5	91	91.5	99	22.5	98	93.5	Degrees of Fah- renheit.				
5î	040	041	042	043	044	045	046	047	ธ์เ				
52	.042	.043	.044	.045	.046	.047	.048	.049	52				
53	.044	.045	.046	.047	.048	.049	.050	.052	53				
54 55	.046 .047	.047 .049	.048 .050	.049 .051	.050 .052	.051 .053	.052 .055	.054 .056	54 55				
33	-0-27	.049	.050	-001	.052	.050	.000	.050	33				
56	049	050	052	053	054	055	057	058	56				
57 58	.051 .053	.052 .054	.054 .055	.055 .057	.056 .058	.057 .059	.059 .061	.060 .062	57 58				
59	.055	.056	.057	.057	.060	.059	.063	.064	59				
60	.056	.058	.059	.061	.062	.063	.065	.066	60				
.	-050	000	061	- 040	064	OCE	067	068	61				
61 62	058 .060	060 .061	.063	062 .064	.066	065 .067	.069	.070	62				
63	.062	.068	.065	.066	.068	.069	.071	.072	63				
64	.063	.065	.067	.068	.070	.071	.073	.075	64				
65	.065	.067	.068	.070	.072	.073	.075	.077	65				
66	067	069	070	072	074	075	077	079	66				
67	.069	.071	.072	.074	.076	.077	.079	.081	67				
68	.071	.072	.074	.076	.078	.079	.081	.083	68				
69	.072	.074	.076	.078	.080	.081	.083	.085	69				
70	.074	-076	.078	.080	.082	.083	.085	.087	70				
71	076	078	080	082	083	085	087	089	71				
72	.078	.080	.082	.084	.085	.087	.089	.091	72				
73	.079	.081	.083	.085	.087	.089	.091	.093	78				
74 75	.081 .083	.083 .085	.085 .087	.087 .089	.089 .091	.091 .093	.093 .095	.095 .098	74 75				
							1000						
76	085	087	089	091	098	095	097	100	76				
77	.087	.089	.091	.093	.095	.097	.100	.102	77				
78	.088	.091	.093 .095	.095	.097	.099	.102	.104	78 79				
79 80	.090 .092	.092 .094	.095	.097 .099	.099 .101	.101 .103	. 104	.106 .108	80				
81	094	098	098	101 .103	103 .105	105 .107	108	110	81 82				
82 83	.095 .097	.098 .100	.100 .102	.103	.105	.107	.110 .112	.112 .114	83				
84	.099	.101	.104	.106	.109	.111	.114	.116	84				
85	.101	.103	.106	.108	.111	.118	116	.118	85				
86	103	105	108	110	<i></i> 113	115	118	120	86				
87	.104	103	.109	.112	.115	.117	.120	.128	87				
88	.106	.109	.111	.114	.117	.119	.122	.125	88				
89	.108	.111	.113	.116	.119	.121	.124	.127	89				
90	.110	.112	.115	.118	.121	.123	.126	.129	90				
91	111	-114	117	120	122	- .125	128	131	91				
92	.113	.116	.119	.122	.124	.127	.130	.133	92				
93	.115	.118	.121	.124	.126	.129	.132	.135	93				
94 95	.117 .118	.120 .121	.122 .124	.125 .127	.128 .130	.131 .133	.134 .136	.137 .139	94 95				
		****	******	****			.100	*108	-				
96	120	123	126	129	132	135	138	141	96				
97	.122	.125	.128	.131	.134	.137	.140	.143	97				
98 99	.124 .125	.127 .129	.130 .132	.133 .135	.136 .138	.189 .141	.142 .144	.145	98 99				
100	.127	130	.134	.137	140	.143	.146	.150	100				
(-			1	1		l	1	-30				

Domes			<u></u>	English	Inches.				Decree
Degrees of Fah- renheit.	94	94.5	95	25.5	26	96.5	27	97.5	Degrees of Fah- renheit.
°	+.061	+.063	+.064	+.065	+.067	+.068	+.069	+.071	°
1	.059	.061	.062	.063	.064	.065	-067	.068	1
2	.057	.058	.060	.061	-062	.063	.064	.066	2
3	.055	.056	.057	.059	.060	.061	.062	.063	3
4 5	.053 .051	.054 .052	.055 .058	.056 .054	.057 .055	.058 .056	.059 .057	.061 .058	5
6	+.049	+.050	+.051	+.052	+.053	+.054	+.055	+.056	6
7 8	.046	.047	.048	.049	.050	.051 .049	.052 .050	.053 .051	7 8
9	.044	.045	.046 .044	.047	.048 .046	.049	.047	.048	ŝ
10	.040	.041	.042	.042	.043	.044	.045	.046	10
11	+.038	+.039	+.039	+.040	+.041	+.042	+.042	+.043	11
12	.036	.036	.037	.038	.039	.039	.040	.041	12
18 14	.033 .031	.034	.035 .033	.036 .038	.086 .084	.037 .035	.038 .035	.038 .036	18 14
15	.029	.030	.030	.031	.032	.032	.083	.033	15
16	+.027	+.028	+.028	+.029	+.029	+.030	+.030	+.031	16
17	.025	.025	.026	.026	.027	.027	.028	.028	17
18 19	.023	.023	.024	.024	.025	.025 .023	.025 .023	.026	18 19
20	.021 .018	.021 .019	.021 .019	.020	.022 .020	.020	-021	.021	20
91	+.016	+.017	+.017	+.017	+.018	+.018	+.018	+.019	21
22	.014	.014	.015	.015	.015	.016	.016	.016	22
23 24	.012	.012	.012	.018	.013	.013 .011	.013 .011	.014	23 24
25	.010 .008	.010 .008	.010 .008	.010 .008	.011 .008	.008	.009	-009	25
26	+.005	+.006	+.006	+.006	+.006	+.006	+.006	+.006	26
27	.003	.008	.008	.003	.004	.004	.004	.004	27
28	.001	.001	.001	.001	.001	.001	.001	.001	28
29 30	001 .003	001 .008	001 .008	001 .004	001 .004	001 .004	001 .004	001 .004	29 80
81	005	006	006	006	006	006	006	006	81
82	.008	.008	.008	.008	.008	.008	.008	.009	82
83	.010	.010	.010	.010	.011	.011	.011	-011	83
84 35	.012 .014	.012 .014	.012 .015	.013 .015	.018 .015	.018 .015	.013 .016	.01 <u>4</u> .016	34 35
36	016	017	017	017	017	018	018	019	86
37	.018	.019	.019	.019	.020	.020	.021	.021	37
88	.020	.021	.021	.022	.022	.023	.023	.023	38
89 40	.028 .025	.023 .025	.024	.024 .026	.024	.025 .027	.025 .028	.026 .028	89 40
41 -	027	027	028	029	029	080	030	031	41
42	.029	.030	.030	.081	.081	.032	.033	.033	42
43	.031	.032	.032	.033	.034	.034	.035	.036	43
44 45	.033 .035	.034 .036	.035 .037	.035 .038	.036 .038	.037 .039	.037 .040	.038 .041	44 45
46	⊸.038	038	039	040	041	042	042	043	46
47	.040	.041	.041	.042	.048	.044	.045	.046	47
48	.042	.043	.044	.045	.045	.046	.047	.048	48
49 50	.044	.045	.046 .048	.047	.048	.049 .051	.050 .052	.050 .053	49 50
30	.040	1 .097	.040	1049	.000	1001	.032	.000	JI 30

				Moglish	Inches.				Degrass
Degrees of Pah- renheit.	94	94.5	95	95.5	96	96.5	97	97.5	of Fah- renheit.
51	048	049	050	051	052	053	054	055	5 <u>î</u>
52	.050	.052	.053	.054	.055	.056	.057	.058	52
53	.058	.054	.055	.056	.057	.058	.059	.060	53
54	.055	.056	.057	.058	.059	.060	.062	.063	54
55	.057	.058	.059	.060	.062	.068	.064	.065	55
56	059	060	061	063	064	065	066	068	56
57	.061	.062	.064	.065	.066	-068	.069	-070	57
58 59	.063 .065	.065	.066 .0 68	.067	.069 .071	.070	.071	.073 .075	58 59
60	.068	.069	.070	.072	.078	.072	.076	.077	60
61	070	071	078	074	075	077	078	080	61
62	.072	.078	.075	.076	.078	.079	.081	.082	62
63	.074	.076	.077	.079	.080	.082	.083	.085	63
64	. 076	.078	.079	.081	.082	.084	.086	.087	64
65	.078	.080	280.	.083	.085	.086	.088	.090	65
66	080	082	084	085	087	089	090	092	66
67	.083	.084	.086	.088	.089	.091	.098	.095	67
68	.085	.086	.088	.090	.092	.094	.095	.097	68
69	.087	.089	.090	.099	.094	.096	.098	.100	69
70	.089	.091	.098	.095	.096	.098	.100	.102	70
71	091	098	095	097	099	101	102	104	71
72	.093	.095	.097	.099	.101	.108	.105	.107	72
78	.095	.097	.099	.101	.103	.105	.107	.109	78
74	.097	.099	.102	.104	.106	.108	.110	.112	74
75	.100	.102	.104	.106	.108	.110	.112	.114	75
76	102	104	106	108	110	112	114	117	76
77	.104	.106	.108	.110	.112	.115	117	.119	77
78	.106	.108	.110	.118	.115	.117	.119	.122	78
79	.108	.110	.118	.115	.117	.119	.122	.124	79
80	.110	.118	.115	.117	.119	.122	.124	.126	80
81	112	115	117	119	122	124	126	129	81
82	.114	.117	.119	.122	.124	.126	.129	.181	89
83	.117	.119	.121	.124	.126	.129	.181	.134	83
84 85	.119 .121	.121 .123	.124 .126	.126 .128	.129 .181	.131 .1 38	.134 .186	.136 .139	84 85
	1	İ			1				
86	123	126	128	131	188	136	188	141	86
87 88	.125	.128	.130 .133	.133 .135	.186 .188	.138	.141	.143 .146	87 88
89	.127	.132	.135	.137	.140	.148	.146	.148	89
90	.131	.134	.137	.140	142	.145	1148	.151	90
91	134	136	139	142	145	148	150	153	91
92	.136	.139	.141	.144	.147	.150	.158	.156	92
98	.138	.141	.144	.147	.149	.152	.155	.158	93
94	.140	.143	.146	.149	.152	.155	.157	.161	94
95	.142	.145	.148	.151	.154	.157	.160	.163	95
96	144	147	150	158	156	159	162	165	96
97	.146	.149	.152	.156	.159	.162	.165	.168	97
98	.148	.152	.155	.158 .160	.161	.164	.167	.170 .178	98
99 100	.151 .153	.154 .156	.157 .159	.162	.168 .165	.166 .169	.172	.175	99 100
-50	-100	1					1		
					20				

Degrees of				English Inche	14.			Degrees of
Fahren- beit.	28	28.5	99	29.5	80	80.5	81	Fahren- heit.
ô	+.072	+.073	+.074	+.076	+.077	+.078	+.080	%
1	.069	.071	.072	.073	.074	.076	.077	1
2	.067	.068	.069	.070	.072	.073	.074	9
8	.064	.065	.067	.068	.069	.070	.071	8
4	.062	.063	.064	.065	.066	.067	-068	4
5	.059	.060	.061	.062	.063	.065	.066	5
6	+.057	+.058	+.059	+.060	+.061	+.062	+.068	6
7 8	.054	.055	.056	.057	.058	.059	.060 .057	7
9	.052 .049	.058 .050	.054 .051	.054	.055 .053	.056	.054	8
10	.047	.047	.048	.052	.050	.051	.052	10
11	+.044	+.045	+.046	+.046	+.047	+.048	+.049	11
12	.042	.042	.043	.044	.045	.045	.046	12
13	.039	.040	.040	.041	.042	.043	.043	13
14	.037	.037	.038	.038	.039	.040	.040	14
15	.034	.035	.035	.036	.036	.037	.038	15
16	+.032	+.032	+.033	+.038	+.034	+.034	+.035	16
17	.029	.030	.030	.031	.031	.032	.032	17
18 19	.026	.027	.027	.028	.028	.029	.029	18
20	.024 .021	.024	.025 .022	.025 .023	.026 .023	.026 .028	.027	19 20
	-021	.022		.020		~~~		
21	+.019	+.019	+.020	+.020	+.020	+.021	+.021	21
22 23	.016 .014	.017 .014	.017	.017 .015	.018	.018 .015	.018	22 23
24	.011	.012	.014	.012	.015	.019	.013	24
25	.009	.009	.009	.009	.009	2010	.010	25
26	+.006	+.006	+.007	+.007	+.007	+.007	+.007	26
27	.004	.004	.004	.004	.004	.004	.004	27
28	.001	.001	.001	.001	.001	.001	.001	28
29	001	001	001	001	001	001	001	29
30	.004	-004	.004	.004	.004	-004	.004	80
31	006	006	007	007	007	007	007	81
32	.009	.009	.009	.009	.009	.010	.010	32
83 34	.011	.019	.012	.019	.012	.012	.019	83
35	.014 .016	.014 .017	.014 .017	.015 .017	.015 .018	.015 .018	.018	84 85
36	019	019	020	020	020	021	021	86
37	.021	.022	.022	.022	.023	.023	.024	37
48	.024	.024	.025	.025	.026	.026	.026	38
39	.026	.027	.027	.028	.028	.029	.029	39
40	.029	.029	.030	.030	-031	.031	.032	40
41	031	032	033	033	034	034	035	41
42	.034	.034	.035	.036	.086	.037	.037	42
43	.036	.037	.038	.038	.039	.040	.040	43
44 45	.039 .041	.040 .042	.040 .048	.041	.042	.042 .045	.043 .046	44 45
46 47	044 .046	045	045	046	047	048	049	46 47
48	.049	.047	.048 .051	.049 .052	.050 .052	.051 .053	.051 .054	48
49	.051	.052	.051	.054	.052	.056	.057	49
50	.054	.055	.056	.057	.058	.059	.060	50

Dogress of				Ragiish Inche	t.			Degrees of Fahren-
Degrees of Fahren- heit.	28	28.5	29	99.5	30	80.5	81	Fahren- heit.
5ì	056	057	058	059	060	061	062	5ั่น
52	.059	.060	.061	.062	.068	.064	.065	52
53	.061	.063	.064	.065	.066	.067	.068	58
54 55	.064 .066	.065 .068	.066 .069	.067 .070	.068 .071	.070 .072	.071 .078	54 55
56	069	070	071	078	074	075	076	56
57	.071	.078	.074	.075	.076	.078	.079	57
58	.074	.075	.077	.078	.079	.081	.082	58
59 60	.076 .079	.078 .080	.079 .082	.080 .083	.082 .085	.083 .086	.085 .087	59 60
61	081	083	084	086	087	089	090	61
62	.084	.085	.087	.088	.090	.091	.098	62
63	.086	.088	.089	.091	.098	.094	.096	63
64	.089	.090	.092	.094	.095	.097	.098	64
65	.091	.098	.095	.096	.098	.100	.101	65
66	094	098	097	099	101	102	104	66
67	.096	.098	.100	.102	.103	.105	.107	67
68	.099	.101	.102	.104	.106	.108	.109	68
69	.101	.103	.105	.107	.109	.110	.112	69
70	.104	.106	.108	.109	.111	.118	.115	70
71	106	108	110	112	114	116	118	71
72	.109	.111	.113	.115	.117	.119	.120	72
78 74	.111 .114	.113 .116	.115 .118	.117 .120	.119 .122	.121	.123 .126	78 74
75	.116	.118	.120	.122	.125	.127	.129	75
76	119	121	128	125	127	129	- .181	76
77	.121	.123	.126	.128	.180	.132	.184	77
78	.124	.126	-128	.130	.138	.185	.187	78
79	.126	.128	.181	.133	.135	.137	.140	79
80	.129	.131	.188	.186	.138	.140	.143	80
81 82	181 .134	184	136	138	141	148	145	81 82
83	.134	.186 .139	.138 .141	.141 .148	.148 .146	.146 .148	.148 .151	83
84	.139	.141	.144	.146	.149	.151	.154	84
85	.141	.144	.146	.149	.151	.154	.156	85
86	144	146	149	151	154	156	159	86
87	.146	.149	.151	.154	.157	.159	.162	87
88	.149	.151	.154	.157	.159	.162	.165	88
89	.151	.154	.156	.159	.162	.165	.167	89
90	.153	.156	.159	.162	.164	.167	170م	90
91	156	159	162	165	167	170	-178	91
92 93	.158 .161	.161 .164	.164 .167	.167 .170	.170 .172	.172 .175	.175 .178	92 93
94	163	.166	.169	.172	.175	.177	.180	94
95	.166	.169	.172	.175	.178	.180	.183	95
96	168	171	174	178	181	- .183	186	96
97	.171	.174	.177	.180	.183	.186	.189	97
98	.173	.176	.179	.183	.186	.188	.191	98
99	.176	.179 .181	.182	.185	.188	.191	.194	99
100	.178		.184	.188	.191	.194	.197	100

TABLE XVIII.

FOR REDUCING THE INDICATIONS OF ENGLISH BAROMETERS, WITH WOODEN OR GLASS SCALES, TO THE FREEZING POINT.

In most of the common barometers the scale is engraved upon a short plate of brass, or of ivory, fixed upon the wooden frame of the instrument. In such a case, the compound expansion of the two substances can only be guessed at, and the correction to be applied to the observations for reducing them to the freezing point cannot be determined with precision. As a near approximation for such imperfect instruments, the following table may be used. In computing this table, the expansion of glass, which is less than that of brass and greater than that of wood, has been substituted for that of brass, as an approximate value for a scale composed of these last two substances. The table thus gives the true correction, in English inches, for the barometers, the graduation of which is engraved on the glass tube itself. It answers equally for any English barometer with wooden scale, whatever be the substance of which the short plate bearing the graduation is made.

CORRECTIONS TO BE APPLIED TO ENGLISH BAROMETERS, WITH WOODEN OR GLASS SCALES, TO REDUCE THE OBSERVATIONS TO THE FREEZING POINT.

Expansion of Mercury for 1° Fahr. = 0.0001001; of Glass for 1° Fahr. = 0.00000444.

Attached Thermom-		Barometer in English Inches.												
eter, Fahren- heit.	26	26.5	97	27.5	28	28.5	29	99.5	80	30.5	31			
ů	+.076	+.077	+.079	+.080	+.082	+.088	+.085	+.086	+.088	+.089	+.090			
1	+.073	+.075	+.076	+.078	+.079	+.080	+.082	+.063	+.085	+.086	+.068			
2	+.071	+.072	+.074	+.075	+.076	+.078	+.079	+.080	+.082	+.083	+.085			
8	+.068	+.070	+.071	+.072	+.074	+.075	+.076	+.078	+.079	+.060	+.082			
4	+.066	+.067	+.069	+.070	+.071	+.072	+.074	+.075	+.076	+.077	+.079			
5	+.064	+.065	+.066	+.067	+.068	+.070	+.071	+.072	+.073	+.074	+.076			
6	+.061	+.062	+.063	+.065	+.066	+.067	+.068	+.069	+.070	+.072	+.073			
7	+.059	+.060	+.061	+.062	+.068	+.064	+.065	+.067	+.068	+.069	+.070			
8	+.056	+.057	+.058	+.059	+.060	+.061	+.068	+.064	+.065	+.066	+.067			
9	+.054	+.055	+.056	+.057	+.058	+.059	+.060	+.061	+.062	+.063	+.064			
10	+.051	+.052	+.053	+.054	+.035	+.056	+.057	+.058	+.059	+.060	+.061			
11	+.049	+.050	+.051	+.051	+.052	+.058	+.054	+.055	+.056	+.057	+.058			
12	+.046	+.047	+.048	+.049	+.050	+.051	+.052	+.052	+.063	+.054	+.055			
13	+.044	+.045	+.045	+.046	+.047	+.048	+.049	+.050	+.050	+.051	+.052			
14	+.041	+.042	+.043	+.044	+.044	+.045	+.046	+.047	+.048	+.048	+.049			
13	+.089	+.089	+.040	+.041	+.042	+.042	+.043	+.044	+.045	+.045	+.046			
16	+.036	+.087	+.038	+.038	+.089	+.040	+.040	+.041	+.042	+.043	+.043			
17	+.034	+.034	+.035	+.036	+.036	+.037	+.038	+.038	+.039	+.010	+.040			
18	+.081	+.082	+.032	+.088	+.034	+.084	+.035	+.086	+.036	+.037	+.037			
19	+.029	+.029	+.030	+.080	+.031	+.082	+.032	+.033	+.088	+.034	+.034			
20	+.026	+.027	+.027	+.028	+.028	+.029	+.029	+.030	+.030	+.031	+.031			

Barometer with Glass or Wooden Scale.

Attached				Dare	meter in	Regish I	nches.				
Thermom- eter, Fahren- heit.	96	26.5	27	97.5	98	98.5	29	99.5	80	80.5	81
21	+.024	+.024	+.025	+.025	+.026	+.026	+.027	+.027	+.028	+.028	+.028
22	+.021	+.022	+.022	+.028	+.022	+.028	+.024	+.024	+.025	+.025	+.025
23	+.019	+.019	+.020	+.020	+.020	+.021	+.021	+.021	+.022	+.022	+.023
21	+.016	+.017 +.014	+.017 +.014	+.017 +.015	+.018	+.018	+.018	+.019	+.019 +.016	+.019	+.020
- 96	+.011	+.012	+ 010				+ 010	+ 030	+.018		+.014
~	+.009	+.009	+.012	+.012	+.012	+.018	+.018	+.018	+.018	+.018	+.014
27 28	+.006	+.007	+.007	+.007	+.007	+.007	+.007	+.007	+.007	+.008	+.008
29	+.004	+.004	+.004	+.004	+.004	+.004	+.004	+.005	+.005	+.005	+.005
30	+.002	+.002	+.002	+.002	+.002	+.002	+.002	+.002	+.002	+.002	+.002
31	001	001	001	001	001	001	001	001	001	001	001
82	008	004	004	004	004	004	004	004	004	004	004
83	006	006	006	006	006	007	007	007	007	007	007
84	008	009	009	009	009	009	009	010	010	010	010
85	011	011	011	012	012	Q1 2	012	012	C18	018	018
86	013	014	014	014	014	015	015	015	C15	016	016
87	016	016	017	017	017	017	018	018	018	019	019
88	018	019	019	019	020	020	020	021	021	022	022
89	021	021	022	022	022	028	028	024	084	024	025
40	023	024	024	025	025	026	026	026	027	027	028
41	026	026	027	027	028	028	029	029	080	030	031
42	028	029	029	~.030	030	081	032	082	083	088	084
43	031	081	032	033	088	034	033	085	086	086	037
44	033	034	035	-035	-:036	086	036	088	088	089	040
45	036	086	087	088	03 8	039	039	041	041	042	048
46	038	039	040	049	-041	042	~042	048	044	045	046
47	041	041	-042	043	~044	045	044	016	047	048	049
48	018	044	-045	-046	-047	-047	-017	049	050	-051	051
49	046	-046	047	048	~049	050	050	052	058	054	054
50	048	049	~050	⊸051	052	058	054	055	056	056	057
51	051	-052	053	054	~055	055	056	057	058	059	060
52	058	054	055	- .056	057	056	059	060	061	062	063
53	056	057	058	059	060	061	062	068	064	065	066
54	058	059	060	061	068	064	065	066	067	068	069
55	061	062	068	-064	065	066	068	069	070	071	072
56	068	064	065	067	068	~069	-070	071	078	074	075
57	065	067	-068	069	071	072	078	074	076	077	078
58	068	069	071	072	078	-074	076	_077	078	080	081
59	070	072	078	074	076	-077	~079	080	081	083	084
60	078	074	076	077	079	⊸080	~081	⊸088	084	085	087

Barometer with Glass or Wooden Scale.

Attached Thermom- eter,		·		Baro	meter in 1	English Ir	oches.				
Fahren- heit.	26	96.5	97	97.5	28	98.5	29	29.5	80	80.5	81
61	075	077	078	080	081	083	084	086	087	088	090
62	078	079	081	082	084	085	087	088	090	091	098
68	080	082	068	085	086	068	090	091	098	094	096
64	083	084	086	088	089	091	092	094	096	097	099
65	085	087	069	090	092	098	095	097	098	100	102
66	088	089	091	093	094	096	098	100	101	108	104
67	090	092	094	095	097	099	101	102	104	106	108
68	098	094	096	098	100	102	108	105	107	109	110
69	095	097	099	101	102	104	106	108	110	112	113
70	098	0 9 9	101	108	105	107	109	111	118	114	116
71	100	102	104	106	108	110	112	114	115	117	-119
72	103	105	106	108	110	112	114	116	118	120	122
78	105	107	109	111	118	115	117	119	121	123	125
74	107	110	112	114	116	118	120	122	124	126	128
75	110	112	114	116	118	121	128	125	127	129	181
76	112	115	117	119	121	128	125	128	180	132	184
77	115	117	119	121	124	126	128	180	188	185	137
78	117	120	122	124	126	129	181	188	135	138	140
79	120	122	124	127	129	181	134	136	138	141	143
80	12 2	125	127	129	182	184	186	139	141	148	146
81	125	127	180	182	134	187	189	142	144	146	149
82	127	130	132	135	137	139	142	144	147	149	152
83	130	182	135	137	140	142	145	147	150	152	155
84	182	135	187	140	142	145	147	150	152	155	158
85	185	187	140	142	145	147	150	158	155	158	160
86	187	140	142	145	148	150	158	155	158	161	163
87	189	142	145	148	150	15 8	156	158	161	164	166
88	142	145	147	150	158	156	158	161	164	167	169
89	144	147	150	158	156	158	161	164	167	169	172
90	147	150	158	155	158	161	164	167	169	172	175
91	149	152	155	158	161	164	167	169	172	175	178
92	152	155	158	161	163	166	169	172	175	178	181
93	154	157	160	163	166	169	172		178	181	184
94	157	160	163	166	169	172	•	178	1	184	1
95	159	162	165	168	171	174	178	181	184	187	190
96	162	165	168	171	174	177	180	188	186	190	193
97	164	167	170	174	177	180	188	186	189	192	196
98	167	170	178	176	179	188	186	189	192	195	199
99	169	172	175	179	182	185	188	192	195	198	201
100	171		1	181	185	188	ı	194	198	201	204

XIX.

METRICAL BAROMETER.

TABLE

FOR

REDUCING TO THE FREEZING POINT THE BAROMETRICAL COLUMN,

MEASURED BY BRASS SCALES, EXTENDING FROM THE CISTERN TO
THE TOP; CALCULATED FROM 260 TO 865 MILLIMETRES,
AND FOR EACH DEGREE CENTIGRADE.
By M. T. Delcros.

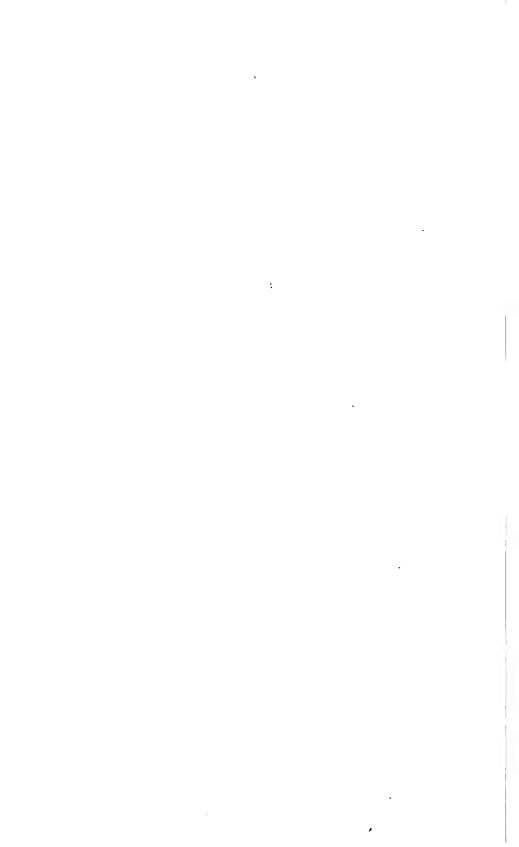


TABLE XIX.

This table has been calculated by using the following coefficients of dilatation: —
Brass, linear dilatation, from Laplace and Lavoisier for 100° C. = 0.0018782.

Mercury, dilatation in volume, from Dulong and Petit for 100° C. = 0.0180180.

Dilatation of the mercurial column for 100° C. . . . = 0.0161398.

Dilatation of the mercurial column for 1° C. . . . = 0.0001614.

Observed height reduced to freezing point,

$$H = h - h \ (0.0001614). \quad T = h - h \ (\frac{T}{6100}).$$

The second term of this last formula is given by the table, when the temperature T and the height h of the barometer are known; this correction must be *subtracted* from the observed height h, when the temperature is above freezing point; it is to be added when the temperature is below zero, or freezing point.

This table allows the barometrical heights taken at the highest summits, and in the deepest mines, to be corrected.

Examples of Calculation.

Barometer, observed height,

567.49

Height				TEMPERA	TURE CE!	NTIGRADE.			
of the Barome- ter.	1°	90	8°	40	5°	•	7°	80	90
Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
260	0.042	0.084	0.126	0.168	0.210	0.252	0.294	0.336	0.378
265	0.048	0.086	0.128	0.171	0.214	0.257	0.299	0.342	0.385
270	0.044	0.087	0.181	0.174 0.178	0.218	0.261 0.266	0.305 0.311	0.349	0.392
275 260	0.044	0.089	0.138 0.136	0.178	0.222	0.200	0.311	0.362	0.407
285	0.046 0.047	0.092	0.188	0.184	0.280	0.276	0.322	0.868	0.414
290 295	0.047	0.094	0.140 0.148	0.187	0.284	0.281 0.286	0.828	0.874	0.421
800	0.048	0.097	0.145	0.194	0.242	0.291	0.889	0.387	0.436
805	0.049	0.098	0.148	0.197	0.246	0.295	0.845	0.394	0.448
	0.070	0.700	0.770	0.000	0.000	0.000	0.620	0.400	0
810	0.050	0.100	0.150	0.200	0.250	0.800	0.850	0.400	0.450
315 320	0.051	0.102	0.152 0.155	0.208	0.254 0.258	0.805 0.810	0.356	0.407	0.465
825	0.052	0.105	0.157	0.210	0.262	0.315	0.367	0.420	0.472
830	0.053	0.106	0.160	0.213	0.266	0.820	0.374	0.426	0.479
	5.555		0.000			,5			
885	0.054	0.108	0.162	0.216	0.270	0.324	0.379	0.432	0.487
840	0.055	0.110	0.165	0.219	0.274	0.829	0.384	0.439	0.494
845	0.056	0.111	0.167	0.223	0.278	0.884	0.390	0.445	0.501
850	0.056	0.118	0.169	0.226	0.282	0.839	0.395	0.452	0.508
355	0.057	0.115	0.172	0.229	0.286	0.844	0.401	0.458	0.516
860	0.058	0.116	0.174	0.282	0.290	0.349	0.407	0.465	0.523
865	0.059	0.118	0.177	0.286	0.294	0.353	0.412	0.471	0.530
870	0.060	0.119	0.179	0.239	0.299	0.358	0.418	0.478	0.537
375	0.060	0.121	0.182	0.242	0.803	0.868	0.424	0.484	0.545
880	0.061	0.123	0.184	0.245	0.307	0.368	0.429	0.491	0.552
885	0.062	0.124	0.186	0.249	0.811	0.878	0.435	0.497	0.559
890	0.063	0.126	0.189	0.252	0.815	0.378	0.441	0.504	0.566
395	0.064	0.127	0.191	0.255	0.819	0.882	0.446	0.510	0.574
400	0.065	0.129	0.194	0.258	0.828	0.887	0.452	0.516	0.581
405	0.065	0.181	0.196	0.261	0.827	0.392	0.457	0.523	0.588
410	0.066	0.132	0.198	0.265	0.831	0.897	0.468	0.529	0.596
415	0.067	0.134	0.201	0.268	0.885	0.402	0.469	0.586	0.603
420	0.068	0.136	0.203	0.271	0.889	0.407	0.474	0.542	0.610
425	0.068	0.187	0.206	0.274	0.848	0.411	0.480	0.549	0.617
480	0.069	0.189	0.208	0.278	0.847	0.416	0.486	0.555	0.625
435	0.070	0.140	0.211	0.281	0.851	0.421	0.491	0.562	0.632
440	0.071	0.142	0.218	0.284	0.855	0.426	0.497	0.568	0.639
445	0.072	0.144	0.215	0.287	0.359	0.431	0.508	0.574	0.646
450	0.073	0.145	0.218	0.290	0.363	0.436	0.508	0.581	0.654
455	0.078	0 147	0.220	0.294	0.867	0.441	0.514	0.587	0.661
	10	200	' 3 °	4 °	5 °	6,	70	80	9°

Height of the	TEMPERATURE CENTIGRADE.									
Barome- tet.	10	90	80	40	50	•	7°	80	90	
Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim. 0.520	Millim.	Million.	
460	0.0742	0.1485	0.2227	0.2970	0.871	0.445		0.594	0.668	
465	0.0750	0.1501	0.2251	0.8002	0.875	0.450	0.525	0.600	0.688	
470	0.0759	0.1517	0.2276	0.3084	0.879	0.480	0.581	0.618	0.690	
475	0.0767	0.1583	0.2824	0.8099	0.887	0.465	0.542	0.620	0.697	
480	0.0775	0.1049	0.2024	0-0088	0.001	0.400	0.042	0.020	0.007	
485	0.0783	0.1565	0.2348	0.8181	0.891	0.470	0.548	0.626	0.704	
490	0.0791	0.1582	0.2878	0.8168	0.395	0.474	0.554	0.688	0.712	
495	0.0800	0.1598	0.2397	0.8195	0.399	0.479	0.559	0.689	0.719	
500	0.0807	0.1614	0.2421	0.8228	0.408	0.484	0.565	0.646	0.726	
505 ·	0.0615	0.1680	0.2445	0.3260	0.407	0.489	0.570	0.652	0.784	
£10	0.0823	0.1646	0.2469	0.8298	0.412	0.494	0.576	0.658	0.741	
510	0.0628	0.1646	0.2498	0.8225	0.412	0.499	0.582	0.665	0.748	
515 520	0.0889	0.1679	0.2518	0.3357	0.420	0.504	0.587	0.671	0.755	
	0.0847	0.1695	0.2542	0.8889	0.424	0.508	0.598	0.678	0.763	
525 530	0.0855	0.1711	0.2566	0.8422	0.428	0.518	0.599	0.684	0.770	
350	0.0000	"	0.2000	•••	0.220	0.020	3.333			
585	0.0863	0.1727	0.2590	0.8454	0.482	0.518	0.604	0.691	0.777	
540	0.0872	0.1748	0.2615	0.8486	0.486	0.528	0.610	0.697	0.784	
545	0.0879	0.1759	0.2639	0.8518	0.440	0.528	0.616	0.704	0.792	
550	0.0888	0.1775	0.2668	0.8551	0.444	0.588	0.621	0.710	0.799	
555	0.0896	0.1791	0.2687	0.8588	0.448	0.537	0.627	0.717	0.806	
				A	0.450	0.740	A 600	0.723	0.818	
560	0-0904	0.1808	0.2712	0.8615	0.452	0.542	0.688	0.728	0.818	
565	0.0912	0.1824	0.2786	0.8647	0.466	0.547 0.552	0.644	0.786	0.828	
570	0-0920	0.1840	0.2760	0.3680	0.464	0.557	0.650	0.743	0.885	
575	0.0928	0.1856	0.2784	0.8712	0.468	0.562	0.655	0.749	0.842	
580	0.0936	0.1872	0.2000	0.0744	0.200	0.002	0.000	0.740	0.012	
585	0.0944	0.1888	0.2888	0.8777	0.472	0.566	0.661	0.755	0.850	
590	0.0952	0.1904	0.2857	0.8809	0.476	0.571	0.667	0.762	0.857	
595	0-0960	0.1921	0.2881	0.8841	0.480	0.576	0.672	0.768	0.864	
600	0.0968	0.1987	0.2905	0.3874	0.484	0.581	0.678	0.775	0.872	
605	0.0976	0.1958	0.2929	0.8906	0.488	0.586	0.682	0.781	0.879	
				0.000	0.400	0.501	0.000	0.788	0.886	
610	0.0965	0.1969	0.2954	0.8988	0.492	0.591 0.595	0.689	0.788	0.898	
615	0.0998	0.1985	0.2978	0.8970	0.496	0.600	0.700	0.794	0.993	
620	0.1001	0.2001	0.8002		0.504	0.605	0.706	0.807	0.908	
625	0.1009	0.2017	0.8026	0.4085	0.504	0.610	0.708	0.813	0.915	
630	0.1017	0.2084	0.000	0.4007	V00	0.010	V.115	0.010		
685	0.1025	0.2050	0.3074	0.4099	0.512	0.615	0.717	0.820	0.922	
640	0.1033	0.2066	0.3099	0.4132	0.516	0.620	0.728	0.826	0.980	
645	0.1041	0.2082	0.3128	0.4164	0.520	0.625	0.729	0.838	0.937	
650	0.1049	0.2098	0.8147	0.4196	0.524	0.629	0.784	0.889	0.944	
655	0.1057	0.2114	0.8172	0.4229	0.529	0.684	0.740	0.846	0.951	
660	0.1065	0.2130	0.3196	0.4261	0.533	0.639	0.746	0.852	0.959	
	1°	200	80	4 °	5°	€	70	80	9 °	

Walshe	TEMPERATURE CENTIGRADE									
Height of the Barome- ter.	10	9°	80	4 º	5°	60	70	8°	90	
Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	
665	0.1078	0.2146	0.8220	0.4293	0.537	0.644	0.751	0.859	0.966	
670	0.1081	0.2163	0.8244	0.4326	0.541	0.649	0.757	0.865	0.973	
675	0.1089	0.2179	0.3268	0.4358	0.545	0.654	0.763	0.871	0.980	
680	0.1097	0.2195	0.3292	0.4390	0.549	0.658	0.768	0.878	0.988	
685	0.1106	0.2211	0.3817	0.4428	0.558	0.668	0.774	0.884	0.995	
690	0.1114	0.2227	0.8341	0.4455	0.557	0.668	0.780	0.891	1.002	
695	0.1122	0.2288	0.8365	0.4487	0.561	0.673	0.785	0.897	1.010	
700	0.1180	0.2260	0.3389	0.4520	0.565	0.678	0.791	0.904	1.017	
705	0.1138	0.2276	0.3414	0.4552	0.569	0.683	0.797	0.910	1.024	
710	0.1146	0.2292	0.3438	0.4584	0.578	0.688	0.802	0.917	1.031	
715	0.1154	0.2808	0.3462	0.4616	0.577	0.691	0.808	0.928	1.039	
720	0.1162	0.2324	0.3486	0.4648	0.581	0.697	0.813	0.930	1.046	
725	0.1170	0.2340	0.3510	0.4680	0.585	0.702	0.819	0.986	1.053	
730	0.1178	0.2356	0.3535	0.4718	0.589	0.707	0.825	0.948	1.060	
785	0.1186	0.2372	0.3559	0.4745	0.598	0.712	0.880	0.949	1.068	
740	0.1104	0.2389	0.3588	0.4777	0.597	0.717	0.886	0.955	1.075	
745	0.1202	0.2405	0.8607	0.4809	0.601	0.721	0.842	0.962	1.082	
750	0.1210	0.2421	0.3631	0.4842	0.605	0.726	0.847	0.968	1.089	
755	0.1218	0.2437	0.8655	0.4874	0.609	0.781	0.858	0.975	1.097	
760	0.1227	0.2453	0.3680	0.4906	0.618	0.786	0.859	0.981	1.104	
765	0.1285	0.2469	0.3704	0.4989	0.617	0.741	0.864	0.988	1.111	
770	0.1243	0.2486	0.3729	0.4971	0.621	0.746	0.870	0.994	1.118	
775	0.1251	0.2502	0.8752	0.5003	0.625	0.750	0.876	1.001	1.126	
780	0.1251	0.2518	0.3777	0.5086	0.629	0.755	0.881	1.007	1.133	
785	0.1267	0.2534	0.3801	0.5068	0.688	0.760	0.888	1.014	1.140	
	A 10mm	0.2550	0.0004	0 5100	0.000	A =0=	0.000	* ***		
790	0.1275		0.3825	0.5100	0.687	0.765	0.898	1.020	1.148	
795 800	0.1288	0.2566 0.2582	0.8849 0.8874	0.5132 0.5165	0.641	0.770 0.775	0.898	1.026	1.155	
805	0.1291	0.2598	0.8874	0.5197	0.646	0.775	0.904	1.088	1.162 1.169	
810	0.1299	0.2615	0.3922	0.5197	0.654	0.784	0.905	1.046	1.177	
		0.000								
815	0.1315	0.2621	0.8946	0.5262	0.658	0.789	0.921	1.052	1.184	
820	0.1323	0.2647	0.8970	0.5294	0.662	0.794	0.926	1.059	1.191	
825	0.1331	0.2658	0.8994	0.5326	0.666	0.799	0.932	1.065	1.198	
830 833	0.1340	0.2679 0.2695	0.4019 0.4043	0.5358 0.5891	0.670 0.674	0.804	0.938	1.072	1.206 1.213	
		,								
840	0.1356	0.2712	0.4067	0.5428	0.678	0.818	0.949	1.085	1.220	
845	0.1864	0.2728	0.4091	0.5455	0.682	0.818	0.935	1.091	1.227	
850	0.1372	0.2744	0.4116	0.5488	0.686	0.828	0.960	1.097	1.235	
855 860	0.1380 0.1388	0.2760 0.2776	0.4140 0.4164	0.5520 0.5552	0.690 0.694	0.828 0.833	0.966 0.972	1.104 1.110	1.242 1.249	
865	0.1396	0.2792	0.4188	0.5584	0.698	0.838	0.977	1.117	1.256	
000										
1	1°	20	8°	4 º	5°	€°	7°	80	9>	

$\mathbf{X}\mathbf{X}$.

METRICAL BAROMETER.

TABLE

POR

REDUCING TO THE FREEZING POINT THE BAROMETRICAL COLUMN,

MEASURED BY BRASS SCALES, EXTENDING FROM THE CISTERN TO THE TOP; CAL-CULATED FOR THE HEIGHTS BETWEEN 605 AND 800 MILLIMETRES, AND FOR EVERY TENTH OF A DEGREE, FROM 0° TO + AND --- 85° CENTIGEADE. By M. T. Haeghens.



TABLE XX.

This table has been calculated by using the same coefficients of dilatation as in the preceding table, viz.:—

Brass, linear dilatation, from Laplace and Lavoisier for 100°C. = 0.0018782.

Mercury, dilatation in volume, from Dulong and Petit for 100°C. = 0.0180180.

Dilatation of the mercurial column for 100°C. . . . = 0.0161398.

Dilatation of the mercurial column for 1°C. . . . = 0.0001614.

This table, calculated for the reduction of long series of meteorological observations, gives immediately the value of the correction for each tenth of a degree up to 35° C. above, and down to 35° C. below, the freezing point, and for mercurial columns extending from 605 to 800 millimetres.

Examples of Calculation.

For finding the correction, seek in the horizontal column, headed barometer, at the head of the pages, the corresponding height of the barometer; it will be found, p. 31, barometer 755^{am} (from 752.50 to 757.50); next seek in the first vertical column, containing the temperatures, 17°, follow then horizontally this line as far as the column of 8 tenths, and you find there 2.17 millimetres, which is the correction, or the quantity to be subtracted for reducing the observed height to zero. We have thus:—

	В	arom	eter a	t zero	,	752.00
Subtractive correction	for +1'	7°.8 =	= .	•	•	— 2.17
Observed height,	•	•	•	•		75 4 .17

If the temperature is below zero, the correction will be additive.

Observed height,	•	•	•		•	•	729.72
Temperature of the	atta	ched t	herm	omete	r, —	3°.4.	
Additive correction		•	•	•	•	•	+0.99
		В	arom	eter a	t zero		730.71

		В	AROME	ETER:	605 ^{mm} .	(from	602.51	to 607 .5	0).	
Centi- grade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.08	Millim. 0.04	Millim, 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millin, 0.09
1 2	0.10 0.20	0.11 0.21	0.12 0.21	0.18 0.22	0.14 0.23	0.15 0.24	0.16 0.25	0.17 0.26	0.18 0.27	0.19 0.28
8	0.29	0.80	0.31	0.32	0.28	0.84	0.85	0.36	0.87	0.38
4	0.39	0.40	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48
5	0.49	0.50	0.51	0.52	0.58	0.54	0.55	0.56	0.57	0.58
6	0.59	0.60	0.61	0.62	0.68	0.68	0.64	0.65	0.66	0.67
7	0.68	0.69	0.70	0.71	0.72	0.78	0.74	0.75	0.76	0.77
8	0.78	0.79	0.80	0.81	0.82	0.88	0.84	0.85	0.86	0.87
9 10	0.88 0.98	0.89	0.90 1.00	0.91 1.01	0.92 1.02	0.93 1.03	0.94 1.04	0.95 1.06	0.96 1.05	0.97 1.06
11	1.07	1.08	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.16
12	1.17	1.18	1.19	1.20	1.21	1.22	1.28	1.24	1.25	1.26
13	1.27	1.28	1.29	1.20	1.81	1.82	1.88	1.84	1.35	1.86
14	1.37	1.38	1.39	1.40	1.41	1.42	1.48	1.44	1.45	1.46
15	1.46	1.47	1.48	1.49	1.50	1.51	1.52	1.53	1.54	1.55
16	1.56	1.57	1.58	1.59	1.60	1.61	1.62	1.68	1.64	1.65
17	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.78	1.74	1.75
18	1.76	1.77	1.78	1.79	1.80	1.81	1.82	1.83	1.84	1.85
19	1.86	1.87	1.87	1.88	1.89	1.90	1.91	1.92	1.93	1.94
20	1.95	1.96	1.97	1.98	1.99	2.00	2.01	2.02	2.08	2.04
21	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.12	2.13	2.14
22	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.22	2.23	2.24
28	2.25	2.26	2.27	2.28	2.29	2.29	2.80	2.31	2.82	2.83
24 25	2.84 2.44	2.35 2.45	2.86 2.46	2.87 2.47	2.38 2.48	2.89 2.49	2.40 2.50	2.41 2.51	2.42 2.52	2.48 2.53
26	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.68
27	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.71	2.71	2.72
28	2.73	2.74	2.75	2.76	2.77	2.78	2.79	2.80	2.81	2.82
29	2.83	2.84	2.85	2.86	2.87	2.88	2.89	2.90	2.91	2.92
80	2.98	2.94	2.95	2.96	2.97	2.98	2.99	8.00	8.01	3.02
81	3.03	8.04	8.05	8.06	3.07	8.08	8.09	8.10	8.11	3.12
82	3.12	3.18	8.14	8.15	3.16	8.17	8.18	8.19	8.20	8.21
88	8.22	8.23	8.24	8.25	3.26	3.27	8.28	8.29	8.80	8.31
84 85	3.82 3.42	3.33 3.43	8.84 8.44	3.85 3.45	8.36 8.46	3.37 3.47	3.48	8.89 3.49	8.40 8.50	3.41 8.51
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

		В	AROMI	ETER:	610 ^{mm} .	(from	607.51	o 612.5	0).	
Centi- grade Degrees.				· · · · · · · · · · · · · · · · · · ·	Tenthe o	f Degrees.				
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millím. 0.02	Millim. 0.08	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.09
1	0.10	0.11	0.12	0.18	0.14	0.15	0.16	0.17	0.18	0.19
2	0.20	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29
3	0.80	0.81	0.82	0.82	0.88	0.34	0.35	0.86	0.37	0.88
4	0.39	0.40	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48
5	0.49	0.50	0.51	0.52	0.58	0.54	0.55	0.56	0.57	0.58
6	0.59	0.60	0.61	0.62	0.63	0.64	0.65	0.66	0.67	0.68
7	0.69	0.70	0.71	0.72	0.78	0.74	0.75	0.76	0.77	0.78
8	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88
9	0.89	0.90	0.91	0.92	0.98	0.94	0.95	0.96	0.96	0.97
10	0.98	0.99	1.00	1.01	1.02	1.08	1.04	1.05	1.06	1.07
11	1.08	1.09	1.10	1.11	1.12	1.18	1.14	1.15	1.16	1.17
12	1.18	1.19	1.20	1.21	1.22	1.28	1.24	1.25	1.26	1.27
13	1.28	1.29	1.30	1.81	1.82	1.33	1.84	1.85	1.86	1.37
14	1.38	1.39	1.40	1.41	1.42	1.48	1.44	1.45	1.46	1.47
15	1.48	1.49	1.50	1.51	1.52	1.58	1.54	1.55	1.56	1.57
16	1.58	1.59	1.59	1.60	1.61	1.62	1.68	1.64	1.65	1.66
17	1.67	1.68	1.69	1.70	1.71	1.72	1.78	1.74	1.75	1.76
18	1.77	1.78	1.79	1.80	1.81	1.82	1.88	1.84	1.85	1.86
19	1.87	1.88	1.89	1.90	1.91	1.92	1.93	1.94	1.95	1.96
20	1.97	1.98	1.99	2.00	2.01	2.02	2.08	2.04	2.05	2.06
21	2.07	2.08	2.09	2.10	2.11	2.12	2.18	2.14	2.15	2.16
22	2.17	2.18	2.19	2.20	2.21	2.22	2.23	2.23	2.24	2.25
23	2.26	2.27	2.28	2.29	2.30	2.31	2.32	2.33	2.84	2.35
24	2.86	2.37	2.38	2.39	2.40	2.41	2.42	2.48	2.44	2.45
25	2.46	2.47	2.48	2.49	2.50	2.51	2.52	2.58	2.54	2.55
26	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65
27	2.66	2.67	2.68	2.69	2.70	2.71	2.72	2.73	2.74	2.75
28	2.76	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.85
29	2.86	2.86	2.87	2.88	2.89	2.90	2.91	2.92	2.98	2.94
80	2.95	2.96	2.97	2.98	2.99	3.00	8.01	3.02	8.08	3.04
81	3.05	8.06	3.07	3.06	3.09	8.10	3.11	3.12	8.18	3.14
32	3.15	3.16	8.17	8.18	3.19	8.20	3.21	3.22	8.23	8.24
88	3.25	8.26	8.27	3.28	8.29	3.30	3.31	8.82	3.88	8.84
84	3.35	3.86	3.37	8.88	8.89	8.40	8.41	8.42	8.48	8.44
35	8.45	8.46	8.47	3.48	8.49	8.50	3.51	8.52	8.58	8.54
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

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		В	AROMI	ETER:	615***.	(from	612.51	to 617.5	0).	
Centi- grade Degrees.					Tenthe o	f Degrees.		-		
	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.
°	Millim.	Millim. 0.01	Millim. 0.02	Millim. 0.08	Millim. 0.04	Millim, 0.05	Millim. 0.06	Million. 0.07	Millim. 0.06	Millim.
ľ	0.00	0.01		5.55	0.02	0.55		0.01	0.00	0.00
1	0.10	0.11	0.12	0.18	0.14	0.15	0.16	0.17	0.18	0.19
2	0.20	0.21	0.22	0.28	0.24	0.25	0.26	0.27	0.28	0.29
8	0.80	0.31	0.32	0.88	0.84	0.35	0.36	0.87	0.38	0.39
4	0.40	0.41	0.42	0.48	0.44	0.45	0.46	0.47	0.48	0.49
5	0.50	0.51	0.52	0.58	0.54	0.55	0.56	0.57	0.58	0.59
6	0.60	0.61	0.62	0.68	0.64	0.65	0.66	0.67	0.68	0.68
7	0.69	0.70	0.71	0.72	0.78	0.74	0.75	0.76	0.77	0.78
8	0.79	0.80	0.81	0.82	0.88	0.84	0.85	0.86	0.87	0.88
9	0.89	0.90	0.91	0.92	0.98	0.94	0.95	0.96	0.97	0.98
10	0.99	1.00	1.01	1.02	1.08	1.04	1.05	1.06	1.07	1.06
11	1.09	1.10	1.11	1.12	1.18	1.14	1.15	1.16	1.17	1.18
12	1.19	1.20	1.21	1.22	1.28	1.24	1.25	1.26	1.27	1.28
13	1.29	1.30	1.31	1.32	1.88	1.34	1.85	1.36	1.87	1.38
14	1.89	1.40	1.41	1.42	1.48	1.44	1.45	1.46	1.47	1.48
15	1.49	1.50	1.51	1.52	1.58	1.54	1.55	1.56	1.57	1.58
16	1.59	1.60	1.61	1.62	1.68	1.64	1.65	1.66	1.67	1.68
17	1.69	1.70	1.71	1.72	1.78	1.74	1.75	1.76	1.77	1.78
18	1.79	1.80	1.81	1.82	1.88	1.84	1.85	1.86	1.87	1.88
19	1.89	1.90	1.91	1.92	1.98	1.94	1.95	1.96	1.97	1.98
20	1.99	2.00	2.01	2.01	2.02	2.08	2.04	2.05	2.06	2.07
21	2.08	2.09	2.10	2.11	2.12	2.18	2.14	2.15	2.16	2.17
22	2.18	2.19	2.20	2.21	2.22	2.23	2.24	2.25	2.26	2.27
23	2.28	2.29	2.80	2.81	2.82	2.38	2.84	2.35	2.86	2.37
24	2.38	2.39	2.40	2.41	2.42	2.43	2.44	2.45	2.46	2.47
25	2.48	2.49	2.50	2.51	2.52	2.53	2.54	2.55	2.56	2.57
26	2.58	2.59	2.60	2.61	2.62	2.68	2.64	2.65	2.66	2.67
27	2.68	2.69	2.70	2.71	2.72	2.73	2.74	2.75	2.76	2.77
28	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.85	2.86	2.87
29	2.88	2.89	2.90	2.91	2.92	2.98	2.94	2.95	2.96	2.97
80	2.98	2.99	3.00	8.01	3.02	8.08	8.04	8.05	8.06	8.07
81	3.08	8.09	8.10	8.11	8.12	8.18	8.14	8.15	8.16	3.17
82	3.18	8.19	3.20	8.21	8.22	3.23	8.24	8.25	8.26	8.27
38	8.28	8.29	8.80	3.31	3.32	8.88	8.34	3.85	8.36	3.36
34	8.37	8.88	8.89	8.40	8.41	8.42	8.43	8.44	8.45	8.46
35	8.47	8.48	8.49	3.50	8.51	8.52	8.58	8.54	8.55	3.56
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

		В	AROME	ETER:	620	(from	617.51 t	o 622 .5	0)	
Centi- grade Degrees.					Tenthe o	f Degrees.				
	0.	1.	9.	8.	4.	5.	6.	7.	Š.	9.
°	Millim. 0.00	Millim. 0.01	Millim. 9.02	Millim. 0.08	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim 0.08	Millim. 0.09
1	0.10	0.11	0.12	0.18	0.14	0.15	0.16	0.17	0.18	0.19
2	0.20	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29
3	0.80	0,81	0.82	0.88	0.84	0.35	0.36	0.37	0.88	0.89
4	9.40	0.41	0.42	0.48	0.44	0.45	0.46	0.47	0.48	0.49
5	Q.50	0.51	0.52	0.58	0.54	0.55	0.56	0.57	0.58	0.59
6	0.60	0:61	0.62	0.68	0.64	0.65	0.66	0.67	0.68	0.69
7	0.70	0.71	0.72	0.78	0.74	0.75	0.76	0.77	0.78	0.79
8	0.80	0.81	0.82	0.88	0.84	0.85	0.86	0.87	0.88	0.89
9	0.90	0.91	0.92	0.98	0.94	0.95	0.96	0.97	0.98	0.99
10	1.00	2.01	1.02	1.08	1.04	1.05	1.06	1.07	1.08	1.09
		١.,,	1.10	1 10	١.,,			١.,_		
11	1.10 1.20	1.11	1.12	1.18 1.28	1.14 1.24	1.15 1.25	1.16	1.17	1.18 1.28	1.19
12	1.30	1.21	1.32	1.33	1.84	1.85	1.26	1.27	1.38	1.29 1.39
18 14	1.40	1.41	1.42	1.48	1.44	1.45	1.46	1.47	1.48	1.49
15	1.50	1.51	1.52	1.58	1.54	1.55	1.56	1.57	1.58	1.59
10	1.50	1.01	1.02	1.00	1.04	1.00	1.00	1.01	1.00	1.00
16	1.60	1.61	1.62	1.68	1.64	1.65	1.66	1.67	1.68	1.69
17	1.70	1.71	1.72	1.78	1.74	1.75	1.76	1.77	1.78	1.79
18	1.80	1.81	1.82	1.88	1.84	1.85	1.86	1.87	1.88	1.89
19	1.90	1.91	1.92	1.98	1.94	1.95	1.96	1.97	1.98	1.99
20	2.00	2.01	2.02	2.08	2.04	2.05	2.06	2.07	2.08	2.09
21	2.10	2.11	2.12	2.18	2.14	2.15	2.16	2.17	2.18	2.19
22	2.20	2.21	2.22	2.23	2.24	2.25	2.26	2.27	2.28	2.29
23	2.30	2.81	2.32	2.38	2.84	2.35	2.36	2.37	2.38	2.39
24	2.40	2.41	2.42	2.43	2.44	2.45	2.46	2.47	2.48	2.49
25	2.50	2.51	2.52	2.53	2.54	2.55	2.56	2.57	2.58	2.59
				-						
26	2.60 2.70	2.61	2.62 2.72	2.63	2.64	2.65	2.66	2.67	2.68	2.69
27 28	2.80	2.71 2.81	2.72	2.78 2.83	2.74 2.84	2.75 2.85	2.76 2.86	2.77 2.87	2.78 2.88	2.79 2.89
28 29	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97	2.98	2.99
8 0	8.00	3.01	8.02	3.03	8.04	8.05	8.06	8.07	8.08	8.09
									5.05	1
81	3.10	8.11	8.12	8.18	8.14	8.15	8.16	8.17	3.18	8.19
82	3.20	8.21	8.22	8.23	8.24	8.25	8.26	3.27	3.28	3.29
33	8.30	3.31	8.82	3.33	3.34	3.35	8.36	3.37	8.38	8.39
34	8.40	8.41	3.42	3.43	3.44	3.45	8.46	8.47	8.48	8.49
85	8.50	8.51	3.52	3.53	3.54	8.55	3.56	8.57	8.58	3.59
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
j		1	I	1	1	ŀ	1	!	I	l

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		В	AROMI	ETER:	625	(from	622.51 (to 627.5	i0).	
Centi- grade Degrees.					Tenths o	Degrees.		_		
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
°	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.08	Millim. 0.04	Millim. 0.05	Millim, 0.08	Millim, 0.07	Millim 0.08	Mittim. 0.09
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19
2	0.20	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29
8	0.30	0.81	0.32	0.88	0.84	0.35	0.86	0.87	0.28	0.39
4	0.40	0.41	0.42	0.48	0.44	0.45	0.46	0.47	0.48	0.49
5	0.50	0.51	0.52	0.58	0.54	0.55	0.56	0.58	0.59	0.60
6	0.61	0.62	0.68	0.64	0.65	0.66	0.67	0.68	0.69	0.70
7	0.71	0.72	0.78	0.74	0.75	0.76	0.77	0.78	0.79	0.80
8	0.81	0.82	0.88	0.84	0.85	0.86	0.87	0.88	0.89	0.90
9	0.91	0.92	0.98	0.94	0.95	0.96	0.97	0.98	0.99	1.00
10	1.01	1.02	1.08	1.04	1.05	1.06	1.07	1.08	1.09	1.10
n	1.11	1.12	1.18	1.14	1.15	1.16	1.17	1.18	1.19	1.20
12	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.28	1.29	1.30
18	1.31	1.32	1.83	1.84	1.35	1.86	1.87	1.88	1.39	1.40
14	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48	1.49	1.50
15	1.51	1.52	1.53	1.54	1.55	1.56	1.57	1.58	1.59	1.60
16	1.61	1.62	1.68	1.64	1.65	1.66	1.67	1.68	1.69	1.70
17	1.71	1.73	1.74	1.75	1.76	1.77	1.78	1.79	1.80	1.81
18	1.82	1.83	1.84	1.85	1.86	1.87	1.38	1.89	1.90	1.91
19	1.92	1.93	1.94	1.95	1.96	1.97	1.98	1.99	2.00	2.01
20	2.02	2.08	2.04	2.05	2.06	2.07	2.08	2.09	2.10	2.11
21	2.12	2.13	2.14	2.15	2.16	2.17	2.18	2.19	2.20	2.21
22	2.22	2.23	2.24	2.25	2.26	2.27	2.28	2.29	2.80	2.31
28	2.32	2.33	2.84	2.85	2.36	2.37	2.88	2.39	2.40	2.41
24	2.42	2.48	2.44	2.45	2.46	2.47	2.48	2.49	2.50	2.51
25	2.52	2.58	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61
26	2.62	2.68	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.71
27	2.72	2.78	2.74	2.75	2.76	2.77	2.78	2.79	2.80	2.81
28	2.82	2.88	2.84	2.85	2.87	2.88	2.89	2.90	2.91	2.92
29	2.93	2.94	2.95	2.96	2.97	2.98	2.99	8.00	3.01	3.02
30	3.08	8.04	8.05	8.06	8.07	3.06	3.09	8.10	8.11	3.12
81	3.13	8.14	8.15	8.16	8.17	3.18	3.19	8.20	8.21	8.22
82	3.23	8.24	3.25	8.26	8.27	3.28	8.29	3.80	8.31	3.32
33	3.88	8.34	3.85	3.86	8.37	3.38	3.39	8.40	8.41	3.42
84	8.43	8.44	8.45	8.46	8.47	3.48	8.49	8.50	8.51	8.52
85	3.58	8.54	3.55	3.56	8.57	8.58	3.59	8.60	8.61	3.62
	0.	1.	9.	3.	4.	5.	6.	7.	8.	9.

	BAROMETER: 630 (from 627.51 to 632.50).											
Centi- grade Degress.					Tenths o	Degrees.						
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.		
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.08	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.09		
1	0.10	0.11	0.12	0.18	0.14	0.15	0.16	0.17	0.18	0.19		
2	0.20	0.21	0.22	0.28	0.24	0.25	0.26	0.27	0.28	0.29		
8	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88	0.39	0.40		
4	0.41	0.42	0.48	0.44	0.45	0.46	0.47	0.48	0.49	0.50		
5	0.51	0.52	0.58	0.54	0.55	0.56	0.57	0.58	0.59	0.60		
6	0.61	0.62	0.63	0.64	0.65	0.66	0.67	0.68	0.69	0.70		
7	0.71	0.72	0.78	0.74	0.75	0.76	0.77	0.78	0.79	0.80		
8	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.90		
9	0.92	0.93	0.94	0.95	0.96	0.97	0.98	0.99	1.00	1.01		
10	1.02	1.03	1.04	1.05	1.06	1.07	1.08	1.09	1.10	1.11		
11	1.12	1.18	1.14	1.15	1.16	1.17	1.18	1.19	1.20	1.21		
12	1.22	1.28	1.24	1.25	1.26	1.27	1.28	1.29	1.30	1.81		
18	1.32	1.83	1.84	1.85	1.36	1.37	1.88	1.89	1.40	1.41		
14	1.42	1.48	1.44	1.45	1.46	1.47	1.48	1.49	1.50	1.52		
15	1.53	1.54	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.62		
16	1.63	1.64	1.65	1.66	1.67	1.68	1.69	1.70	1.71	1.72		
17	1.78	1.74	1.75	1.76	1.77	1.78	1.79	1.80	1.81	1.82		
18	1.83	1.84	1.85	1.86	1.87	1.88	1.99	1.90	1.91	1.92		
19	1.93	1.94	1.95	1.96	1.97	1.98	1.99	2.00	2.01	2.02		
20	2.03	2.04	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.13		
21	2.14	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.22	2.23		
22	2.24	2.25	2.26	2.27	2.28	2.29	2.80	2.31	2.82	2.83		
28	2.84	2.85	2.86	2.87	2.88	2.39	2.40	2.41	2.42	2.48		
24	2.44	2.45	2.46	2.47	2.48	2.49	2.50	2.51	2.52	2.58		
25	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63		
26	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.71	2.78	2.74		
27	2.75	2.76	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84		
28	2.85	2.86	2.87	2.88	2.89	2.90	2.91	2.92	2.93	2.94		
29	2.95	2.96	2.97	2.98	2.99	8.00	3.01	8.02	8.08	3.04		
80	8.05	3.06	8.07	8.08	8.09	8.10	8.11	8.12	8.18	3.14		
31	3.15	3.16	3.17	8.18	8.19	8.20	8.21	8.23	3.28	8.24		
82	3.25	8.26	8.27	8.28	8.29	8.80	8.81	8.82	8.34	8.35		
83	8.36	3.37	3.38	8.89	8.40	8.41	8.42	8.48	8.44	8.45		
34	8.46	3.47	3.48	3.49	8.50	8.51	3.52	3.58	8.54	3.55		
85	8.56	8.57	3.58	8.59	3.60	8.61	3.62	8.63	3.64	8.65		
	0.	1.	2,	8.	4.	5.	6.	7.	8.	9.		

0 Mii 0. 1 0. 2 0. 3 0. 4 0. 6 0. 7 0. 8 0. 9 0. 10 1. 11 1. 12 1. 13 1. 14 1. 15 1. 16 1. 17 1. 18 1. 19 1. 20 2. 21 2. 22 2. 24 2. 25 2. 26 2. 27 2.	0. fillim. 0.00 0.10 0.20 0.81 0.41 0.51 0.61 0.72 0.82 0.92 1.02	Millim. 0.01 0.11 0.22 0.82 0.42 0.52 0.63 0.73 0.88 0.98 1.04	Millim. 0.02 0.13 0.28 0.33 0.43 0.53 0.64 0.74 0.84 0.94 1.05	Millim. 0.03 0.13 0.24 0.34 0.44 0.54 0.65 0.75 0.85 0.95 1.06	Tenths o Millim. 0.04 0.14 0.25 0.35 0.45 0.55 0.66 0.76 0.86 0.96 1.07	5. Million. 0.05 0.15 0.26 0.36 0.46 0.56 0.67 0.77 0.87 0.97	Millim. 0.06 0.16 0.27 0.37 0.47 0.57 0.68 0.78 0.88	7. Millim. 0.07 0.17 0.28 0.38 0.48 0.58 0.69 0.79 0.89	Millim. 0.08 0.18 0.29 0.39 0.49 0.59	9. Millim 0.09 0.19 0.80 0.40 0.50 0.60
0 Mii 0. 1 0. 2 0. 3 0. 4 0. 6 0. 7 0. 8 0. 9 0. 10 1. 11 1. 12 1. 13 1. 14 1. 15 1. 16 1. 17 1. 18 1. 19 1. 20 2. 21 2. 22 2. 24 2. 25 2. 26 2. 27 2.	0.10 0.20 0.31 0.41 0.51 0.61 0.72 0.82 0.92 1.02	Millim. 0.01 0.11 0.22 0.82 0.42 0.52 0.68 0.73 0.89 0.98 1.04	Millim. 0.02 0.12 0.28 0.38 0.48 0.53 0.64 0.74 0.84 0.94 1.05	Millim. 0.08 0.13 0.24 0.84 0.44 0.54 0.65 0.75 0.85 0.95	Million. 0.04 0.14 0.25 0.85 0.45 0.55 0.66 0.76 0.86 0.96	Millin. 0.05 0.15 0.26 0.36 0.46 0.56 0.67 0.77	Millim. 0.06 0.16 0.27 0.37 0.47 0.57	Millim. 0.07 0.17 0.28 0.38 0.48 0.58	Millim. 0.08 0.18 0.29 0.39 0.49 0.59	Millim 0.09 0.19 0.80 0.40 0.50 0.60
0 0.0. 1 0.0. 2 0.0. 8 0.0. 6 0.7 0.0. 8 0.0. 10 1.1 11 1.1 12 1.1 13 1.1 15 1.1 16 1.1 17 1.1 18 1.1 19 1.1 20 2.1 21 2.2 22 2.2 24 2.2 25 2.2 26 2.2 27 2.2	0.00 0.10 0.20 0.81 0.41 0.51 0.61 0.72 0.82 0.92 1.02 1.13 1.28 1.38	0.01 0.11 0.22 0.82 0.42 0.52 0.63 0.73 0.88 0.98 1.04	0.02 0.12 0.28 0.88 0.48 0.53 0.64 0.74 0.84 0.94 1.05	0.08 0.18 0.24 0.84 0.14 0.54 0.65 0.75 0.85 0.95	0.04 0.14 0.25 0.85 0.45 0.55 0.66 0.76 0.86 0.96	0.05 0.15 0.26 0.36 0.46 0.56 0.67 0.77 0.87	0.06 0.16 0.27 0.37 0.47 0.57	0.07 0.17 0.28 0.38 0.48 0.58 0.69 0.79	0.08 0.18 0.29 0.39 0.49 0.59 0.70 0.80	0.09 0.19 0.80 0.40 0.50 0.60
2 0. 8 0. 9 0. 10 1. 11 1. 12 1. 13 1. 14 1. 15 1. 16 1. 17 1. 18 1. 19 2. 21 2. 22 2. 24 2. 25 2. 26 2. 27 2.	0.20 0.81 0.41 0.51 0.61 0.72 0.82 0.92 1.02 1.13 1.23 1.33	0.22 0.82 0.42 0.62 0.68 0.73 0.83 0.98 1.04	0.28 0.38 0.48 0.53 0.64 0.74 0.84 0.94 1.05	0.24 0.84 0.44 0.54 0.65 0.75 0.85 0.95	0.25 0.85 0.45 0.55 0.66 0.76 0.86 0.96	0.26 0.36 0.46 0.56 0.67 0.77	0.27 0.37 0.47 0.57 0.68 0.78	0.28 0.38 0.48 0.58 0.69 0.79	0.29 0.89 0.49 0.59 0.70 0.80	0.80 0.40 0.50 0.60
2 0. 8 0. 9 0. 10 1. 11 1. 12 1. 13 1. 14 1. 15 1. 16 1. 17 1. 18 1. 19 2. 21 2. 22 2. 24 2. 25 2. 26 2. 27 2.	0.20 0.81 0.41 0.51 0.61 0.72 0.82 0.92 1.02 1.13 1.23 1.33	0.22 0.82 0.42 0.62 0.68 0.73 0.83 0.98 1.04	0.28 0.38 0.48 0.53 0.64 0.74 0.84 0.94 1.05	0.24 0.84 0.44 0.54 0.65 0.75 0.85 0.95	0.25 0.85 0.45 0.55 0.66 0.76 0.86 0.96	0.26 0.36 0.46 0.56 0.67 0.77	0.27 0.37 0.47 0.57 0.68 0.78	0.28 0.38 0.48 0.58 0.69 0.79	0.29 0.89 0.49 0.59 0.70 0.80	0.80 0.40 0.50 0.60
8 0.4 0.5 0.0 0.0 0.0 0.1 0.1 1.1 1.1 1.1 1.1 1.1	0.81 0.41 0.51 0.61 0.72 0.82 0.92 1.02 1.13 1.23 1.33	0.82 0.42 0.52 0.68 0.78 0.88 0.98 1.04	0.88 0.48 0.53 0.64 0.74 0.84 0.94 1.05	0.84 0.44 0.54 0.65 0.75 0.85 0.95	0.85 0.45 0.55 0.66 0.76 0.86 0.96	0.36 0.46 0.56 0.67 0.77 0.87	0.37 0.47 0.57 0.68 0.78	0.88 0.48 0.58 0.69 0.79	0.89 0.49 0.59 0.70 0.80	0.40 0.50 0.60 0.71
4 0. 6 0. 0. 6 0. 0. 8 0. 0. 10 1. 11 1. 12 1. 12 1. 15 1. 15 1. 15 1. 15 1. 12 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.	0.41 0.51 0.61 0.72 0.82 0.92 1.02	0.42 0.52 0.63 0.73 0.83 0.98 1.04	0.48 0.58 0.64 0.74 0.84 0.94 1.05	0.44 0.54 0.65 0.75 0.85 0.95	0.45 0.55 0.66 0.76 0.86 0.96	0.46 0.56 0.67 0.77 0.87	0.47 0.57 0.68 0.78	0.48 0.58 0.69 0.79	0.49 0.59 0.70 0.80	0.50 0.60 0.71
6 0. 6 0. 7 0. 8 0. 9 0. 10 1. 11 1. 12 1. 13 1. 14 1. 15 1. 16 1. 17 1. 18 1. 19 2. 21 2. 22 2. 24 2. 25 2. 26 2. 27 2.	0.51 0.61 0.72 0.82 0.92 1.02 1.13 1.28 1.33	0.52 0.68 0.73 0.83 0.98 1.04	0.58 0.64 0.74 0.84 0.94 1.05	0.54 0.65 0.75 0.85 0.95	0.55 0.66 0.76 0.86 0.96	0.56 0.67 0.77 0.87	0.57 0.68 0.78	0.58 0.69 0.79	0.59 0.70 0.80	0.60
7 0. 8 0. 9 0. 10 1. 11 1. 12 1. 13 1. 15	0.72 0.82 0.92 1.02 1.13 1.23	0.78 0.88 0.98 1.04	0.74 0.84 0.94 1.05	0.75 0.85 0.95	0.76 0.86 0.96	0.77 0.87	0.78	0.79	0.80	1
8 0. 9 0. 10 1. 11 1. 12 1. 13 1. 14 1. 15 1. 16 1. 17 1. 18 1. 19 1. 20 2. 21 2. 22 2. 24 2. 25 2. 26 2. 27 2.	0.82 0.92 1.02 1.13 1.23	0.83 0.98 1.04 1.14 1.24	0.84 0.94 1.05	0.85 0.95	0.86 0.96	0.87		1	i	0.81
9 0. 10 1. 11 1. 12 1. 13 1. 14 1. 15 1. 16 1. 17 1. 18 1. 19 1. 20 2. 21 2. 22 2. 24 2. 25 2. 26 2. 27 2.	0.92 1.02 1.13 1.23 1.33	0.98 1.04 1.14 1.24	0.94 1.05 1.15	0.95	0.96		0.88	0.89		
10 1. 11 1. 12 1. 13 1. 14 1. 15 1. 16 1. 17 1. 18 1. 19 1. 20 2. 21 2. 22 2. 24 2. 25 2. 26 2. 27 2.	1.02 1.13 1.23 1.33	1.04 1.14 1.24	1.05	1		0.97		1	0.90	0.91
11 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	1.13 1.23 1.33	1.14 1.24	1.15	1.06	1.07		0.98	0.99	1.00	1.01
12 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	1.23 1.33	1.24			1.07	1.06	1.09	1.10	1.11	1.12
18 1. 14 1. 15 1. 16 1. 17 1. 18 1. 19 1. 20 2. 21 2. 22 2. 24 2. 26 2. 27 2.	1.33			1.16	1.17	1.18	1.19	1.20	1.21	1.22
14 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.			1.25	1.26	1.27	1.28	1.29	1.80	1.31	1.32
15 1. 16 1. 17 1. 18 1. 19 1. 20 2. 21 2. 22 2. 24 2. 25 2. 26 2. 27 2.		1.34	1.85	1.36	1.87	1.38	1.89	1.40	1.41	1.42
16 1. 17 1. 18 1. 19 1. 20 2. 21 2. 22 2. 24 2. 25 2. 26 2. 27 2.	1.43	1.45	1.46	1.47	1.48	1.49	1.50	1.51	1.52	1.58
17 1. 18 1. 19 1. 20 2. 21 2. 22 2. 23 2. 24 2. 25 2. 26 2. 27 2.	1.54	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.62	1.63
18 1. 19 1. 20 2. 21 2. 22 2. 23 2. 24 2. 25 2. 26 2. 27 2.	1.64	1.65	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.73
19 1. 20 2. 21 2. 22 2. 23 2. 24 2. 25 2. 26 2. 27 2.	1.74	1.75	1.76	1.77	1.78	1.79	1.90	1.81	1.82	1.93
20 2. 21 2. 22 2. 23 2. 24 2. 25 2. 26 2. 27 2.	1.84	1.86	1.87	1.88	1.89	1.90	1.91	1.92	1.98	1.94
21 2. 22 2. 23 2. 24 2. 25 2. 26 2. 27 2.	1.95	1.96	1.97	1.96	1.99	2.00	2.01	2.02	2.03	2.04
22 2. 28 2. 24 2. 25 2. 26 2. 27 2.	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.12	2.13	2.14
28 2. 24 2. 25 2. 26 2. 27 2.	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.22	2.23	2.2
24 2. 25 2. 26 2. 27 2.	2.25	2.27	2.28	2.29	2.30	2.31	2.32	2.33	2.34	2.3
25 2. 26 2. 27 2.	2.36	2.37	2.38	2.39	2.40	2.41	2.42	2.48	2.44	2.4
26 2. 27 2.	2.46	2.47	2.48	2.49	2.50	2.51	2.52	2.53	2.54	2.50
27 2.	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.68
11	2.66	2.67	2.69	2.70	2.71	2.72	2.78	2.74	2.75	2.70
28 2.	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.85	2.8
	2.87	2.88	2.89	2.90	2.91	2.92	2.98	2.94	2.95	2.9
	2.97	2.98	2.99	8.00	8.01	8.02	8.08	3.04	8.05	8.00
80 8.	8.07	8.08	8.10	8.11	3.12	8.18	8.14	8.15	8.16	3.17
11	3.18	8.19	3.20	8.21	3.22	8.23	8.24	8.25	8.26	3.2
	3.28	8.29	8.80	8.81	8.82	8.88	8.84	8.35	3.36	3.3
1		8.39	8.40	8.41	8.42	3.43	8.44	8.45	8.46	3.47
11	3.38	3.49 8.60	8.51 8.61	8.52 8.62	8.58 8.63	8.54 3.64	8.55 8.65	3.66	8.57 8.67	3.58
	3.38 8.48 3.59		2.	3.	4	5.	6.	7.	8.	9.

Mullim. Mull			В	AROME	ETER:	640 ^{mm.}	(from	3 37 .51 t	o 642 .5	0).	
Million Mill	Centi- grade Degrees.					Tenthe o	Dogrees.		-		
0 0.00 0.01 0.02 0.08 0.04 0.05 0.06 0.07 0.08 0.0 1 0.10 0.11 0.12 0.18 0.14 0.15 0.17 0.18 0.19 0.2 2 0.21 0.22 0.23 0.24 0.25 0.28 0.27 0.28 0.29 0.3 3 0.81 0.32 0.83 0.84 0.85 0.48 0.48 0.49 0.50 0.4 4 0.41 0.42 0.43 0.44 0.45 0.48 0.48 0.49 0.50 0.6 5 0.52 0.63 0.64 0.65 0.66 0.67 0.88 0.89 0.50 0.60 0.67 6 0.62 0.63 0.64 0.85 0.66 0.67 0.88 0.69 0.70 0.7 7 0.72 0.73 0.74 0.75 0.76 0.77 0.78 0.80 0.81 </th <th></th> <th>0.</th> <th>1.</th> <th>2.</th> <th>8.</th> <th>4.</th> <th>5.</th> <th>6.</th> <th>7.</th> <th>8.</th> <th>9.</th>		0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
1 0.10 0.11 0.12 0.13 0.14 0.15 0.17 0.18 0.19 0.2 2 0.21 0.32 0.28 0.24 0.25 0.26 0.27 0.28 0.29 0.3 3 0.21 0.32 0.83 0.34 0.35 0.38 0.37 0.88 0.39 0.4 4 0.41 0.42 0.43 0.44 0.45 0.46 0.48 0.49 0.50 0.5 5 0.52 0.53 0.54 0.55 0.56 0.57 0.58 0.59 0.60 0.6 6 0.62 0.63 0.64 0.65 0.66 0.67 0.68 0.69 0.70 0.7 7 0.72 0.73 0.74 0.75 0.76 0.77 0.78 0.80 0.81 0.9 9 0.93 0.94 0.95 0.96 0.97 0.98 0.99 1.00 1.01 1.01 1.03 1.04 1.05 1.06 1.07 1.08 1.09 1.11 1.12 1.1 11 1.14 1.15 1.16 1.17 1.18 1.19 1.20 1.21 1.22 1.2 12 1.24 1.25 1.26 1.27 1.28 1.29 1.80 1.81 1.82 1.81 1.82 1.81 1.85 1.86 1.87 1.88 1.99 1.40 1.41 1.42 1.45 1.46 1.47 1.48 1.49 1.50 1.51 1.52 1.53 1.51 1.55 1.56 1.57 1.58 1.59 1.60 1.61 1.62 1.63 1.61 1.77 1.78 1.79 1.80 1.61 1.82 1.83 1.84 1.85 1.86 1.87 1.88 1.99 1.90 1.91 1.92 1.93 1.94 1.81 1.99 1.90 1.91 1.92 2.03 2.03 2.05 2.09 2.09 2.00 2.07 2.08 2.09 2.10 2.11 2.12 2.13 2.12 2.2 2.27 2.28 2.29 2.30 2.31 2.32 2.33 2.34 2.35 2.66 2.67 2.68 2.69 2.70 2.71 2.72 2.73 2.74 2.75 2.76 2.77 2.77 2.78 2.80 2.90 2.91 2.92 2.93 2.90 2.91 2.92 2.93 2.94 2.95 2.96 2.97 2.98 2.99 2.90 2.91 2.92 2.83 2.84 2.85 2.86 2.87 2.88 2.89 2.90 2.91 2.92 2.83 2.94 2.95 2.96 2.97 2.13 2.13 3.14 3.15 3.13 3.13 3.14 3.13 3.13 3.14 3.13 3.13											Millim
2 0.21 0.22 0.28 0.24 0.25 0.28 0.27 0.28 0.29 0.3 0.44 0.25 0.38 0.37 0.88 0.39 0.4 0.41 0.42 0.43 0.44 0.25 0.38 0.37 0.88 0.39 0.4 0.45 0.46 0.48 0.49 0.50 0.50 0.55 0.56 0.57 0.88 0.49 0.50 0.61 1.60<	0	0.00	0.01	0.02	0.08	0.04	0.05	0.06	0.07	0.08	0.09
3 0.81 0.82 0.83 0.84 0.85 0.36 0.57 0.88 0.89 0.44 4 0.41 0.42 0.43 0.44 0.45 0.46 0.48 0.49 0.50 0.5 5 0.52 0.53 0.54 0.55 0.56 0.57 0.58 0.59 0.60 0.6 6 0.62 0.63 0.64 0.65 0.66 0.67 0.88 0.69 0.70 0.7 7 0.72 0.73 0.74 0.75 0.76 0.77 0.78 0.80 0.91 0.9 9 0.83 0.94 0.95 0.96 0.97 0.98 0.99 1.00 1.01 1.0 10 1.03 1.04 1.05 1.06 1.07 1.08 1.09 1.11 1.12 1.1 11 1.14 1.15 1.16 1.17 1.18 1.19 1.20 1.21 1.21 1.21	1	0.10	0.11	0.12	0.18	0.14	0.15	0.17	0.18	0.19	0.20
4 0.41 0.42 0.43 0.44 0.45 0.46 0.48 0.49 0.50 0.56 5 0.52 0.53 0.54 0.55 0.56 0.57 0.88 0.59 0.60 0.6 6 0.62 0.63 0.64 0.65 0.66 0.67 0.68 0.69 0.70 0.7 7 0.72 0.73 0.74 0.75 0.76 0.77 0.78 0.80 0.61 0.8 8 0.83 0.84 0.86 0.86 0.87 0.88 0.89 0.90 0.91 0.9 10 1.03 1.04 1.05 1.06 1.07 1.08 1.09 1.11 1.12 1.1 11 1.14 1.15 1.16 1.17 1.18 1.19 1.20 1.21 1.21 1.21 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1	2	0.21	0.22	0.28	0.24	0.25	0.26	0.27	0.28	0.29	0.80
5 0.52 0.53 0.54 0.55 0.56 0.57 0.58 0.59 0.60 0.66 6 0.62 0.63 0.64 0.65 0.66 0.67 0.68 0.69 0.70 0.77 7 0.72 0.73 0.74 0.75 0.76 0.77 0.78 0.80 0.61 0.81 8 0.83 0.84 0.85 0.86 0.87 0.88 0.89 0.90 0.91 0.93 9 0.93 0.94 0.95 0.96 0.97 0.98 0.99 1.00 1.01 1.0 10 1.03 1.04 1.05 1.06 1.07 1.08 1.09 1.11 1.12 1.1 11 1.14 1.15 1.16 1.17 1.18 1.19 1.20 1.21 1.22 1.21 1.12 1.1 1.11 1.12 1.1 1.11 1.12 1.1 1.11 1.12 1.1 <t< td=""><td>3</td><td>0.81</td><td>0.82</td><td>0.83</td><td>0.84</td><td>0.85</td><td>0.36</td><td>0.37</td><td>0.88</td><td>0.89</td><td>0.40</td></t<>	3	0.81	0.82	0.83	0.84	0.85	0.36	0.37	0.88	0.89	0.40
6	4	0.41	0.42	0.43	0.44	0.45	0.46	0.48	0.49	0.50	0.51
7 0.72 0.73 0.74 0.75 0.76 0.77 0.78 0.80 0.81 0.88 8 0.83 0.84 0.85 0.86 0.87 0.88 0.89 0.90 0.91 0.9 9 0.93 0.94 0.95 0.96 0.97 0.98 0.99 1.00 1.01 1.0 10 1.03 1.04 1.05 1.06 1.07 1.08 1.09 1.11 1.12 1.1 11 1.14 1.15 1.16 1.17 1.18 1.19 1.20 1.21 1.22 1.2 12 1.24 1.25 1.26 1.27 1.28 1.29 1.30 1.31 1.82 1.3 13 1.34 1.35 1.36 1.37 1.38 1.39 1.40 1.42 1.43 1.4 14 1.45 1.46 1.47 1.48 1.49 1.50 1.51 1.52 1.53 1	5	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61
7 0.72 0.73 0.74 0.75 0.76 0.77 0.78 0.80 0.81 0.88 8 0.83 0.84 0.85 0.86 0.87 0.88 0.89 0.90 0.91 0.98 9 0.93 0.94 0.95 0.96 0.97 0.98 0.99 1.00 1.01 1.0 10 1.03 1.04 1.05 1.06 1.07 1.08 1.09 1.11 1.12 1.1 11 1.14 1.15 1.16 1.17 1.18 1.19 1.20 1.21 1.22 1.2 12 1.24 1.25 1.26 1.27 1.28 1.29 1.30 1.31 1.82 1.3 13 1.34 1.35 1.36 1.37 1.38 1.39 1.40 1.42 1.43 1.4 14 1.45 1.46 1.47 1.48 1.49 1.50 1.51 1.52 1.53	6	0.62	0.63	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71
8 0.83 0.84 0.85 0.86 0.87 0.88 0.89 0.90 0.91 0.93 9 0.93 0.94 0.95 0.96 0.97 0.98 0.99 1.00 1.01 1.0 10 1.03 1.04 1.05 1.06 1.07 1.08 1.09 1.11 1.12 1.1 11 1.14 1.15 1.16 1.17 1.18 1.19 1.20 1.21 1.22 1.2 12 1.24 1.25 1.26 1.27 1.28 1.29 1.80 1.81 1.82 1.81 13 1.34 1.85 1.86 1.87 1.88 1.89 1.40 1.42 1.43 1.44 14 1.45 1.46 1.47 1.48 1.49 1.50 1.51 1.52 1.53 1.5 15 1.56 1.57 1.58 1.59 1.60 1.61 1.62 1.63 1.6		1	1						1	1	0.82
9		1	1	1	ı				ľ	_	0.92
10 1.03 1.04 1.05 1.06 1.07 1.08 1.09 1.11 1.12 1.12 1.11 1.12 1.11 1.12 1.12 1.11 1.12 1.12 1.21 1.22 1.23 1.23 1.23 1.23 1.23 1.23 1.23 1.23 1.23 1.23 1.23 1.23 1.24 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1.42 1					l					ı	1.02
12 1.24 1.25 1.26 1.27 1.28 1.29 1.80 1.31 1.82 1.32 18 1.34 1.35 1.86 1.37 1.88 1.39 1.40 1.42 1.43 1.43 14 1.45 1.46 1.47 1.48 1.49 1.50 1.51 1.52 1.53 1.5 15 1.55 1.56 1.57 1.58 1.59 1.60 1.61 1.62 1.63 1.6 16 1.65 1.66 1.67 1.68 1.69 1.70 1.71 1.72 1.74 1.7 17 1.76 1.77 1.78 1.79 1.80 1.81 1.82 1.88 1.84 1.8 18 1.96 1.97 1.98 1.99 2.00 2.01 2.02 2.03 2.05 2.0 20 2.07 2.08 2.09 2.10 2.11 2.12 2.13 2.14 2.15 <		II.	1							l .	1.18
12 1.24 1.25 1.26 1.27 1.28 1.29 1.80 1.31 1.82 1.32 18 1.34 1.35 1.86 1.37 1.88 1.39 1.40 1.42 1.43 1.43 14 1.45 1.46 1.47 1.48 1.49 1.50 1.51 1.52 1.53 1.5 15 1.55 1.56 1.57 1.58 1.59 1.60 1.61 1.62 1.63 1.6 16 1.65 1.66 1.67 1.68 1.69 1.70 1.71 1.72 1.74 1.7 17 1.76 1.77 1.78 1.79 1.80 1.81 1.82 1.88 1.84 1.8 18 1.96 1.97 1.98 1.99 2.00 2.01 2.02 2.03 2.05 2.0 20 2.07 2.08 2.09 2.10 2.11 2.12 2.13 2.14 2.15 <	11	1.14	1.15	1.16	1.17	1.18	1.19	1.20	1.91	1.22	1.28
13 1.34 1.35 1.36 1.37 1.38 1.39 1.40 1.42 1.43 1.43 1.44 1.45 1.46 1.47 1.48 1.49 1.50 1.51 1.52 1.53 1.53 1.51 1.52 1.53 1.53 1.51 1.52 1.53 1.53 1.51 1.52 1.53 1.63 1.63 1.63 1.63 1.63 1.63 1.63 1.63 1.63 1.61 1.62 1.63 1.61 1		1	1	4	•				1		1.33
14 1.45 1.46 1.47 1.48 1.49 1.50 1.51 1.52 1.53 1.58 15 1.55 1.56 1.57 1.58 1.59 1.60 1.61 1.62 1.68 1.68 16 1.65 1.66 1.67 1.68 1.69 1.70 1.71 1.72 1.74 1.7 17 1.76 1.77 1.78 1.79 1.80 1.81 1.82 1.83 1.84 1.8 18 1.86 1.87 1.88 1.89 1.90 1.91 1.92 1.93 1.94 1.5 19 1.96 1.97 1.98 1.99 2.00 2.01 2.02 2.03 2.05 2.0 20 2.07 2.08 2.09 2.10 2.11 2.12 2.18 2.14 2.15 2.1 21 2.17 2.18 2.19 2.20 2.21 2.22 2.28 2.24 2.25 2.5 2.2 2.27 2.28 2.29 2.80 2.81 2.42 </td <td></td> <td>II.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1</td> <td>1.44</td>		II.								1	1.44
15 1.55 1.56 1.57 1.58 1.59 1.60 1.61 1.62 1.68 1.67 16 1.65 1.66 1.67 1.68 1.69 1.70 1.71 1.72 1.74 1.7 17 1.76 1.77 1.78 1.79 1.80 1.81 1.82 1.88 1.84 1.8 18 1.86 1.87 1.88 1.89 1.90 1.91 1.92 1.93 1.94 1.9 19 1.96 1.97 1.98 1.99 2.00 2.01 2.02 2.03 2.05 2.0 20 2.07 2.08 2.09 2.10 2.11 2.12 2.18 2.14 2.15 2.1 21 2.17 2.18 2.19 2.20 2.21 2.22 2.28 2.24 2.25 2.1 22 2.27 2.28 2.29 2.80 2.81 2.42 2.43 2.44 2.42 2.43 2.44 2.42 2.43 2.44 2.45 2.46 2.42 2.43				1				1	i .	1	1.54
17 1.76 1.77 1.78 1.79 1.80 1.81 1.82 1.88 1.84 1.8 18 1.86 1.87 1.88 1.89 1.90 1.91 1.92 1.93 1.94 1.5 19 1.96 1.97 1.98 1.99 2.00 2.01 2.02 2.03 2.05 2.0 20 2.07 2.08 2.09 2.10 2.11 2.12 2.13 2.14 2.15 2.1 21 2.17 2.18 2.19 2.20 2.21 2.22 2.23 2.24 2.25 2.2 22 2.27 2.28 2.29 2.80 2.81 2.32 2.83 2.34 2.86 2.5 23 2.38 2.39 2.40 2.41 2.42 2.43 2.44 2.45 2.46 2.4 2.48 2.49 2.50 2.51 2.52 2.53 2.54 2.55 2.56 2.5 2.5 2.58 2.59 2.60 2.61 2.62 2.63 2.64 </td <td></td> <td>l I</td> <td>1</td> <td></td> <td></td> <td>•</td> <td></td> <td>1</td> <td>i e</td> <td>1</td> <td>1.64</td>		l I	1			•		1	i e	1	1.64
17 1.76 1.77 1.78 1.79 1.80 1.81 1.82 1.88 1.84 1.8 18 1.86 1.87 1.88 1.89 1.90 1.91 1.92 1.93 1.94 1.5 19 1.96 1.97 1.98 1.99 2.00 2.01 2.02 2.03 2.05 2.0 20 2.07 2.08 2.09 2.10 2.11 2.12 2.13 2.14 2.15 2.1 21 2.17 2.18 2.19 2.20 2.21 2.22 2.23 2.24 2.25 2.2 22 2.27 2.28 2.29 2.80 2.81 2.32 2.83 2.34 2.86 2.5 23 2.38 2.39 2.40 2.41 2.42 2.43 2.44 2.45 2.46 2.4 2.48 2.49 2.50 2.51 2.52 2.53 2.54 2.55 2.56 2.5 2.5 2.58 2.59 2.60 2.61 2.62 2.63 2.64 </td <td>16</td> <td>1.85</td> <td>1.66</td> <td>1.67</td> <td>1.68</td> <td>1.69</td> <td>1.70</td> <td>1.71</td> <td>1.79</td> <td>1.74</td> <td>1.75</td>	16	1.85	1.66	1.67	1.68	1.69	1.70	1.71	1.79	1.74	1.75
18 1.86 1.87 1.88 1.89 1.90 1.91 1.92 1.93 1.94 1.92 19 1.96 1.97 1.98 1.99 2.00 2.01 2.02 2.03 2.05 2.0 20 2.07 2.08 2.09 2.10 2.11 2.12 2.18 2.14 2.15 2.1 21 2.17 2.18 2.19 2.20 2.21 2.22 2.28 2.24 2.25 2.5 22 2.27 2.28 2.29 2.80 2.81 2.32 2.83 2.34 2.86 2.8 23 2.39 2.40 2.41 2.42 2.43 2.44 2.45 2.46 2.4 2.4 2.48 2.49 2.50 2.51 2.52 2.53 2.54 2.55 2.56 2.5 2.5 2.53 2.59 2.60 2.61 2.62 2.63 2.64 2.65 2.66 2.6 2.6 2.69 2.70 2.71 2.72 3.73 3.74 2.75<	-		1	1	1				l		1.85
19 1.96 1.97 1.98 1.99 2.00 2.01 2.02 2.03 2.05 2.05 20 2.07 2.08 2.09 2.10 2.11 2.12 2.13 2.14 2.15 2.1 21 2.17 2.18 2.19 2.20 2.21 2.22 2.28 2.24 2.25 2.5 22 2.27 2.28 2.29 2.80 2.81 2.32 2.83 2.34 2.86 2.8 23 2.38 2.39 2.40 2.41 2.42 2.43 2.44 2.45 2.46 2.4 24 2.48 2.49 2.50 2.51 2.52 2.53 2.54 2.55 2.56 2.6 25 2.58 2.59 2.60 2.61 2.62 2.63 2.64 2.65 2.66 2.6 26 2.69 2.70 2.71 2.72 3.73 3.74 2.75 2.76 2.77 2.7 2.79 2.80 2.81 2.82 2.83 2.84 2.85 2.86 2.87 2.5 28 2.89 2.90 2.91 2.92 2.93 2.94 2.95 2.96		1	1			1		1	•	1	1.95
20 2.07 2.08 2.09 2.10 2.11 2.12 2.18 2.14 2.15 2.1 21 2.17 2.18 2.19 2.20 2.21 2.22 2.28 2.24 2.25 2.5 22 2.27 2.28 2.29 2.80 2.81 2.32 2.83 2.34 2.86 2.8 23 2.38 2.39 2.40 2.41 2.42 2.43 2.44 2.45 2.46 2.4 24 2.48 2.49 2.50 2.51 2.52 2.53 2.54 2.55 2.56 2.6 25 2.58 2.59 2.60 2.61 2.62 2.63 2.64 2.65 2.66 2.6 26 2.69 2.70 2.71 2.72 2.73 3.74 2.75 2.76 2.77 2.7 27 2.79 2.80 2.81 2.82 2.83 2.84 2.85 2.86 2.87 2.5 28 2.89 2.90 2.91 2.92 2.93 2.94 2.95 2.96 2.97 2.1 29 3.00 3.01 3.02 3.03 3.04 3.05 3.06 <			1	1	1	1				1	2.06
22 2.27 2.28 2.29 2.80 2.51 2.32 2.83 2.34 2.86 2.5 23 2.39 2.40 2.41 2.42 2.43 2.44 2.45 2.46 2.4 24 2.48 2.49 2.50 2.51 2.52 2.53 2.54 2.55 2.56 2.56 25 2.59 2.60 2.61 2.62 2.63 2.64 2.65 2.66 2.6 26 2.69 2.70 2.71 2.72 2.73 2.74 2.75 2.76 2.77 2.7 27 2.79 2.80 2.81 2.82 2.83 2.94 2.85 2.86 2.87 2.6 28 2.89 2.90 2.91 2.92 2.93 2.94 2.95 2.96 2.97 2.1 29 3.00 3.01 3.02 3.03 3.04 3.05 3.06 3.07 3.08 3.1 31		1		1		l.					2.16
22 2.27 2.28 2.29 2.80 2.81 2.32 2.83 2.34 2.86 2.5 23 2.39 2.40 2.41 2.42 2.43 2.44 2.45 2.46 2.46 24 2.48 2.49 2.50 2.51 2.52 2.53 2.54 2.55 2.56 2.56 25 2.59 2.60 2.61 2.62 2.63 2.64 2.65 2.66 2.6 26 2.69 2.70 2.71 2.72 2.73 2.74 2.75 2.76 2.77 2.7 27 2.79 2.80 2.81 2.82 2.83 2.94 2.85 2.86 2.87 2.6 28 2.89 2.90 2.91 2.92 2.93 2.94 2.95 2.96 2.97 2.1 29 3.00 3.01 3.02 3.03 3.04 3.05 3.06 3.07 3.08 3.1 3	91	2 17	2.18	9.10	9.90	9.91	9.92	2 22	9.94	9.95	2.26
23 2.38 2.39 2.40 2.41 2.42 2.43 2.44 2.45 2.46 2.46 2.42 2.43 2.44 2.45 2.46 2.46 2.45 2.55 2.56 2.56 2.56 2.56 2.55 2.56 2.66 2.67 2.77 2.72 2.79 2.52 2.58 2.84 2.85 2.86 2.87 2.56 2.57 2.56 2.57 2.57 2.77 2.77 2.77 2.77 2.77 2.77 2.77 2.77 2.77 2.77 2.77 2.77 2.77 2.77 2.79 2.98 2.94 2.95 2		1				i .		4	I.	1	2.87
24 2.48 2.49 2.50 2.51 2.52 2.53 2.54 2.55 2.56 2.56 25 2.58 2.59 2.60 2.61 2.62 2.63 2.64 2.65 2.66 2.66 26 2.69 2.70 2.71 2.72 2.73 2.74 2.75 2.76 2.77 2.7 27 2.79 2.80 2.81 2.82 2.88 2.84 2.85 2.86 2.87 2.8 28 2.89 2.90 2.91 2.92 2.93 2.94 2.95 2.96 2.97 2.4 29 3.00 3.01 3.02 3.03 3.04 3.05 3.06 3.07 3.08 3.4 30 3.10 3.11 3.12 3.13 3.14 3.15 3.16 3.17 3.18 3.1 31 3.20 3.21 3.22 3.23 3.24 3.25 3.26 3.27 3.28 3.3 32 3.31 3.32 3.83 3.84 3.85 3.86 3.87 3.88 3.39 3.3 34 3.51 3.52 3.53 3.54 3.45 3.46 3.47			1		I .	1		1	1	1	2.47
25 2.53 2.59 2.60 2.61 2.62 2.63 2.64 2.65 2.66 2.6 26 2.69 2.70 2.71 2.72 2.73 2.74 2.75 2.76 2.77 2.7 27 2.79 2.80 2.81 2.82 2.88 2.84 2.85 2.86 2.87 2.5 28 2.89 2.90 2.91 2.92 2.98 2.94 2.95 2.96 2.97 2.4 29 3.00 3.01 3.02 3.03 3.04 3.05 3.06 3.07 3.06 3.6 30 3.10 3.11 3.12 3.13 3.14 3.15 3.16 3.17 3.18 3.1 31 3.20 3.21 3.22 3.23 3.24 3.25 3.26 3.27 3.28 3.3 32 3.31 3.32 3.83 3.34 3.35 3.86 3.87 3.88 3.39 <td< td=""><td></td><td>11</td><td>1</td><td></td><td>1</td><td>1</td><td></td><td></td><td></td><td>1</td><td>2.57</td></td<>		11	1		1	1				1	2.57
27 2.79 2.80 2.81 2.82 2.83 2.84 2.85 2.86 2.87 2.87 28 2.89 2.90 2.91 2.92 2.93 3.94 2.95 2.96 2.97 2.1 29 3.00 3.01 3.02 3.03 3.04 8.05 3.06 3.07 3.06 3.0 30 3.10 3.11 3.12 3.13 3.14 3.15 3.16 3.17 3.18 3.1 31 3.20 3.21 3.22 3.23 3.24 3.25 3.26 3.27 3.28 3.2 32 3.31 3.82 3.83 3.94 3.85 3.86 3.87 3.88 3.39 3.2 33 3.41 3.42 3.43 3.44 3.45 3.46 3.47 3.48 3.49 3.4 34 3.51 3.52 3.53 3.54 3.55 3.56 3.57 3.58 3.69 <t< td=""><td></td><td></td><td></td><td>i</td><td>I</td><td></td><td></td><td></td><td>1</td><td>1</td><td>2.68</td></t<>				i	I				1	1	2.68
27 2.79 2.80 2.81 2.82 2.83 2.84 2.85 2.86 2.87 2.87 28 2.89 2.90 2.91 2.92 2.93 3.94 2.95 2.96 2.97 2.1 29 3.00 3.01 3.02 3.03 3.04 3.05 3.06 3.07 3.08 3.0 30 3.10 3.11 3.12 3.13 3.14 3.15 3.16 3.17 3.18 3.1 31 3.20 3.21 3.22 3.23 3.24 3.25 3.26 3.27 3.28 3.2 32 3.31 3.82 3.83 3.34 3.35 3.36 3.87 3.88 3.39 3.2 33 3.41 3.42 3.43 3.44 3.45 3.46 3.47 3.48 3.49 3.4 34 3.51 3.52 3.53 3.54 3.55 3.56 3.57 3.58 3.69 <t< td=""><td>26</td><td>2.60</td><td>2.70</td><td>2.71</td><td>2.72</td><td>9,78</td><td>9.74</td><td>2.75</td><td>2.78</td><td>2.77</td><td>2.78</td></t<>	26	2.60	2.70	2.71	2.72	9,78	9.74	2.75	2.78	2.77	2.78
28 2.89 2.90 2.91 2.92 2.93 3.94 2.95 2.96 2.97 2.1 29 3.00 3.01 3.02 3.03 3.04 3.05 3.06 3.07 3.06 3.07 30 3.10 3.11 3.12 3.13 3.14 3.15 3.16 3.17 3.18 3.1 31 3.20 3.21 3.22 3.23 3.24 3.25 3.26 3.27 3.28 3.2 32 3.31 3.32 3.83 3.34 3.35 3.36 3.37 3.88 3.39 3.3 33 3.41 3.42 3.43 3.44 3.45 3.46 3.47 3.48 3.49 3.4 34 3.51 3.52 3.53 3.54 3.55 3.56 3.57 3.58 3.69 3.70 3.68 35 3.62 3.63 3.64 3.65 3.66 3.67 3.68 3.69 <		l I		1	1			1			2.88
29 8.00 3.01 3.02 3.03 3.04 8.05 3.06 3.07 8.06 3.07 30 8.10 3.11 3.12 3.13 3.14 3.15 3.16 3.17 3.18 8.3 31 3.20 3.21 3.22 3.23 3.24 3.25 3.26 3.27 3.28 3.2 32 3.31 3.82 3.83 3.34 3.35 3.36 3.87 3.88 3.39 3.3 33 3.41 3.42 3.43 3.44 3.45 3.46 3.47 3.48 3.49 3.4 34 3.51 3.52 3.53 3.54 3.55 3.56 3.57 3.58 3.69 3.70 3. 35 3.62 3.63 3.64 3.65 3.66 3.67 3.68 3.69 3.70 3.		i I	1	1	II .			1	ı		2.98
30 8.10 8.11 8.12 3.13 3.14 8.15 3.16 3.17 3.18 8.3 31 3.20 8.21 8.22 8.23 8.24 8.25 8.26 3.27 8.28 3.3 32 3.31 3.82 3.83 8.34 8.35 3.36 8.87 3.88 3.39 3.3 33 3.41 3.42 3.48 8.44 8.45 3.46 3.47 3.48 3.49 2.4 34 3.51 3.52 3.53 3.54 3.55 3.56 3.57 3.58 3.69 3.70 3.49 35 8.62 8.63 3.64 3.65 3.66 3.67 3.68 3.69 3.70 3.49				1	1			ı		1	8.09
32 3.31 3.82 3.83 3.84 3.85 3.86 3.87 3.88 3.39 3.2 33 3.41 3.42 3.48 3.44 3.45 3.46 3.47 3.48 3.49 3.4 34 3.51 3.52 3.53 3.54 3.55 3.56 3.57 3.58 3.69 3.70 3.4 35 3.62 3.63 3.64 3.65 3.66 3.67 3.68 3.69 3.70 3.4		11	1 .					1	1		8.19
32 3.31 3.82 3.83 3.84 3.85 3.86 3.87 3.88 3.39 3.2 33 3.41 3.42 3.48 3.44 3.45 3.46 3.47 3.48 3.49 3.4 34 3.51 3.52 3.53 3.54 3.55 3.56 3.57 3.58 3.69 3.70 3.4 35 3.62 3.63 3.64 3.65 3.66 3.67 3.68 3.69 3.70 3.4	21	2 20	8 91	R 99	2 22	8.94	2 25	2 94	2 97	9.00	3.80
33 8.41 8.42 8.48 8.44 8.45 8.46 8.47 8.48 8.49 8.3 34 8.51 8.52 8.53 8.54 8.55 8.56 8.57 3.58 8.59 8.6 35 8.62 8.63 3.64 8.65 3.66 3.67 3.68 3.69 8.70 3.6			ì	1	1	1		1		1	8.40
34 3.51 3.52 3.53 3.54 3.55 3.56 3.57 3.58 3.59 3.69 35 3.62 3.63 3.64 3.65 3.66 3.67 3.68 3.69 3.70 3.			1	1	1				1	1	8.50
35 S.62 S.63 S.64 S.65 S.66 S.67 S.68 S.69 S.70 S.		H	1					1	1	1	8.60
		1)		1	1	1		1		1	8.7
		0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

		BA	ROME	TER:	645 ^{um.}	(from 6	342.51 t	o 647 .5	0).	
Centi- grade Degrees.			_	·	Tenths of	Degrees.				
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.08	Millim, 0.04	Millim. 0.05	Millim. 0.06	Millim.	Millim. 0.08	Millim.
1	0.10	0.11	0.12	0.14	0.15	0.16	0.17	0.18	0.19	0.20
2	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.30
8	0.31	0.32	0.38	0.84	0.85	0.36	0.37	0.89	0.40	0.41
4	0.42	0.48	0.44	0.45	0.46	. 0.47	0.48	0.49	0.50	0.51
5	0.52	0.58	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61
6	0.62	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.72
7	0.73	0.74	0.75	0.76	0.77	0.78	0.79	0.80	0.81	0.82
8	0.88	0.84	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.93
9	0.94	0.95	0.96	0.97	0.98	0.99	1.00	1.01	1.02	1.03
10	1.04	1.05	1.06	1.07	1.08	1.09	1.10	1.11	1.12	1.13
11	1.15	1.16	1.17	1.18	1.19	1.20	1.21	1.22	1.23	1.24
12	1.25	1.26	1.27	1.28	1.29	1.80	1.81	1.82	1.33	1.34
13	1.85	1.36	1.87	1.38	1.89	1.41	1.42	1.48	1.44	1.45
14	1.46	1.47	1.48	1.49	1.50	1.51	1.52	1.58	1.54	1.55
15	1.56	1.57	1.58	1.59	1.60	1.61	1.62	1.68	1.64	1.66
16	1.67	1.68	1.69	1.70	1.71	1.72	1.73	1.74	1.75	1.76
17	1.77	1.78	1.79	1.80	1.81	1.82	1.88	1.84	1.85	1.86
18	1.87	1.88	1.89	1.91	1.92	1.98	1.94	1.95	1.96	1.97
19	1.98	1.99	2.00	2.01	2.02	2.03	2.04	2.05	2.06	2.07
20	2.08	2.09	2.10	2.11	2.12	2.18	2.14	2.15	2.17	2.18
21	2.19	2.20	2.21	2.22	2.23	2.24	2.25	2.26	2.27	2.28
22	2.29	2.80	2.31	2.82	2.88	2.34	2.35	2.36	2.37	2.38
28	2.39	2.40	2.42	2.48	2.44	2.45	2.46	2.47	2.48	2.49
24	2.50	2.51	2.52	2.58	2.54	2.55	2.56	2.57	2.58	2.59
25	2.60	2.61	2.62	2.63	2.64	2.65	2.66	2.67	2.69	2.70
26	2.71	2.72	2.78	2.74	2.75	2.76	2.77	2.78	2.79	2.80
27	2.61	2.82	2.88	2.84	2.85	2.86	2.87	2.88	2.89	2.90
28	S.9 .	2.98	2.94	2.95	2.96	2.97	2.98	2.99	3.00	8.01
29	8.02	8.03	3.04	8.05	8.06	8.07	3.08	8.09	8.10	8.11
80	3.12	3.13	8.14	3.15	8.16	8.18	8.19	3.20	3.21	8.22
31	3.23	8.24	3.25	8.26	8.27	8.28	8.29	3.30	8.31	8.32
82	3.33	3.84	8.35	8.86	8.87	3.38	8.89	8.40	8.41	8.42
23	3.44	8.45	3.46	3.47	8.48	8.49	8.50	3.51	8.52	3.53
84	8.54	8.55	8.56	8.57	8.58	8.59	8.60	8.61	3.62	3.63
35	8.64	8.65	8.66	8.67	8.68	8.69	8.70	8.71	8.72	3.73
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

		В	AROMI	ETER :	650-	(from	647.51	to 652 .5	0).	
Centi- grade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
°	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.08	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.09
1	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.20
2	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.80
3	0.82	0.33	0.34	0.85	0.36	0.87	0.88	0.89	0.40	0.41
4	0.42	0.48	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.51
5	0.58	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61	0.62
6	0.63	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.72
7	0.73	0.75	0.76	0.77	0.78	0.79	0.80	0.81	0.82	0.88
8	0.84	0.85	0.86	0.87	0.88	0.89	0.90	0.91	0.92	0.93
9	0.94	0.96	0.97	0.98	0.99	1.00	1.01	1.02	1.03	1.04
10	1.05	1.06	1.07	1.08	1.09	1.10	1.11	1.12	1.18	1.14
11	1.15	1.17	1.18	1.19	1.20	1.21	1.22	1.28	1.24	1.25
12	1.26	1.27	1.28	1.29	1.80	1.31	1.82	1.38	1.34	1.35
13	1.36	1.87	1.89	1.40	1.41	1.42	1.43	1.44	1.45	1.46
14	1.47	1.48	1.49	1.50	1.51	1.52	1.53	1.54	1.55	1.56
15	1.57	1.58	1.60	1.61	1.62	1.68	1.64	1.65	1.66	1.67
16	1.68	1.69	1.70	1.71	1.72	1.78	1.74	1.75	1.76	1.77
17	1.78	1.79	1.81	1.82	1.88	1.84	1.85	1.86	1.87	1.88
18	1.89	1.90	1.91	1.92	1.93	1.94	1.95	1.96	1.97	1.98
19	1.99	2.00	2.01	2.03	2.04	2.05	2.06	2.07	2.08	2.09
20	2.10	2.11	2.12	2.13	2.14	2.15	2.16	2.17	2.18	2.19
21	2.20	2.21	2.22	2.24	2.25	2.26	2.27	2.28	2.29	2.30
22	2.31	2.32	2.83	2.84	2.35	2.26	2.37	2.38	2.29	2.40
23	2.41	2.42	2.43	2.44	2.46	2.47	2.48	2.49	2.50	2.51
24	2.52	2.58	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61
25	2.62	2.63	2.64	2.65	2.67	2.68	2.69	2.70	2.71	2.72
	9 700	901	9 84	9 140	ا	0.70	9 80	0.60	9.01	0.00
26	2.78	2.84	2.75	2.76	2.77	2.78	2.79	2.80	2.81	2.82
27	2.83 2.94	2.84 2.95	2.85 2.96	2.86 2.97	2.88 2.98	2.89 2.99	2.90 8.00	2.91	2.92 3.02	2.93
28 29	3.04	2.95 8.05	3.06	3.07	2.95 8.08	2.99 8.10	8.11	8.01 8.12	8.18	3.03 8.14
30	3.15	8.16	8.17	3.18	3.19	3.20	8.21	3.22	3.23	8.24
.	3.25	3.26	0.00	2 00			0.00		001	0.07
81		1	8.27	8.28	8.29	3.81	8.82	3.83	8.84	3.83
32	3.36 3.46	3.37	3.38 3.48	8.89	8.40	8.41	8.42	3.48	8.44	8.45
33 34	8.40	8.47 8.58	8.48	8.49 8.60	8.50 8.61	3-52 8-62	8.58 8.63	8.54 3.64	8.55 8.65	3.56 3.66
35	3.67	8.68	3-69	8.70	3.71	8.72	8.74	3.75	8.76	3.00 3.77
	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.
						_				

		В	AROME	TER:	655***	(from	652.51 t	o 657.5	0).	
Centi- grade Degrees.					Tenthe o	f Degrees.				
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.08	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim, 0.09	Millim. 0.10
1	0.11	0.12	0.18	0.14	0.15	0.16	0.17	0.18	0.19	0.20
2	0.21	0.22	0.23	0.24	0.25	0.26	0.28	0.29	0.30	0.31
8	0.82	0.88	0.84	0.85	0.86	0.87	0.38	0.39	0.40	0.41
4	0.42	0.48	0.44	0.46	0.47	0.48	0.49	0.50	0.51	0.52
5	0.58	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61	0.62
6	0.68	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.72	0.73
7	0.74	0.75	0.76	0.77	0.78	0.79	0.80	0.81	0.83	0.84
8	0.85	0.86	0.87	0.88	0.89	0.90	0.91	0.92	0.93	0.94
9	0.95	0.96	0.97	0.96	0.99	1.00	1.02	1.03	1.04	1.05
10	1.06	1.07	1.08	1.09	1.10	1.11	1.12	1.13	1.14	1.15
11	1.16	1.17	1.18	1.20	1.21	1.22	1.28	1.24	1.25	1.26
12	1.27	1.28	1.29	1.80	1.31	1.82	1.33	1.84	1.35	1.36
13	1.87	1.89	1.40	1.41	1.42	1.48	1.44	1.45	1.46	1.47
14	1.48	1.49	1.50	1.51	1.52	1.58	1.54	1.55	1.57	1.58
15	1.59	1.60	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.68
16	1.69	1.70	1.71	1.72	1.78	1.74	1.76	1.77	1.78	1.79
17	1.80	1.81	1.82	1.88	1.84	1.85	1.86	1.87	1.88	1.89
18	1.90	1.91	1.92	1.94	1.95	1.96	1.97	1.98	1.99	2.00
19	2.01	2.02	2.03	2.04	2.05	2.06	2.07	2.08	2.09	2.10
20	2.11	2.13	2.14	2.15	2.16	3.17	2.18	2.19	2.20	2.21
91	2.22	2.28	2.24	2.25	2.26	2.27	2.28	2.29	2.81	2.32
22	2.33	2.84	2.85	2.36	2.87	2.38	2.89	2.40	2.41	2.42
28	2.48	2.44	2.45	2.46	2.47	2.48	2.50	2.51	2.52	2.53
24	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.68
25	2.64	2.65	2.66	2.68	2.69	2.70	2.71	2.72	2.73	2.74
26	2.25	2.76	2.77	2.78	2.79	2.80	2.81	2.82	2.88	2.84
27	2.85	2.87	2.88	2.89	2.90	2.91	2.92	2.93	2.94	2.95
28	2.96	2.97	2.98	2.99	8.00	8.01	8.02	3.03	8.05	3.06
29	3.07	3.08	8.09	8.10	3.11	8.12	3.13	8.14	8.15	3.16
30	8.17	3.18	3.19	8.20	8.21	8.22	8.24	3.25	3.26	3.27
21	8.28	8.29	3.30	3.31	8.82	8.83	8.84	8-85	3.36	8.37
32	8.88	8.39	8.40	3.42	8.48	8.44	8.45	8.46	3.47	3.48
83	8.49	8.50	3.51	8.52	8.58	8.54	8.55	8.56	3.57	3.58
84	8.59	8.61	8.62	3.63	8.64	8.65	3.66	3.67	3.68	3.69
85	3.70	8.71	8.72	8.78	8.74	8.75	8.76	8.77	3.79	8.90
	0.	1.	2.	3.	4.	5,	6.	7.	8.	9.

		В	AROMI	ETER :	660mm	(from	657.51 t	o 662.5	0).	
Conti- grade Degrees.					Tenths of	Degrees.				
	6.	1.	2.	8.	4.	5.	6.	7.	8.	9.
°	Millim, 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.03	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.08	Millim. 0.09	Millim. 0.10
1	0.11	0.12	0.18	0.14	0.15	0.16	0.17	0.18	0.19	0.20
2	0.21	0.22	0.28	0.25	0.26	0.27	0.28	0.29	0.80	0.81
8	0.32	0.88	0.34	0.85	0.36	0.37	0.88	0.89	0.41	0.42
4	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.51	0.52
5	0.58	0.54	0.55	0.57	0.58	0.59	0.60	0.61	0.62	0.63
6	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.72	0.74
7	0.75	0.76	0.77	0.78	0.79	0.80	0.81	0.82	0.88	0.84
8	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.98	0.94	0.95
9	0.96	0.97	0.98	0.99	1.00	1.01	1.02	1.08	1.04	1.06
10	1.07	1.08	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.16
11	1.17	1.18	1.19	1.20	1.21	1.28	1.24	1.25	1.26	1.27
12	1.28	1.29	1.30	1.31	1.82	1.83	1.84	1.85	1.36	1.87
13	1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48
14	1.49	1.50	1.51	1.52	1.58	1.55	1.56	1.57	1.58	1.59
15	1.60	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.68	1.69
16	1.70	1.72	1.78	1.74	1.75	1.76	1.77	1.78	1.79	1.80
17	1.81	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91
18	1.92	1.93	1.94	1.95	1.96	1.97	1.98	1.99	2.00	2.01
19	2.02	2.04	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.12
20	2.13	2.14	2.15	2.16	2.17	2.18	2.19	2.21	2.22	2.28
21	2.24	2.25	2.26	2.27	2.28	2.29	2.80	2.81	2.32	2.88
22	2.84	2.35	2.87	2.38	2.89	2.40	2.41	2.42	2.43	2.44
23	2.45	2.46	2.47	2.48	2.49	2.50	2.51	2.58	2.54	2.55
24	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65
25	2.66	2.67	2.68	2.70	2.71	2.72	2.78	2.74	2.75	2.76
26	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.86	2.87
27	2.88	2.89	2.90	2.91	2.92	2.98	2.94	2.95	2.96	2.97
28	2.98	2.99	8.00	8.02	8.08	8.04	8.05	8.06	8.07	8.08
29	8.09	8.10	3.11	3.12	3.18	3.14	8.15	8.16	8.17	8.19
30	8.20	8.21	3.22	8.28	8.24	3.25	8.26	3.27	8.28	8.29
81	8.80	3.31	3.82	3.88	3.85	8.36	3.87	8.88	8.89	8.40
82	8.41	8.42	8.43	3.44	8.45	8.46	3.47	8.48	8.49	8.51
33	3.52	8.58	8.54	8.55	3.56	3.57	3.58	8.59	8.60	3.61
84	8.62	3.63	3.64	3.65	3.66	8.68	3.69	8.70	8.71	3.72
85	8.73	8.74	8.75	8.76	3.77	8.78	3.79	8.80	3.81	8.82
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROMI	ETER :	665***	(from	662.51	to 667.5	0).	
Centi- grade Degrees.					Tenths o	C Degrees.				
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
ő	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.08	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.08	Millim. 0.09	Millim. 0.10
1	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.20
2	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.30	0.31
8	0.82	0.33	0.34	0.35	0.37	0.88	0.39	0.40	0.41	0.42
4	0.48	0.44	0.45	0.46	0.47	0.48	0.49	0.51	0.52	0.53
5	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61	0.62	0.63
6	0.64	0.66	0.67	0.68	0.69	0.70	0.71	0.72	0.78	0.74
7	0.75	0.76	0.77	0.78	0.79	0.81	0.82	0.83	0.84	0.85
8	0.86	0.87	0.88	0.89	0.90	0.91	0.92	0.93	0.95	0.96
9	0.97	0.98	0.99	1.00	1.01	1.02	1.03	1.04	1.05	1.06
10	1.07	1.08	1.10	1.11	1.12	1.18	1.14	1.15	1.16	1.17
11	1.18	1.19	1.20	1.21	1.22	1.28	1.25	1.26	1.27	1.28
12	1.29	1.30	1.31	1.82	1.88	1.34	1.85	1.36	1.87	1.39
18	1.40	1.41	1.42	1.48	1.44	1.45	1.46	1.47	1.48	1.49
14	1.50	1.51	1.52	1.54	1.55	1.56	1.57	1.58	1.59	1.60
15	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.69	1.70	1.71
16	1.72	1.78	1.74	1.75	1.76	1.77	1.78	1.79	1.80	1.81
17	1.88	1.84	1.85	1.86	1.87	1.88	1.89	1.90	1.91	1.92
18	1.93	1.94	1.95	1.96	1.98	1.99	2.00	2.01	2.02	2.03
19	2.04	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.18	2.14
20	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.22	2.23	2.24
21	2.25	2.27	2.28	2.29	2.80	2.81	2.32	2.33	2.84	2.35
22	2.86	2.87	2.38	2.89	2.40	2.42	2.43	2.44	2.45	2.46
23	2.47	2.48	2.49	2.50	2.51	2.52	2.53	2.54	2.56	2.57
24	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65	2.66	2.67
25	2.68	2.69	2.71	2.72	2.78	2.74	2.75	2.76	2.77	2.78
26	2.79	2.80	2.81	2.82	2.88	2.84	2.86	2.87	2.88	2.89
27	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97	2.98	8.00
28	3.01	8.02	8.03	8.04	3.05	8.06	3.07	8.08	8.09	3.10
29	8.11	8.12	8.18	3.15	3.16	8.17	8.18	8.19	3.20	5.21
30	8.22	8.23	8.24	8.25	3.26	8.27	3.28	3.30	3.31	3.32
81	8.33	3.84	3.35	8.86	3.37	8.88	8-89	8.40	3-41	3.42
32	8.44	8.45	8.46	8.47	3.48	3.49	3.50	3.51	3.52	8.53
33	8.54	8.55	8.56	8.57	3.59	8.60	8.61	3.62	3.63	3.64
34	8.65	8.66	8.67	8.68	3.69	8.70	3.71	3.72	3.74	3.75
85	8.76	8.77	3-78	8.79	8.80	8.81	8.82	3.88	3.84	3.85
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROME	TER :	670 ^{mm}	(from	667.51 (o 672 .5	0.)	
Centi- grade Dogrece.					Tenths o	f Degrees.				•
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
ů	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.03	Millim. 0.04	Millim. 0.05	Millim. 0.07	Millim. 0.08	Millim. 0.09	Millim. 0.10
1	0.11	0.12	0.18	0.14	0.15	0.16	0.17	0.18	0.20	0.21
2	0.22	0.28	0.24	0.25	0.26	0.27	0.28	0.29	0.30	0.81
8	0.32	0.34	0.85	0.86	0.87	0.88	0.89	0.40	0.41	0.42
4	0.43	0.44	0.45	0.47	0.48	0.49	0.50	0.51	0.52	0.53
5	0.54	0.55	0.56	0.57	0.58	0.60	0.61	0.62	0.68	0.64
6	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.73	0.74	0.75
7	0.76	0.77	0.78	0.79	0.80	0.81	0.82	0.88	0.84	0.85
8	0.87	0.88	0.89	0.90	0.91	0.92	0.93	0.94	0.95	0.96
9	0.97	0.98	1.00	1.01	1.02	1.08	1.04	1.05	1.06	1.07
· 10	1.08	1.09	1.10	1.11	1.13	1.14	1.15	1.16	1.17	1.18
11	1.19	1.20	1.21	1.22	1.23	1.24	1.25	1.27	1.28	1.29
12	1.80	1.31	1.32	1.83	1.84	1.35	1.86	1.87	1.38	1.40
13	1.41	1.42	1.48	1.44	1.45	1.46	1.47	1.48	1.49	1.50
14	1.51	1.58	1.54	1.55	1.56	1.57	1.58	1.59	1.60	1.61
15	1.62	1.63	1.64	1.66	1.67	1.68	1.69	1.70	1.71	1.72
16	1.78	1.74	1.75	1.76	1.77	1.78	1.80	1.81	1.82	1.83
17	1.84	1.85	1.86	1.87	1.88	1.89	1.90	1.91	1.92	1.94
18	1.95	1.96	1.97	1.98	1.99	2.00	2.01	2.02	2.03	2.04
19	2.06	2.07	2.08	2.09	2.10	2.11	2.12	2.18	2.14	2.15
20	2.16	2.17	2.18	2.20	2.21	2.22	2.23	2.24	2.25	2.26
21	2.27	2.28	2.29	2.30	2.31	2.83	2.84	2.35	2.36	2.87
22	2.38	2.89	2.40	2.41	2.42	2.43	2.44	2.46	2.47	2.48
23	2-49	2.50	2.51	2.52	2.58	2.54	2.55	2.56	2.57	2.59
24	2.60	2.61	2.62	2.68	2.64	2.65	2.66	2.67	2.68	2.69
25	2.70	2.71	2.78	2.74	2.75	2.76	2.77	2.78	2.79	2.80
26	2-81	2.82	2.88	2.84	2.86	2.87	2.88	2.89	2.90	2.91
27	2.92	2.93	2.94	2.95	2.96	2.97	2.99	3.00	8.01	8,02
28	8-03	8.04	3.05	3.06	8.07	8.08	3.09	8.10	8.11	3.13
29	8-14	8.15	3.16	8.17	8.18	8.19	8.20	8.21	8.22	8.28
30	3.24	3.26	3.27	3.28	8.29	8.80	8.31	8.32	8.88	3.34
31	8-85	3-36	8.37	3.39	3.40	8.41	8-42	8-48	8.44	8.45
32	3.46	8.47	3.48	3.49	8.50	3.52	8.58	3.54	8.55	8.56
33	8.57	3.58	3.59	8.60	3.61	8.62	8.63	8.64	B.66	3.67
84	3-68	8.69	8.70	8.71	8.72	3.78	8.74	3.75	8.76	3 77
35	3.79	8.80	3.81	3.82	3.88	3.84	3.85	8.86	3.87	3.88
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

		В	AROME	ETER:	675	(from	572.51 t	o 67 7.5	0).	
Centi- grade Degrees.					Tenths of	Degrees.				
,	6.	1.	2.	8.	4.	5.	6.	7.	8.	9.
°	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.08	Millim. 0.04	Millim. 0.05	Millim. 0.07	Millim. 0.08	Millim. 0.09	Millim. 0.10
1	0.11	0.12	0.18	0.14	0.15	0.16	0.17	0.19	0.20	0.21
2	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.81	0.32
8	0.38	0.84	0.85	0.86	0.87	0.88	0.39	0.40	0.41	0.42
4	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.53
5	0.54	0.56	0.57	0.58	0.59	0.60	0.61	0.62	0.63	0.64
6	0.65	0.66	0.68	0.69	0.70	0.71	0.72	0.78	0.74	0.75
7	0.76	0.77	0.78	0.80	0.81	0.82	0.88	0.84	0.85	0.86
8	0.87	0.88	0.89	0.90	0.92	0.93	0.94	0.95	0.96	0.97
9	0.98	0.99	1.00	1.01	1.02	1.08	1.05	1.06	1.07	1.08
10	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.17	1.18	1.19
11	1.20	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.29	1.30
12	1.81	1.82	1.83	1.84	1.35	1.86	1.37	1.88	1.29	1.41
18	1.42	1.48	1.44	1.45	1.46	1.47	1.48	1.49	1.50	1.51
14	1.53	1.54	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.62
15	1.68	1.65	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.73
16	1.74	1.75	1.76	1.78	1.79	1.80	1.81	1.82	1.88	1.84
17	1.85	1.86	1.87	1.88	1.90	1.91	1.92	1.93	1.94	1.95
18	1.96	1.97	1.98	1.99	2.00	2.02	2.08	2.04	2.05	2.06
19	2.07	2.08	2.09	2.10	2.11	2.12	2.14	2.15	2.16	2.17
20	2.18	2.19	2.20	2.21	2.22	2.28	2.24	2.26	2.27	2.28
21	2.29	2.30	2.81	2.82	2.33	2.84	2.35	2.86	2.88	2.39
22	2.40	2.41	2.42	2.48	2.44	2.45	2.46	2.47	2.48	2.49
28	2.51	2.52	2.58	2.54	2.55	2.56	2.57	2.58	2.59	2.60
24	2.61	2.68	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.71
25	2.72	2.78	2.75	2.76	2.77	2.78	2.79	2.80	2-81	2.82
26	2.83	2.84	2.85	2.87	2.88	2.89	2.90	2.91	2.92	2.93
27	2.94	2.95	2.96	2.97	2.99	8.00	3.01	8.02	3.08	3.04
28	8.05	8.06	8.07	8.08	8.09	3.10	3.12	8.13	8-14	3.15
29	8.16	8.17	8.18	3.19	8.20	3.21	8.22	8.24	3.25	3.26
30	8.27	3.28	3.29	3.30	8.81	3.32	8.88	8.84	8-86	8.37
31	8.88	8.39	3.40	8.41	3.42	3.48	8.44	8-45	3.46	3.48
82	3.49	8.50	8.51	8.52	3.58	3.54	8.55	8.56	8-57	3.5 8
33	3.60	3.61	8.62	8.63	8.64	8.65	8.66	8.67	8.68	2.6 9
34	8.70	8.72	8.78	3.74	8.75	3.76	3.77	8.78	8.79	3.80
85	8.81	8.82	8.88	3.85	3.86	8.87	3.88	8.89	3.90	8.91
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

		В.	AROMI	ETER:	680	(from (677.51 t	o 682.5	0).	
Centi- grade Degrees.					Tenths o	f Dogress.				
	6.	1.	2.	3.	4.	5.	6.	7.	8.	9.
°	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.08	Millim 0.04	Millim. 0.05	Millim. 0.07	Millim. 0.08	Millim. 0.09	Millim. 0.10
1	0.11	0.12	0.18	0.14	0.15	0.16	0.18	0.19	0.20	0.21
2	0.22	0.28	0.24	0.25	0.26	0.27	0.29	0.80	0.81	0.82
8	0.33	0.84	0.35	0.36	0.87	0.88	0.40	0.41	0.42	0.48
4	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.52	0.58	0.54
ii 5	0.55	0.56	0.57	0.58	0.59	0.60	0.61	0.68	0.64	0.65
6	0.66	0.67	0.68	0.69	0.70	0.71	0.72	0.74	0.75	0.76
7	0.77	0.78	0.79	0.80	0.81	0.82	0.88	0.85	0.86	0.87
9 8	0.88	0.89	0.90	0.91	0.92	0.98	0.94	0.95	0.97	0.98
9	0.99	1.00	1.01	1.02	1.08	1.04	1.05	1.06	1.08	1.09
10	1.10	1.11	1.12	1.18	1.14	1.15	1.16	1.17	1.19	1.20
11	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.29	1.80	1.31
12	1.82	1.88	1.84	1.85	1.86	1.87	1.38	1.39	1.40	1.42
13	1.43	1.44	1.45	1.46	1.47	1.48	1.49	1.50	1.51	1.58
14	1.54	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.62	1.64
15	1.65	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.73	1.75
_										
16	1.76	1.77	1.78	1.79	1.80	1.81	1.82	1.88	1.84	1.85
17	1.87	1.88	1.89 2.00	1.90	1.91	1.92 2.03	1.93	1.94	1.95	1.96
18 19	1.98 2.09	1.99 2.10	2.11	2.01 2.12	2.02 2.13	2.14	2.04 2.15	2.05 2.16	2.06 2.17	2.07 2.18
20	2.20	2.21	2.22	2.28	2.24	2.25	2.26	2.27	2.28	2.29
21	2.30	2.32	2.88	2.84	2.35	2.86	2.87	2.88	2.89	2.40
22	2.41	2.48	2.44	2.45	2.46	2.47	2.48	2.49	2.50	2.51
23	2.52	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61	2.62
24	2.63	2.65	2.66	2.67	2.68	2.69	2.70	2.71	2.72	2.78
25	2.74	2.75	2.77	2.78	2.79	2.80	2.81	2.82	2.88	2.84
26	2.85	2.86	2.88	2.89	2.90	2.91	2.92	2.98	2.94	2.95
27	2.96	2.97	2.99	3.00	3.01	3.02	3.08	3.04	8.05	8.06
28	8.07	8.08	3.10	8.11	3.12	3.18	8.14	8.15	3.16	8.17
29	3.18	3.19	8.20	8.22	8.28	8.24	8.25	3.26	3.27	8.28
30	3.29	8.80	3.31	8.88	8.84	3.85	3.36	8.37	3.88	3.39
31	8.40	8-41	8.42	3.44	3.45	8.46	3.47	3.48	8.49	8.50
32	3.51	8.52	8.53	8.54	3.56	8.57	3.58	3.59	8.60	8.61
33	3.62	3.63	8.64	8.65	8.67	3.68	3.69	8.70	8.71	3.72
34	8.78	3.74	3.75	3.76	3.78	8.79	3.80	8.81	3.82	3.83
85	3.84	8.85	8.86	8.87	3.89	8.90	8.91	8.92	3.98	3.94
	0.	1.	2.	8.	4	5.	6.	7.	8.	9.

		В	AROMI	ETER :	685 	(from	682.51 (o 6 87.5	0).	
Centi- grade Dogrees.					Touthe o	f Degrees.				
	6.	1.	2.	8.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.03	Millim. 0.04	Millim. 0.06	Millim.	Millim.	Millim.	Millim. 0.10
0	0.00	0.01	0.02	0.00	0.04	0.00	0.02	0.00	0.00	0.10
1	0.11	0.12	0.13	0.14	0.15	0.17	0.18	0.19	0.20	0.21
2	0.22	0.23	0.24	0.25	0.27	0.28	0.29	0.80	0.81	0.32
8	0.88	0.84	0.85	0.36	0.88	0.89	0.40	0.41	0.42	0.43
4	0.44	0-45	0.46	0.48	0.49	0.50	0.51	0.52	0.53	0.54
5	0.55	0.56	0.57	0.59	9.60	0.61	0.62	0.63	0.64	0.65
6	0.66	0.67	0.69	0.70	0.71	0.72	0.78	0.74	0.75	0.76
7	0.77	0.78	0.80	0.81	0.82	0.88	0.84	0.85	0.86	0.87
8	0.88	0.90	0.91	0.92	0.98	0.94	0.95	0.96	0.97	0.98
9	1.00	1.01	1.02	1.08	1.04	1.06	1.06	1.07	1.08	1.09
10	1.11	1.12	1.18	1.14	1.15	1.16	1.17	1.18	1.19	1.21
ا ا		1.00					1.00			
1i	1.22	1.28 1.84	1.24	1.25	1.26	1.27	1.28	1.29	1.80	1.32
12	1.44	1.45	1.85	1.36 1.47	1.37	1.88 1.49	1.89 1.50	1.40	1.42	1.43
13	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.63	1.64	1.65
14 15	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.74	1.75	1.76
13	1.00	2.00	2.40	1.03	. 2.10		1	****	1510	
16	1.77	1.78	1.79	1.80	1.81	1.82	1.84	1.85	1-86	1.87
17	1.88	1.89	1.90	1.91	1.92	1.98	1.95	1.96	1.97	1.96
18	1.99	2.00	2.01	2.02	3.08	2.05	2.06	2.07	2.06	2.09
19	2.10	2.11	2.12	2.13	2.14	2.16	2.17	2.18	2.19	2.20
20	2.21	2.22	2.23	2.24	2.26	2.27	2.28	2.29	2.80	2.31
21	2.32	2.88	2.84	2.85	2.87	2.88	2.89	2.40	2.41	2.42
22	2.48	2.44	2.45	2.47	2.48	2.49	2.50	2.51	2.52	2.53
28	2.54	2.55	2.56	2.58	2.59	2.60	2.61	2.62	2.63	2.64
24	2.65	2.66	2.68	2.69	2.70	2/1	2.72	2.78	2.74	2.75
25	2.76	2.78	2.79	2.80	2.61	2.82	2.83	2.84	2.85	2.86
	9.05	2.89	2.90	2.91	2.92	2.98	2.94	9 AF		9.04
26	2.87	3.00	2.90 8.01	8.02	3.08	2.98 3.04	3.94 3.05	2-95 8-06	2.96 3.07	2.97 3.08
27 28	3.10	3.11	8.12	3.18	8.14	3.15	3.16	8.17	3.18	8.20
29	8.21	8-22	8.23	8.24	8.25	3.26	8.27	8.28	3.29	S.31
80	8.82	8.88	8.84	3.35	8.86	8.87	8.88	3-89	8.41	3.42
~							1		1	
31	8.48	8.44	8.45	3.46	8-47	3.48	8.49	3.59	8-52	8.53
82	8.54	3.55	8.56	3.57	8.58	8.59	3.60	3.62	8.63	3.64
88	8.65	8.66	8.67	3.68	3.69	8-70	8.71	3.73	8.74	8.75
84 85	3.76 3.87	3.77 3.88	8.78 3-89	8.79 8.90	3.80 3.91	3.61 3.92	8.82 3.94	3.84 3.95	8.85 8.96	3-86 3-97
-50	9-07	0.00			9:31	9.8A	0.74			9-51
	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.

		В.	AROME	TER:	690°	(from	687.51	to 692 .5	0).	
Centi- grade Degrees.					Tenthe o	f Dogress.				
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
°	Millim. 0.00	Millim. 0.01	Millim, 0.02	Millim. 0.08	Millim. 0.04	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.09	Millim. 0.10
1	0.11	0.12	0.13	0.14	0.16	0.17	0.18	0.19	0.20	0.21
2	0.22	0.28	0.25	0.26	0.27	0.28	0.29	0.80	0.31	0.82
8	0.83	0.35	0.36	0.37	0.88	0.89	0.40	0.41	0.42	0.43
4	0.45	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.53	0.55
5	0.56	0.57	0.56	0.59	0.60	0.61	0.62	0.63	0.65	0.66
. 6	0.67	0.68	0.69	0.70	0.71	0.72	0.74	0.75	0.76	0.77
7	0.78	0.79	0.80	0.81	0.82	0.84	0.85	0.86	0.87	0.88
8	0.89	0.90	0.91	0.92	0.94	0.95	0.96	0.97	0.98	0.99
9	1.00	1.01	1.02	1.04	1.05	1.06	1.07	1.08	1.09	1.10
10	1.11	1.12	1.14	1.15	1.16	1.17	1.18	1.19	1.20	1.21
11	1.28	1.24	1.25	1.26	1.27	1.28	1.29	1.80	1.81	1.38
12	1.84	1.85	1.36	1.87	1.88	1.39	1.40	1.41	1.48	1.44
13	1.45	1.46	1.47	1.48	1.49	1.50	1.51	1.58	1.54	1.55
14	1.56	1.57	1.58	1.59	1.60	1.61	1.68	1.64	1.65	1.66
15	1.67	1.68	1.69	1.70	1.72	1.78	1.74	1.75	1.76	1.77
16	1.78	1.79	1.80	1.82	1.88	1.84	1.85	1.86	1.87	1.88
17	1.99	1.90	1.92	1.98	1.94	1.95	1.96	1.97	1.96	1.99
18	2.00	2.02	2.08	2.04	2.05	2.06	2.07	2.08	2.09	2.10
19	2.12	2.18	2.14	2.15	2.16	2.17	2.18	2.19	2.21	2.22
20	2.23	2.24	2.25	2.26	2.27	2.28	2.29	2.81	2.82	2.88
21	2.34	2.85	2.86	2.87	2.88	2.89	2.41	2.42	2.43	2.44
22	2.45	2.46	2.47	2.48	2.49	2.51	2.52	2.58	2.54	2.55
23	2-56	2.57	2.58	2.59	2.61	2.62	2.63	2.64	2.65	2.66
24	2.67	2.68	2.70	2.71	2.72	2.73	2.74	2.75	2.76	2.77
25	2.78	2.80	2.81	2.82	2.88	2.84	2.85	2.86	2.87	2.88
26	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97	2.98	8.00
27	8.01	3.02	3.08	8.04	3.05	8.06	8.07	3.08	8.10	8.11
28	8.12	8.13	8.14	8.15	3.16	8.17	8.19	8.20	8.21	3.22
29	2.28	8.24	3.25	8.26	8.27	8.29	8.80	3.81	8.82	8.88
30	3.34	8.85	3.36	8.87	8.89	8.40	8.41	8.42	3.43	8.44
31	8.45	3.46	8.47	3,49	3.50	8.51	3.52	8-58	3.54	8.55
82	8.56	8.57	8.59	8.60	2.61	8.62	8.63	8.64	8.65	8.66
83	8.68	3.69	3.70	8.71	8.72	8.73	8.74	8.75	3.76	3.78
84	8.79	3.80	8.81	3.82	8.83	8.84	8.85	8.86	8.88	3.89
35	3.90	3.91	8.92	8-93	8.94	8.95	8.96	3.98	8.99	4.00
	6.	1.	2.	8.	4.	5.	6.	7.	8.	9.

		В	AROME	ETER:	695 ^{mm} .	(from 6	92.51 t	o 697.5 (9).	
Centi- grade Degrees.					Tenths of	Degrees.				
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
°°	Millim. 0.00	Millim. 0.01	Millim.	Millim.	Millim 0.04	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim.	Millim 0.10
U	0.00	0.01	0.02	0.08	0.04	0.00	0.07	0.06	0.09	0.10
1	0.11	0.12	0.13	0.15	0.16	0.17	0.18	0.19	0.20	0.21
2	0.22	0.24	0.25	0.26	0.27	0.28	0.29	0.30	0.31	0.83
8	0.84	0.85	0. 36 0.47	0. 87 0.48	0.88	0.89 0.50	0.40	0.42	0.48 0.54	0.44
4 5	0.56	0.57	0.58	0.59	0.61	0.62	0.68	0.64	0.65	0.66
			}		5.52	3.32			5.155	5.55
6	0.67	0.68	0.70	0.71	0.72	0,78	0.74	0.75	0.76	0.77
7	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.89
8	0.90	0.91	0.92	0.98	0.94	0.95	0.96	0.98	0.99	1.00
9 10	1.01	1.02	1.08 1.14	1.04	1.05	1.07 1.18	1.08	1.09	1.10 1.21	1.11 1.22
	1	1.10	2.22	1.20			1	1120		1
11	1.23	1.25	1.26	1.27	1.28	1.29	1.80	1.31	1.82	1.33
12	1.85	1.36	1.87	1.88	1.89	1.40	1.41	1.42	1.44	1.45
13	1.46	1.47	1.48	1.49	1.50	1.51	1.52	1.54	1.55	1.56
14	1.57	1.58	1.59	1.60	1.61	1.68	1.64	1.65	1.66	1.67
15	1.68	1.69	1.71	1.72	1.78	1.74	1.75	1.76	1.77	1.78
16	1.79	1.81	1.82	1.83	1.84	1.85	1.86	1.87	1.88	1.90
17	1.91	1.92	1.93	1.94	1.95	1.96	1.97	1.99	2.00	2.01
18	2.02	2.03	2.04	2.05	2.06	2.08	2.09	2.10	2.11	2.12
19	2.13	2.14	2.15	2.16	2.18	2.19	2.20	2.21	2.22	2.23
20	2.24	2.25	2.27	2.28	2.29	2.30	2.31	2.32	2.83	2.84
21	2.36	2.37	2.88	2.29	2.40	2.41	2.42	2.48	2.45	2.46
22	2.47	2.48	2.49	2.50	2.51	2.52	2.53	2.55	2.56	2.57
23	2.58	2.59	2.60	2.61	2.62	2.64	2.65	2.66	2.67	2.68
24	2.69	2.70	2.71	2.78	2.74	2.75	2.76	2.77	2.78	2.79
25	2.80	2.82	2.88	2.84	2.85	2.86	2.87	2.88	2.89	2.91
26	2.92	2.98	2.94	2.95	2.96	2.97	2.98	3.00	3.01	8.02
27	8.03	8.04	8.05	3.06	3.07	8.08	8.10	3.11	3.12	3.13
28	8.14	8.15	3.16	8.17	8.19	8.20	3.21	3.22	3.23	3.24
29	3.25	8.26	3.28	3.29	3.80	3.31	3.32	8.38	8.84	3.35
80	3.37	3.38	8.89	8.40	8.41	8.42	3.48	8.44	8.45	3.47
81	8.48	3.49	3.50	3.51	3.52	8.58	3.54	3.56	8-57	3.58
32	3.59	8.60	8.61	8.62	8.63	3.65	8.66	8.67	3.68	3.69
88	3.70	8.71	3.72	8.74	8.75	3.76	8.77	3.78	8.79	3.90
84	3.81	8.88	3.84	3.85	3.86	8.87	8.88	3.89	3.90	3.91
35	3.93	8.94	8.95	8.96	3.97	8.98	3.99	4.00	4.02	4.03
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

		В	AROMI	ETER :	700°	(from	697.51 t	o 702.5	0).	
Centi- grade Degrees.					Tenths o	f Degrees.				
	6.	1.	9.	8.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
ů	0.00	0.01	0.02	0.03	0.05	0.06	0.07	0.08	0.09	0.10
	0.11	0.12	0.14	0.15	0.16	0.17	0.18	0.19	0.20	0.21
2	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.31	0.82	0.33
•	0.84	0.35	0.36	0.87	0.88	0.40	0.41	0.42	0.48	0.44
4	0.45	0.46	0.47	0.49	0.50	0.51	0.52	0.58	0.54	0.55
Б	0.56	0.53	0.59	0.60	0.61	0.62	0.68	0.64	0.66	0.67
6	0.68	0.69	0.70	0.71	0.72	0.73	0.75	0.76	0.77	0.78
7	0.79	0.80	0.81	0.82	0.84	0.85	0.86	0.87	0.88	0.89
8	0.90	0.92	0.98	0.94	0.95	0.96	0.97	0.96	0.99	1.01
9	1.02	1.08	1.04	1.03	1.06	1.07	1.06	1.10	1.11	1.12
10	1.13	1.14	1.15	1.16	1.17	1.19	1.20	1.21	1.22	1.23
n	1.24	1.25	1.27	1.28	1.29	1.80	1.81	1.32	1.83	1.84
12	1.36	1.87	1.88	1.39	1.40	1.41	1.42	1.43	1.45	1.46
13	1.47	1.48	1.49	1.50	1.51	1.58	1.54	1.55	1.56	1.57
14	1.58	1.59	1.60	1.62	1.63	1.64	1.65	1.66	1.67	1.68
15	1.69	1.71	1.72	1.78	1.74	1.75	1.76	1.77	1.79	1.80
1.5									2.112	1.00
16	1.81	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91
17	1.92	1.93	1.94	1.95	1.97	1.98	1.99	2.00	2.01	2.02
18	2.03	2.04	2.06	2.07	2.08	2.09	2.10	2.11	2.12	2.14
19	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.23	2.24	2.25
20	2.26	2.27	2.28	2.29	2.80	2.82	2.88	2.84	2.35	2.86
~										
21	2.37	2.38	2.40	2.41	2.42	2.48	2.44	2.45	2.46	2.47
22	2.49	2.50	2.51	2.52	2.58	2.54	2.55	2.56	2.58	2.59
23	2.60	2.61	2.62	2.63	2.64	2.66	2.67	2.68	2.69	2.70
24	2.71	2.72	2.78	2.75	2.76	2.77	2.78	2.79	2.80	2.81
25	2.82	2.84	2.85	2.86	2.87	2.88	2.89	2.90	2.91	2.93
					1					
26	2.94	2.95	2.96	2.97	2.98	2.99	3.01	8.02	8.03	8.04
27	8.05	3-06	8.07	8.08	8.10	8.11	8.12	8.18	3.14	8.15
28	3.16	8.17	3.19	3.20	8.21	8.22	3.28	8.24	8.25	8.27
29	8.28	8.29	3.30	8.81	3.82	8.38	8.84	8.36	3.87	\$.38
30	8.89	8.40	8.41	8.42	8.48	8.45	3.46	3.47	3.48	8.49
'	1	1	1		ł	l		1	l	
31 32 33 34	8.50	3.51	8.52	8.54	8.55	3.56	3.57	8.58	8.59	3.60
82	3.62	3.68	3.64	3.65	3.66	8.67	8.68	3.69	8.71	8.72
33	3.73	3.74	3.75	3.76	8.77	3.78	3.80	3.81	8.82	3.83
34	8.84	3.85	3.86	3.88	8.89	8.90	8.91	3.92	8.93	8.94
35	8.95	8.97	8-98	8.99	4.00	4.01	4.02	. 4.03	4.04	4.06
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

		В	AROME	ETER :	705	(from	702.51	to 70 7.5	0).	24-7-
Centi- grade Dogress.					Tenthe o	f Degrees.				
	0.	1.	2.	8.	4.	5.	6.	7.	s.	9.
°	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.08	Millim. 0.05	Millim, 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.09	Millim. 0-10
1	0.11	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.20	0.22
2	0.28	0.24	0.25	0.26	0.27	0.28	0.30	0.81	0.82	0 83
8	0.84	0.85	0.36	0.88	0.89	0.40	0.41	0.42	0.43	0.44
4	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.53	0.55	0.56
5	0.57	0.58	0.50	0.60	0.61	0.68	0.64	0.65	0.66	0.67
6	0.68	0.69	0.71	0.72	0.78	0.74	0.75	0.76	0.77	0.79
7	0.80	0.81	0.82	0.88	0.84	0.85	0.86	0.88	0.89	0.90
8	0.91	0.92	0.98	0.94	0.96	0.97	0.98	0.99	1.00	1.01
9	1.02	1.04	1.06	1.06	1.07	1.08	1.09	1.10	1.12	1.18
10	1.14	1.15	1.16	1.17	1.18	1.19	1.21	1.22	1.23	1.24
11	1.25	1.26	1.27	1.29	1.80	1.31	1.82	1.83	1.84	1.35
12	1.87	1.88	1.89	1.40	1.41	1.42	1.48	1.45	1.46	1.47
18	1.48	1.49	1.50	1.51	1.52	1.54	1.55	1.56	1.57	1.58
14	1.59	1.60	1.62	1.68	1.64	1.65	1.66	1.67	1.68	1.70
15	1.71	1.72	1.78	1.74	1.75	1.76	1.78	1.79	1.80	1.81
16	1.82	1.88	1.84	1.85	1.87	1.88	1.89	1.90	1.91	1.92
17	1.98	1.95	1.96	1.97	1.98	1.99	2.00	2.01	2.08	2.04
18	2.05	2.06	2.07	2.06	2.09	2.11	2.12	2.13	2.14	2.15
19	2.16	2.17	2.18	2.20	2.21	2.22	2.28	2.24	2.25	2.26
20	2.28	2.29	2.30	2.31	2.82	2.88	2.84	2.36	2.37	2.88
21	2.39	2.40	2.41	2.42	2.44	2.45	2.46	2.47	2.48	2.49
22	2.50	2.51	2.58	2.54	2.55	2.56	2.57	2.58	2.59	2.61
28	2.62	2.68	2.64	2.65	2.66	2.67	2.69	2.70	2.71	2.72
24	2.78	2.74	2.75	2.77	2.78	2.79	2.80	2.81	2.82	2.83
25	2.84	2.86	2.87	2.88	2.89	2.90	2.91	2.92	2.94	2.95
26	2.96	2.97	2.98	2.99	8.00	8.02	8.08	8.04	8.05	8.06
27	8.07	8.08	8.10	3.11	8.12	3.13	8.14	8.15	3.16	8.17
28	3.19	8.20	8.21	8.22	3.28	8.24	3.25	8.27	3.28	3.29
29	3.30	8.31	8.82	3.33	3.85	8.86	3.87	8.88	8.89	3.40
30	8.41	8.42	8.44	8.45	8.46	8.47	8.48	3.49	3.50	3.52
31	8.58	8.54	3.55	3.56	8.57	8.58	3.60	3-61	3.62	3.63
82	8.64	3.65	3.66	8.68	3.69	8.70	8.71	8.72	8.78	3.74
88	3.75	8.77	3.78	3.79	8.80	8.81	8.82	8.88	8.85	8.86
84	3.87	8.88	8.89	3.90	8.91	3.93	8.94	8.95	8.96	3.97
35	3.98	3.99	4.01	4.02	4.03	4.04	4.05	4.06	4.07	4.08
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

		В	AROME	TER :	710==-	(from 7	707.51 t	o 712.5	0).	
Centi- grade Degraes.					Tenthe of	f Degrees.			•	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.00	0.01	0.02	0.08	0.05	0.06	0.07	0.08	0.09	0.10
1	0.11	0.18	0.14	0.15	0.16	0.17	0.18	0.19	0.21	0.22
2	0.23	0.24	0.25	0.26	0.28	0.29	0.30	0.13	0.32	0.38
3	0.34	0.36	0.37	0.88	0.39	0.40	0.41	0.42	0.44	0.45
	0.46	0.47	0.48	0.49	0.50	0.52	0.58	0.54	0.55	0.56
4 5	0.57	0.58	0.60	0.61	0.62	0.63	0.64	0.65	0.86	0.68
"	7.07	0.00	J.00	0.01	U.U.	V.00	0.04	0.00	0.00	0.00
6	0.69	0.70	0.71	0.72	0.78	0.74	0.76	0.77	0.78	0.79
7	0.80	0.81	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.91
8	0.92	0.93	0.94	0.95	0.96	0.97	0.99	1.00	1.01	1.02
9	1.03	1.04	1.05	1.07	1.08	1.09	1.10	1.11	1.12	1.18
10	1.15	1.16	1.17	1.18	1.19	1.20	1.21	1.28	1.24	1.25
"				1120	,	2.20		2.20		2.50
11	1.26	1.27	1.28	1.29	1.31	1.32	1.33	1.84	1.85	1.36
12	1.38	1.89	1.40	1.41	1.42	1.48	1.44	1.46	1.47	1.48
13	1.49	1.50	1.51	1.52	1.54	1.55	1.56	1.57	1.58	1.59
14	1.60	1.62	1.63	1.64	1.65	1.66	1.67	1.68	1.70	1.71
15	1.72	1.78	1.74	1.75	1.76	1.79	1.79	1.80	1.81	1.82
1 10		2.70	1	1.75	20	1.70	1.75	1.50	1.01	1.02
16	1.88	1.84	1.86	1.87	1.88	1.89	1.90	1.91	1.98	1.94
17	1.95	1.96	1.97	1.98	1.99	2.01	2.02	2.06	2.04	2.05
18	2.06	2.07	2.09	2.10	2.11	2.12	2.13	2.14	2.15	2.17
19	2.18	2.19	2.20	2.21	2.22	2.28	2.25	2.26	2.27	2.28
20	2.29	2.80	2.81	2.88	2.84	2.85	2.36	2.37	2.38	2.40
	2.20	2.00		2.00	2.01	2.00	2.00	2-01	2.00	2.40
21	2.41	2.42	2.48	2.44	2.45	2.46	2.48	2.49	2.50	2.51
22	2.52	2.58	2.54	2.56	2.57	2.58	2.59	2.60	2.61	2.62
23	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.72	2.78	2.74
24	2.75	2.76	2.77	2.78	2.80	2.81	2.82	2.88	2.84	2.85
25	2.86	2.88	2.89	2.90	2.91	2.92	2.98	2.95	2.96	2.97
~										
26	2.98	2.99	8.00	8.01	8.08	8.04	8.05	8.06	8.07	8.08
27	8.09	8.11	8.12	3.18	8.14	8.15	8.16	8.17	8.19	8.20
28	8.21	8.22	3.28	8.24	8.25	8.27	3.28	3.29	8.80	3.31
29	8.32	3.83	3.35	8.86	3.87	8.88	3.89	8.40	8.41	8.48
30	8.44	8.45	3.46	8.47	8.48	8.50	8.51	8.52	8.58	8.54
31	3.55	8.56	3.58	8.59	8.60	8.61	8.62	8-63	8.64	3.66
	3.67	8.68	3.69	3.70	8.71	8.72	8.74	8.75	8.76	8.77
33 34	3.78	8.79	8.80	8.82	8.88	8.84	8.85	3.86	3.87	8.88
34	8.90	8.91	8.92	8.93	8.94	8.95	8.96	8.98	8.99	4.00
85	4.01	4.02	4.08	4.05	4.06	4.07	4.08	4.09	4.10	4.11
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

	BAROMETER: 715 (from 712.51 to 717.50).										
Centi- grade Dogress.					Tenths o	f Degrees.					
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
0	Millim.	Millim.	Millim.	Millim.	Millim	Millim.	Millim.	Millim.	Millim.	Millim.	
0	0.00	0.01	0.02	0.04	0.06	0.06	0.07	0.08	0.09	0.10	
1	0.12	0.18	0.14	0.15	0.16	0.17	0.18	0.20	0.21	0.22	
2	0.23	0.24	0.25	0.27	0.28	0.29	0.80	0.31	0.32	0.33	
8	0.35	0.86	0.87	0.38	0.89	0.40	0.42	0.43	0.44	0.45	
4	0.46	0.47	0.48	0.50	0.51	0.52	0.58	0.54	0.55	0.57	
5	0.58	0.59	0.60	0.61	0.62	0.63	0.65	0.66	0.67	0.68	
6	0.69	0.70	0.72	0.78	0.74	0.75	0.76	0.77	0.78	0.80	
7	0.81	0.82	0.88	0.84	0.85	0.87	0.88	0.89	0.90	0.91	
8	0.92	0.98	0.95	0.96	0.97	0.98	0.99	1.00	1.02	1.03	
9	1.04	1.05	1.06	1.07	1.08	1.10	1.11	1.12	1.18	1.14	
10	1.15	1.17	1.18	1.19	1.20	1.21	1.22	1.23	1.25	1.26	
	1.00	1.00	1.00	1 60	1.00	1 00					
11	1.27 1.88	1.28	1.29 1.41	1. 3 0 1.42	1.82	1.88 1.44	1.84	1.85	1.86	1.37	
12 13	1.50	1.51	1.52	1.58	1.55	1.56	1.45 1.57	1.47 1.58	1.48 1.59	1.49	
13	1.62	1.68	1.64	1.65	1.66	1.67	1.68	1.70	1.71	1.60 1.72	
15	1.78	1.74	1.75	1.77	1.78	1.79	1.80	1.81	1.82	1.83	
					24.0		1.00		1.02	1.00	
16	1.85	1.86	1.87	1.88	1.89	1.90	1.92	1.98	1.94	1.95	
17	1.96	1.97	1.98	2.00	2.01	2.02	2.03	2.04	2.05	2.07	
18	2.08	2.09	2.10	2.11	2.12	2.18	2.15	2.16	2.17	2.18	
19	2.19	2.20	2.22	2.28	2.24	2.25	2.26	2.27	2.28	2.30	
20	2.31	2.32	2.33	2.34	2.35	2.37	2.38	2.29	2.40	2.41	
21	2.42	2.48	2.45	2.46	2.47	2.48	2.49	2.50	2.52	2.53	
22	2.54	2.55	2.56	2.57	2.58	2.60	2.61	2.62	2.68	2.64	
28	2.65	2.67	2.68	2.69	2.70	2.71	2.72	2.74	2.75	2.76	
24	2.77	2.78	2.79	2.80	2.82	2.88	2.84	2.85	2.86	2.87	
25	2.89	2.90	2.91	2.92	2.98	2.94	2.95	2.97	2.98	2.99	
26	8.00	8.01	3.02	8.04	8.05	8.06	3.07	8.08	3.09	3.10	
27	8.12	3.13	8.14	8.15	3.16	8.17	8.19	8.20	8.21	8.22	
28	8.23	8.24	8.25	8.27	8.28	8.29	3.80	8.81	8.32	8.34	
29	8.85	8.36	8.37	3.38	8.89	3.40	8.42	8.43	8.44	8.45	
30	8.46	8.47	8.49	8.50	8.51	8.52	8.58	8.54	8.55	8.57	
.	3.58	9.50	- 00		8.62	8.64	0.65	9.64			
81 82	8.69	3.59 3.70	8.60 8.72	3.61 3.78	8.62 3.74	8.75	3.65 3.76	8.66 3.77	8.67 3.79	3.68 3.90	
33	8.81	3.70	3.83	8.84	3.74 3.85	3.87	3.88	3.89	8.90	8.91	
34	8.92	8.94	8.95	8.96	8.97	3.98	3.99	4.00	4.02	4.03	
35	4.04	4.05	4.06	4.07	4.09	4.10	4.11	4.12	4.18	4.14	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

	BAROMETER: 720- (from 717.51 to 722.50).											
Centi- grade Degrass.					Tenths o	f Degrees.						
	9.	1.	2.	3.	4.	5.	6,	7.	8.	9.		
°	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.03	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.09	Millim. 0.10		
1 2	0.12 0.23	0.18 0.24	0.14 0.26	0.15 0.27	0.16 0. 2 8	0.17 0.29	0.19 0. 3 0	0.20 0.81	0.21 0.88	0.22 0.34		
8	0.35	0.36	0.87	0.38	0.40	0.41	0.42	0.43	0.44	0.45		
4	0.46	0.43	0.49	0.50	0.51	0.52	0.58	0.55	0.56	0.57		
5	0.58	0.59	0.60	0.62	0.68	0.64	0.65	0.66	0.67	0.69		
6	0.70	0.71	0.73	0.78	0.74	0.76	0.77	0.78	0.79	0.80		
7	0.81	0.88	0.84	0.85	0.86	0.87	0.88	0.89	0.91	0.92		
8	0.93	0.94	0.95	0.96	0.98	0.99	1.00	1.01	1.02	1.03		
9	1.05	1.06	1.07	1.08	1.09	1.10	1.12	1.18	1.14	1.15		
10	1.16	1.17.	1.19	1,20	1.21	1.22	1.28	1.24	1.26	1.27		
.,	1.28	1.29	1.80	1.81	1.82	1.84	1.85	1.86	1.87	1.38		
11	1.39	1.41	1.42	1.48	1.44	1.45	1.46	1.48	1.49	1.50		
13	1.51	1.52	1.58	1.55	1.56	1.57	1.58	1.59	1.60	1.62		
14	1.63	1.64	1.65	1.66	1.67	1.69	1.70	1.71	1.72	1.78		
15	1.74	1.75	1.77	1.78	1.79	1.80	1.81	1.82	1.84	1.85		
		- **										
16	1.86	1.87	1.88	1.89	1.91	1.92	1.98	1.94	1.95	1.96		
17	1.98	1.99	2.00	2.01	2.02	2.08	2.05	2.06	2.07	2.06		
18	2.09	2.10	2.11	2.18	2.14	2.15	2.16	2.17	2.18	2.20		
19	2.21	2.22	2.23	2.24	2.25	2.27	2.28	2.29	2.80	2.81		
20	2.82	2.84	2.85	2.86	2.37	2.38	2.89	2.41	2.42	2.43		
	2.44	2.45	2.46	2.48	2.49	2.50	2.51	2.52	2.53	2.54		
21 22	2.44	2.57	2.40	2.59	2.60	2.61	2.63	2.64	2.65	2.66		
23	2.67	2.68	2.70	2.71	2.72	2.78	2.74	2.75	2.77	2.78		
24	2.79	2.80	2.81	2.82	2.84	2.85	2-86	2.87	2.88	2.89		
25	2.91	2.92	2.98	2.94	2.95	2.96	2.97	2.99	8.00	3.01		
26	3.02	3.03	8.04	8.06	8.07	3.06	8.09	8.10	8.11	8.18		
27	8.14	8- 15	3.16	8.17	3.18	8.20	8.21	3.22	3.23	8.24		
29	8.25	8.27	8.28	3.29	3.30	3.81	8-82	8.84	3.35	3.36		
29	3.87	3.88	8.89	8.40	3.42	8.48	8-44	3.45	8.46	8.47		
30	3.49	8.50	8.51	8.52	8.58	8.54	8-56	8.57	8.58	3.59		
31 32 33 34	8.60	8.61	8.68	8.64	2.65	8.66	8-67	8.68	8.70	3.71		
82	8.72	8.78	8.74	2.75	8.77	8.78	8.79	8.80	8.81	8.82		
33	3.88	8.85	8.86	3.87	8.88	8-89	8.90	8.92	8.98	3.94		
34	3.95	8.96	3.97	8.99	4.00	4.01	4.02	4.08	4.04	4.06		
35	4.07	4.08	4-09	4.10	4.11	4.13	4-14	4.15	4.16	4.17		
	0.	1.	2.	3.	4.	5.	Ġ,	7.	8.	9.		

	BAROMETER: 725 (from 722.51 to 727.50).											
Centigrade Dogrees.				_	Tenths o	f Degrees.						
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.		
°	Millim. 0.00	Millim. 0.01	Mittim, 0.02	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim, 0.09	Millim. 0.11		
1	0.12	0.18	0.14	0.15	0.16	0.18	0.19	0.20	0.21	0.22		
2	0.28	0.25	0.26	0.27	0.28	0.29	0.80	0.82	0.38	0.34		
8	0.85	0.36	0.87	0.89	0.40	0.41	0.42	0.48	0.44	0.46		
4	0.47	0.48	0.49	0.50	0.51	0.58	0.54	0.55	0.56	0.57		
5	0.59	0.60	0.61	0.62	0.68	0.64	0.66	0.67	0.68	0.69		
6	0.70	0.71	0.78	0.74	0.75	0.76	0.77	0.78	0.80	0.81		
7	0.82	0.83	0.84	0.85	0.87	0.88	0.89	0.90	0.91	0.92		
8	0.94	0.95	0.96	0.97	0.98	0.99	1.01	1.02	1.08	1.04		
9	1.05	1.06	1.08	1.09	1.10	1.11	1.12	1.14	1.15	1.16		
10	1.17	1.18	1.19	1.21	1.22	1.28	1.24	1.25	1.26	1.28		
11	1.29	1.80	1.31	1.82	1.88	1.35	1.86	1.87	1.88	1.39		
12	1.40	1.42	1.48	1.44	1.45	1.46	1.47	1.49	1.50	1.51		
13	1.52	1.58	1.54	1.56	1.57	1.58	1.59	1.60	1.61	1.63		
14	1.64	1.65	1.66	1.67	1.69	1.70	1.71	1.72	1.73	1.74		
15	1.76	1.77	1.78	1.79	1.80	1.81	1.88	1.84	1.85	1.86		
16	1.87	1.88	1.90	1.91	1.92	1.93	1.94	1.95	1.97	1.96		
17	1.99	2.00	2.01	2.02	2.04	2.05	2.06	2.07	2.08	2.09		
18	2.11	2.12	2.13	2.14	2.15	2.16	2.18	2.19	2.20	2.21		
19	2.22	2.28	2.25	2.26	2.27	2.28	2.29	2.81	2.82	2.33		
20	2.84	2.85	2.36	2.88	2.39	2.40	2.41	2.43	2.48	2.45		
21	2.46	2.47	2.48	2.49	2.50	2.52	2.58	2.54	2.55	2.56		
22	2.57	2.59	2.60	2.61	2.62	2.68	2.64	2.66	2.67	2.68		
23	2.69	2.70	2.71	2.78	2.74	2.75	2.76	2.77	2.78	2.80		
24	2.81	2.82	2.83	2.84	2.86	2.87	2.88	2.89	2.90	2.91		
25	2.93	2.94	2.95	2.96	2.97	2.98	8.00	8.01	3.02	3.06		
26	8.04	8.05	8.07	8.08	8.09	8.10	8.11	8-12	8.14	3.15		
27	8-16	8.17	8.18	8.19	8.21	8.22	3.23	8.24	3.25	3.26		
28	8.28	8.29	8.80	8.81	8.82	8.83	3.85	8.86	8.37	3.38		
29	8.89	8.41	3.42	8.48	8.44	8.45	8.46	8.48	8.49	8.50		
30	3.51	8.52	8.58	8.55	8.56	8.57	8.58	8.59	8.60	3.62		
81	8.63	8.64	8.65	8.66	8.67	8.69	8.70	8.71	8.72	8.73		
32	8.74	8.76	8.77	3.78	8.79	8.80	8.81	3.88	8.84	3.85		
88	3.86	8.87	3.88	3.90	8.91	8.92	3.93	8.94	8.96	3.97		
34	8.98	3.99	4.00	4.01	4.08	4.04	4.05	4.06	4.07	4.06		
35	4.10	4.11	4.12	4.18	4.14	4.15	4.17	4.18	4.19	4.20		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

	BAROMETER: 730 ^{mm} (from 727.51 to 732.50).												
Centi- grade Degrees.	Tenths of Degrees.												
	9.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
-	Millim.	Millim.	Millim.	Millim.	Millim,	Millim.	Millim.	Millim.	Millim.	Millim			
0	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.08	0.09	0.11			
1	0.12	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.21	0.22			
2	0.24	0.25	0.26	0.27	0.28	0.29	0.81	0.32	0.88	0.84			
3	0.35	0.87	0.88	0.39	0.40	0.41	0.42	0.44	0.45	0.46			
4	0.47	0.48	0.49	0.51	0.52	0.53	0.54	0.55	0.57	0.58			
5	0.59	0.60	0.61	0.62	0.64	0.65	0.66	0.67	0.68	0.70			
6	0.71	0.72	0.78	0.74	0.75	0.77	0.78	0.79	0.80	0.81			
7	0.82	0.84	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.93			
8	0.94	0.95	0.97	0.98	0.99	1.00	1.01	1.03	1.04	1.05			
9	1.06	1.07	1.08	1.10	1.11	1.12	1.13	1.14	1.15	1.17			
10	1.18	1.19	1.20	1.21	1.23	1.24	1.25	1.26	1.27	1.28			
11	1.30	1.81	1.32	1.83	1.84	1.35	1.87	1.88	1.39	1.40			
12	1.41	1.43	1.44	1.43	1.46	1.47	1.48	1.50	1.51	1.52			
13	1.53	1.54	1.56	1.57	1.58	1.59	1.60	1.61	1.68	1.64			
14	1.65	1.66	1.67	1.68	1.70	1.71	1.72	1.73	1.74	1.76			
15	1.77	1.78	1.79	1.80	1.81	1.88	1.84	1.85	1.86	1.87			
16	1.89	1.90	1.91	1.92	1.98	1.94	1.96	1.97	1.98	1.99			
17	2.00	2.01	2.03	2.04	2.05	2.06	2.07	2.09	2.10	2.11			
18	2.12	2.13	2.14	2.16	2.17	2.18	2.19	2.20	2.22	2.23			
19	2.24	2.25	2.26	2.27	2.29	2.80	2.81	2.32	2.33	2.34			
20	2.36	2.87	2.38	2.89	2.40	2.43	2.43	2.44	2.45	2.46			
21	2.47	2.49	2.50	2.51	2.52	2.58	2.54	2.56	2.57	2.58			
22	2.59	2.60	2.62	2.63	2.64	2.65	2.66	2.67	2.69	2.70			
23	2.71	2.72	2.78	2.75	2.76	2.77	2.78	2.79	2.80	2.82			
24	2.83	2.84	2.85	2.86	2.87	2.89	2.90	2.91	2.92	2.93			
25	2.95	2.96	2.97	2.98	2.99	8.01	3.02	8.08	8.04	3.06			
26	3.06	3.08	8.09	8.10	8.11	8.12	3.13	8.15	3.16	8.17			
27	8.18	3.19	8.20	3.22	3.28	8.24	8.25	3.26	3.28	3.29			
28	3.30	3.81	3.32	3.83	3.35	3.36	8.37	3.38	3.39	8.41			
29	3.42	3.43	8.44	3.45	8.46	8.48	8.49	8.50	8.51	8.52			
30	3.58	3.55	8.56	8.57	8.56	8.59	8.61	3.62	3.63	3.64			
31	3.65	3.66	8.68	3.69	8.70	8.71	3 72	8.78	8-75	8.76			
82	3.77	8.78	8.79	8.81	3.82	3.88	3.84	8.85	8.86	8.88			
38	3.89	8.90	8.91	3.92	3.94	8.95	3.96	3.97	8.96	3.99			
84	4.01	4.02	4.08	4.04	4.05	4.06	4.07	4.09	4.10	4-11			
35	4.12	4.14	4.15	4.16	4.17	4.18	4.19	4.21	4.22	4.28			
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			

	BAROMETER: 735 (from 732.51 to 737.50).											
Centigrade Dogress.					Tenths o	f Degrees.						
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
°	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.09	Millim 0-11		
1	0.12	0.18	0.14	0.15	0.17	0.18	0.19	0.20	0.21	0.23		
2	0.24	0.25	0.26	0.27	0.28	0.30	0.31	0.82	0.33	0.84		
8	0.86	0.87	0.88	0.89	0.40	0.42	0.48	0.44	0.45	0.46		
4	0.47	0.49	0.50	0.51	0.52	0.58	0.55	0.56	0.57	0.58		
5	0.59	0.61	0.62	0.68	0.64	0.65	0.66	0.68	0.69	0.70		
6	0.71	0.72	0.74	0.75	0.76	0.77	0.78	0.79	0.81	0.82		
7	0.88	0.84	0.85	0.87	0.88	0.89	0.90	0.91	0.98	0.94		
8	0.95	0.96	0.97	0.98	1.00	1.01	1.02	1.08	1.04	1.06		
9	1.07	1.08	1.09	1.10	1.12	1.18	1.14	1.15	1.16	1.17		
10	1.19	1.20	1.21	1.22	1.23	1.25	1.26	1.27	1.28	1.29		
-			_									
11	1.30	1.82	1.33	1.84	1.85	1.36	1.37	1.39	1.40	1.41		
12	1.42	1.44	1.45	1.46	1.47	1.48	1.49	1.51	1.52	1.53		
18	1.54	1.55	1.57	1.58	1.59	1.60	1.61	1.63	1.64	1.65		
14	1.66	1.67	1.69	1.70	1.71	1.72	1.73	1.74	1.76	1.77		
15	1.78	1.79	1.80	1.82	1.83	1.84	1.85	1.86	1.87	1.89		
16	1.90	1.91	1.92	1.98	1.95	1.96	1.97	1.98	1.99	2.00		
17	2.02	2.08	2.04	2.05	2.06	2.08	2.09	2.10	2.11	2.12		
18	2.14	2.15	2.16	2.17	2.18	2.19	2.21	2.22	2.23	2.24		
19	2.25 2.87	2.27	2.28	2.29	2.80	2.31	2.33	2.84	2.85	2.36		
20	2.01	2.88	2.40	2.41	2.42	2.48	2.44	2.46	2.47	2.48		
21	2.49	2.50	2.51	2.53	2.54	2.55	2.56	2.57	2.59	2.60		
22	2.61	2.62	2.63	2.65	2.66	2.67	2.68	2.69	2.70	2.72		
23	2.73	2.74	2.75	2.76	2.78	2.79	2.80	2.81	2.82	2.84		
24	2.85	2.86	2.87	2.88	2.89	2.91	2.92	2.93	2.94	2.96		
25	2.97	2.98	2.99	8.00	3.01	3.08	8.04	8.05	8.06	8.07		
26	8.08	8.10	8.11	8.12	8.18	8.14	3.16	8-17	3.18	3.19		
27	8.20	3.21	8.23	3.24	8.25	8.26	8.27	3.29	3.30	3.31		
28	8.32	8.88	3.85	3.86	8.87	3.88	8.39	3.40	3.42	3.43		
29	8.44	8.45	3.46	8.48	8.49	8.50	3.51	8-52	8.54	3.55		
20	3.56	8.57	8.58	3.59	3.61	8.62	8.63	3.64	3.65	3.67		
31	8.68	3.69	3.70	8.71	8.72	8.74	8.75	8-76	8.77	3.78		
82	8.80	3.81	8.82	8.83	8.84	3.86	3.87	3.88	8.89	8.90		
88	8.91	8.93	8.94	8.95	8.96	8.97	8.99	4.00	4.01	4.02		
84	4.03	8.05	4.06	4.07	4.08	4.09	4.10	4.12	4.13	4.14		
85	4.15	4.16	4.18	4-19	4.20	4.21	4.22	4.24	4.25	4.26		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

	BAROMETER: 740 (from 737.51 to 742.50).											
Centi- grade Degrees					Tenthe o	Degrees.	-					
	0.	L	2.	8.	4.	5.	6.	7.	8.	9.		
ő	Millim, 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.04	Millim.	Millim. 0.06	Million. 0.07	Millim, 0.08	Millim. 0.09	Millim. 0.11		
1	0.12	0.18	0.14	0.16	0.17	0.18	0.19	0.20	0.21	0.28		
2	0.24	0.25	0.26	0.27	0.29	0.80	0.31	0.82	0.33	0.35		
, 3	0.36	0.87	0.38	0.39	0.41	0.42	0.48	0.44	0.45	0.47		
4	0.48	0.49	0.50	0.51	0.58	0.54	0.55	0.56	0.57	0.59		
5	0.60	0.61	0.62	0.68	0.64	0.66	0.67	0.68	0.69	0.70		
6	0.72	0.78	0.74	0.75	0.76	0.78	0.79	0.80	0.81	0.82		
7	0.84	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.98	0.94		
8	0.96	0.97	0.98	0.99	1.00	1.02	1.03	1.04	1.05	1.06		
9	1.07	1.09	1.10	1.11	1.12	1.18	1.15	1.16	1.17	1.18		
10	1.19	1.21	1.22	1.28	1.24	1.25	1.27	1.28	1.29	1.30		
11	1.81	1.88	1.84	1.35	1.36	1.87	1.39	1.40	1.41	1.42		
12	1.43	1.45	1.46	1.47	1.48	1.49	1.50	1.52	1.58	1.54		
18	1.55	1.56	1.58	1.59	1.60	1.61	1.62	1.64	1.65	1.66		
14	1.67	1.68	1.70	1.71	1.72	1.78	1.74	1.76	1.77	1.78		
15	1.79	1.80	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90		
16	1.91	1.92	1.98	1.95	1.96	1.97	1.98	1.99	2.01	2.02		
17	2.03	2.04	2.05	2.07	2.08	2.09	2.10	2.11	2.13	2.14		
18	2.15	2.16	2.17	2.19	2.20	2.21	2.22	2.23	2.25	2.26		
19	2.27	2.28	2.29	2.81	2.82	2.83	2.34	2.35	2.36	2.38		
20	2.39	2.40	2.41	2.42	2.44	2.45	2.46	2.47	2.48	2.50		
21	2.51	2.52	2.58	2.54	2.56	2.57	2.58	2.59	2.60	2.62		
22	2.63	2.64	2.65	2.66	2.68	2.69	2.70	2.71	2.72	2.74		
23	2.75	2.76	2.77	2.78	2.79	2.81	2.82	2.88	2.84	2.85		
24	2.87	2.88	2.89	2.90	2.91	2.93	2.94	2.95	2.96	2.97		
25	2.99	8.00	8.01	3.02	3.08	3.05	8.06	8.07	8.08	8.09		
26	8.11	8.12	8.13	8.14	3.15	8.17	8.18	8.19	8.20	8.21		
27	8.22	8.24	8.25	3.26	3.27	3.28	3.30	3.31	8.32	8.38		
28	8.84	8.86	3.37	3.38	8.39	8.40	8.42	8.48	8.44	3.45		
29	3.46	3.48	8.49	3.50	3.51	8.52	8.54	8.55	3.56	8.57		
30	8.58	3.60	3.61	8.62	3.68	8.64	3.65	8.67	3.68	3.69		
81	8.70	3.71	3.78	8.74	8.75	8.76	8.77	8.79	8.80	8.81		
82	3.82	3.88	3.85	8.86	3.87	8.88	3.89	3.91	3.92	3.93		
33	8.94	3.95	3.97	3.98	3.99	4.00	4.01	4.02	4.04	4.05		
34	4.06	4.07	4.08	4.10	4.11	4.12	4.18	4.14	4.16	4.17		
35	4.18	4.19	4.20	4.22	4.23	4.24	4.25	4.26	4.28	4.29		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

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	BAROMETER: 745*** (from 742.51 to 747.50).											
Centi- grade Degrees.					Tenths of	f Degrees.						
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
	Millim.	Millim.	Millim.	Millim.	Millim	Millim.	Millim.	Millim.	Millim.	Millim.		
0	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.08	0.10	0.11		
1 1	0.12	0.13	0.14	0.16	0.17	0.18	0.19	0.20	0.22	0.23		
2	0.24	0.25	0.26	0.28	0.29	0.80	0.31	0.32	0.84	0.35		
8	0.36	0.37	0.88	0.40	0.41	0.42	0.48	0.44	0.46	0.47		
4	0.48	0.49	0.51	0.52	0.53	0.54	0.55	0.57	0.58	0.59		
5	0.60	0.61	0.63	0.64	0.65	0.66	0.67	0.69	0.70	0.71		
j		1	l			i	ľ		1	l		
6	0.72	0.78	0.75	0.76	0.77	0.78	0.79	0.81	0.82	0.83		
7	0.84	0.85	0.87	0.88	0.89	0.90	0.91	0.98	0.94	0.95		
8	0.96	0.97	0.99	1.00	1.01	1.02	1.03	1.05	1.06	1.07		
9	1.08	1.09	1.11	1.12	1.13	1.14	1.15	1.17	1.18	1.19		
10	1.20	1.21	1.28	1.24	1.25	1.26	1.27	1.29	1.30	1.31		
11	1.32	1.88	1.85	1.36	1.87	1.88 1.50	1.89	1.41	1.42	1.43		
12	1.44	1.45	1.47	1.48	1.49 1.61	1.62	1.52	1.53	1.54	1.55 1.67		
13	1.56 1.68	1.58 1.70	1.59 1.71	1.60 1.72	1.78	1.74	1.64 1.76	1.65	1.78	1.79		
14 15	1.80	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91		
10	1.00	1.02	1.00	1.04	1.00	1.00	1.00	1.00	1.50	1.51		
16	1.92	1.94	1.95	1.96	1.97	1.98	2.00	2.01	2.02	2.03		
17	2.04	2.06	2.07	2.08	2.09	2.10	2.12	2.18	2.14	2.15		
18	2.16	2.18	2.19	2.20	2.21	2.22	2.24	2.25	2.26	2.27		
19	2.28	2.30	2.31	2.32	2.33	2.34	2.36	2.37	2.38	2.39		
20	2.40	2.42	2.48	2.44	2.45	2.46	2.48	2.49	2.50	2.51		
ĺ		}						l				
21	2.53	2.54	2.55	2.56	2.57	2.59	2.60	2.61	2.62	2.63		
22	2.65	2.66	2.67	2.68	2.69	2.71	2.72	2.78	2.74	2.75		
28	2.77	2.78	2.79	2.80	2.81	2.83	2.84	2.85	2.86	2.87		
24	2.89	2.90	2.91	2.92	2.93	2.95	2.96	2.97	2.98	2.99		
25	8.01	8.02	8.08	8.04	8.05	8.07	3.06	8.09	8.10	8.11		
26	8.18	8.14	8.15	3.16	8.17	8.19	8.20	8.21	8.22	3.23		
27	8.25	8.26	8.27	8.28	3.29	3.31	3.32	8.88	8.84	8.35		
28	8.87	8.88 8.50	3.39	8.40 8.52	8.41 8.54	3.43 3.55	3.44	8.45 8.57	3.46 3.58	3.48 3.60		
29 30	8.49 8.61	8.62	3.51 3.68	3.64	3.66	3.67	8.68	3.69	8.70	3.72		
30	9.01	0.02	3.00	0.04	5.00	0.07	0.00	3.05	8.70	5.72		
31	3.73	3.74	8.75	8.76	3.78	8.79	3.80	3.81	3.82	8.84		
82	8.85	8.86	8.87	3.88	8.90	8.91	8.92	8.98	8.94	3.96		
38	8.97	3.98	3.99	4.00	4.02	4.03	4.04	4.05	4.06	4.08		
84	4.09	4.10	4.11	4.12	4.14	4.15	4.16	4.17	4.18	4.20		
85	4.21	4.22	4.23	4.24	4.26	4.27	4.28	4.29	4.30	4.32		
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.		

	BAROMETER: 750 (from 747.51 to 752.50).										
Centi- grade Degraes.					Tenths of	Degrees.					
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
ő	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.10	Millim. 0.11	
1	0.12	0.18	0.15	0.16	0.17	0.18	0.19	0.21	0.22	0.23	
2	0.24	0.25	0.27	0.28	0.29	0.30	0.31	0.33	0.84	0.35	
3	0.86	0.38	0.39	0.40	0.41	0.42	0.44	0.45	0.46	0.47	
4	0.48	0.50	0.51	0.52	0.53	0.55	0.56	0.57	0.58	0.59	
5	0.61	0.62	0.63	0.64	0.65	0.67	0.68	0.69	0.70	0.71	
6	0.78	0.74	0.75	0.76	0.77	0.79	0.80	0.81	0.82	0.84	
7	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.93	0.94	0.96	
8	0.97	0.98	0.99	1.00	1.02	1.03	1.04	1.05	1.07	1.08	
9	1.09	1.10	1.11	1.13	1.14	1.15	1.16	1.17.	1.19	1.20	
10	1.21	1.22	1.23	1.25	1.26	1.27	1.28	1.80	1.81	1.32	
11	1.88	1.84	1.86	1.87	1.38	1.89	1.40	1.42	1.43	1.44	
12	1.45	1.46	1.48	1.49	1.50	1.51	1.53	1.54	1.55	1.56	
13	1.57	1.59	1.60	1.61	1.62	1.63	1.65	1.66	1.67	1.68	
14	1.69	1.71	1.72	1.73	1.74	1.76	1.77	1.78	1.79	1.80	
15	1.82	1.88	1.84	1.85	1.86	1.88	1.89	1.90	1.91	1.92	
16	1.94	1.95	1.96	1.97	1.99	2.00	2.01	2.02	2.08	2.05	
17	2.06	2.07	2.08	2.09	2.11	2.12	2.13	2.14	2.15	2.17	
18	2.18	2.19	2.20	2.21	2.23	2.24	2.25	2.26	2.28	2.29	
19	2.30	2.31	2.82	2.34	2.35	2.36	2.37	2.38	2.40	2.41	
20	2.42	2.43	2.45	2.46	2.47	2.48	2.49	2.51	2.52	2.53	
21	2.54	2.55	2.57	2.58	2.59	2.60	2.61	2.63	2.64	2.65	
22	2.66	2.68	2.69	2.70	2.71	2.72	2.78	2.75	2.76	2.77	
23	2.78	2.80	2.81	2.82	2.88	2.84	2.86	2.87	2.88	2.89	
24	2.91	2.92	2.93	2.94	2.95	2.97	2.98	2.99	3.00	8.01	
25	3.03	8.04	8.05	2.06	8.07	3.09	8.10	8.11	3.12	3.14	
26	3.15	3.16	8.17	3.18	8.20	3.21	8.22	8.28	8.24	3.26	
27	8.27	8.28	8.29	3.30	3.82	3.33	8.84	3.85	8.87	3.38	
28	8.89	8.40	8.41	8.48	8.44	8.45	8.46	8.47	8.49	8.50	
29	3.51	8.52	8.54	8.55	3.56	8.57	8.58	8.60	3.61	3.62	
30	3.68	8.64	3.66	8.67	3.68	8.69	8.70	8.72	8.78	8.74	
31	8.75	8.76	8.78	8.79	3.80	8.81	8.88	8.84	3.85	8.86	
82	8.87	3.89	8.90	3.91	3.92	3.98	8.95	8.96	8.97	3.98	
38	8.99	4.01	4.02	4.08	4.04	4.06	4.07	4.08	4.09	4.10	
34	4.12	4.13	4.14	4.15	4.16	4.18	4.19	4.20	4.21	4.22	
85	4.24	4.25	4.26	4.27	4.29	4.30	4.81	4.82	4.38	4.85	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

	BAROMETER: 755*** (from 752.51 to 757.50).										
Centigrade Degrees.					Tenths of	Degrees,					
	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.	
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	
0	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.09	0.10	0.11	
1	0.12	0.18	0.15	0.16	9.17	0.18	0.19	0.21	0.22	0.23	
2	0.24	0.26	0.27	0.28	0.29	0.80	0.32	0.88	0.84	0.35	
8	0.87	0.88	0.39	0.40	0.41	0.48	0.44	0.45	0.46	0.48	
4	0.49	0.50	0.51	0.52	0.54	0.55	0.56	0.57	0.58	0.60	
5	0.61	0.62	0.63	0.65	0.66	0.67	0.68	0.69	0.71	0.72	
6	0.78	0.74	0.76	0.77	0.78	0.79	0.80	0.82	0-88	0.84	
7	0.85	0.74	0.76	0.89	0.90	0.75	0.93	0.94	0.95	0.96	
8	0.97	0.99	1.00	1.01	1.02	1.04	1.05	1.06	1.07	1.08	
9	1.10	1.11	1.12	1.18	1.15	1.16	1.17	1.18	1.19	1.21	
10	1.22	1.28	1.24	1.96	1.27	1.28	1.29	1.30	1.82	1.33	
1											
11	1.84	1.85	1.86	1.38	1.89	1.40	1.41	1.43	1.44	1.45	
12	1.46	1.47	1.49	1.50	1.51	1.52	1.54	1.55	1.56	1.57	
18	1.58	1.60	1.61	1.62	1.63	1.65	1.66	1.67	1.68	1.69	
14	1.71	1.72	1.78	1.74	1.75	1.77	1.78	1.79	1.80	1.82	
15	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91	1.93	1.94	
10	1.95	1.96	1.97	1.99	2.00	2.01	2.02	2.04	2.05	2.06	
16 17	2.07	2.08	2.10	2.11	2.12	2.18	2.03	2.16	2.17	2.18	
18	2.19	2.05	2.22	2.28	2.24	2.25	2.27	2.28	2.29	2.30	
19	2.82	2.88	2.34	2.35	2.36	2.38	2.89	2.40	2.41	2.42	
20	2.44	2.45	2.46	2.47	2.49	2.50	2.51	2.52	2.58	2.55	
									•	<u> </u>	
21	2.56	2.57	2.58	2.60	2.61	2.62	2.68	2.64	2.66	2.67	
22	2.68	2.69	2.71	2.72	2.78	2.74	2.75	2.77	2.78	2.79	
23	2.80	2.81	2.82	2.84	2.85	2.86	2.88	2.89	2.90	2.91	
24	2.92	2.94	2.95	2.96	2.97	2.99	3.00	8.01	8.02	8.03 i	
25	8.05	8.06	3.07	3.0 8	8.10	8.11	8.12	8.13	8.14	8.16	
	0.10	9 10	9 10	3.20	8.22	8.23					
26	3.17 3.29	8.18 8.80	8.19 3.3 1	8.88	8.22	8.85	8.24 8.36	3.25 3.38	3.27 3.89	3.2 8 3.4 0	
27 28	8.41	3.42	8.44	3.45	8.46	8.47	3.49	8.50	8.51	3.52	
29	3.53	8.55	8.56	3.57	3.58	3.59	8.61	8.62	8.68	8.64	
30	8.66	8.67	8.68	8.69	8.70	8.72	3.78	8.74	3.75	8.77	
					,	=	. •=				
31	3.78	8.79	8.80	8.81	8.88	8.84	8.85	8.86	8.88	8.89	
82	8.90	8.91	8.92	8.94	8.95	8.96	8.97	8.98	4.00	4.01	
88	4.02	4.08	4.05	4.06	4.07	4.08	4.09	4.11	4.12	4.13	
84	4.14	4.16	4.17	4.18	4.19	4.20	4.22	4.23	4.24	4.25	
85	4.26	4.28	4.29	4.80	4.81	4.88	4.34	4.35	4.36	4.37	
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.	

		BAROMETER: 760- (from 757.51 to 762.50).										
Nillim. Millim. Millim. Millim. Millim. Millim. Millim. Millim. O.06 O.07 O.09 O.01	Centigrade grade Dograde.					Tenthe e	f Dogress.					
0 0.00 0.01 0.02 0.04 0.06 0.07 0.09 0.1 1 0.12 0.18 0.15 0.16 0.17 0.18 0.20 0.21 0.2 2 0.25 0.26 0.27 0.28 0.29 0.31 0.32 0.38 0.3 3 0.37 0.38 0.29 0.40 0.42 0.43 0.44 0.45 0.4 4 0.49 0.50 0.52 0.53 0.54 0.55 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.57 0.79 0.70 <th></th> <th>0.</th> <th>1.</th> <th>2.</th> <th>3.</th> <th>4.</th> <th>5.</th> <th>6.</th> <th>7.</th> <th>8.</th> <th>9.</th>		0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
2 0.25 0.26 0.27 0.28 0.29 0.51 0.52 0.53 0.3 3 0.57 0.88 0.39 0.40 0.42 0.43 0.44 0.45 0.4 0.45 0.4 0.43 0.44 0.45 0.4 0.43 0.44 0.45 0.4 0.43 0.44 0.44 0.44 0.44 0.46 0.65 0.66 0.55 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.57 0.60 0.61 0.66 0.67 0.69 0.70 0.7 6 0.74 0.75 0.76 0.77 0.79 0.80 0.81 0.82 0.8 8 0.98 0.99 1.01 1.02 1.03 1.04 1.05 1.07 1.5 9 1.10 1.12 1.13 1.14 1.15 1.17 1.18 1.19 1.2 10 1.23 1.24 1.25 1.26										Millim. 0.10	Millim. 0.11	
2 0.26 0.26 0.27 0.28 0.29 0.31 0.32 0.38 0.3 3 0.57 0.88 0.39 0.40 0.42 0.43 0.44 0.45 0.4 4 0.49 0.50 0.52 0.58 0.56 0.55 0.56 0.57 0.66 0.67 0.69 0.70		0.12	0.18	0.15	0.16	0.17	0.18	0.20	0.21	0.22	0.23	
4 0.49 0.50 0.52 0.58 0.64 0.65 0.66 0.67 0.69 0.70 1.70 1.70 1.70 1.70 1.70 1.70 1.70 1.70 1.70 1.70 1.70 1.70 1.70 1.70 1.		1			1	l			1	0.34	0.86	
6 0.61 0.63 0.64 0.65 0.66 0.67 0.69 0.70 0.73 6 0.74 0.76 0.77 0.79 0.80 0.81 0.82 0.5 7 0.86 0.87 0.88 0.90 0.91 0.92 0.93 0.94 0.5 8 0.98 0.99 1.01 1.02 1.03 1.04 1.05 1.07 1.0 9 1.10 1.12 1.18 1.14 1.15 1.17 1.18 1.19 1.5 10 1.23 1.24 1.25 1.26 1.28 1.29 1.30 1.31 1.3 11 1.35 1.36 1.37 1.39 1.40 1.41 1.42 1.44 1.4		0.87	0.88	0.39	0.40	0.42	0.48	0.44	0.45	0.47	0.48	
6 0.74 0.75 0.76 0.77 0.79 0.80 0.81 0.82 0.82 7 0.86 0.87 0.88 0.90 0.91 0.92 0.93 0.94 0.8 8 0.98 0.99 1.01 1.02 1.03 1.04 1.05 1.07 1.0 9 1.10 1.12 1.13 1.14 1.15 1.17 1.18 1.19 1.2 10 1.23 1.24 1.25 1.26 1.28 1.29 1.30 1.31 1.3 11 1.25 1.36 1.57 1.59 1.40 1.41 1.42 1.44 1.4 12 1.47 1.48 1.50 1.51 1.52 1.58 1.56 1.56 1.5 13 1.59 1.61 1.62 1.68 1.44 1.06 1.67 1.68 1.6 1.4 1.72 1.73 1.74 1.75 1.77 1.78 <th>4</th> <th>0.49</th> <th>0.50</th> <th>0.52</th> <th>0.58</th> <th>0.54</th> <th>0.55</th> <th>0.56</th> <th>0.58</th> <th>0.59</th> <th>0.60</th>	4	0.49	0.50	0.52	0.58	0.54	0.55	0.56	0.58	0.59	0.60	
7 0.86 0.87 0.88 0.90 0.91 0.92 0.93 0.94 0.58 8 0.98 0.99 1.01 1.02 1.03 1.04 1.05 1.07 1.0 9 1.10 1.12 1.18 1.14 1.15 1.17 1.18 1.19 1.2 10 1.23 1.24 1.25 1.26 1.28 1.29 1.20 1.31 1.4 11 1.85 1.86 1.87 1.89 1.40 1.41 1.42 1.44 1.4 12 1.47 1.48 1.50 1.51 1.52 1.58 1.55 1.56 1.5 13 1.59 1.61 1.62 1.68 1.44 1.44 1.44 1.44 1.44 1.44 1.47 1.73 1.74 1.75 1.77 1.78 1.79 1.80 1.68 1.69 1.81 1.81 1.90 1.91 1.92 1.92 1.92	5	0.61	0.63	0.64	0.65	0.66	0.67	0.69	0.70	0.71	0.72	
7 0.86 0.87 0.88 0.90 0.91 0.92 0.93 0.94 0.5 8 0.96 0.99 1.01 1.02 1.03 1.04 1.06 1.07 1.0 9 1.10 1.12 1.13 1.14 1.15 1.17 1.18 1.19 1.2 10 1.23 1.24 1.25 1.26 1.28 1.29 1.30 1.31 1.4 11 1.85 1.86 1.87 1.89 1.40 1.41 1.42 1.44 1.4 12 1.47 1.48 1.50 1.51 1.52 1.53 1.55 1.56 1.5 13 1.59 1.61 1.62 1.68 1.64 1.66 1.67 1.68 1.6 14 1.72 1.73 1.74 1.75 1.77 1.78 1.79 1.80 1.8 15 1.84 1.85 1.86 1.88 1.89 1.90 <th>6</th> <th>0.74</th> <th>0.75</th> <th>0-76</th> <th>0.77</th> <th>0.79</th> <th>0.80</th> <th>0.81</th> <th>0.82</th> <th>0.88</th> <th>0.85</th>	6	0.74	0.75	0-76	0.77	0.79	0.80	0.81	0.82	0.88	0.85	
8 0.98 0.99 1.01 1.02 1.03 1.04 1.05 1.07 1.6 9 1.10 1.12 1.18 1.14 1.15 1.17 1.18 1.19 1.2 10 1.23 1.24 1.25 1.26 1.28 1.29 1.20 1.31 1.3 11 1.35 1.36 1.37 1.39 1.40 1.41 1.42 1.44 1.4 12 1.47 1.48 1.50 1.51 1.53 1.55 1.56 1.5 13 1.59 1.61 1.62 1.68 1.64 1.66 1.67 1.68 1.6 14 1.72 1.73 1.74 1.75 1.77 1.78 1.79 1.80 1.8 15 1.84 1.85 1.86 1.88 1.89 1.90 1.91 1.92 1.9 1.91 1.92 1.9 1.90 1.91 1.92 1.9 1.82 1.90 1.91 1.92 1.91 1.92 1.92 1.92 1.92 1.92	- 11									0.96	0.97	
10 1.23 1.24 1.25 1.26 1.28 1.29 1.30 1.31 1.3 11 1.85 1.36 1.87 1.39 1.40 1.41 1.42 1.44 1.4 12 1.47 1.48 1.50 1.51 1.52 1.58 1.55 1.56 1.5 13 1.59 1.61 1.62 1.68 1.64 1.66 1.67 1.68 1.6 14 1.72 1.73 1.74 1.75 1.77 1.78 1.79 1.80 1.8 15 1.84 1.85 1.88 1.89 1.90 1.91 1.93 1.9 16 1.96 1.97 1.99 2.00 2.01 2.02 2.04 2.05 2.0 17 2.09 2.19 2.11 2.12 2.13 2.15 2.16 2.17 2.1 18 2.21 2.22 2.23 2.24 2.26 2.27 2.28 2.29 2.3 19 2.33 2.84 2.36 2.37	- 1							ŀ		1.08	1.09	
11 1.85 1.36 1.87 1.39 1.40 1.41 1.42 1.44 1.4 12 1.47 1.48 1.50 1.51 1.52 1.58 1.55 1.56 1.5 13 1.59 1.61 1.62 1.68 1.64 1.66 1.67 1.68 1.6 14 1.72 1.73 1.74 1.75 1.77 1.78 1.79 1.80 1.8 15 1.84 1.86 1.88 1.89 1.90 1.91 1.93 1.9 16 1.96 1.97 1.99 2.60 2.01 2.02 2.04 2.05 2.05 17 2.09 2.19 2.11 2.12 2.13 2.15 2.16 2.17 2.1 18 2.21 2.22 2.23 2.24 2.26 2.27 2.28 2.29 2.3 19 2.33 2.84 2.36 2.87 2.38 2.39 2.40	9	1.10	1.12	1.18	1.14	1.15	1.17	1.18	1.19	1.20	1.21	
12 1.47 1.48 1.50 1.51 1.52 1.58 1.55 1.56 1.56 1.56 1.56 1.56 1.56 1.56 1.56 1.56 1.68 1.68 1.66 1.67 1.68 1.68 1.61 1.62 1.68 1.68 1.68 1.68 1.68 1.68 1.68 1.68 1.68 1.68 1.69 1.77 1.78 1.79 1.80 1.8 1.80 1.80 1.81 1.81 1.81 1.81 1.81 1.81 1.82 1.81 1.81 1.81 1.81 1.81 1.82 1.81 1.82 1.81 1.82 1.81 1.82 1.	10	1.23	1.24	1.25	1.26	1.28	1.29	1.20	1.31	1.82	1.84	
13 1.59 1.61 1.62 1.68 1.64 1.66 1.67 1.68 1.61 1.62 1.68 1.77 1.78 1.79 1.80 1.8 15 1.84 1.85 1.86 1.88 1.89 1.90 1.91 1.80 1.8 16 1.96 1.97 1.99 2.60 2.01 2.02 2.04 2.05 2.0 17 2.09 2.10 2.11 2.12 2.13 2.15 2.16 2.17 2.1 18 2.21 2.22 2.23 2.24 2.26 2.27 2.28 2.29 2.3 19 2.53 2.44 2.36 2.37 2.38 2.39 2.40 2.42 2.4 20 2.45 2.47 2.48 2.49 2.50 2.51 2.53 2.54 2.6 21 2.58 2.59 2.60 2.61 2.63 2.84 2.65 2.66 2.6	11	1.85	1.86	1.87	1.89	1.40	1.41	1.42	1.44	1.45	1.46	
14 1.72 1.78 1.74 1.75 1.77 1.78 1.79 1.80 1.81 15 1.84 1.85 1.86 1.88 1.89 1.90 1.91 1.98 1.81 16 1.96 1.97 1.99 2.00 2.01 2.02 2.04 2.05 2.05 17 2.09 2.10 2.11 2.12 2.13 2.15 2.16 2.17 2.1 18 2.21 2.22 2.28 2.24 2.26 2.27 2.28 2.29 2.3 19 2.33 2.84 2.36 2.87 2.38 2.89 2.40 2.42 2.4 20 2.45 2.47 2.48 2.49 2.50 2.51 2.53 2.54 2.4 20 2.45 2.47 2.48 2.49 2.50 2.51 2.53 2.54 2.5 21 2.58 2.59 2.61 2.63 2.64 2.65 2.66 2.6 22 2.70 2.71 2.72 2.74 2.75 2.76 2.77 2.78 2.8 23 2.82 2.83 2.85 2.86 2.87 2.88	12	1.47	1.48	1.50	1.51	1.52	1.58	1.55	1.56	1.57	1.58	
15 1.84 1.85 1.86 1.88 1.89 1.90 1.91 1.98 1.9 16 1.96 1.97 1.99 2.00 2.01 2.02 2.04 2.05 2.0 17 2.09 2.19 2.11 2.12 2.13 2.15 2.16 2.17 2.1 18 2.21 2.22 2.28 2.24 2.26 2.27 2.28 2.29 2.3 19 2.33 2.84 2.36 2.87 2.38 2.89 2.40 2.42 2.4 20 2.45 2.47 2.48 2.49 2.50 2.51 2.53 2.54 2.4 21 2.58 2.59 2.60 2.61 2.63 2.84 2.65 2.66 2.6 22 2.70 2.71 2.72 2.74 2.75 2.76 2.77 2.78 2.8 23 2.82 2.83 2.85 2.86 2.87 2.88 2.89 2.91 2.9 24 2.94 2.96 2.97 2.98 2.99 3.01 3.02 3.08 26 3.19 3.20 3.21 3.22 3.24 3.25 3.	18	1.59	1.61	1.62	1.68	1.64	1.66	1.67	1.68	1.69	1.71	
16 1.96 1.97 1.99 2.00 2.01 2.02 2.04 2.05 2.0 17 2.09 2.10 2.11 2.12 2.13 2.15 2.16 2.17 2.1 18 2.21 2.22 2.23 2.24 2.26 2.27 2.28 2.29 2.3 19 2.33 2.84 2.36 2.87 2.38 2.39 2.40 2.42 2.4 20 2.45 2.47 2.48 2.49 2.50 2.51 2.53 2.54 2.4 21 2.58 2.59 2.60 2.61 2.63 2.64 2.65 2.66 2.6 22 2.70 2.71 2.72 2.74 2.76 2.77 2.78 2.8 23 2.82 2.83 2.85 2.86 2.87 2.88 2.89 2.91 2.9 24 2.94 2.96 2.97 2.96 2.99 3.01 3.02 3.08 25 3.07 3.08 3.09 3.10 3.12 3.13 3.14 3.15 3.1 26 3.19 3.20 3.21 3.22 3.24 3.25 3.26 3.	14	1.72	1.78	1.74	1.75	1.77	1.78	1.79	1.80	1.82	1.88	
17 2.09 2.10 2.11 2.12 2.13 2.15 2.16 2.27 2.21 18 2.21 2.22 2.28 2.24 2.26 2.27 2.28 2.29 2.3 19 2.83 2.84 2.86 2.87 2.88 2.89 2.40 2.42 2.4 20 2.45 2.47 2.48 2.49 2.50 2.51 2.53 2.54 2.4 21 2.58 2.59 2.60 2.61 2.68 2.64 2.65 2.66 2.6 22 2.70 2.71 2.72 2.74 2.75 2.76 2.77 2.78 2.8 23 2.82 2.63 2.95 2.86 2.87 2.88 2.69 2.91 2.9 24 2.94 2.96 2.97 2.96 2.99 3.01 3.02 3.03 3.0 25 3.07 3.08 3.09 3.10 3.12 3.13	15	1.84	1.85	1.86	1.88	1.89	1.90	1.91	1.98	1.94	1.95	
18 2.21 2.22 2.28 2.24 2.26 2.27 2.28 2.29 2.3 19 2.33 2.34 2.36 2.37 2.38 2.39 2.40 2.42 2.4 20 2.45 2.47 2.48 2.49 2.50 2.51 2.53 2.54 2.5 21 2.58 2.59 2.60 2.61 2.63 2.64 2.65 2.66 2.6 22 2.70 2.71 2.72 2.74 2.75 2.76 2.77 2.78 2.8 23 2.82 2.83 2.85 2.86 2.87 2.88 2.89 2.91 2.9 24 2.94 2.96 2.97 2.86 2.89 3.01 3.02 3.08 3.0 25 3.07 3.08 3.09 3.10 3.12 3.13 3.14 3.15 3.1 26 3.19 3.20 3.21 3.23 3.24 3.25<	16	1.96	1.97	1.99	2.00	2.01	2.02	2.04	2.05	2.06	2.07	
19 2.83 2.84 2.36 2.87 2.38 2.89 2.40 2.42 2.42 20 2.45 2.47 2.48 2.49 2.50 2.51 2.53 2.54 2.5 21 2.58 2.59 2.60 2.61 2.63 2.64 2.65 2.66 2.6 22 2.70 2.71 2.72 2.74 2.75 2.76 2.77 2.78 2.8 23 2.82 2.83 2.85 2.86 2.87 2.88 2.89 2.91 2.9 24 2.94 2.96 2.97 2.86 2.99 3.01 3.02 3.03 3.0 25 3.07 3.08 3.09 3.10 3.12 3.13 3.14 3.15 3.1 26 3.19 3.20 3.21 3.23 3.24 3.25 3.26 3.28 3.2 27 3.31 3.82 3.34 3.35 3.36 3.51 3.52 3.5 28 3.48 3.45 3.46 3.47 3.48 3.50 3.51 3.52 3.5 29 3.63 3.69 3.70 3.72 3.73 3.74 3.	17	2.09	2.10	2.11	2.12	2.18	2.15	2.16	2.17	2.18	2.20	
20 2.45 2.47 2.48 2.49 2.50 2.51 2.53 2.54 2.5 21 2.58 2.59 2.60 2.61 2.63 2.64 2.65 2.66 2.6 22 2.70 2.71 2.72 2.74 2.75 2.76 2.77 2.78 2.8 23 2.82 2.83 2.85 2.86 2.87 2.88 2.89 2.91 2.9 24 2.94 2.96 2.97 2.86 2.99 3.01 3.02 3.03 3.0 25 3.07 3.08 3.09 3.10 3.12 3.13 3.14 3.15 3.1 26 3.19 3.20 3.21 3.23 3.24 3.25 3.26 3.28 3.2 27 3.31 3.82 3.34 3.35 3.36 3.51 3.52 3.5 28 3.48 3.45 3.46 3.47 3.48 3.50 3.51<	18	2.21	2.22	2.28	2.24	2.26	2.27	2.28	2.29	2.31	2.32	
21 2.58 2.59 2.60 2.61 2.63 2.64 2.65 2.66 2.6 22 2.70 2.71 2.72 2.74 2.75 2.76 2.77 2.78 2.8 23 2.82 2.83 2.85 2.86 2.87 2.88 2.89 2.91 2.9 24 2.94 2.96 2.97 2.86 2.98 3.01 3.02 3.08 3.0 25 3.07 3.08 3.09 3.10 3.12 3.13 3.14 3.15 3.1 26 3.19 3.20 3.21 3.23 3.24 3.25 3.26 3.28 3.2 27 3.31 3.82 3.34 3.35 3.36 3.27 3.89 3.40 3.4 28 3.42 3.45 3.45 3.45 3.45 3.50 3.51 3.52 3.5 29 3.56 3.57 3.88 3.89 3.61 3.62<	19	2.88	2.84	2.36	2.87	2.38	2.89	2.40	2.42	2.48	2.44	
22 2.70 2.71 2.72 2.74 2.76 2.76 2.77 2.78 2.8 23 2.82 2.83 2.85 2.86 2.87 2.68 2.89 2.91 2.9 24 2.94 2.96 2.97 2.96 2.99 3.01 3.02 3.08 3.0 25 3.07 3.08 3.09 3.10 3.12 3.18 3.14 3.15 3.1 26 3.19 3.20 3.21 3.22 3.24 3.25 3.26 3.28 3.2 27 2.31 3.82 3.34 3.35 3.36 3.29 3.40 3.4 28 3.43 3.45 3.46 3.47 3.48 3.50 3.51 3.52 3.5 29 3.56 3.57 3.88 3.89 3.61 3.62 3.63 3.64 3.6 30 3.68 3.69 3.70 3.72 3.73 3.74 3.75<	20	2.45	2.47	2.48	2.49	2.50	2.51	2.58	2.54	2.55	2.56	
22 2.70 2.71 2.72 2.74 2.76 2.76 2.77 2.78 2.8 23 2.82 2.83 2.85 2.86 2.87 2.68 2.89 2.91 2.9 24 2.94 2.96 2.97 2.96 2.99 3.01 3.02 3.08 3.0 25 3.07 3.08 3.09 3.10 3.12 3.18 3.14 3.15 3.1 26 3.19 3.20 3.21 3.22 3.24 3.25 3.26 3.28 3.2 27 2.31 3.82 3.34 3.35 3.36 3.26 3.28 3.2 28 3.43 3.45 3.46 3.47 3.48 3.50 3.61 3.63 3.64 3.6 29 3.56 3.57 3.88 3.89 3.61 3.62 3.63 3.64 3.6 30 3.68 3.69 3.70 3.72 3.73 3.74<	21	2.58	2.59	2.60	2.61	2.68	2.64	2.65	2.66	2.67	2.69	
23 2.82 2.83 2.85 2.86 2.87 2.88 2.89 2.91 2.9 24 2.94 2.96 2.97 2.86 2.99 3.01 3.02 3.08 3.0 25 3.07 3.06 3.09 3.10 3.12 3.13 3.14 3.15 3.1 26 3.19 3.20 3.21 3.23 3.24 3.25 3.26 3.28 3.2 27 2.31 3.82 3.34 3.35 3.36 2.37 3.39 3.40 3.4 28 3.43 2.45 3.46 3.47 3.48 3.50 3.51 3.52 3.5 29 3.56 3.57 3.58 3.89 3.61 3.62 3.63 3.64 3.6 30 3.68 3.69 3.70 3.72 3.73 3.74 3.75 3.77 3.7 31 3.80 3.81 3.83 3.84 3.85 3.86<	N									2.80	2.81	
25 3.07 8.06 8.09 3.10 8.12 8.18 3.14 8.15 3.1 26 3.19 3.20 3.21 3.22 3.24 3.25 3.26 3.28 3.2 27 2.31 3.82 3.34 3.35 3.36 3.37 3.39 3.40 3.4 28 3.48 2.45 3.46 3.47 3.48 3.50 3.51 3.52 3.5 29 3.56 3.57 3.58 3.09 3.61 3.62 3.63 3.64 3.6 30 3.68 3.69 3.70 3.72 3.73 3.74 3.75 3.77 3.7 31 3.80 3.81 3.83 3.84 3.85 3.86 3.88 3.89 3.9 32 3.93 3.94 3.95 3.96 3.97 3.99 4.00 4.01 4.01										2.92	2.93	
26 3.19 3.20 3.21 3.22 3.24 3.25 3.26 3.28 3.2 27 2.31 3.82 3.34 3.35 3.36 3.37 3.39 3.40 3.4 28 3.43 3.45 3.46 3.47 3.48 3.50 3.51 3.52 3.5 29 3.66 3.57 3.58 3.99 3.61 3.62 3.63 3.64 3.6 30 3.68 3.69 3.70 3.72 3.73 3.74 3.75 3.77 3.7 31 3.80 3.81 3.83 3.84 3.85 3.86 3.88 3.89 3.9 32 3.93 3.94 3.95 3.96 3.97 3.99 4.00 4.01 4.01	24	2.94	2.96	2.97	2.96	2.99	8.01	8.02	8.08	3.04	3.05	
27 2.31 3.82 3.34 3.35 3.36 3.37 3.39 3.40 3.4 28 3.43 3.45 3.46 3.47 3.48 3.50 3.51 3.52 3.5 29 3.66 3.57 3.88 3.89 3.61 3.62 3.63 3.64 3.6 30 3.68 3.69 3.70 3.72 3.73 3.74 3.75 3.77 3.7 31 3.80 3.81 3.83 3.84 3.85 3.86 3.88 3.89 3.9 32 3.93 3.94 3.95 3.96 3.97 3.99 4.00 4.01 4.01	25	8.07	8.08	8-09	8.10	3.12	8.18	8.14	8-15	3.16	3 .18	
27 3.31 8.82 3.34 3.85 8.36 3.87 8.39 8.40 8.4 28 3.48 3.45 3.46 3.47 3.48 3.50 3.51 3.52 3.5 29 8.56 3.57 3.88 3.89 3.61 3.62 3.63 3.64 3.6 30 3.68 3.69 3.70 3.72 3.73 3.74 3.75 3.77 3.7 31 3.80 3.81 3.83 3.84 3.85 3.86 3.88 3.89 3.9 32 3.93 3.94 3.95 3.96 3.97 3.99 4.00 4.01 4.01		* 10	8.90	2 01	9.99	. 94	9 9K	2 94	0 90	8.29	8.80	
28 3.48 3.45 3.46 3.47 3.48 3.50 3.51 3.52 3.5 29 3.56 3.57 3.58 3.89 3.61 3.62 3.63 3.64 3.6 30 3.68 3.69 3.70 3.72 3.73 3.74 3.75 3.77 3.7 31 3.80 3.81 3.83 3.84 3.85 3.86 3.88 3.89 3.9 32 3.93 3.94 3.95 3.96 3.97 3.99 4.00 4.01 4.01										8.41	3.42	
29 8.56 8.57 8.88 8.89 8.61 8.62 8.63 8.64 8.6 30 3.68 8.69 8.70 8.72 8.73 8.74 8.75 8.77 8.7 31 8.80 3.81 3.83 3.84 8.85 8.86 8.88 8.89 8.9 32 3.93 3.94 3.95 3.96 3.97 8.99 4.00 4.01 4.0										8.58	8.54	
30 3.68 3.69 8.70 8.72 8.73 3.74 8.75 8.77 8.7 31 3.80 3.81 3.88 3.84 3.85 3.86 3.88 3.89 3.9 32 3.93 3.94 3.95 3.96 3.97 3.99 4.00 4.01 4.0	11									3.66	8.67	
32 3.98 3.94 3.95 3.96 3.97 3.99 4.00 4.01 4.0										8.78	8.79	
32 3.98 3.94 3.95 3.96 3.97 3.99 4.00 4.01 4.0	81	8.80	2.81	2.88	3.84	2.85	2.86	8.88	2.89	8.90	3.91	
	- 0									4.02	4.04	
88 4.05 4.06 4.07 4.96 4.10 4.11 4.12 4.13 4.1	88	4.05	4.06	4.07	4.08	4.10	411	4.12	4.13	4.15	4.16	
	- 11		4-18	4.20	4.21					4.27	4.28	
35 4.29 4.81 4.82 4.33 4.84 4.35 4.87 4.38 4.8	35	4.29	4-81	4.82	4.33	4.84	4-85	4.87	4.38	4.89	4.40	
0. 1. 2. 3. 4. 5. 6. 7. 8.		0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

	BAROMETER: 765** (from 762.51 to 767.50).											
Centi- grade Dogress					Tenths o	f Degrees.						
	0.	1.	2.	3.	4.	5.	6,	7.	s.	9.		
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.09	Millim. 0.10	Millim. 0.11		
1	0.12	0.14	0.15	0.16	0.17	0.19	0.20	0.21	0.22	0.23		
2	0.25	0.26	0.27	0.28	0.80	0.81	0.32	0.33	0.35	0.86		
8	0.87	0.38	0.40	0.41	0.42	0.48	0.44	0.46	0.47	0.48		
4	0.49	0.51	0.52	0.58	0.54	0.56	0.57	0.58	0.59	0.61		
5	0.62	0.68	0.64	0.65	0.67	0.68	0.69	0.70	0.72	0.73		
6	0.74	0.75	0.77	0.78	0.79	0.80	0.82	0.88	0.84	0.85		
7	0.86	0.88	0.89	0.90	0.91	0.93	0.94	0.95	0.96	0.98		
8	0.99	1.00	1.01	1.02	1.04	1.05	1.06	1.07	1.09	1.10		
9	1.11	1.12	1.14	1.15	1.16	1.17	1.19	1.20	1.21	1.22		
10	1.28	1.25	1.26	1.27	1.28	1.30	1.81	1.82	1.33	1.35		
11	1.86	1.37	1.38	1.40	1.41	1.42	1.48	1.44	1.46	1.47		
12	1.48	1.49	1.51	1.52	1.53	1.54	1.56	1.57	1.58	1.59		
13	1.61	1.62	1.63	1.64	1.65	1.67	1.68	1.69	1.70	1.72		
14	1.78	1.74	1.75	1.77	1.78	1.79	1.80	1.82	1.83	1.84		
15	1.85	1.86	1.88	1.89	1.90	1.91	1.93	1.94	1.95	1.96		
16	1.98	1.99	2.00	2.01	2.02	2.04	2.05	2.06	2.07	2.09		
17	2.10	2.11	2.12	2.14	2.15	2.16	2.17	2.19	2.20	2.21		
18	2.22	2.23	2.25	2.26	2.27	2.28	2.30	2.31	2.82	2.83		
19	2.85	2.36	2.37	2.88	2.40	2.41	2.42	2.48	2.44	2.46		
20	2.47	2.48	2.49	2.51	2.52	2.53	2.54	2.56	2.57	2.58		
21	2.59	2.61	2.62	2.63	2.64	2.65	2.67	2.68	2.69	2.70		
22	2.72	2.73	2.74	2.75	2.77	2.78	2.79	2.80	2.82	2.83		
28	2.84	2.85	2.86	2.88	2.89	2.90	2.91	2.98	2.94	2.95		
24	2.96	2.98	2.99	8.00	8.01	8.03	8.04	8.05	3.06	3.07		
25	3.09	8.10	8.11	8.12	8.14	8.15	8.16	8.17	3.19	8.20		
26	3.21	3.22	8.23	3.25	8.26	8.27	8.28	8.30	8.81	3.82		
27	8.33	3.35	8.36	8.87	8.88	8.40	8.41	3.42	3.48	8.44		
28	3.46	3.47	3.48	8.49	8.51	8.52	8.58	8.54	3.56	8.57		
29	8.58	8.59	8.61	8.62	3.68	8.64	3.65	3.67	3.68	3.69		
30	3.70	8.72	8.78	8.74	3.75	8.77	8.78	8.79	3.80	8.82		
81	3.88	8.84	8.85	8.86	8.88	3.89	8.90	8-91	3.98	8.94		
32	3.95	8.96	8.98	8.99	4.00	4.01	4.08	4.04	4.05	4.06		
33	4.07	4.09	4.10	4.11	4.12	4.14	4.15	4.16	4.17	4.19		
84	4.20	4.21	4.22	4.24	4.25	4.26	4.27	4.28	4.30	4.31		
85	4.82	4.38	4.35	4.86	4.87	4.88	4.40	4.41	4.42	4.43		
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.		

		BAROMETER: 770 (from 767.51 to 772.50).										
Centi- grade Degrees.					Tenths of	Degrees.						
- - -	0.	1.	9.	3.	4.	5.	6,	7.	8.	9.		
0	Millim. 0.00	Million. 0.01	Millim. 0.02	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.09	Millim. 0.10	Millim. 0.11		
1	0.12	0.14	0.15	0.16	0.17	0.19	0.20	0.21	0.22	0.24		
· 2	0.25	0.26	0.27	0.29	0.30	0.31	0.82	0.84	0.35	0.86		
3	0.87	0.89	0.40	0.41	0.42	0.48	0.45	0.46	0.47	0.48		
4	0.50	0.51	0.52	0.58	0.55	0.56	0.57	0.58	0.60	0.61		
5	0.62	0.68	0.65	0.66	0.67	0.68	0.70	0.71	0.72	0.78		
6	0.75	0.76	0.77	0.78	0.80	0.81	0.82	0.83	0.85	0.86		
7	0.87	0.88	0.89	0.91	0.92	0.93	0.94	0.96	0.97	0.98		
8	0.99	1.01	1.02	1.08	1.04	1.06	1.07	1.08	1.09	1.11		
¦ 9	1.12	1.18	1.14	1.16	1.17	1.18	1.19	1.21	1.22	1.23		
10	1.24	1.26	1.27	1.28	1.29	1.80	1.82	1.33	1.94	1.85		
11	1.87	1.88	1.39	1.40	1.42	1.43	1.44	1.45	1.47	1.48		
12	1.49	1.50	1.52	1.58	1.54	1.55	1.57	1.58	1.59	1.60		
13	1.62	1.63	1.64	1.65	1.67	1.68	1.69	1.70	1.72	1.73		
14	1.74	1.75	1.76	1.78	1.79	1.80	1.81	1.83	1.84	1.85		
15	1.86	1.88	1.89	1.90	1.91	1.98	1.94	1.95	1.96	1.98		
16	1.99	2.00	2.01	2.03	2.04	2.05	2.06	2.08	2.09	2.10		
17	2.11	2.13	2.14	2.15	2.16	2.17	2.19	2.20	2.21	2.22		
18	2.24	2.25	2.26	2.27	2.29	2.80	2.31	2.32	2.84	2.85		
19	2.86	2.87	2.39	2.40	2.41	2.42	2.44	2.45	2.46	2.47		
20	2.49	2.50	2.51	2.52	2.54	2.55	2.56	2.57	2.58	2.60		
21	2.61	2.62	2.63	2.65	2.66	2.67	2.68	2.70	2.71	2.72		
22	2.78	2.75	2.76	2.77	2.78	2.80	2.81	2.82	2.88	2.85		
23	2.86	2.87	2-88	2.90	2.91	2.92	2.93	2.95	2.96	2.97		
24	2.96	8.00	8.01	8.02	8.03	3.04	8.06	8.07	8.08	8.09		
25	8.11	3.12	8.18	8.14	8.16	8.17	8.18	8.19	8.21	8.22		
26	8.28	8.24	8-26	8.27	3.28	8.29	3.81	3.82	3.33	3.84		
27	8.86	8.87	8.88	3.89	8.41	8.42	8.43	3.44	8.45	3.47		
28	3.48	8.49	8.50	8.52	8.58	8.54	3.55	8.57	8-59	3.59		
29	3.60	8.62	8.63	3.64	3.65	8.67	8.68	8.69	3.70	3.72		
80	8.78	3.74	3-75	8.77	8.78	8.79	8.80	3.82	8.68	8.84		
31	8.86	8.87	8-88	8.89	8.90	8.91	3.98	8.94	3.95	8.96		
82	8.98	8.99	4.00	4.01	4.08	4.04	4.05	4.06	4.08	4.09		
33	4.10	4.11	4.18	4.14	4.15	4.16	4.18	4.19	4.20	4.21		
84	4.28	4.24	4.25	4.26	4.28	4.29	4.39	4.81	4.82	4.84		
35	4.85	4.36	4.87	4.89	4.40	4.41	4.42	4.44	4.45	4.46		
	0.	1.	9.	3.	4.	5.	6.	7.	8.	9.		

		BAROMETER: 775*** (from 772.51 to 777.50).								
Centi- grade Degrees.					Teaths of	Degrees,				
	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.
°	Millim. 0.00	Millim. 0.01	Millim. 0.03	Millim. 0.04	Millim 0.05	Millim. 0.06	Millim. 0.08	Millim. 0.09	Millim. 0.10	Millim. 0.11
1	0.18	0.14	0.15	0.16	0.18	0.19	0.20	0.21	0.23	0.24
2	0.25	0.26	0.28	0.29	0.80	0.81	0.38	0.84	0.35	0.36
8	0.88	0.89	0.40	0.41	0.48	0.44	0.45	0.46	0.48	0.49
4	0.50	0.51	0.58	0.54	0.55	0.56	0.58	0.59	0.60	0.61
5	0.68	0.64	0.65	0.66	0.68	0.69	0.70	0.71	0.73	0.74
6	0.75	0.76	0.78	0.79	0.80	0.81	0.83	0.84	0.86	0.86
7	0.78	0.76	0.90	0.75	0.98	0.94	0.95	0.96	0.98	0.99
8	1.00	1.01	1.08	1.04	1.05	1.06	1.08	1.09	1.10	1.11
9	1.18	1.14	1.15	1.16	1.18	1.19	1.20	1.21	1.23	1.24
10	1.25	1.26	1.28	1.29	1.30	1.81	1.33	1.84	1.85	1.86
		1								
11	1.88	1.89	1.40	1.41	1.48	1.44	1.45	1.46	1.48	1.49
12	1.50	1.51	1.53	1.54	1.55	1.56	1.58	1.59	1.60	1.61
18	1.63	1.64	1.65	1.66	1.68	1.69	1.70	1.71	1.78	1.74
14	1.75	1.76	1.78	1.79	1.80	1.81	1.88	1.84	1.85	1.86
15	1.88	1.89	1.90	1.91	1.93	1.94	1.95	1.96	1.98	1.99
16	2.00	2.01	2.03	2.04	2.05	2.06	2.08	2.09	2.10	2.11
17	2.18	2.14	2.15	2.16	2.18	2.19	2.20	2.21	2.28	2.24
18	2.25	2.26	2.28	2.29	2.80	2.31	2.33	2.84	2.85	2.36
19	2.88	2.89	2.40	2.41	2.48	2.44	2.45	2.46	2.48	2-49
20	2.50	2.51	2.58	2.54	2.55	2.56	2.58	2.59	2.60	2.61
21	2.63	2.64	2.65	2.66	2.68	2.69	2.70	2.71	2.78	2.74
22	2.75	2.76	2.78	2.79	2.80	2.81	2.83	2.84	2.85	2.86
23	2.88	2.89	2.90	2.91	2.98	2.94	2.95	2.96	2.98	2.99
24	8.00	8.01	8.08	8.04	8.05	3.06	3.06	8.09	8-10	8.11
25	8.18	8.14	8.15	8.16	8.18	8.19	8.20	8.21	8.23	8.24
26	8.25	8.26	8.28	8.29	8.80	8.81	3.38	8.84	3.85	8.36
27	8.88	8.39	8.40	8.41	8.43	8.44	8.45	8.46	2.48	3.49
29	3.50 3.63	8.51 3.64	3.53 3.65	3.54 2.66	2.55 2.66	3.69	8.58 8.70	8.59 8.72	3.60 3.73	3.61 3.74
20 20	8.75	3.77	3.78	3.79	2.80	3.65 3.82	8.88	3.84	3-85	3.87
30	0.70		- 10		2.00			A-0.6		
81	8.88	8-89	8.80	8.93	3.98	3.94	8.96	3.97	3.98	3.99
82	4.00	4.02	4.03	4.04	4.05	4.07	4-08	4.09	4.10	4.12
33	4.18	4.14	4.15	4.17	4.16	4.19	4.20	4.28	4.23	4.34
84	4.25	4.27	4.28	4.29	4.30	4.82	4.33	4.84	4.85	4-87
35	4.88	4.89	4.40	4.43	4.48	4.44	1.45	4.47	4.48	4.49
	0.	1.	2.	3.	4.	5.	4	2.	8.	9.

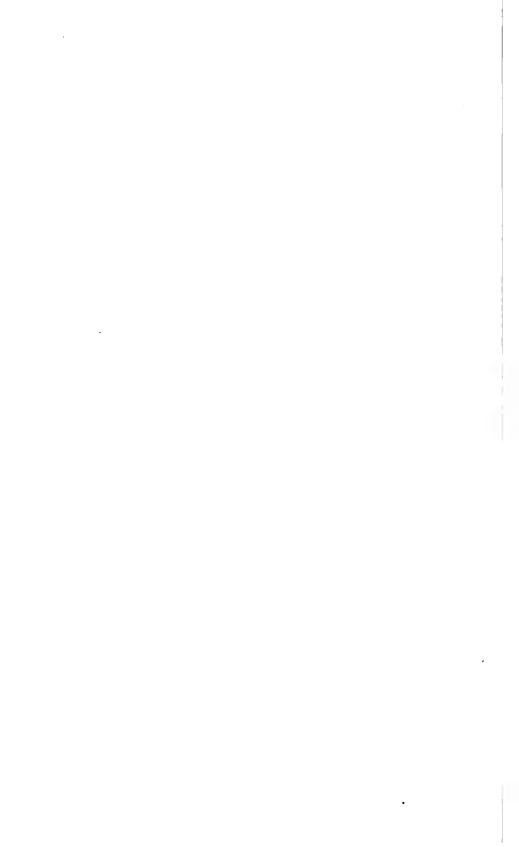
		В	AROMI	ETER :	780	(from '	777.51 t	o 782.5	0).	
Centi- grade Degrees.					Tenthe o	f Degrees,				
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.00	0.01	0.08	0.04	0.05	0.06	0.08	0.09	0.10	0.11
	0.13	0.14	0.15	0.16	0.18	0.19	0.30	0.21	0.23	0.24
1 2	0.13	0.14	0.18	0.10	0.10	0.15	0.88	0.84	0.25	0.24
8	0.38	0.39	0.40	0.42	0.48	0.44	0.45	0.47	0.48	0.49
4	0.50	0.52	0.53	0.54	0.55	0.57	0.58	0.59	0.60	0.62
5	0.63	0.64	0.65	0.67	0.68	0.69	0.70	0.72	0.78	0.74
ii l	1		1		I	1	1		l	
6	0.76	0.77	0.78	0.79	0.81	0.82	0.88	0.84	0.86	0.87
7	0.88	0.89	0.91	0.92	0.98	0.94	0.96	0.97	0.96	0.99
8	1.01	1.02	1.08	1.04	1.06	1.07	1.06	1.10	1.11	1.12
9	1.13	1.15	1.16	1.17	1.18	1.20	1.21	1.22	1.23	1.25
10	1.26	1.27	1.28	1.80	1.81	1.82	1.88	1.85	1.36	1.87
n	1.88	1.40	1.41	1.42	1.44	1.45	1.46	1.47	1.49	1.50
12	1.51	1.52	1.54	1.55	1.56	1.57	1.59	1.60	1.61	1.62
13	1.64	1.65	1.66	1.67	1.69	1.70	1.71	1.72	1.74	1.75
14	1.76	1.78	1.79	1.80	1.81	1.88	1.84	1.85	1.86	1.88
15	1.89	1.90	1.91	1.98	1.94	1.95	1.96	1.98	1.99	2.00
16	2.01	2.03	2.04	2.05	2.06	2.08	2.09	2.10	2.11	2.18
17	2.14	2.15	2.17	2.18	2.19	2.20	2.22	2.23	2.24	2.25
18	2.27	2.29	2.29	2.30	2.82	2.88	2.84	2.85	2.37	2.88
19	2.39	2.40	2.42	2.48	2.44	2.45	2.47	2.48	2.49	2.51
20	2.52	2.58	2.54	2.56	2.57	2.58	2.59	2.61	2.62	2.68
21	2.64	2.66	2.67	2.68	2.69	2.71	2.72	2.78	2.74	2.76
22	2.77	2.78	2.79	2.81	2.82	2.83	2.85	2.86	2.87	2.88
28	2.90	2.91	2.92	2.98	2.95	2.96	2.97	2.98	3.00	3.01
24	8.02	3.03	3.05	8.06	8.07	8.08	8.10	3.11	8.12	8.14
25	3.15	8.16	8.17	8.19	8.20	8.21	8.22	3.24	8.25	8.26
26	8.27	3.29	3.80	8.81	3.82	8.84	8.25	8.86	8.87	8.89
27	8.40	8.41	8.42	8.44	8.45	8.46	8.47	8.49	3.50	8.51
28	8.52	8.54	8.55	8.56	8.58	8.59	8.60	8.61	8.68	8.64
29	8.65	8.66	8.68	3.69	8.70	8.71	8.78	8.74	3.75	8.76
30	8.78	8.79	8.86	8.81	3.53	8.84	8.85	8.86	3.88	8.89
31	3.90	8.92	8.98	3.94	3.95	8.97	3.98	8.99	4.00	4.02
82	4.08	4.04	4.05	4.07	4.08	4.09	4.10	4.12	4.18	4.14
33	4.15	4.17	4.18	4.19	4.20	4.22	4.28	4.24	4.26	4.27
34	4.28	4.29	4.31	4.32	4.35	4.84	4.36	4.87	4.88	4.89
35	4.41	4.42	4-48	4.44	4.46	4.47	4.48	4.49	4.51	4.52
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В.	AROMI	ETER :	785***	(from	782.51	to 78 7.5	0).	
Centi- grade Dogress.					Tenths o	Degrees.				-
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.03	Millim, 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.08	Millim. 0.09	Millim, 0.10	Millim. 0.11
1	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.22	0.23	0.24
2	0.25	0.27	0.28	0.29	0.30	0.82	0.33	0.84	0.85	0.87
8	0.88	0.89	0.41	0.42	0.48	0.44	0.46	0.47	0.48	0.49
4	0.51	0.52	0.58	0.54	0.56	0.57	0.58	0.60	0.61	0.62
5	0.68	0.65	0.66	0.67	0.68	0.70	0.71	0.72	0.78	0.75
6	_0.76	0.77	0.79	0.80	0.81	0.82	0.84	0.85	0.86	0.87
7	0.89	0.90	0.91	0.92	0.94	0.95	0.96	0.98	0.99	1.00
8	1.01	1.03	1.04	1.05	1.06	1.08	1.09	1.10	1.11	1.13
9	1.14	1.15	1.17	1.18	1.19	1.20	1.22	1.23	1.24	1.25
10	1.27	1.28	1.29	1.80	1.82	1.88	1.84	1.36	1.87	1.38
11	1.89	1.41	1.42	1.48	1.44	1.46	1.47	1.48	1.50	1.51
12	1.52	1.58	1.55	1.56	1.57	1.58	1.60	1.61	1.62	1.63
13	1.65	1.66	1.67	1.69	1.70	1.71	1.72	1.74	1.75	1.76
14	1.77	1.79	1.80	1.81	1.82	1.84	1.85	1.86	1.88	1.89
15	1.90	1.91	1.93	1.94	1.95	1.96	1.98	1.99	2.00	2.01
16	2.03	2.04	2.05	2.07	2.08	2.09	2.10	2.12	2.18	2.14
17	2.15	2.17	2.18	2.19	2.20	2.22	2.23	2.24	2.26	2.27
18	2.28	2.29	2.81	2.32	2.83	2.34	2.36	2.37	2.88	2.39
19	2.41	2.42	2.43	2.45	2.46	2.47	2.48	2.50	2.51	2.52
20	2.58	2.55	2.56	2.57	2.58	2.60	2.61	2.62	2.64	2.65
21	2.66	2.67	2.69	2.70	2.71	2.72	2.74	2.75	2.76	2.77
22	2.79	2.80	2.81	2.83	2.84	2.85	2.86	2.88	2.89	2.90
28	2.91	2.93	2.94	2.95	2.96	2.98	2.99	3.00	3.02	3.03
24	8.04	8.05	8.07	3.06	8.09	8.10	8.12	3.13	8.14	8.15
25	8.17	8.18	8.19	8.21	3.22	8.23	8.24	3.26	3.27	8.28
26	3.29	8.31	8.82	8.88	8.84	8.36	8.37	3.38	3.40	3.41
27	3.42	8.43	8.45	8.46	8.47	8.48	8.50	8.51	3.52	3.53
28	8.55	8.56	8.57	8.59	3.60	3.61	8.62	3.64	3.65	8.66
29	8.67	8.69	8.70	8.71	3.72	8.74	8.75	8.76	8.78	8.79
80	3.80	8.81	8.83	8.84	8.85	8.86	3.88	3.89	3.90	3.91
81	8.98	8.94	3.95	3.97	3.98	3.99	4.00	4-02	4.08	4.04
82	4.05	4.07	4.08	4.09	4.11	4.12	4.13	4.14	4.16	4-17
88	4-18	4.19	4.21	4.22	4.28	4.24	4.26	4.27	4.28	4.30
84	4.31	4.82	4.83 4.46	4.85	4.86	4.87	4.88	4.40	4.41	4.42
85	4.43	4.45	5.40	4-47	4.49	4.50	4.51	4.52	4.54	4.55
	0.	1,	2.	8.	4.	5.	6.	7.	8.	9.

		BAROMETER: 790 ^{mm.} (from 787.51 to 792.50).									
Centi- grade Degrees.					Tenthe of	f Dogrees.					
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.	
Ö	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	
0	0.00	0.01	0.03	0.04	0.05	0.06	0.08	0.09	0.10	0.11	
1	0.13	0.14	0.15	0.17	0.18	0.19	0.20	0.22	0.23	0.24	
2	0.26	0.27	0.28	0.29	0.81	0.32	0.88	0.34	0.36	0.87	
8	0.88	0.40	0.41	0.42	0.48	0.45	0.46	0.47	0.48	0.50	
4	0.51	0.52	0.54	0.55	0.56	0.57	0.59	0.60	0.61	0.62	
5	0.64	0.65	0.66	0.68	0.69	0.70	0.71	0.78	0.74	0.75	
ا ۾ ا	0.77	0.78	0.79	0.80	0.82	0.83	0.84	0.85	0.87	0.88	
6 7	0.77	0.78	0.79	0.93	0.82	0.96	0.84	0.85	0.87	1.01	
8	1.02	1.03	1.05	1.06	1.07	1.08	1.10	1.11	1.12	1.18	
9	1.15	1.16	1.17	1.19	1.20	1.31	1.22	1.24	1.25	1.26	
10	1.28	1.29	1.80	1.81	1.38	1.84	1.35	1.36	1.38	1.89	
11	1.40	1.42	1.48	1.44	1.45	1.47	1.48	1.49	1.50	1.52	
12	1.58	1.54	1.56	1.57	1.58	1.59	1.61	1.62	1.68	1.64	
13	1.66	1.67	1.68	1.70	1.71	1.72	1.73	1.75	1.76	1.77	
14	1.79	1.80	1.81	1.82	1.84	1.85	1.86	1.87	1.89	1.90	
15	1.91	1.98	1.94	1.95	1.96	1.98	1.99	2.00	2.01	2.03	
16	2.04	2.05	2.07	2.08	2.09	2.10	2.12	2.18	2.14	2.15	
17	2.17	2.18	2.19	2.21	2.22	2.28	2.24	2.26	2.27	2.28	
18	2.80	2.81	2.82 2.45	2.88 2.46	2.85	2.36	2.37 2.50	2.88	2.40	2.41	
19 20	2.42 2.55	2.44 2.56	2.45 2.58	2.46	2.47 2.60	2.49 2.61	2.63	2.51 2.64	2.52 2.65	2.54 2.66	
20	0.00	2.00	D. UC	2.09	2.00	2.01	2.03	a.04	00.م	2.00	
21	2.68	2.69	2.70	2.72	2.73	2.74	2.75	2.77	2.78	2.79	
22	2.81	2.82	2.88	2.84	2.86	2.87	2.88	2.89	2.91	2.92	
23	2.93	2.95	2.96	2.97	2.98	8.00	8.01	8.02	8.03	8.05	
24	8.06	8.07	8.09	8.10	3.11	3.12	8.14	8.15	8.16	3.17	
25	3.19	8.20	3.21	8.28	8.24	8.25	3.26	8.28	8.29	8.30	
							\				
26	8.82	8.83	8.84	8.85	8.87	8.88	8.89	8.40	8.42	3.48	
27	8.44	3.46	8.47	8.48	3.49	8.51	3.52	3.58	8.54	8.56	
28	8.57	3.58	8.60	8.61	3.62	8.68	3.65	8.66	8.67	3.68	
29	8.70	8.71	8.72	8.74	8.75	3.76	8.77	8.79	8.80	8.81	
30	8.83	8.84	8.85	8.86	8.88	8.89	8.90	3.91	3.98	8.94	
81	3.95	8.97	3.98	8.99	4.00	4.02	4.03	4.04	4.05	4.07	
32	4.08	4.09	4.11	4.12	4.18	4.14	4.16	4.17	4.18	4.19	
83	4.21	4.22	4.28	4.25	4.26	4.27	4.28	4.80	4.81	4.32	
84	4.84	4.85	4.86	4.87	4.89	4.40	4.41	4.42	4.44	4.45	
85	4.46	4.48	4.49	4.50	4.51	4.53	4.54	4.55	4.56	4.58	
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.	

		В	AROME	ETER:	795····	(from '	792.51 1	o 79 7.5	0).	
Centi- grade Degrees.					Tenthe o	f Degrees.				
	0.	1.	2.,	3.	4.	5.	6.	7.	8.	9.
٥٥	Millim. 0.00	Millim. 0.01	Millim. 0.08	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.08	Millim. 0.09	Millim. 0.10	Millim. 0.12
1	0.18	0.14	0.15	0.17	0.18	0.19	0.21	0.22	0.23	0.24
2	0.26	0.27	0.28	0.30	0.81	0.32	0.88	0.85	0.36	0.37
8	0.88	0.40	0.41	0.42	0.44	0.45	0.46	0-47	0.49	0.50
4	0.51	0.58	0.54	0.55	0.56	0.58	0.59	0.60	0.62	0.63
5	0.64	0.65	0.67	0.68	0.69	0.71	0.72	0.78	0.74	0.76
اما		0.80	0.80	0.01	0.00	0.00	0.00	0.00	0.00	0.89
6 7	0.77	0.78 0.91	0.92	0.81 0.94	0.82 0.95	0.88	0.85	0.86	0.87 1.00	1.01
8	1.03	1.04	1.05	1.06	1.08	1.09	1.10	1.12	1.18	1.14
9	1.15	1.17	1.18	1.19	1.21	1.22	1.22	1.24	1.26	1.27
10	1.28	1.30	1.81	1.82	1.88	1.35	1.86	1.87	1.89	1.40
									i	1
11	1.41	1.42	1.44	1.45	1.46	1.48	1.49	1.50	1.51	1.58
12	1.54	1.55	1.57	1.58	1.59	1.60	1.62	1.63	1.64	1.66
13	1.67	1.68	1.69	1.71	1.72	1.73	1.75	1.76	1.77	1.78
14	1.80	1.81	1.82	1.88	1.85	1.86	1.87	1.89	1.90	1.91
15	1.92	1.94	1.95	1.96	1.98	1.99	2.00	2.01	2.03	2.04
16	2.05	2.07	2.08	2.09	2.10	2.12	2.18	2.14 2.27	2.16 2.28	2.17 2.30
17 18	2.18 2.81	2.19 2.82	2.21 2.84	2.22 2.85	2.28 2.86	2.25 2.87	2.26 2.39	2.40	2.41	2.43
19	2.44	2.45	2.46	2.48	2.49	2.50	2.51	2.58	2.54	2.55
20	2.57	2.58	2.59	2.60	2.62	2.68	2.64	2.66	2.67	2.68
-					_10_			2.00	2.0.	
21	2.69	2.71	2.72	2.78	2.75	2.76	2.77	2.78	2.80	2.81
22	2.82	2.84	2.85	2.86	2.87	2.89	2.90	2.91	2.93	2.94
23	2.95	2.96	2.96	2.99	3.00	8.02	8.03	8.04	8.05	8.07
24	8.08	8.09	8.11	8.12	8.18	8.14	8.16	8.17	8.18	8.19
25	8.21	3.22	8.28	8.25	8.26	8.27	8.28	8.80	8.31	8.32
									·	
26	8.84	8.85	3.36	8.37	8.89	8.40	8.41	8.48	8.44	3.45
27	8.46	8.48	3.49	3.50	8.52	3.53	8.54	8.55	8.57	3.58
28 29	8.59	8.61 8.78	3.62 3.75	8.63 8.76	3.64	8.66 8.79	3.67 8.80	3.68	8.70 3.82	8.71 8.84
80	8.72 8.85	8.86	8.88	3.89	8.77 8.90	8.79 8.91	8.98	8.81 8.94	8.95	8.96
55	0.00	2.50	2.55	0.05	J.00	J.31	U-90	0.54	2.50	
81	8.98	8.99	4.00	4.09	4-08	4.04	4.05	4.07	4.08	4.09
82	4.11	4.12	4.18	4.14	4.16	4.17	4.18	4.20	4.21	4.22
88	4.28	4.25	4.26	4.27	4.29	4.30	4.81	4.32	4.84	4.85
84	4.86	4.88	4.89	4.40	4-41	4.48	4.44	4.45	4.47	4.48
85	4.49	4.50	4.52	4.58	4.54	4.56	4.57	4.58	4.59	4.61
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

		BAROMETER: 800 (from 797.51 to 802.50).									
Centi- grade Degrees.					Tenths o	f Degrees.					
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.	
°	Millim. 0.00	Millim. 0.01	Millim. 0.03	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.08	Millim. 0.09	Millim. 0.10	Millim, 0.12	
1	0.13	0.14	0.15	0.17	0.18	0.19	0.21	0.22	0.23	0.25	
2	0.26	0.27	0.28	0.80	0.81	0.32	0.84	0.85	0.86	0.87	
8	0.89	0.40	0.41	0.48	0.44	0.45	0.46	0.48	0.49	0.50	
4	0.52	0.58	0.54	0.56	0.57	0.58	0.59	0.61	0.62	0.63	
5	0.65	0.66	0.67	0.68	0.70	0.71	0.72	0.74	0.75	0.76	
6	0.77	0.79	0.80	0.81	0.83	0.84	0.85	0.87	0.88	0.89	
7	0.90	0.92	0.93	0.94	0.96	0.97	0.98	0.99	1.01	1.02	
8	1.08	1.05	1.06	1.07	1.08	1.10	1.11	1.12	1.14	1.15	
9	1.16	1.17	1.19	1.20	1.21	1.23	1.24	1.25	1.27	1.28	
10	1.29	1.80	1.82	1.83	1.84	1.86	1.87	1.88	1.89	1.41	
n	1.42	1.43	1.45	1.46	1.47	1.48	1.50	1.51	1.52	1.54	
12	1.55	1.56	1.58	1.59	1.60	1.61	1.63	1.64	1.65	1.67	
13	1.68	1.69	1.70	1.72	1.73	1.74	1.76	1.77	1.78	1.79	
14	1.81	1.82	1.83	1.85	1.86	1.87	1.89	1.90	1.91	1.92	
15	1.94	1.95	1.96	1.98	1.99	2.00	2.01	2.08	2.04	2.05	
16	2.07	2.08	2.09	2.10	2.12	2.18	2.14	2.16	2.17	2.18	
17	2.20	2.21	2.22	2.23	2.25	2.26	2.27	2.29	2.80	2.31	
18	2.82	2.84	2.85	2.86	2.88	2.39	2.40	2.41	2.48	2.44	
19	2.45	2.47	2.48	2.49	2.50	2.52	2.53	2.54	2.56	2.57	
20	2.58	2.60	2.61	2.62	2.68	2.65	2.66	2.67	2.69	2.70	
21	2.71	2.72	2.74	2.75	2.76	2.78	2.79	2.80	2.81	2.83	
22	2.84	2.85	2.87	2.88	2.89	2.91	2.92	2.98	2.94	2.96	
23	2.97	2.98	8.00	8.01	8.02	8.03	3.05	8.06	8.07	8.09	
24	8.10	8.11	3.12	8.14	8.15	3.16	8.18	8.19	3.20	8.22	
25	8.28	8.24	3.25	8.27	8.28	3.29	3.81	8.82	3.83	8.84	
26	8.86	3.87	3.38	8.40	8.41	8.42	3.43	8.45	8.46	8.47	
27	8.49	8.50	3.51	8.52	8.54	8.55	8.56	3.58	8.59	8.60	
28	8.62	8.63	3.64	8.65	8.67	8.68	3.69	8.71	8.72	8.73	
29	3.74	3.76	8.77	8.78	8.80	8.81	8.82	8.88	3.85	8.86	
30	3.87	8.89	8.90	8.91	8.98	8.94	8.95	8.96	8.98	8.99	
31	4.00	4.02	4.08	4.04	4.05	4.07	4.08	4-09	4.11	4.12	
32	4.18	4.14	4.16	4.17	4.18	4.20	4.21	4.22	4.24	4.25	
33	4.26	4.27	4.29	4.80	4.81	4.83	4.84	4.85	4.36	4.38	
34	4.89	4.40	4.42	4.48	4.44	4.45	4.47	4.48	4.49	4.51	
35	4.52	4.58	4.55	4-56	4.57	4.58	4.60	4.61	4.62	4.64	
-	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.	
	•					l 🦈		••	•	- •	



XXI.

OLD FRENCH BAROMETER.

TABLE

FOR

REDUCING TO THE FREEZING POINT THE OBSERVATIONS

TAKEN WITH OLD FRENCH BAROMETERS,

PROVIDED WITH BRASS SCALES, EXTENDING FROM THE CISTERN TO THE
TOP OF THE MERCURIAL COLUMN; CALCULATED FROM 240 TO 345
LINES, OF FROM 28 INCHES 4 LINES TO 28 INCHES 9 LINES.

By Karmtz.

TABLE XXI.

This table is taken from KARMTZ's Lehrbuch der Meteorologie, Vol. II. p. 236. To render it more useful, the first page, giving the corrections for Barometrical Heights between 240 and 280 Paris lines, has been added.

The values adopted by Kaemtz for reducing the Old French Barometer are the following: —

Let h =observed height in French lines.

- " t = temperature of attached thermometer in degrees of Reaumur.
- " $m = \text{expansion of mercury between 0 and 80}^{\circ}$ Reaumur = 0.018018.
- " l = linear expansion of brass between 0 and 80" Reaumur = 0.0018782.

The normal temperature of standard being = 13° Reaumur.

And the formula becomes, —

Observed height

$$-h \cdot \frac{m \times t - l \cdot (t - 13)}{1 + m \times t}$$

The Table gives the corrections only for full degrees and for every fifth line; but the intermediate values can easily be found by an interpolation at sight.

Example of Reduction.

925 22 lines

Cosetted neight	•	•	•	•	•	•		323.04	i imce
Attached thermon	eter	•	•				=	12.5	Reaumur.
In the line beginning w	rith 12	°, ar	nd in t	he v	ertic	al col	umn h	eaded	325 lines,
we find,	Cor	recti	on for	19	2°	=-	-0.89	lines.	
	Inte	rpol	ation f	or (0°.5	= -	-0.03	"	
	Cor	recti	on for	19	2°.5	=-	-0.92		
And we have,									
	Obe	erve	d heig	ht,		3	25.32	44	
	Cor	recti	on for	12°.	5,	-	-0.92	66	
н	eight s	it the	freez	ing	point	$=$ $\frac{1}{3}$	24.40	lines.	

Normal Temperature of the Scale = 180 Resumur.

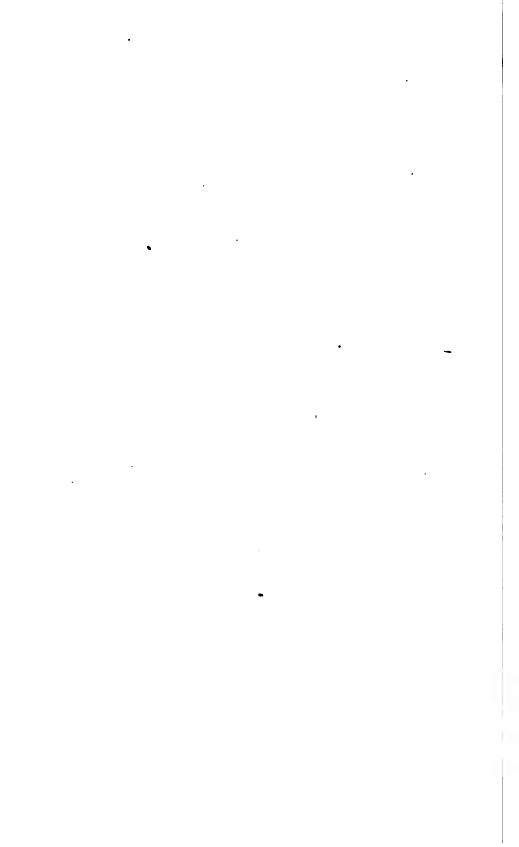
Attached Thermom- eter.		Barometer in Paris Lines.									
Degrees of Resumur.	240	245	250	255	260	265	270	275	Degrees of Resumur.		
0	Par. Lines.		Par. Lines.						0		
-15	+0.65	+0.66	+0.68	+0.69	+0.70	+0.72	+0.78	+0.75	-15		
-14	0.60	0.61	0.68	0.64	0.65	0.67	0.68	0.69	-14		
-18 -12	0.55	0.57	0.58	0.59	0.60	0.61	0.62	0.64	-13 -12		
-12 -11	0.51	0.52	0.58 0.48	0.54	0.55	0.56 0.51	0.57 0.52	0.58	-12		
-10	0.41	0.47	0.43	0.49	0.50	0.45		0.47	-10		
-10	0.41	0.44	0.40	0.44	0.44	0.40	9.46	0.47	-10		
- 9	+0.36	+0.87	+0.88	+0.38	+0.29	+0.40	+0.41	+0.41	- 9		
-8	0.31	0.82	0.88	0.88	0.84	0.85	0.85	0.36	-8		
-7	0.27	0.27	0.28	0.28	0.29	0.29	0.80	0.80	-7		
-6	0.22	0.22	0.28	0.28	0.24	0.24	0.24	0.25	-6		
- 5	0.17	0.17	0.18	0.18	0.18	0.19	0.19	0.19	- 5		
			0120								
-4	+0.12	+0.12	+0.18	+0.18	+0.18	+0.18	+0.14	+0.14	-4		
-8	0.07	0.07	0.08	0.08	0.08	0.06	0.08	0.08	-8		
- 2	+0.02	+0.03	+0.03	+0.03	+0.08	+0.03	+0.08	+0.03	- 2		
-1	-0.02	-0.03	-0.03	-0.03	-0.03	-0.08	-0.08	-0.03	-1		
0	-0.07	-0.07	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	0		
			i					1	<u> </u>		
+1	-0.12	-0.12	-0.13	-0.18	-0.18	−0.18	-0.14	-0.14	+1		
2	0.17	0.17	0.18	0.18	0.18	0.19	0.19	0.19	2		
3	0.22	0.22	0.28	0.28	0.24	0.24	0.24	0.25	8		
4	0.27	0.27	0.28	0.28	0.29	0.29	0.30	0.80	4		
5	0.81	0.82	0.88	0.38	0.84	0.85	0.85	0.86	5		
					0.00	0.40		-0.41			
+ 6	-0.86	-0.87	-0.38	-0.88	-0.29	-0.40 0.45	-0.41 0.46	0.47	+ 6		
7	0.41	0.42	0.43	0.44	0.44	0.45	0.52	0.52	8		
8	0.46	0.47	0.48 0.53	0.49	0.55	0.56	0.57	0.58	9		
10	0.55	0.52	0.58	0.59	0.60	0.61	0.62	0.64	10		
10	0.55	0.07	V-55	0.09	0.00	0.01	U-04	0.01	"		
+11	-0.60	-0.61	-0.63	-0.64	-0.65	-0.67	-0.68	-0.69	+11		
12	0.65	0.66	0.68	0.69	0.70	0.72	0.78	0.75	12		
13	0.70	0.71	0.78	0.74	0.76	0.77	0.79	0.80	18		
14	0.75	0.76	0.78	0.79	0.81	0.82	0.84	0.86	14		
15	0.80	0.81	0.88	0.84	0.86	0.88	0.89	0.91	15		
	I		l	1			1				
+16	-0.84	-0.86	-0.88	-0.90	-0.91	-0.98	-0.95	-0.97	+16		
17	0.89	0.91	0.93	0.95	0.97	0.96	1.00	1.02	17		
18	0.94	0.96	0.96	1.00	1.02	1.04	1.06	1.08	18		
19	0.99	1.01	1.08	1.05	1.07	1.09	1.11	1.18	19		
20	1.04	1.06	1.08	1.10	1.12	1.14	1.17 -	1.19	20		
}	ì	l									
+21	-1.08	-1.11	-1.18	-1.15	-1.17	-1.20	-1.22	-1.24	+21		
22	1.18	1.16	1.18	1.20	1.28	1.25	1.27	1.30	22		
28	1.18	1.20	1.28	1.25	1.28	1.80	1.88	1.85	28		
24	1.28	1.25	1.28	1.81	1.38	1.86	1.38	1.41	24		
25	1.28	1.80	1.33	1.36	1.88	1.41	1.44	1.46	25		

Normal Temperature of the Scale == 13° Resumur.

Attached Thermom- eter.			Baron	peter in Paris	Lines.			Attached Thormom- ster.
Degrees of Resumur.	250	285	290	295	300	80 5	310	Degrees of Reaumur.
0	Par. Lines.	Par. Lines.	Par. Lines.	Par. Lines.	Par. Lines.	Par. Lines.	Par. Lines.	
-15	+0.77	+0.78	+0.79	+0.81	+0.82	+0.84	+0.85	-15
-14	0.71	0.78	0.74	0.75	0.76	0.77	0.79	-14
-18	0.65	0.67	0.68	0.69	0.70	0.71	0.72	-18
-12 -11	0.60	0.61	0.62	0.68	0.64	0.65	0.66	-12
-10	0.54	0.49	0.50	0.57	0.58	0.59	0.60	-11
-10	0.48	. 0.43	0.50	0.51	0.52	0.58	0.54	-10
- 9	+0.48	+0.44	+0.44	+0.45	+0.46	+0.46	+0.47	- 9
-8	0.87	0.88	0.38	0.89	0.40	0.40	0.41	- 8
- 7	0.81	0.82	0.32	0.83	0.84	0.84	0.35	- 7
- 6	0.26	0.26	0.26	0.27	0.27	0.28	0.28	-6
- 5	0.20	0.20	0.21	0.21	0.21	0.22	0.22	- 5
		10.15	+0.15		.0.75			
- 4 - 3	+0.14	+0.15	0.09	+0.15	+0.15 0.09	+0.16 0.09	+0.16 0.09	-4 -8
- 2	+0.08	+0.08	+0.08	+0.08	+0.08	+0.03	+0.03	-3
-1	-0.08	-0.03	-0.08	-0.08	-0.08	-0.03	-0.08	- i
i	-0.08	-0.09	-0.09	-0.09	-0.09	-0.09	-0.09	
ľ	0.06	-0.09	0.00	-0.09	-0.09	-0.09	-0.00	Ů
+1	-0.14	-0.14	-0.15	-0.15	-0.15	-0.15	−0.16	+ 1
2	0.20	0.20	0.21	0.21	0.21	0.22	0.22	2
8	0.26	0.26	0.27	0.27	0.27	0.28	0.28	8
- 4	0.81	0.82	0.82	0.38	0.88	0.34	0.85	4
5	0.37	0.87	0.28	0.89	0.40	0.40	0.41	5
+ 6	-0.43	-0.43	-0.44	-0.45	-0.46	-0.46	0.47	+6
7	0.48	0.49	0.50	0.51	0.52	0.58	0.58	7
8	0.54	0.55	0.56	0.57	0.58	0.59	0.60	8
9	0.60	0.61	0.62	0.68	0.64	0.65	0.66	9
10	0.65	0.66	0.68	0.69	0.70	0.71	0.72	10
				_	_			
+11	-0.71	-0.72	-0.74	-0.75	-0.76	-0.77	-0.79	+11
12	0.77	0.78	0.80	0.81	0.82	0.84	0.85	12
13	0.82	0.84	0.85	0.87	0.88	0.90	0.91	13
14	0.88	0.90	0.91	0.93	0.94	0.96	0.96	14
15	0.94	0.95	0.97	0.99	1.00	1.02	1.04	15
+16	-0.99	-1.01	-1.08	-1.05	-1.07	-1.08	-1.10	+16
17	1.05	1.07	1.09	1.11	1.18	1.15	1.16	17
18	1.11	1.13	1.15	1.17	1.19	1.21	1.23	18
19	1.16	1.18	1.21	1.28	1.25	1.27	1.29	19
20	1.22	1.24	1.27	1.29	1.81	1.83	1.35	200
101	-1.28	-1.80	-1.33	_1 0#	_1 ===	_1 00	_1.6	L01
+21 22	1.84	1.36	1.38	-1.85	-1.87	-1.89 1.45	-1.42	+21 22
23	1.39	1.41	1.44	1.41 1.47	1.43 1.49		1.48 1.54	23
24	1.45	1.47	1.50	1.47	1.49	1.52 1.58	1.60	24
25	1.50	1.58	1.56	1.58	1.61	1.64		25
20	1.50	1.00	1 1.00	1.09	1.61	1.04	1.67	150

Normal Temperature of the Scale == 13° Resumur.

Attached Thermom- eter.			Baron	eter in Paris	Lines.			Attached Thermom- eter.
Degrees of Resumur.	315	820	325	380	885	340	845	Degrees of Resumur.
	Par. Lines.	Par. Lines.	Par. Lines.	Par. Lines.	Par. Lines.	Par. Lines.	Par. Lines.	
-15	+0.86	+0.88	+0.89	+0.90	+0.92	+0.98	+0.95	-15
-14	0.80	0.81	0.88	0.84	0.85	0.86	0.88	-14
-13	0.74	0.75	0.76	0.78	0.78	0.79	0.81	-18
-12	0.67	0.68	0.69	0.70	0.71	0.78	0.74	-12
-11	0.61	9.62	0.68	0.64	0.65	0.66	0.67	-11
-10	0.54	0.55	0.56	0.57	0.58	0.59	0.60	-10
- 9	+0.48	+0.49	+0.50	+0.50	+0.51	+0.52	+0.58	- 9
-8	0.42	0.42	0.48	0.44	0.44	0.45	0-46	- 8
- 7	0.85	0.36	0.86	0.87	0.87	0.88	0.39	- 7
- 6	0.29	0.29	0.30	0.30	0.31	0.81	0.32	- 6
- 5	0.22	0.23	0.28	0.24	0.24	0.24	0.25	- 5
-4	+0.16	+0.16	+0.17	+0.17	+0.17	+0.17	+0.18	-4
-8	0.10	0.10	0.10	0.10	0.10	0.10	0.11	- 8
- 2	+0.03	+0.03	+0.03	+0.03	+0.03	+0.03	+0.04	- 2
- 1	-0.03	-0.03	-0.03	-0.03	−0.03	-0.03	-0.08	-1
0	-0.10	-0.10	-0.10	-0.10	-0 .10	-0.10	-0.10	0
+ 1	-0.16	-0.16	-0.16	-0.17	-0.17	-0.17	-0.17	+1
2	0.22	0.23	0.23	0.28	0.24	0.24	0.24	2
8	0-29	0.29	0.30	0.30	0.31	0.81	0.81	8
4	0.35	0.36	0.36	0.37	0.37	0.38	0.88	4
5	0.42	0.42	0.43	0.44	0.44	0.45	0.45	5
+6	-0.48	-0.49	-0.49	-0.50	-0.51	-0.52	-0.53	+ 6
7	0.54	0.55	0.56	0.57	0.58	0.59	0.60	7
8	0.61	0.62	0.63	0.64	0.65	0.66	0.67	8
9	0.67	0.68	0.69	0.70	0.71	0.72	0.74	9
10	0.74	0.75	0.76	0.77	0.78	0.79	0.81	10
+11	-0.80	-0.81	-0.82	-0.84	-0.85	-0.86	-0.88	+11
12	0.86	0.88	0.89	0.90	0.92	0.98	0.95	12
13	0.93	0.94	0.96	0.97	0.99	1.00	1.02	18
14	0.99	1.01	1.02	1.04	1.05	1.07	1.09	14
15	1.05	1.07	1.09	1.10	1.12	1.14	1.16	15
+16	-1.12	-1.14	-1.15	-1.17	-1.19	-1.21	-1.23	+16
17	1.18	1.20	1.22	1.24	1.26	1.28	1.30	17
18	1.25	1.27	1.29	1.31	1.33	1.85	1.87	18
19	1.81	1.33	1 85	1.87	1.89	1.41	1.44	19
20	1.87	1.40	1.42	1.44	1.46	1.48	1.51	220
+21	-1.44	-1.46	-1.48	-1.51	-1.53	-1.55	-1.58	+21
22	1.50	1.58	1.55	1.57	1.60	1.62	1.65	22
23	1.57	1.59	1.62	1.64	1.67	1.69	1.72	28
24	1.63	1.66	1.68	1.71	1.78	1.76	1.79	24
25	1.69	1.72	1.75	1.78	1.80	1.88	1.86	25



TABLES

FOR CORRECTING THE

DEPRESSION OF THE BAROMETRICAL COLUMN

DUE TO CAPILLARY ACTION.

CORRECTION FOR CAPILLARY ACTION.

It is known that the effects of capillary action are not the same in different liquids. In a tube plunged in water, the liquid in the tube rises higher than the level of the water in the vessel, and terminates by a concave surface, which is called a concave meniscus. In a tube plunged in mercury the liquid in the tube stands lower than the mercury in the vessel, and terminates by a convex surface, or a convex meniscus. It is thus evident that the mercurial column in the tube of a Barometer does not rise to its true height, and that it needs to be corrected for the depression due to capillarity, before it indicates the real pressure of the atmosphere.

La Place, in the Mécanique Céleste, Tom. IV., has shown that the value of that correction depends upon the form of the meniscus, and gave a formula to compute it. As this form varies in tubes of different bores, so does the depression, which diminishes as the diameter of the tube increases. The form of the meniscus, however, was supposed to be the same in tubes of the same diameter, and constant in the same tube; and on this supposition the tables generally used for correcting the capillary action have been computed. But more accurate observations have proved that, owing to various causes not yet all well understood, the form of the meniscus is often different in tubes of the same diameter, and that it is even variable in the tube of the same instrument.

It thus became necessary to construct new tables, taking into consideration, in a given case, both the diameter of the tube and the form of the meniscus. Such tables, with a double entry, have been given by Schleiermacher, in the Bibliothèque Universelle de Genève, Tom. VIII.; by Bravais, in the Annales de Physique et de Chimie, Tom. V. p. 508; and by Delcros. The numbers in these tables agree very closely; but as Delcros's table is more extended than that of Schleiermacher, and in a more convenient form than that of Bravais, it is given below, together with a reduction of it to English measures, for the ordinary use.

The other tables may serve for comparison.

Table XXII., from the Report of the Committee of Physics and Meteorology of the Royal Society of London, 1840, gives the correction to be applied to English barometers for capillary action in boiled and unboiled tubes. It takes into account the diameter of the tube, but not the variations of the height of the meniscus, or of the convexity which terminates the barometrical column. This last element is supposed to be in its normal state, and constant.

Tables XXIII. and XXIV., by Delcros, in the Annuaire Météorologique de France, for 1849, give the means of finding the true correction to be applied to metrical barometers for capillary action.

The first shows the normal height of the meniscus when in contact with the air (as is the case in the inferior branch of a siphon barometer), and in the barometric vacuum at the top of the column, in tubes of different bores. It enables the observer to judge better of its variations.

Table XXIV. has been calculated by Delcros after the formulas of Schleiermacher, making the constant x equal to $6^{mn}.5278$, being the mean value between that of Gay-Lussac = $6^{mn}.5262$, and that of Schleiermacher = $6^{mn}.5295$. It gives the amount of the capillary action in millimetres of mercury, taking into account both the size of the bore, or the internal radius of the tube, which will be found in the vertical argument, and the height of the meniscus, given in the horizontal argument. The internal radius of the tube is supposed to be known; the height of the meniscus, or the vertical distance from the base, that is, from the sharp line where the mercury ceases to be in contact with the walls of the tube, to the very top of the convexity, can be ascertained by measuring it several times by means of the vernier.

Example: — Suppose the internal radius of the tube to be $3^{mm}.2$, and the height of the meniscus to be $0^{mm}.8$; seek in the first vertical column the number $3^{mm}.2$; follow then the horizontal line as far as the vertical column headed $0^{mm}.8$, you find there the number $0^{mm}.776$, which is the amount of the depression due to capillary action, or the value of the correction to be added to the observation.

Table XXV. is taken from Pouillet's Eléments de Physique, Vol. II. p. 698 (1853). Table XXVI. is found in Gehler's Physicalisches Wörterbuch, and in Schubarth, Physicalische Tabellen, p. 21.

Table XXVII., which is Delcros's table reduced into English measures, gives the means of correcting with more accuracy the indications of the English barometers. For its use, see, above, the explanation to Table XXIV.

Table XXVIII. is from Baily's Astronomical Tables.

XXII. Table for the Correction to BE ADDED TO ENGLISH BAROMETERS FOR CAPILLARY ACTION.

Diameter	Correct	ion for
of Tube.	Unboiled Tubes.	Boiled Tubes.
Inch.	Inch.	Inch.
0.60	0.004	0.002
0.50	0.007	0.008
0.45	0.010	0.005
0.40	0.014	0.007
0.35	0.020	0.010
0.80	0.028	0.014
0.25	0.040	0.020
0.20	0.060	0.029
0.15	0.088	0.044
0.10	0.142	0.070

XXIII. TABLE OF THE HEIGHT OF THE MENISCUS OF THE BAROMETRICAL COLUMN.

Internal Radius of the Tube in	Normal Heig niscus in M	ht of the Me- fillimetres.
Millimetres.	In the Air.	In the Vacuum.
1	0.427	0.34
2	0.795	0.64
8	1.079	0.86
4	1.287	1.08
5	1.418	1.13
6	1.488	1.19
7	1.524	1.22

VERTICAL ARGUMENT = INTERNAL RADIUS OF TUBE. HORIZONTAL ARGUMENT = HEIGHT OF MENISCUS IN MILLIMETERS.

C	ladius of							-	Height of	the Men	Height of the Meniscus in Millimetres	(Illimetre	ار							Raditos of
	in Milli- metres.	0.1	0.3	0.8	4.0	0.5	9.0	0.7	9.0	6.0	1.0	1.1	1.9	8.1	4.1	1.5	1.6	1.7	1.8	the Tube to Milli- metrer.
	9	Millin.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millian.	Millen.	Millin.	Millim.	Milita.	Millim.	Millim.	Miller.	Millim.	Main.	٩
_	9	0.876		2.484	3.162	3.728	4.190	3	3	3	3	*	8	3	3		8	*		9
-	7	0.638		1.836	2.363	2.825	3.218	8.542	3	3	3	×	*	3	*	*	3	* :	3 :	7
=	9.	0.484	_	24	1.820	2.196	2.528	2.813	3.050	3	3		*		*		*			1.6
_	1.8	0.378		1.103	1.437	1.746	2.024	2.270	2.483	2.662	3	8		3		•	,		4	1.8
	6.0	0.302		0.885	1,158	1.413	1.648	1.859	2.046	908	9.348	*				*			*	0.6
-	6	0.245	0.48	0.723	0.948	1911	1.860	1.541	1.705	1.851	1.978	2.087	*		*	*				6
_	4	0.303	_	0.599	0.787	0.966	1.135	1.292	1.436	1.565	1.680	1.780	1.866	*		*				7
_	9	0.170	_	0.502	0.661	0.813	0.958	1.093	1.218	1.332	1.436	1.528	1.608	1.676	*	8		4		9
_	8.8	0.143	0.285	0.425	0.560	0.691	0.815	0.932	1.041	1.142	1.235	1.318	1.392	1.456	1.611		*.		¥	80
_	•	9		0 960	0.73		909	8	-	100	900	- 071	010	020	900	900	*		¥	
) e	0.132	_	0.002	0.10	180.0	0.00	3 6	0.000	0.800	999	2 2	1.210	7.7	1.022		000			9 6
-	9 0	3 5		7100	7140	2000	200.0	160.0	0,70	2 2 2 2	0.920	0.880	200	2117	100	3 5	1.200			7
1	e (160.0		202.0	0000	144.0	37.0	100.0	0.00	2 .	0.010	700	0.820	0.00	1.021	90.0	0.00			4 0
13	9 0	0.078	_	100 C	0.810	200	2	7700	26.0	0.652	0.710	0.76	418.0	900	3 5	5.50	0.870			9.0
2	20 20	0.069	_	0.202	0.271	9220	985.0	0.459	0.517	0.572	0.624	0.673	0.718	0.760	0.797	0.831	198.0	0.887	•	20 20
=	4.0	090.0		0.180	0.238	0.295	0.850	0.404	0.455	0.504	0.551	0.594	0.635	0.673	0.707	0.788	0.766	0.790	*	4.0
=	4.0	0.053		0.158	0.210	0.260	_	0.356	0.403	0.446	0.487	0.526	0.568	0.597	0.628	0.657	0.682	0.705	3	4
	7	0.047	0.094	0.140	0.185	0.230	_	0.315	0.356	0.395	0.432	0.467	0.500	0.531	0.559	0.585	0.609	0.630	•	7
-	9.	0.042	_	0.124	0.164	0.804		0.280	0.316	0.351	0.384	0.416	0.445	0.478	0.499	0.522	0.544	0.563		4.6
-	4. 8.	0.037		0:110	0.146	0.181	0.215	0.249	0.281	0.312	0.342	0.870	0.397	0.422	0.445	0.467	0.486	0.504		4 .8
_	2.0	0.033		0.098	0.130	0.161	0.192	0.221	0.250	0.278		0.830	0.354	0.877	0.398	0.418	.0.436	0.452		9.0
	5.2	0.029	_	0.087	0.116	0.144	_	0.198	0.224	0.248	_	0.295	0.817	0.337	0.356	0.374	0.390	0.405	0.418	6.9
-	4.0	0.026		0.078	0.103	0.128	_	0.177	0.200	0.222	_	0.264	0.384	0.302	9180	0.336	0.350	0.364	0.376	4.0
-		0.028	0.047	0.070	0.092	0.115	0.137	0.158	0.179	0.199	0.218	0.837	0.255	0.871	0.287	0.301	0.815	0.327	0.838	6
	o o	0.021		0.062	20.0	0.103	0.1%	0.142	91.0	0.178		2120	0.828	0.243	0.857	0.271	0.188	484.0	200.	20 40
==	6.0	0.019		0.056	0.074	0.092		0.127	0.144	0.160	0.176	0.191	0.205	0.219	0.231	0.243	0.254	0.264	0.273	6.0
_	6.2	0.017	0.034	0.050	0.067	0.083	_	0.114	0.129	0 144	_	0.172	0.185	0.197	0.308	0.219	0.229	0.238	0.246	6.9
-	4	0.015	_	0.045	0.060	0.074	_	0.108	0.116	0.130	0.149	0.154	0.166	0.177	0.187	0.197	0.206	0.214	0.221	4.9
_	6.6	0.014	_	0.041	0.054	0.067	0.090	0.093	0 105	0.117		0.139	0.150	0.160	0.169	0.178	0.186	0.193	0.800	9.9
	6.8	0012		0.037	0.049	0.061		0.084	0.095	0.106	0.116	0.126	0.185	0.144	0.153	0.160	0.168	0.174	0.180	.
_	7.0	0.011	0.022	0.033	0.044	0.055	0.065	0.075	0.085	0.095	0.105	0.114	0.122	0:130	0.138	0.145	0.152	0.158	0.163	7.0
_11		=	_	-																

FROM POULLET.

Internal Dismeter of Tube Tube 2.00 2.50 8.00 8.50 4.00	Depression. Millimetres. 4.579 8.595 2.902 2.415 2.058	Differences. Millimet. 0.965 0.892 0.487 0.363 0.301	Internal Diameter of Tube. Millimetres. 8.50 9.00 9.50 10.00 10.50	Depression. Millimetres. 0.604 0.534 0.478 0.419 0.872	Differences. Millimet. 9.070 9.061 0.084 0.047 0.027	Internal Dismeter of Tube of Tube 15.00 15.50 16.00 16.50 17.00 17.50	Depression. Millimotres. 0.127 0.112 0.099 0.067 0.077	Differences Millimet. 0.015 0.018 0.019 0.009
5.00 5.50 6.00 6.50	1.507 1.306 1.186 0.995	0.201 0.170 0.141 0.118	11.50 12.00 12.50 18.00	0.298 0.260 0.280 0.204	0.038 0.030 0.026 0.028	18.50 18.50 19.60 19.50	0.060 0.058 0.047 0.041	0.007 0.006 0.008 0.00a
7.00 7.50 8.00	0.877 0.775 0.684	0-102 0-091 0-080	18.50 14.00 14.50	0.181 0.161 0.148	0.020 0.018 0.016	20.00 20.50 21.00	0.036 0.082 0.028	0-004 0-004

XXVL DEPRESSION OF THE BAROMETRICAL COLUMN DUE TO CAPILLARY ACTION.

Internal		Depression	according t	ю	Internal		Depression	according (ko .
Diameter of Tube.	La Place.	Young.	Ivory.	Cavendish.	Diameter of Tube.	La Place.	Young.	Ivory.	Cavendish.
Millimetres.	Millim.	Millim.	Millim.	Million.	Millimetres.	Millim.	Millim.	Millim.	Millim.
2.00	4.454	4.887	4.888	4.472	11.50	0.815			l
2.50	8.568			1	12.00	0.281	0.242	0.253	0.200
8.00	2.918	2.986	2.988	8.054	12.50	0.250			ł
3.50	2.442	l		1	18.00	0.228	0.188	0.196	0.170
4.00	2.068	2.063	2.066	2.187	18.50	0.198			
4.50	1.774	İ		ł	14.00	0.176	0.144	0.152	0.150
5.00	1.584	1.510	1.518	1.785	14.50	0.156			1
5.50	1.837	•			15.00	0.187	0.111	0.118	0.181
6.00	1.171	1.189	1.184	1.877	15.50	0.121			
6.50	1.030			İ i	16.00	0.107	0.088	0.087	
7.00	0.909	0.869	0.868	1.078	16.50	0.094			
7.50	0.808	1	İ	1 1	17.00	0.088	0.068	0.071	i
8.00	0.712	0.669	0.678	0.820	17.50	0.078		l	
8.50	0.682	İ		1	18.00	0.064	0.058	0.054	1
9.00	0.562	0.517	0.521	0.608	18.50	0.056			
9.50	0.500				19.00	0.049	0.041	0.042	
10.00	0.445	0.402	0.406	0.406	19.50	0.048		ļ	1
10.50	0.397	1			20.00	0.088	0.081	0.031	
11.00	0.854	0.811	0.316	0.270	20.50	0.084		1	
11.50	0.315				21.00	0.080	0.024	0.024	

EXVII. DEPRESSION OF THE BAROMETRICAL COLUMN DUE TO CAPILLARY ACTION, REDUCED INTO ENGLISH INCHES FROM DELCROS'S TABLE.

Internal Diam- oter				Holgi	at of Mo	miscus !	in Thou	madths	of an l	loglish	Inch.			
of Tube.	5	10	15	90	25	80	25	40	45	50	55	60	65	70
Eng. In.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch
0.10	0.040	0.076	0.109	0.186	0.155		i							
0.12	.027	.058	.076	.097	.114			ł						
0.14	.019	.038	.056	.071	.085	0.097	}							
0.16	.015	.029	.042	.055	.066	1	0.084							Ì
0.18	.011	.022	.088	.048	.052	.060	.067	0.078						
0.20	.009	.018	.026	.034	.042	.049	.055	.060	0.064					
0.22	.007	.014	.021	.028	.034	.010	.045	.049	.058	0.057		ĺ		
0.24	.006	.012	.017	.028	.028	.038	.087	.041	-045	.048	0.050		i I	
0.26	.005	.010	.014	.019	.028	.027	.031	.085	.088	.040		0.045	1	
0.28	.004	.008	.012	.016	.019	.028	.026	.029	.032	.034	.036	.088	1 1	
0.80	.003	.007	.010	.018	.016	.019	.022	.025	.027	.029	.081	.033	0.034	
0.82	.003	.006	.009	.011	.014	.016	.019	.021	.028	.025	.027	.028	.030	
0.84	.002	.005	.007	.010	.012	.014	.016	.018	.020	.022	.023	.024	.026	
0.36	.002	.004	.006	.008	.010	.012	.014	.016	.017	.019	.020	.021	.022	
0.38	.002	.004	.005	.007	.009	.010	.012	.018	.015	.016	.017	.018	.019	1
0.40	.002	.003	.005	.006	.008	.009	.010	.012	.013	.014	.015	.016	.017	
0.42	.001	.003	.004	.005	.007	.008	.009	.010	-011	.012	.018	.014	.015	0.01
0.44	.001	.002	.004	.005	.006	.007	.008	.009	.010	.011	.011	.012	.013	.01
0.46	.001	.002	.008	.004	.005	.006	.007	.008	.008	.009	.010	.011	.011	.01
0.48	.001	.002	.003	.004	.004	.005	.006	.007	.007	.008	.009	.009	.010	.01
0.50	.001	.002	.002	.003	.004	.004	.005	.006	.006	.007	.008	.008	.008	.00
0.52	.001	.001	.002	.003	.008	.004	.005	.005	.006	.006	.007	.007	.007	.00
0.54	.001	.001	.002	.002	.008	.003	.004	.004	.005	.005	.006	.006	.006	.00
	5	10	15	20	25	30	35	40	45	50	55	60	65	70

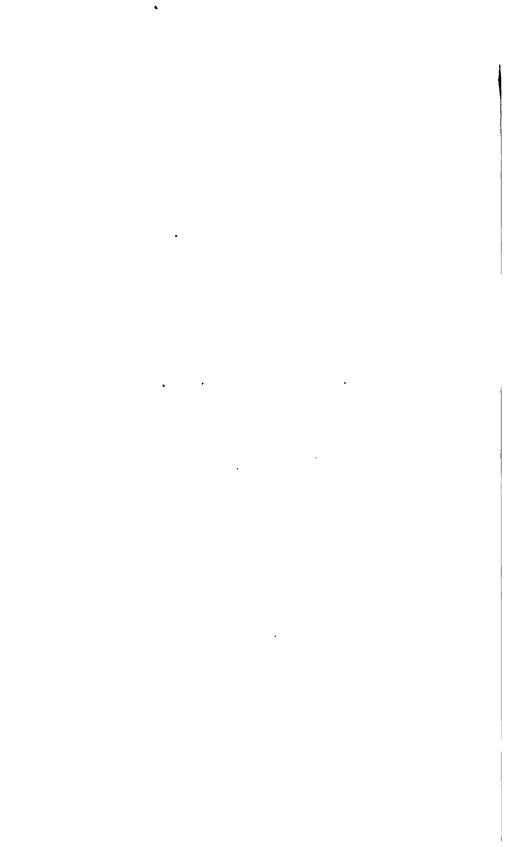
EXVIII. DEPRESSION OF THE BAROMETRICAL COLUMN DUE TO CAPILLARY ACTION, EXPRESSED IN ENGLISH INCHES. — BAILY.

Diameter	Depr	ession accordin	ng to	Diameter	Depr	endon accordi	ng to
of Tube.	Ivory.	Young.	La Place.	of Tube.	Ivory.	Young.	La Place.
Eng. Inch.	Eng. Inch.	Eng. Inch. 0.2964	Eng. Inch.	Eng. Inch.	Bng. Inch.	Eng. Inch. 0.0196	Eng. Inch
	0.2949		0		0.0212		0.0216
0.10	.1404	.1424	.1894	0.40	.0154	.0189	-0159
0.15	.0865	.0880	.0854	0.45	.0112	.0100	-0117
0.20	.0583	.0589	.0580	0.50	.0082	.0074	.0087
0.25	.0409	.0404	.0412	0.60	.0048	.0045	.0046
0.30	.0298	.0280	.0296	0.70	.0023	•. • •	.0024
0.85	0.0212	0.0196	0.0216	0.80	0.0012	0	0.0013

METEOROLOGICAL TABLES

IV.

HYPSOMETRICAL TABLES.



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BAROMETRICAL

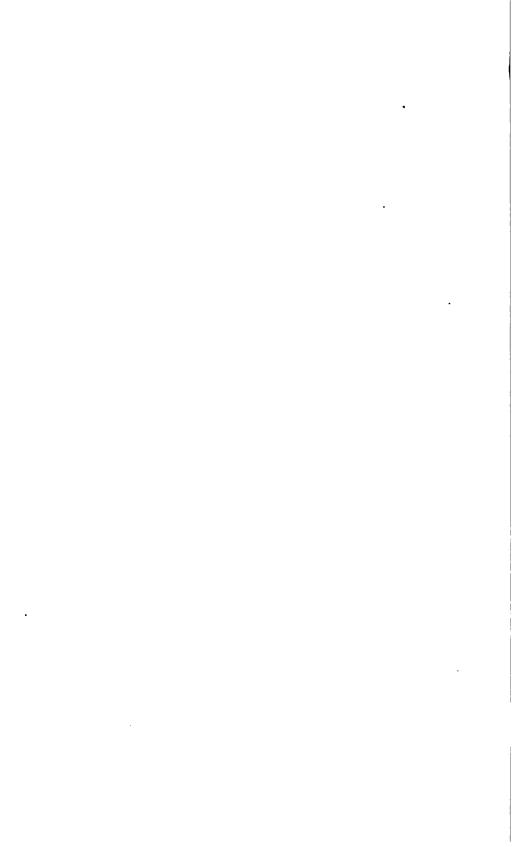
MEASUREMENT OF HEIGHTS,

OR

TABLES

FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS.

 \mathbf{D}



HYPSOMETRICAL TABLES

FOR.

COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS.

Numerous determinations of altitude are one of the great desiderata of physical science, and no more ready means for obtaining them is at the disposal of the scientific man than the Barometer. A traveller, furnished with the improved and convenient instruments we can now command, and with some experience in using them, can take a large number of barometric observations for determining heights, at the cost of little trouble or time. It is, however, quite otherwise with the computations by which the results are obtained. The prospect of that tedious and time-robbing labor not only too often cools the zeal of the observer, but a vast amount of data actually collected remain of no avail from the want of having been computed.

The object of this much enlarged set of Hypsometrical Tables is to facilitate the task of the computer. It contains practical tables adapted to the three usual barometrical scales, and, among them, No. I., II., and V. are so disposed as to dispense with the use of logarithms, and to reduce the computation to the simplest arithmetical operations. The others suppose the use of logarithms, a method which may still be preferred by some observers.

As these various tables represent the development of the principal formulæ which have been proposed, the computer is enabled to compare the results obtained by each of them, and to select that which he most approves.

These formulæ may be referred to two classes, the respective types of which are Laplace's and Bessel's formulæ.

Laplace, in the Mécanique Céleste, Tom. IV. p. 292, gave a complete solution of the problem, and proposed a formula which soon superseded the older and less accurate formulæ of De Luc, Shuckburgh, and others. The coefficients which enter in it were derived from the best determinations of the needed physical constants which science could then furnish, the most important of which are the relative weight of the air and of the mercury, and the rate of expansion of air by heat. The first was assumed to be 10487, according to the experiments of Biot and Arago; and the barometrical coefficient deduced from it, 18317 metres. This coefficient was, however, empirically increased to 18336 metres, in order to adjust the results of the formula to those furnished by the careful trigonometrical measurements made by Ramond for the purpose of testing its correctness. It becomes 18393 metres when including the correction due to the effect of the decrease of gravity with the height on the density of the mercurial column and of the air. The coefficient expressing the expansion of the air by heat, as determined by Gay-Lussac, viz. 0.00375 of its bulk for one Centigrade degree, was adopted, but Laplace increased it to 0.004, in order to take into the account the effect of the greater expansive power of the vapors contained in the atmosphere.

HYPSOMETRICAL TABLES.

These values have been retained in the different formulæ proposed later by Gauss, in Schumacher's Jahrbuch for 1840, by Schmidt, Mathem. und Physische Geographie, II. p. 205, and by Baily, Astronomical Tables, p. 183, which, therefore, only change the form without changing the results. D'Aubuisson, in his formula and tables, Traité de Géognosie, p. 488, only reduced the barometrical coefficient to its theoretical value, which he determined to be 18365 metres, leaving unchanged the other coefficients of Laplace's formula.

Bessel first introduced, in his formula, Astronomische Nachrichten, No. 356, a separate correction for the effect of moisture. The correction for the temperature of the air is computed in his tables for two values of the coefficient, that of Gay-Lussac, 0.00375, and that of Rudberg, 0.00365. Laplace's barometrical coefficient is retained, but the correction for the decrease of gravity is considerably modified.

In Elie Ritter's formula, in the *Mémoires de la Societé de Physique de Genère*, Tom. XIII. p. 343, the corrections for temperature and moisture are also separated; but other values of the barometrical and thermometrical coefficients, derived from Regnault's determinations, are used, and a new method is proposed for applying the correction due to the expansion of air, which is made proportional to the square of the difference between the observed temperatures at each station.

Baeyer's formula, recently published in Poggendorf's Annalen der Physik und Chemie, Tom. XCVIII. p. 371, does not belong to either of the two classes just mentioned; for while it keeps Laplace's barometrical and thermometrical coefficients, it corrects the effect of temperature by a method analogous to that of Ritter, and it entirely neglects the effect of aqueous vapor.

In the following set the tables of Delcros, Guyot, and Loomis develop the formula of Laplace. The much larger tables of Delcros render unnecessary those of Oltmanns, which are yearly reprinted in the Annuaire du Bureau des Longitudes. Instead of Gauss's tables will be found the tables of Dippe, which are computed from the same formula, but are more extended. Baily's tables close the first series. The tables of Plantamour, computed from Bessel's formula, are given here in preference to Bessel's tables, because Plantamour substituted for Laplace's barometrical coefficient that derived from the probably more accurate determination of the relative weight of the air and mercury by Regnault, viz. 18404.8 metres. E. Ritter's tables, computed from his own formula, give perhaps, in extreme cases, better results; but as, in ordinary circumstances, the altitudes obtained do not much differ from those furnished by the less complicated tables of Plantamour, they were not reprinted here.

The miscellaneous tables which follow furnish useful materials for solving several questions connected with the barometrical measurements.

Regnault's table of Barometric Pressures corresponding to Temperatures of the Boiling Point of Water, revised by Moritz, and its reduction to English measures, will be found a valuable addition for thermometrical measurements of heights.

The Appendix to the Hypsometrical Tables now offers, in a new form, a complete series of tables for the comparison of the different measures of length generally used for indicating altitudes, the convenience of which will be fully appreciated by those who have attempted to collect and to use the abundant contributions furnished by all civilized nations to that branch of geographical science.

TABLES

POR

DETERMINING DIFFERENCES OF LEVEL BY MEANS OF BAROMETRICAL OBSERVATIONS,

COMPUTED FROM THE COMPLETE FORMULA OF LAPLACE,

By M. T. DELCROS.

Construction of the Tables.

If we take z = difference of level of the two barometers, a = earth's mean radius = 6366200 metres, L = mean latitude between the two stations,

and further: -

At Station.
$$\begin{cases} h = \text{observed height of the barometer,} \\ T = \text{temperature of the barometer,} \\ t = \text{temperature of the air,} \\ W = \text{observed height of the barometer,} \\ T' = \text{temperature of the barometer,} \\ t' = \text{temperature of the air,} \end{cases}$$

and if we make finally H = h + h'. $\left(\frac{T - T'}{6196}\right)$,

we shall have, according to Laplace, the following general and complete equation: ---

$$z = 18336 \text{ metres} \times \left\{ \begin{array}{l} \left(1 + \frac{2 \cdot (t + t^2)}{1000}\right) \\ \left(1 + 0.0028371 \cos 2 \cdot L\right) \\ \left(\left(1 + \frac{z}{a}\right) \cdot \text{Log.} \left(\frac{A}{H}\right) + \frac{z}{a} \cdot 0.868589\right) \end{array} \right\}$$

after the proper transformations this equation becomes: —

$$z = \text{Log.} \left(\frac{h}{H}\right) \text{ 18336 metres} \times \left\{ \begin{array}{l} \left(1 + \frac{2 \cdot (t + f)}{1000}\right) \\ \left(1 + 0.0028371 \cos. 2. \text{ L}\right) \\ \left(1 + \frac{\left(\log. \left(\frac{h}{H}\right) + 0.868589\right). \frac{z}{a}}{\text{Log.} \left(\frac{h}{H}\right)} \right) \end{array} \right\}$$

introducing into this expression the value in metres of α , the earth's mean radius, making $z = \text{Log.}\left(\frac{h}{H}\right)$ 18336 and Log. $\left(\frac{h}{H}\right) = \left(\frac{z}{18336}\right)$, which can be done without sensible error, the above formula takes the following form, sufficiently accurate for practical purposes:—

$$z = \text{Log.}\left(\frac{\lambda}{H}\right)$$
. 18336 metres $\times \left\{ \begin{array}{l} \left(1 + \frac{c2 \cdot (c + f')}{1000}\right) \\ \left(1 + 0.0028371 \text{ cos. 2. L}\right) \\ \left(1 + \frac{s + 16998}{6366200}\right) \end{array} \right\}$

the four factors of which can easily be developed in tables, as has been done by Mr. Oltmanns. But though this *savant* chose to develop also the second factor, I found it better not to do so, partly because the calculation of it is very easy, and also or account of the great extent it would have been necessary to give to this table, in order to avoid troublesome interpolations.

In the calculation of h'. $\binom{T-T}{6186}$, Mr. Oltmanns used the constant coefficient of the absolute expansion of the mercurial column; I took that of the relative expansion of the mercury and of the brass scale. It is obvious, therefore, that if the scale of the barometer employed was of wood, glass, iron, or of another substance, it would be necessary to make use of as many different coefficients, and the Table II. could not be used. Moreover, Oltmanns combined the last two factors of the general formula in one single table with double entry. This table I have calculated, extending it sufficiently to avoid a double interpolation; but as it seemed to me much too extensive, I substituted for it Tables III. and IV., which are more condensed, without rendering any troublesome interpolation necessary.

I carried the calculation of these tables beyond the limits at which Oltmanns chose to stop, in order that they may answer for the most extreme cases.

At the head of each table will be found the factor of which it is the development; this makes any other explanation superfluous.

All these tables give, at sight, the numbers wanted; only when very great precision is desired, a slight interpolation, at sight, and very easy to apply, may be required. My principal object was to relieve the computer of the troublesome and annoying labor of interpolations.

I added to these four tables the small Table V., taken from the Annuaire du Bureau des Longitudes of Paris. It will be seldom used.

When calculating differences of level, in the same order, with the tables, and by the complete formula of Laplace, the results thus obtained never differ by more than one decimetre in the most extreme cases. The following example will illustrate this statement: I take the observation made in a balloon, by Gay-Lussac, at Paris, as an extreme case, which is very well adapted to manifest the errors of the tables, if there were any, by comparing the results obtained by means of them with those of the direct calculation according to the complete formula of Laplace, from which they are derived.

Example of Calculation by the complete Formula of Laplace and by the Tables

Height of the Balloon of Gay-Lussac.

The observation gave: -

Balloen
$$h' = 328.80$$
 $T' = -9.5$ $t' = -9.5$
Paris $h = 765.68$ $T = +30.8$ $t = +30.8$

$$T - T' = +40.3$$
 $(t+t') = +21.3$ et $2(t+t') = 42^{\circ}.6$

With these data the formula of Laplace gives the following calculation: -

Log.
$$h'$$
. = 328.80 = 2.5169318
Log. $(T - T') = +40.3$ = 1.6053050

Log. dilat. coefficient =
$$0.0001614 = 6.2079035$$

$$H = 330.94 \log. = 2.5197480$$
 $log. h = 765.68 = 2.8840473$

(Log.
$$\lambda$$
 — Log. H) = Difference of Log. = 0.3642993

Log. of (Log.
$$h - \log H$$
) = 9.5614583

Log.
$$\left({\frac{A}{H}} \right)$$
 18336 $\right) = (A + a) = 3.8247629$
Corresponding number = 6679.79 = $(A + a)$

Log. cos.
$$2 L = 97^{\circ} 40' = -$$
 9.1251872

$$Log. constant = 0.0028871 = +$$
 7.4528746

Log.
$$(A + a) = 6679.79. = +$$
 3.8247629

Log. (
$$(0.0028371. \text{ Cos. 2 L}) \times (A + a)$$
) = -0.4028247

Corresponding number = -2.53

$$(A + \alpha + \beta) = 6677.26$$

Corr. temp. air =
$$v = 284.45$$
 = (6.677×42.6)

$$(A + \alpha + \beta + \nu) = 6961.71$$

Constant =. + 15926

Comp¹.
$$\log \nu a = 6366200 \dots \log \dots = 3.1961197$$

 $(A + a + \beta + \nu) = 6961.71 \dots \log \dots = 3.8427153$

$$\delta = +$$
 25.08 Log. $= + 1.3984372$

$$(\Lambda + a + \beta + v + \lambda) = 6986.74$$

Altitude of balloon = 7035.44 by the formula of Laplace.

Now let us calculate by the tables, placing side by side the corresponding results given by the formula of Laplace.

Balloon
$$h' = 328.80$$
 $T' = -9.5$ $t' = -9.5$
Paris $h = 765.68$ $T = +30.8$ $t = +30.8$

with $\begin{cases} h' = 328.80 \\ h = 765.68 \end{cases}$ Table I. gives $\begin{cases} 1478.4 \\ 8209.8 \end{cases}$ By the formula of 8209.8 Laplace we found:

$$A = 6731.4$$
with $(T' - T) = -40^{\circ}.3$, Table II. gives $a = -52.0$

$$(A + a) = 6679.4 \qquad 6679.79$$
with $L = 48^{\circ}.50^{\circ}$, Table III. gives $a = -2.3 \qquad -2.53$

$$(A + a + \beta) = 6677.1 \qquad 6677.26$$
with $2(t + t')$ direct calculation gives $v = +284.5 \qquad +284.45$

$$(A + a + \beta + v) = 6961.6 \qquad 6961.71$$
with 6960, Table IV. gives $b = -2.3 \qquad -2.53$

$$(A + a + \beta + v) = 6961.6 \qquad 6961.71$$
with 6960, Table IV. gives $b = -2.3 \qquad -2.53$

$$(A + a + \beta + v) = 6961.6 \qquad 6961.71$$
Altitude of barometer at Paris $b = -2.3 \qquad -2.53$
Therefore altitude of balloon $b = -2.3 \qquad -2.53$

Two results which are sensibly identical. This ought not to astonish us; the tables being the exact development of the formula, they ought to give the same results, provided in both cases nothing has been neglected, and the four factors have been calculated in the same relative order.

DELCROS.

Disposition and Use of the Tables.

The disposition of the tables is the following: -

In Table I., the first column on the left contains the height of the barometer in millimetres, corrected for the error of the instrument.

The second column headed N (number), gives in metres the first two figures of the number corresponding to each height of the barometer in the first column; the third column, headed 0.0, gives the remaining figures for the full number of millimetres; the following columns give the remaining figures for the same number of millimetres and each decimal fraction of a millimetre which may follow it. The value of the hundredths is to be found in the last column.

Example: — Height of Barometer = 761.00.

We look out in the first column for the number 761, and we find on the same line in the second column, 81; in the third column, headed 0.0, or full number, 61.1. The corresponding number is thus 8161.1 metres.

Height of barometer = 761.35.

The second column gives 81; the column headed 0.3 gives, on the same line, 64.2. The corresponding number is then 8164.2. Adding the value of five hundredths of millim., being 0°.5, as indicated in the last column, we have 8164.7 metres, corresponding to 761.35 millim.

The other four tables need no further explanation.

To calculate, by means of the tables, a difference of level from two barometrical observations, proceed in the following manner:—

- 1. Take the height of the barometer at the lower station, or h, and seek in Table I. the number corresponding to this height. Seek likewise the number corresponding to the height of the barometer at the upper station. Subtract the second from the first. The remainder is the approximate difference of level between the two stations. Then apply the following corrections.
 - 2. Correction to be applied for the temperature of the barometers.

If T' be the temperature of the attached thermometer at the upper station, and T that of the attached thermometer at the lower station, take the difference, or T' — T, and seek in Table II. the number corresponding to this difference.

When T' is smaller than T, that is, when the temperature of the attached thermometer of the upper station is lower than that of the lower station, the correction is to be *subtracted* from the approximate height; when T' is greater than T, it is to be *added*.

3. Correction for the temperature of the air.

The first correction having been applied, multiply the number obtained, or N, by the double sum of the temperatures of the air at both stations, and divide the product by 1000; the number thus found, or the quantity expressed by $\frac{N}{1000}$. 2 (t + t') is the correction in metres which is to be added to the preceding number N.

- 4. Tables III. and IV. give two corrections; the first due to the decrease of gravitation in latitude, which is to be added when the mean latitude of the places of observation is between the 45th parallel and the equator; and to be subtracted when it is between the same parallel and the poles, as indicated at the head of the columns. The second correction, due to the decrease of gravitation on the vertical line, is always additive.
- 5. Table V. gives another small correction to be added in the case of the lower station being very elevated above the level of the ocean.

EXAMPLES OF CALCULATION.

Measurement of the Height of Guanazuato. By M. de Humboldt.

Barometer at the upper station, $h' = 600.95 \quad T' = 21.3 \quad t' = 21.3$ Barometer at the level of the sea, $h = 763.15 \quad T = 25.3 \quad t = 25.3$ D

Table I. gives the corresponding numbers,	•	h = 8183.5 $h' = 6280.8$
Tuble II. gives for T' — T,	Difference,	1902.7 — 5.2
$\frac{N}{1000}$. 2 $(t+t')=1.897\times 93.2$,	Difference,	1897.5 = N + 176.8
	Sum,	2074.3
Table III. gives for mean latitude of 21°, Table IV. gives for decrease of gravitation	in the vertical line	+ 4.3 o, + 6.0
Hence altitude of Guanaxuato above the o	cean,	2084.6

Measurement of the height of Mont Blanc, August 29, 1844. By MM. Braveis and Martins.

Barometer at one metre below the summit, Barometer of the Observatory of Geneva,		
Table I. gives for numbers corresponding	to $\begin{cases} h \\ h' \end{cases}$	= 7826.0 = 3504.4
	Difference,	4321.6
Table II. gives for T' — T,		— 29.3
	Difference,	4292.3 = N
$\frac{N}{1000}$. 2 $(t+t') = 4292 \times 23.4 =$	·	+ 100.4
	Sum,	4392.7
Table III. gives for the mean latitude of 4	6°,	0.4
	Difference,	4392.3
Table IV. for decrease of gravitation in th	e vertical line	+ 13.7
Table V. for the elevation of the lower sta	tion,	+ 0.5
	Sum,	4406.5
Elevation of the lower barometer above the	e ocean,	407.0
Hence elevation of upper barometer above	the ocean,	4813.5
Finally, height of the summit of Mont Bla	nc above the ocean,	4814.5

TABLE I. — Giving $A=18336 \times \log$. H or A..., argument H or A in Millimetres.

Barom												Parts
eter H or h.	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	for each 0.01mm.
Milli.	Metr.	Metree.	Metres.	Metres.	Metres.	Motres.		Metres.	Metres,	Metres,	Metres.	Metr.
288	4	23.4	26.2	28.9	81.7	84.4	87.2	40.0	42.7	45.5	48.2	1 0.8
289	4	51.0	53.8	56.5	59.8	62.0	64.8	67.5	70.8	78.0	75.8	2 0.5
290 290	5	78.5	81.8	84.0	86.7	89.5	92.2	95.0	97.7	20.4	000	8 0.8
291	5	05.9	08.7	11.4	14.1	16.8	19.6	22.8	25.0	27.8	03.2 30.5	5 1.4
292	5	83.2	86.0	88.7	41.4	44.1	46.8	49.6	52.8	55.0	57.7	6 1.6
293	5	60.5	68.2	65.9	68.6	71.8	74.0	76.7	79.5	82.2	84.9	7 1.9
904	5	87.6	90.8	98.0	95.7	98.4	73.0	10.1		92.2	04.0	8 2.2
294	6		30.0	35.5	33	30.4	01.1	08.8	06.5	09.2	11.9	9 2.4
295	6	14.6	17.8	20.0	22.7	25.4	28.1	80.8	33.5	86.2	88.9	
296	6	41.6	44.8	47.0	49.6	52.8	55.0	57.7	60.4	63-1	65.8	
297	6	68.4	71.1	78.8	76.5	79.1	81.8	84.5	87.2	89.9	92.5	
298	6	95.2	97.9	•	İ							1 1
296	7	1	1	00.5	08.2	05.9	08.6	11.2	18.9	16.6	19.2	
299	7	21.9	24.5	27.2	29.9	82.5	35.2	87.8	40.5	48.2	45.8	
1	Ħ	1	l	ł				1				
390	7	48.5	51.1	53.8	56.4	59.1	61.7	64.4	67.0	69.7	72.8	
801	7	75.0	77.6	80.8	82.9	85.5	88.2	90.8	93.5	96.1	98.7	
302	8	01.4	04.0	06.6	09.8	11.9	14.5	17.2	19.8	22.4	25.1	1 1
303	8	27.7	80.8	\$3.0	35.6	38.2	40.8	48.5	46.1	48.6	51.8	}
884	8	54.0	56.6	59.2	61.8	64.4	67.0	69.6	72.8	74.9	77.5	
305	8	80.1	82.7	85.8	87-9	90.5	98.1	95.7	98.3			i i
305	9	i	•	1		1				01.0	08.6	
806	•	06.2	08.8	11.4	14.0	16.6	19.2	21.8	24.4	27.0	29.6	1 0.8
307	9	82.1	84.7	87.8	89.9	42.5	45.1	47.7	50.8	52. 9	55.5	2 0.5
308	9	\$8.0	60.6	63.2	65.8	68.4	70.9	73.5	76.1	78.7	81.3	8 0.8
309	9	83.9	86.4	89.0	91.6	94.1	96.7	99.8				4 1.0
809	10								01.9	04.4	07.0	5 1.8
310	10	69.6	12.1	14.7	17.8	19.8	22.4	25.0	27.5	80.1	82.7	6 1.5
811	10	35.2	87.8	40-8	42.9	45.5	48.0	50.6	58.1	55.7	58.2	7 1.8
312	10	60.8	68.8	65.9	68.4	71.0	78.5	76.1	78.6	81.2	83.7	8 2.1
318	10	86.8	88.8	91.4	98.9	96.4	99.0	01.6		00.0	00.1	9 2.8
313	11	11.7	14.2	16.7	19.8	91.0	24.8	01.5	04.1	06.6	09.1]
314 315	11	87.0	39.5	42.0	44.6	21.8 47.1	49.6	26.9 52.1	29.4 54.7	81.9 57.2	84.5 59.7	
316	11	62.2	64.8	67.8	69.8	72.8	74.8	77.8	79.9	82.4	84.9	1
317	11	87.4	89.9	92.4	94.9	97.4	99.9				U-110	l
817	12	~				···-		02.4	05.0	07.5	10.0	ŀ
818	12	12.5	15.0	17.5	20.0	22.5	25.0	27.5	80.0	82.5	85.0	
819	12	87.5	40.0	42.5	45.0	47.5	50.0	52.4	54.9	57.4	59.9	
320	12	62.4	64.9	67.4	69.9	72.8	74.8	77.8	79-8	82.8	84.8	
321	12	87.2	89.7	92.2	94.7	92.1	99.6		-	-		
821	13			4	ł			02.1	04.6	07.1	09.5	
322	13	12.0	14.5	17.0	19.4	21.9	24.4	26.8	29.8	81.8	84.2	
823	18	86.7	89.2	41.6	44.1	46.6	49.0	51.5	58.9	56.4	58.9	.
824	18	61.3	63.6	66.2	68.7	71.1	73.6	76.1	78.5	81.0	83.4	
325	18	85.9	88.8	90.8	98-2	95.7	98.1			- 1		
825	14	İ		1				00.5	0.80	05.4	07.9	
Barom- eter Hor h.	W.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
HOT IL				1	<u> </u>				1			winn.

326 to **364**mm.

						10 a	-					
Barom- eter H or h.	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01 mm
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metr
826	14	10.8	12.8	15.2	17.6	20.1	22.5	25.0	27.4	29.8	32.8	1 0.2
827	14	84.7	87.2	89.6	42.0	44.5	46.9	49.8	51.7	54.2	56.6	2 0.5
328	14	59.0	61.5	68.9	66.3	68.7	71.2	78.6	76.0	78.4	80.9	3 0.7
329	14	88.8	85.7	88.1	90.5	92.9	95.4	97.8			ŀ	4 1.0
829	15				1		1		00.2	02.6	05.0	5 1.2
330	15	07.4	09.9	12.8	14.7	17.1	19.5	21.9	24.8	26.7	29.1	6 1.5
881	15	81.5	88.9	36.3	38.7	41.2	43.6	46.0	48.4	50.8	58.2	7 1.7
332	15	55.6	58.0	60.4	62.8	65.1	67.5	69.9	72.8	74.7	77.1	8 2.0
383	15	79.5	81.9	84.8	86.7	89.1	91.4	93.8	96.2	98.6	07.0	9 2.2
833	16		0						-00	00.4	01.0	
834 335	16	03.4	05.8	08.1	10.5	12.9	15.8	17.7	20.0	22.4 46.2	24.8 48.8	
836	16	27.2	29.6	81.9	34.8	86.7	39.1	41.4	43.8	69.9	72.2	1 0.2
837	16	50.9	58.3	55.7	58.0	60.4	62.8	65.1 88.8	67.5 91.1	93.5	95.8	2 0.4
338	16 16	74.6 98.2	77.0	79.8	81.7	84.0	86.4	00.0	91.1	50.0	50.5	3 0.7
338	17	90.Z	00.5	02.9	05-2	07.6	10.0	12.8	14.7	17.0	19.4	4 1.0
839	17	21.7	24.1	26.4	28.8	81.1	88.4	35.8	88.1	40.5	42.8	5 1.2
340	17	45.2	47.5	49.8	52.2	54.5	56.9	59.2	61.5	63.9	66.2	6 1.5
841	17	68.6	70.9	73.2	75.6	77.9	80.2	82.6	84.9	87.2	89.5	7 1.7
342	17	91.9	94.2	96.5	98.9	****						8 1.9
842	18					01.2	03.5	05.8	08.2	10.5	12.8	9 2.2
848	18	15.1	17.4	19.8	22.1	24.4	26.7	29.0	31.4	88.7	36.0	
844	18	38.3	40.6	42.9	45.2	47.6	49.9	52.2	54.5	56.8	59.1	
845	18	61.4	63.7	66.0	68.8	70.6	78.0	75.8	77.6	79.9	82.2	
346	18	84.5	86.8	89.1	91.4	93.7	96.0	98.8				
846	19								00.6	02.9	05.2	
347	19	07.5	09.6	12.0	14.8	16.6	18.9	21.2	23.5	25.8	28.1	
348	19	80.4	32.7	84.9	87.2	89.5	41.8	44.1	46.4	48.6	50.9	1
849	19	53.2	55.5	57.8	60.1	62.8	64.6	66.9	69.2	71.5	73.7	
										04.0		
850	19	76.0	78.8	80.6	82.8	85.1	87.4	89.6	91.9	94.2	96.5	1 0.2
851 851	19	98.7	01.0	00.0	05.5	07.8	10.1	12.3	14.6	16.8	19.1	2 0.4
852	20	21.4	01.0 23.6	03.8 25.9	28.2	80.4	82.7	34.9	87.2	39.5	41.7	4 0.9
353	20 20	44.0	46.2	48.5	50.7	53.0	55.2	57.5	59.7	62.0	64.2	5 1.1
854	20	66.5	68.7	71.0	73.2	75.5	77.7	80.0	82.2	84.5	86.7	6 1.3
855	20	89.0	91.2	98.4	95.7	97.9	' '''		~			7 1.6
855	21	-5.0		~30.2	1		00.2	02.4	04.6	06.9	09.1	8 1.8
856	21	11.4	13.6	15.8	18.1	20.3	22.5	24.8	27.0	29.2	31.5	9 2.1
857	21	83.7	85.9	88.2	40.4	42.6	44.8	47.1	49.8	51.5	53.7	
859	21	56.0	58.2	60.4	62.6	64.9	67.1	69.8	71.5	78.7	76.0	
859	21	78.2	80.4	82.6	84.8	87.0	89.8	91.5	93.7	95.9	98.1	
360	22	00.3	02.5	04.8	07.0	09.2	11.4	18.6	15.8	18.0	20.2	
861	22	22.4	24.6	26.8	29.0	81.2	38.4	85.6	87.9	40.1	42.3	
862	22	44.5	46.7	48.9	51.0	53.2	55.4	57.6	59.8	62.0	64.2	
863	22	66.4	68.6	70.8	78.0	75.2	77.4	79.6	81.8	83.9	86.1	
864	22	88.8	90.5	92.7	94.9	97.1	99.8					
364	23							01.4	03.6	05.8	08.0	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01 mm.

					900	, 10 4	08	•				
ster i or h.	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Parts for eac 0.01mm
Milli.	Metr.	Metres.	Metres,	Metres.	Metres.	Motres.	Motres.	Metres.	Metres.	Metres,	Metres.	Met
365	28	10.2	12.4	14.5	16.7	18.9	21.1	28.2	25.4	27.6	29.8	1 0.2
366	28	32.0	84.1	36.3	88.5	40.7	42.8	45.0	47.2	49.8	51.5	2 0.4
367	23	58.7	55.9	58.0	60.2	62.4	64.5	66.7	68.9	71.0	78.2	8 0.6
368	23	75.4	77.5	79.7	81.8	84.0	86.2	88.8	90.5	92.6	94.8	4 0.1 5 1.
369 369	23	97.0	99.1	01.8	08.4	05.6	07.7	09.9	12.1	14.2	16.4	6 1.
370	24	18.5	20.6	22.8	24.9	27.1	29.2	81.4	83.5	85.7	87.8	7 1.
371	24	40.0	42.1	44.8	46.4	48.6	50.7	52.9	55.0	57.2	59.3	8 1.
872	24	61.5	63.6	65.8	67.9	70.1	72.2	74.8	76.5	78.6	80.8	9 1.
878	24	82.9	85.0	87.2	89.8	91.4	98.6	95.7	97.8	99.9		1
373	25	ļ		ŀ		į	•	ł	1		02.1	l
374	25	04.2	06.8	08.4	10.6	12.7	14.8	16.9	19.0	21.2	23.8	
875	25	25.4	27.5	29.6	31.8	88.9	86.0	38.1	40-2	42.4	44.5	
576	25	46.6	48.7	50.8	53.0	55.1	57.2	59.3	61.4	63.6	65.7	
377	25	67.8	69.9	72.0	74.1	76.2	78.8	80.5	82.6	84.7	86.8	}
378	25	88.9	91.0	98-1	95.2	97.8	99.4	07.5	00.0	05.7	07.8	
878 879	26 26	09.9	12.0	14.1	16.2	18.3	20.4	01.5 22.5	08.6 24.6	05.7 26.7	28.8	
280	26	80.9	88.0	35.1	87.2	89.8	41.8	48.4	45.5	47.6	49.7	
281	26	51.8	58.9	56.0	58.1	60.2	62.2	64.8	66.4	68.5	70.6	
382	26	72.7	74.8	76.9	78.9	81.0	88.1	85.2	87.8	89.8	91.4	1
383	26	93.5	95.6	97.7	99.7	ı	į .		1			
283	27	į	1		1	01.8	03.9	06.0	08.1	10.1	12.2	1 0.2
384	27	14.8	16.4	18.4	20.5	22.6	24.6	26.7	28.8	80.9	82.9	2 0.4
385	27	85.0	87.1	89.1	41.2	48.2	45.8	47.4	49.4	51.5	53.5	8 0.6
286	27	55.6	57.7	59.7	61.8	63.8	65.9	68.0	70.0	72.1	74.1	4 0.8
387 388	27	76.2 96.8	78.8 98.8	80.8	82.4	84.4	86.5	88.6	90.6	92.7	94.7	6 1.5
388	28	50.0	20.0	00.9	02.9	05.0	07.0	09.1	11.1	18.2	15.2	7 1.8
289	28	17.8	19.8	21.4	23.4	25.5	27.5	29.6	31.6	88.7	35.7	8 1.7
890	28	87.8	89.8	41.9	48.9	46.0	48.0	50.0	52.1	54.1	56.2	9 1.9
891	28	58.2	60.2	62.8	64.8	66.8	68.8	70.4	72.4	74.4	76.5	
392	28	78.5	80.5	82.6	84.6	86.6	88.6	90.7	92.7	94.7	96.8	1
393	28	98.8										
398	29		00.8	02.8	04.9	06.9	08.9	10.9	12.9	15.0	17.0	1
394	29	19.0	21.0	23.0	25.1	27.1	29.1	81.1	88.1	85.2	87.2	1
395 296	29 29	89.2 59.8	41.2 61.3	43.2 63.3	45.2 65.8	47.2 67.8	49.2 69.3	51.8 71.4	58.8 73.4	55.8 75.4	57.8 77.4	
297	29	79.4	81.4	83.4	85.4	87.4	89.4	91.5	98.5	95.5	97.5	1
298	29	99.5				57.4						
898	80		01.5	08-5	05.5	07.5	09.5	11.5	13.5	15-5	17.5	1
299	80	19.5	21.5	23.5	25.5	27.5	29.4	81.4	88.4	85-4	37.4	
400	80	89.4	41.4	43.4	45.4	47.4	49.4	51.8	53.8	55.8	57.8]
401	80	59.8	61.8	68.8	65.2	67.2	69.2	71.2	78.2	75.1	77.1	
402	80	79.1	81.1	83.1	85.0	87.0	89.0	91.0	98.0	94.9	96.9	
403	80	98.9	<u> </u>	 			<u> </u>					
etor ctor or h.	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Parts for eac 0.01mr

408 to 442mm.

Milli. Mi	M. Metr. 81 81 81 81 82 82 82 82 82 83 88 88	Metres. 18.6 38.3 57.9 77.5 97.1 16.6 36.0 55.4 74.8 94.1	Metres. 00.9 20.6 40.3 59.9 79.5 99.0 18.5 37.9 57.8 76.7 96.0	Metres. 02.8 22.5 42.2 61.8 81.4 01.0 20.5 89.9	Metres. 04.8 24.5 44.2 63.8 88.4 02.9 22.4 41.8	Metres 06.8 26.5 46.1 65.7 85.3 04.9 24.4	Metres. 08.7 28.4 48.1 67.7 87.3	Metres. 10.7 80.4 50.1 69.7 89.8	O.7 Motres. 12.7 32.4 52.0 71.6 91.2	Motres. 14.7 84.4 54.0 78.6 98.2	O.9 Metres. 16.6 86.3 55.9 75.5 95.1	Parts for eac 0.01mm Met 1 0.2 2 0.4 3 0.6 4 0.5 5 1.0
408 404 405 406 407 408 408 409 410 411 412	81 81 81 31 81 82 82 82 82 82 82 82 82 83	18.6 38.3 57.9 77.5 97.1 16.6 36.0 55.4 74.8	00.9 20.6 40.3 59.9 79.5 99.0 18.5 87.9 57.8 76.7	02.8 22.5 42.2 61.8 81.4 01.0 20.5 89.9 59.8	04.8 24.5 44.2 63.8 88.4 02.9 22.4 41.8	06.8 26.5 46.1 65.7 85.3	08.7 28.4 48.1 67.7 87.8	10.7 80.4 50.1 69.7	12.7 32.4 52.0 71.6	14.7 84.4 54.0 78.6	16.6 86.3 55.9 75.5	1 0.5 2 0.4 8 0.4 4 0.5 5 1.0
404 405 406 407 408 408 409 410 411 412	81 81 31 81 82 82 32 82 82 82 82 83	38.3 57.9 77.5 97.1 16.6 36.0 55.4 74.8	20.6 40.3 59.9 79.5 99.0 18.5 37.9 57.8 76.7	22.5 42.2 61.8 81.4 01.0 20.5 89.9 59.8	24.5 44.2 63.8 88.4 02.9 22.4 41.8	26.5 46.1 65.7 85.3	28.4 48.1 67.7 87.3	80.4 50.1 69.7	32.4 52.0 71.6	84.4 54.0 78.6	86.3 55.9 75.5	2 0.4 8 0.6 4 0.8 5 1.0
405 406 407 408 408 409 410 411 412	81 31 31 81 82 82 32 82 82 82 82 83	38.3 57.9 77.5 97.1 16.6 36.0 55.4 74.8	40.8 59.9 79.5 99.0 18.5 37.9 57.8 76.7	42.2 61.8 81.4 01.0 20.5 89.9 59.8	44.2 63.8 88.4 02.9 22.4 41.8	46.1 65.7 85.3 04.9	48.1 67.7 87.8	50.1 69.7	52.0 71.6	54.0 78.6	55.9 75.5	8 0.6 4 0.8 5 1.0
406 407 408 408 409 410 411 412	31 31 31 32 32 32 32 32 32 32 32 33	57.9 77.5 97.1 16.6 86.0 55.4 74.8	59.9 79.5 99.0 18.5 37.9 57.8 76.7	61.8 81.4 01.0 20.5 89.9 59.8	63.8 88.4 02.9 22.4 41.8	65.7 85.3 04.9	67.7 87.3	69.7	71.6	73.6	75.5	4 0.8 5 1.0
407 408 408 409 410 411 412	31 31 32 32 32 32 32 32 33	77.5 97.1 16.6 86.0 55.4 74.8	79.5 99.0 18.5 37.9 57.8 76.7	81.4 01.0 20.5 89.9 59.8	02.9 22.4 41.8	85.3 04.9	87.8					5 1.0
408 409 410 411 412	31 32 32 32 32 32 32 32 33	97.1 16.6 36.0 55.4 74.8	99.0 18.5 37.9 57.8 76.7	01.0 20.5 89.9 59.8	02.9 22.4 41.8	04.9		89.8	91.2	98.2	95.1	1 - 1
408 409 410 411 412	82 82 32 82 82 82 83	16.6 86.0 55.4 74.8	18.5 87.9 57.8 76.7	20.5 39.9 59.8	22.4 41.8		00.0					
409 410 411 412	82 32 32 82 82 83 83	36.0 55.4 74.8	37.9 57.8 76.7	20.5 39.9 59.8	22.4 41.8							6 1.2
410 411 412	32 32 82 82 83 33	36.0 55.4 74.8	37.9 57.8 76.7	89.9 59.8	41.8	24.4	06.8	06.8	10.7	12.7	14.6	7 1.4
411 412	32 82 32 33	55.4 74.8	57.8 76.7	59.8			26.8	28.2	80.2	82.1	34.1	8 1.6
412	82 82 83 83	74-8	76.7			48.8	45.7	47.6	49.6	51.5	58.5	9 1.8
	82 83 38				61.2	63.2	65.1	67.0	69.0	70.9	72.9	
	83 33	94-1	202	78.7	80.6	82.5	84.4	86.4	88.8	90.2	92.2	
	33	l	1	97.9	99.9	A1 0	A9 **	05.6	07.5	09.5	11.4	
		13.8	15.2	17.1	19.1	91.8 21.0	08.7 22.9	24.8	26.7	28.7	80.6	l
		13.5 82.5	34.4	36.8	88.8	40.2	42.1	44.0	45.9	47.9	49.8	İ
	88	51.7	53.6	55.5	57.4	59.8	61.2	63.2	65.1	67.0	68.9	
	83	70.8	72.7	74.6	76.5	78.4	80.8	82.8	84.2	86.1	88.0	
11	33	89.9	91.8	98.7	95.6	97.5	99.4	02.0	0100	u	0010	l
	34	33.3		1	55.5		20.4	01.8	08.2	05.1	07.0	
	84	08.9	10.8	12.7	14.6	16.5	18.4	20.8	22.2	24.1	26.0	
	84	27.9	29.8	81.7	33.6	35.5	87.8	89.2	41.1	48.0	44.9	
421	84	46.8	48.7	50.6	52.5	54.4	56.2	58.1	60.0	61.9	63.8	
	84	65.7	67.6	69.5	71.4	73.3	75.1	77.0	78.9	80.8	82.7	1 0.2
428	34	84.6	86.5	88.4	90.2	92.1	94.0	95.9	97.8	99.6		2 0.4
428	36	1	İ	l							01.5	8 0.6
424	35	03.4	05.8	07.2	09.0	10.9	12.8	14.7	16.6	18.4	20.8	4 0.8
			·									5 1.0
	35	22.2	24.1	25.9	27.8	29.6	81.5	33.4	35.2	87.1	38.9	6 1.2
	35	40.8	42.7	44.5	46.4	48.3	50.1	52.0	58.9	55.8	57.8	7 1.4
	85	59.5	61.4	68.2	65.1	67.0	68.8	70.7	72.6	74.5	76.8	8 1.6
	85	78.2	80.1	81.9	88.8	85.6	87.5	89.4	91.2	98.1	94.9	9 1.8
13	35	96.8	98.6	00.5	02.8	04.0	000	0~0	00.7	11.6	18.4	
	36 36	15.3	17.1	19.0	20.8	04.2 22.7	06.0 24.6	07.9 26.4	09.7 28.2	11.6	31.9	
	36	33.8	35.6	87.5	39.8	41.2	48.0	44.8	46.7	48.5	50.4	1
	36	52.2	54.0	53.9	57.7	59.6	61.4	68.2	65.1	66.9	68.8	1
	36	70.6	72.4	74.8	76-1	78.0	79.8	81.6	88.5	85.8	87.2	
	86	89.0	90.8	92.7	94.5	96.8	98.1	01.0		55.0	J	
	87							00.0	01.8	03.6	05.5	
	87	07.8	09.1	11.0	12.8	14.6	16.4	18.8	20.1	21.0	28.8	
	87	25.6	27.4	29.2	31.1	32.9	34.7	36.5	88.8	40.2	42.0	1
	87	43.8	45.6	47.5	49.8	51.1	52.0	54.8	56.6	58.4	60.8	ı
	37	62.1	63.9	65.7	67.6	69.4	71.2	73.0	74.8	76.7	78.5	ı
	87	80.3	82.1	83.9	85.7	87.5	89.3	91.2	93.0	94.8	96.6	
1 11	37	98.4										
440	88		00.2	02.0	03.8	05.6	07.5	09.8	11.1	12.9	14.7	
441	38	16.5	18.3	20.1	21.0	28.7	25.5	27.3	29.1	30.9	32.7	
442	88	34.5	86.8	88.1	39.9	41.7	43.5	45.8	47.1	48.9	50.7	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01snm.

448 to 482 ma.

							35:22	 					i
Barom		-					Millimet		-	1 40 0		Parts for each	
H or b.	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	0.01mm	
										l 		<u> </u>	٠,
Milli. 448	Metr.	Metres. 52.5	Motres.	Metres. 56.1	Metres.	Metres.	Metres.	Metres.	Metres.	Metres, 66.8	Metres. 68.6	Metr	٠,
		l .	54.8		57.9	59.7	61.4	63.2	65.0				1
444	38	70.4	72.2	74.0	75.8	77.6	79,3	81.1	82.9	84.7	86.5		1
445	38	88.8	90.1	91.9	93.7	95.5	97.2	99.0				1	ı
445	89								00.8	02.6	04.4		ı
146	89	06.2	08.0	09.8	11.5	13.3	15.1	16.9	18.7	20.4	22.2	1	ı
447	39	24.0	25.8	27.6	29.8	81.1	32.9	34.7	86.5	88.2	40.0	1	1
448	39	41.8	43.6	45.4	47.1	48.9	50.7	52.5	54.3	56.0	57.8		1
449	89	59.6	61.4	68.1	64.9	66.7	68.4	70.2	72.0	73.8	75.5	İ	l
												l	I
450	39	77.8	79.1	80.8	82.6	84.8	86.1	87.9	89.6	91-4	93.1		I
451	89	94.9	96.7	98.4									l
451	40				00.2	02.0	03.7	05.5	07.8	09.1	10.8		I
452	40	12.6	14.4	16.1	17.9	19.6	21.4	28.2	24.9	26.7	28.4		1
458	40	30.2	82.0	83.7	85.5	87.2	89.0	40.8	42.5	44.8	46.0		1
454	40	47.8	49.5	51.3	58.0	54.8	56.5	58.3	60.0	61.8	63.5		1
455	40	65.3	67.0	68.8	70.5	72.8	74.0	75.8	77.5	79.3	81.0	1 0.2	1
456	40	82.8	84.5	86.3	88.0	89.8	91.5	93.2	95.0	96.7	98.5	2 0.8	1
457	41	00.2	01.9	03.7	05.4	07.2	08.9	10.6	12.4	14.1	15.9	8 0.5	١
458	41	17.6	19.8	21.1	22.8	24.6	26.3	28.0	29.8	81.5	83.3	4 0.7	İ
459	41	85.0	36.7	88.5	40.2	41.9	43.6	45.4	47.1	48.8	50.6	5 0.9	١
460	41	52.8	54.0	55.8	57.5	59.2	60.9	62.7	64.4	66.1	67.9	6 1.0	1
461	41	69.6	71.3	78.1	74.8	76.5	78.2	80.0	81.7	88.4	85.2	7 1.2	ŀ
462	41	86.9	88.6	90.3	92.1	93.8	95.5	97.2	98.9	-		8 1.4	I
462	42									00.7	02.8	9 1.6	i
463	42	04.1	05.8	07.5	09.8	11.0	12.7	14.4	16.1	17.9	19.6		١
464	42	21.3	23.0	24.7	26.4	28.1	29.8	31.6	83.8	85.0	86.7		
465	42	38.4	40.1	41.8	43.5	45.2	46.9	48.7	50.4	52.1	53.8		I
466	42	55.5	57.2	58.9	60.6	62.3	64.0	65.8	67.5	69.2	70.9		l
467	42	72.6	74.3	76.0	77.7	79.4	81.1	82.8	84.5	86.2	87.9		ł
468	42	89.6	91.8	98.0	94.7	96.4	98.1	99.8					ľ
468	48								01.5	08.2	04.9		1
469	48	06.6	08.8	10.0	11.7	18.4	15.1	16.8	18.5	20.2	21.9		l
470	48	23.6	25.3	27.0	28.7	80.4	32.0	88.7	35.4	87.1	38.8		١
471	48	40.5	42.2	43.9	45.6	47.8	48.9	50.6	52.3	54.0	55.7		I
472	48	57.4	59.1	60.8	62.5	64.2	65.8	67.5	69.2	70.9	72.6		
478	43	74.8	76.0	77.7	79.3	81.0	82.7	84.4	86.1	87.7	89.4		l
474	43	91.1	92.8	94.5	96.1	97.8	99.5						1
474	44		i l					01.2	02.9	04.5	06.2		1
						<u>. </u>							1
475	44	07.9	09.6	11.2	12.9	14.6	16.2	17.9	19.6	21.8	22.9		1
476	44	24.6	26.8	27.9	29.6	81.8	33.9	85.6	87.8	89.0	40.6		ł
477	44	41.8	43.0	44.6	46.3	48.0	49.6	51.3	58.0	51.7	56.3		١
478	44	58.0	59.7	61.8	63.0	64.7	66.8	68.0	69.7	71.4	78.0	j	١
479	44	74.7	76.4	78.0	79.7	81.8	83.0	84.7	86.8	83.0	89.6		1
480	44	91.8	93.0	94.6	96-8	97.9	99.6						
480	45							01.3	02.9	04.6	06.2	1	
481	45	07.9	09.5	11.2	12.8	14.5	16.1	17.7	19.4	21.0	22.7	1	-
482	45	24.3	25.9	27.6	29.2	80.9	32.5	84.2	85.8	87.5	39.1		١
Baroca												Parts	1
eter	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Gre mach	١
H or h.			l				l	<u> </u>		<u> </u>	l	0.01 mm	
<u> </u>						01					=		-

488 to 524-.

						5 to 3	~- '					
Barom- eter H or h.	N.	0.0	0.1	0.2	0.8	0.4	0.8	0.6	0.7	0.8	0.9	Parts for each 0.01 mm
Mill.	Metr.	Metres.	Motres,	Motres.	Metres.	Metres	Metres.	Metres.	Metres.	Metres.	Metres.	Metr
483	45	40.8	42.4	44.1	45.7	47.4	49.0	50.7	52.3	64.0	55.6	1 0.2
484	45	57.8	58.9	60.6	62.2	63.9	65 5	67.1	68.8	70.4	72.1	2 0.3
485	45	73.7	75.8	77.0	78.6	80.8	81.9	83.6	85-2	86.9	88.5	3 0.5
486	45	90.2	91.8					03.0	00-2	00.5	00.0	1 1
486		80.2	91.0	93.5	95.1	96.8	98.4	00.0			05.0	4 0.6
	46	00.0		09.9	l		l	00.0	01.7	03.8	05.0	5 0.8
487	46	06.6	08.2		11.5	18.1	14.7	16.4	18.0	19.6	21.3	6 1.0
488	46	22.9	24.5	26.2	27.8	29.4	31.0	82.7	84.3	85.9	37.6	7 1.1
489	46	39.2	40.8	42.4	44.1	45.7	47.8	48.9	50.5	52.2	53.8	8 1.3
490	46	55.4	57.0	68.6	60.3	61.9	63.5	65.1	66.7	68.4	70.0	9 1.4
491	46	71.6	73.2	74.9	76.5	78.1	79.7	81.4	88.0	84.6	86.8	l
492	46	87.9	89.5	91.1	92.8	94.4	96.0	97.6	99.2			i
492	47					1				00.9	02.5	Ì
498	47	04.1	05.7	07.8	08.9	10.5	12.1	13.8	15.4	17.0	18.6	
494	47	20.2	21.8	28.4	25.0	26.6	28.2	29.9	81.5	33.1	84.7	1
495	47	86.8	87.9	89.5	41.1	42.7	44.8	45.9	47.5	49.1	50.7	ĺ
496	47	52.3	53.9	55.5	57.1	58.7	60.8	61.9	63.5	65.1	66.7	ł
497	47	68.3	69.9	71.5	78.1	74.7	76.8	78.0	79.6	81.2	82.8	1
498	47	84.4	86.0	87.6	89.2	90.8	92.4	94.0	95.6	97.2	98.8	1
499	48	00.4	02.0	03.6	05-2	06.8	08.3	09.9	11.5	18.1	14.7	1
1	}											l
500	48	16.8	17.9	19.5	21.1	22.7	24.2	25.8	27.4	89.0	80.6	1
501	48	82.2	88-8	35.4	87.0	88.6	40.1	41.7	43.8	44.9	46.5	l
502	48	48.1	49.7	51.8	52.9	54.5	56.0	57.6	59.2	60.8	62.4	1
503	48	64.0	65.6	67.2	68.7	70.8	71.9	78.5	75.1	76.6	78.2	l
504	48	79.8	81.4	88.0	84.5	86.1	87.7	89.8	90.9	92.4	94.0	
505	48	95.6	97.2	98.7		50.2		30.0				
505	49		0		00.8	01.9	08.4	05.0	06.6	08.2	09.7	l
506	49	11.8	12.9	14.4	16.0	17.6	19.1	20.7	22.3	28.9	25.4	1
507	49	27.0	28.6	80.1	81.7	88.8	34.8	86.4	38.0	39.6	41.1	
508	49	42.7	44.3	45.8	47.4	49.0	50.5	52.1	58.7	55.3	56.8	
509	49	58.4	60.0	61.5	68.1	64.6	66.2	67.8	69.8	70.9	72.4	1
510	49	74.0	75.6	77.1	78.7	80.2	81.8	83.4	84.9	86.5	88.0	l
511		89.6	91.2	92.7	94.8			99.0	04.0	00.0	00.0	l
511	49	08.0	91.2	92.4	54.0	95.8	97.4	99.0	00.5	02.1	A9 A	
1	50	AF 6	00.0	00.0	00.0						03.6	
512	50	05.2	06.7	08.8	09.8	11.4	12.9	14.5	16.0	17.6	19.1	
518	50	20.7	22.2	28.8	25.3	26.9	28.4	80.0	81.5	88.1	34.6	
514	50	86.2	87.7	39.8	40.8	42.4	43.9	45.5	46.0	48.6	50.1	
515	50	51.7	58.2	54.8	56.8	57.9	59.4	61.0	62.5	64.1	65.6	
516	50	67.2	68.7	70.8	71.8	78.4	74.9	76.4	78.0	79.5	81.1	
517	50	82.6	84.1	85.7	87.2	88.7	90.2	91.8	93.3	94.8	96.4	
518	50	97.9	99.4									
518	51			01.0	02.5	04.1	05.6	07.1	08.7	10.2	11.8	į į
519	51	13.3	14.8	16.4	17.9	19.4	20.9	22.5	24.0	25.5	27.1	
520	51	28.6	30.1	81.7	83.2	84.7	86.2	87.8	89.3	40.8	42.4	
521	51	43.9	45.4	47.0	48.5	50.0	51.5	53.1	54.6	56.1	57.7	
522	51	59.2	60.7	62.2	63.8	65.3	66.8	68.8	69.8	71.4	72.9	
523	51	74.4	75.9	77.5	79.0	80.5	82.0	83.6	85.1	86.6	88.2	
524	51	89.7	91.2	92.7	94.8	95.8	97.8	98.8				
Barom- eter H or h.	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01 mm.

524 to **565*****.

i i					 				- 2	1		
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01 mm.
Milli.	Metr.	Metres.	Metres.	Metres.	Metree.	Metres	Motres.	Metres.	Metres.	Motres.	Metres.	Mese.
524	52		Ì		ļ				00.3	01.9	03.4	1
525	52	04.9	06.4	07.9	09.4	10.9	12.4	14.0	15.5	17.0	18.5	1
526	52	20.0	21.5	28.0	24.5	26.0	27.5	29.1	30.6	82.1	33.6	1
527	52	35.1	36.6	88.1	39.6	41.1	42.6	44.2	45.7	47.2	48.7	1
528	52	50.2	51.7	58.2	54.7	56.2	57.7	59.3	60.8	62.3	68.8	
529	52	65.8	66.8	68.3	69.8	71.3	72.8	74.8	75.8	77.8	78.8	1 0.1
530	52	80.8	81.8	83.3	84.8	86.8	87.8	89.8	90.8	92.8	93.8	2 0.8
531	52	95.3	96.8	98.8	99.8	l	1	ļ	1		l	3 0.4
531	53	l	ł			01.3	02.8	04.8	05.8	07.3	08.8	4 0.6
532	53	10.8	11.8	18.8	14.8	16.8	17.8	19.3	20.8	22.3	28.8	5 0.7
533	53	25.3	26.8	28.8	29.8	31.8	32.7	34.2	35.7	87.2	38.7	6 0.9
534	53	40.2	41.7	48.2	44.7	16.2	47.6	49.1	50.6	52.1	58.6	7 1.0
535	53	55.1	56.5	58.1	59.6	61.1	62.5	64.0	65.5	67.0	68.5	8 1.2
536	58	70.0	71.5	78.0	74.4	75.9	77.4	78.9	80.4	81.8	83.8	9 1.3
537	53	84.8	86.3	87.8	89.2	90.7	92.2	93.7	95.2	96.6	98.1	l
538	53	99.6			İ		ì	1	1			l
538	54	1	01.1	02.6	04.0	05.5	07.0	08.5	10.0	11.4	12.9	
539	54	14.4	15.9	17.4	18.8	20.3	21.8	23.3	24.8	26.2	27.7	1
540	54	29.2	30.7	32.1	88.6	85.1	36.5	88.0	89.5	41.0	42.4	ł
541	54	43.9	45.4	46.8	48.3	49.8	51.2	52.7	54.2	55.7	57.1	
542	54	58.6	60.1	61.5	68.0	64.5	66.0	67.4	68.9	70.4	71.8	i
543	54	78.3	74.8	76.2	77.7	79.1	80.6	82.1	88.5	85.0	86.4	İ
544	54	87.9	89.4	90.8	92.3	93.7	95.2	96.7	98.1	99.6		
544	55	1		ł	1		1				01.0	
545	55	02.5	04.0	05.4	06.9	08.4	09.8	11.8	12.8	14.3	15.7	
546	55	17.2	18.7	20.1	21.6	23.0	24.5	26.0	27.4	28.9	30.3	1
547	55	31.8	33.8	84.7	36.1	37.6	39. 0	40.5	41.9	43.4	44.8	İ
548	55	46.3	47.7	49.2	50.6	52.1	53.5	55.0	56.4	57.9	59.3	1
549	55	60.8	62.2	68.7	65-1	66.6	68.0	69.5	70.9	72.4	78.8	
1	j	1						1		ľ		!
550	55	75.8	76.7	78.2	79.6	81.1	82.5	84.0	85.4	86.9	88.8	Ì
551	55	89.8	91.2	92.7	94.1	95.6	97.0	98.4	99.9		İ	
551	56	ł			i		i ·			01.8	02.8	1 0.1
552	56	04.2	05.6	07.1	08.5	10.0	11.4	12.8	14.3	15.7	17.2	2 0.8
553	56	18.6	20.0	21.5	22.9	24.4	25.8	27.2	28.7	30.1	31.6	3 0.4
554	56	33.0	84.4	35.9	87.8	38.8	40.2	41.6	48.1	44.5	46.0	4 0.6
555	56	47.4	48.8	50.8	51.7	53.1	54.5	56.0	57.4	58.8	60.8	5 0.7
556	56	61.7	68.1	61.6	66.0	67.4	68.8	70.8	71.7	73.1	74.6	6 0.9
557	56	76.0	77.4	78.9	80.8	81.7	83.1	84.6	86.0	87.4	88.9	7 1.0
558	57	90.3	91.7	93.2	94.6	96.0	97.4	98.9	00.5		00.0	8 1.2
558	57		00.0						00.8	01.7	03.2	9 1.8
559	57	04.6	06.0	07.4	08.9	10.3	11.7	18.1	14.5	16.0	17.4	i
560	57	18.8	20.2	21.6	23.1	24.5	25.9	27.8	28.7	30.2	31.6	1
561	57	33.0	84.4	85.8	87.3	88.7	40.1	41.5	42.9	44.4	45.8	
562	57	47.2	48.6	50.0	51.4	52.8	54.2	55.7	57-1	58.5	59.9	l .
563	57	61.8	62.7	64.1	65.5	66.9	68.3	69.8	71.2	72.6	74.0	1
564	57	75.4	76.8	78.2	79.6	81.0	82.4	88.9	85.8	86.7	88.1	İ
565	57	89.5	90.9	92.4	93.8	95.2	96.6	98.0	99.4	l	l	
Barom- eter H or h	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01 mm.

565 to 605mm.

					200	to	U5	· · · · · · · · · · · · · · · · · · ·				
Burom- eter H or h.	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
Milli.	Metr.	Motres.	Metres.	Metres.	Metres.	Metree.	Metres.	Metres.	Metres.	Metres.	Metres.	Metr.
565	58	İ		}		i	Ì	1		8.00	02.2	
566	58	08.6	05.0	06.4	07.8	09.2	10.6	12.1	13.5	14.9	16.8	1
567	58	17.7	19.1	20.5	21.9	28.8	24.7	26.1	27.5	28.9	80.8	
568	58	31.7	38.1	84.5	35.9	87.8	88.7	40.1	41.5	42.9	44.8	
569	58	45.7	47.1	48.5	49.9	51.3	52.7	54.1	55.5	56.9	58.8	1
570	58	59.7	61.1	62.5	63.9	65.8	66.7	68.1	69.5	70.9	72.3	1
571	58	78.7	75.1	76.5	77.9	79.3	80.6	82.0	88.4	84.8	86.2	
572	58	87.6	89.0	90.4	91.8	98.2	94.5	95.9	97.8	96.7		
572	59										00.1	
578	59	01.5	02.9	04.8	05.7	07.1	08.4	09.8	11.2	12.6	14.0	
574	59	15.4	16.8	18.2	19.6	21.0	22.3	28.7	25.1	26.5	27.9	li
575	59	29.8	30.7	82.1	83.4	84.8	36.2	87.6	89.0	40.8	41.7	
576	59	48.1	44.5	45.9	47.2	48.6	50.0	51.4	52.8	54.1	55.5	1 0.1
577	59	56.9	58.3	59.7	61.0	62.4	68.8	65.2	66.6	67.9	69.8	2 0.3
578	59	70.7	72.1	78.5	74.8	76.2	77.6	79.0	80.4	81.7	83.1	8 0.4
579	59	84.5	85.9	87.2	88.6	90.0	91.3	92.7	94.1	95.5	96.8	4 0.5
580	59	98.2	99.6			i		İ	į			5 0.7
580	60	1		00.9	02.3	03.7	05.0	06.4	07.8	09.2	10.5	6 0.8
581	60	11.9	13.8	14.6	16.0	17.4	18.7	20.1	21.5	22.9	24.2	7 1.0
582	60	25.6	27.0	28.3	29.7	81.1	82.4	88.8	35.2	36.6	37.9	8 1.1
583	60	39.3	40.7	42.0	43.4	44.7	46.1	47.5	48.8	50.2	51.5	9 1.2
584	60	52.9	54.8	55.6	57.0	58.4	59.7	61.1	62.5	63.9	65.2]
585	60	66.6	68.0	69.3	70.7	72.0	78.4	74.8	76.1	77.5	78.8	1 !
596	60	80.2	81.6	82.9	84.8	85.6	87.0	88.4	89.7	91.1	92.4	
587	60	98.8	95.1	96.5	97.8	99.2						1
587	61				i		00.5	01.9	03.2	04.6	05.9	
588	61	07.8	08.6	10.0	11.8	12.7	14.0	15.4	16.7	18.1	19.4	
589	61	20.8	22.1	28.5	24.8	26.2	27.5	28.9	30.2	81.6	32.9	·
590	61	34.8	85.6	37.0	38.3	89.7	41.0	42.4	48.7	45.1	46.4	
591	61	47.8	49.1	50.5	51.8	53.2	54.5 68.0	55.9 69.3	57.2	58.6 72.0	59.9	i '
592	61	61.8	62.6 76.0	64.0	65.3 78.7	66.7 80.1	81.4	82.7	70.7 84.1	85.4	78.4 86.8	l
593	61 61	88.1	89.4	90.8	92.1	98.5	94.8	96.1	97.5	98.8	09.0	l i
594 594	62	80.1	09.4	30.0	92.1	90.0	54.0	50.1	97.5	90.0	00.2	
595	62	01.5	02-8	04.2	05.5	06.9	08.2	09.5	10.9	12.2	13.6	
596	62	14.9	16.2	17.6	18.9	20.2	21.5	22.9	24.2	25.5	26.9	
597	62	28.2	29.5	30.9	32.2	88.6	84.9	36.2	87.6	88.9	40.8	
598	62	41.6	42.9	44.3	45.6	46.9	48.2	49.6	50.9	52.2	58.6	
599	62	54.9	56.2	57.6	58.9	60.2	61.5	62.9	64.2	65.5	66.9	
1 1	İ			1	ĺ							
600	62	68.2	69.5	70.8	72.2	78.5	74.8	76.1	77.4	78-8	80.1	
601	62	81.4	82.7	84.1	85.4	86.7	88.0	89.4	90.7	92.0	93.4	[
602	62	94.7	96.0	97.8	98.7							ĺ
602	68					00.0	01.8	02.6	03.9	05.8	06.6	
(1)3	68	07.9	09.2	10.5	11.9	18.2	14.5	15.8	17.1	18.5	19.8	
604	63	21.1	22.4	28.7	25.1	26.4	27.7	29.0	80.8	81.7	88.0	
605	68	34.8	85.6	36.9	38.2	89.5	40.8	42.2	48.5	44.8	46.1	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01 mm.

606 to 647**.

											_		=
Barom- ster H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for eac 0.01 am	
Milli.	Metr	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Met	. 1
606	63	47.4	48.7	50.0	51.3	52.6	53.9	55.8	56.6	57.9	59.2		ii
607	63	60.5	61.8	63.1	64.5	65.8	67.1	68.4	69.7	71.1	72.4	1	li
608	68	73.7	75.0	76.8	77.6	78.9	80.2	81.5	82.8	84.1	85.4		-
609	63	86.7	88.0	89.3	90.6	91.9	93.2	94.6	95.9	97.2	98.5	ł	
610	63	99.8	l			.					ŀ	i	H
610	64		01.1	02.4	08.7	05.0	06 8	07.6	08.9	10.2	11.5		
611	64	12.8	14.1	15.4	16.7	18.0	19.3	20.7	22.0	23.8	24.6	İ	I
612	64	25.9	27.2	28.5	29.8	81.1	32.4	33.7	85.0	36.3	87.6		ı
613	64	38.9	40.2	41.5	42.8	44.1	45.4	46.7	48.0	49.3	50.6		1
614	64	51.9	53.2	54.5	55.8	57.1	58.3	59.6	60.9	62.2	63.5		- 11
615	64	64.8	66.1	67.4	68.7	70.0	71.2	72.5	78.8	75.1	76.4		Ŋ
616	64	77.7	79.0	80.8	81.6	82.9	84.2	85.5	86.8	88.1	89.4		-11
-617	64	90.7	92.0	93.8	94.6	95.9	97.1	98.4	99.7				-
617	65		ł					1		01.0	02.8		ı
618	65	03.6	04.9	06.2	07.4	08.7	10.0	11.8	12.6	13.8	15.1		1
619	65	16.4	17.7	19.0	20.8	21.6	22.8	24.1	25.4	26.7	28.0	1	I
620	65	29.3	80.6	81.9	33.1	84.4	35.7	87.0	38.3	89.5	40.8		H
621	65	42.1	48.4	44.7	45.9	47.2	48.5	49.8	51.1	52.3	53.6	1 0.1	- 11
622	65	54.9	56.2	57.5	58.7	60.0	61.8	62.6	63.9	65.1	66.4	2 0.2	- 11
628	65	67.7	69.0	70.8	71.5	72.8	74.1	75.4	76.7	77.9	79.2	3 0.4	- 11
624	65	80.5	81.8	83.0	84.8	85.6	86.8	88.1	89.4	90.7	91.9	4 0.8	1
1 1		1						1				5 0.6	1
625	65	98.2	94.5	95.8	97.0	98.3	99.6				l	6 0.8	· II
625	66	1	1					00.9	02.2	03.4	04.7	7 0.9	۱
626	66	06.0	07.8	08.5	09.8	11.1	12.3	13.6	14.9	16.2	17.4	8 1.0	١
627	66	18.7	20.0	21.2	22.5	23.8	25.0	26.3	27.6	28.9	30.1	9 1.1	
628	66	31.4	82.7	83.9	86.2	56.4	87.7	39.0	40.2	41.5	42.7		H
629	66	44.0	45.8	46.5	47.8	49.1	50.3	51.6	52.9	54.2	55.4		ı
630	66	56.7	58.0	59.2	60.5	61.7	63.0	64.8	65.5	66.8	68.0		I
631	66	69.8	70.6	71.8	73.1	74.4	75.6	76.9	78.2	79.5	80.7		il
632	66	82.0	83.2	84.5	85.7	87.0	88.2	89.5	90.7	92.0	93.2		∦
633	66	94.5	95.8	97.0	98.3	99.5		1					l
633	67				}		00.8	02.1	03.8	04.6	05.8		l
634	67	07.1	08.4	09.6	10.9	12.1	13.4	14.7	15.9	17.2	18.4		۱
633	67	19.7	20.9	22.2	23.4	24.7	25.9	27.2	28.4	29.7	80.9		I
636	67	32.2	33.4	84.7	35.9	37.2	38.4	39.7	40.9	42.2	43.4		
637	67	44.7	45.9	47.2	48.4	49.7	50.9	52.2	53.4	54.7	55.9		I
638	67	57.2	58.4	59.7	60.9	62.2	63.4	64.7	65.9	67.2	68.4		I
639	67	69.7	70.9	72.2	78.4	74.7	75.9	77.1	78.4	79.6	80.9		
640	67	82.1	83.3	84.6	85.8	87.1	88.8	89.6	90.8	92.1	93.8		1
641	67	94.6	95.8	97.1	98.3	99.6							
641	68	1			1	1	-00.8	02.0	03.3	04.5	05.8		
642	68	07.0	08.2	09.5	10.7	12.0	13.2	14.4	15.7	16.9	18.2		
643	68	19.4	20.6	21.9	23.1	24.8	25.5	26.8	28.0	29.2	80.5		
644	68	81.7	32.9	84.2	85.4	86.7	37.9	89.1	40.4	41.6	42.9		1
645	68	44.1	45.3	46.6	47.8	49.0	50.2	ŏ1.5	52.7	53.9	55.2		ľ
646	68	56.4	57.6	58.9	60.1	61.3	62.5	63.8	65.0	66.2	67.5		
647	68	68.7	69.9	71.2	72.4	73.6	74.8	76.1	77.8	78.5	79.8		
Burners- eter H or h.	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Parts for eac 0.01 mm	

648 to 689mm.

					040	ь 60 0		· Y			r	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Parte for each 0.01mm
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metr.
648	68	81.0	82.2	83.5	84.7	85.9	87.1	88.4	89.6	90.8	92.1	İ
649	68	93.3	94.5	95.8	97.0	98.2	99.4			1	ĺ	1
649	69							00.7	01.9	08.1	04.4	
650	69	05.6	06.8	08.0	09.3	10.5	11.7	12.9	14.1	15.4	16.6	
631	69	17.8	19.0	20.2	21.5	22.7	23.9	25.1	26.8	27.6	28.8	İ
652	69	80.0	31.2	32.4	33.7	84.9	86.1	37.8	38.5	39-8	41.0	
658	69	42.2	43.4	44.6	45.9	47.1	48.3	49.5	50.7	52.0	53.2	İ
654	69	54.4	55.6	56.8	58.1	59.3	60.5	61.7	62.9	64.2	65.4	l
655	69	66.6	67.8	69.0	70.2	71.4	72.6	78.9	75.1	76.3	77.5	ĺ
656	69	78.7	79.9	81.1	82.4	83.6	84.8	86.0	87.2	88.5	89.7	ĺ
657	69	90.9	92.1	98.8	94.5	95.7	96.9	98.2	99.4			
657	70									00.6	01.8	
658	70	03.0	04.2	05.4	06.6	07.8	09.0	10.8	11.5	12.7	13.9	ĺ
659	70	15.1	16.8	17.5	18.7	19.9	21.1	22.4	23.6	24.8	26.0	
660	70	27.2	28.4	29.6	80.8	82.0	83.2	34.4	35.6	86.8	88.0	1 0.1
661	70	39.2	40.4	41.6	42.8	44.0	45.2	46.4	47.6	48.8	50.0	2 0.2
662	70	51.2	52.4	53.6	54.8	56.0	57.2	58.5	59.7	60.9	62.1	3 0.4
663	70	63.8	64.5	65.7	66.9	68.1	69.3	70.5	71.7	72.9	74.1	4 0.5
664	70	75.8	76.5	77.7	78.9	80.1	81.2	82.4	83.6	84.8	86.0	5 0.6
665	70	87.2	88.4	89.6	90.8	92.0	93.2	94.4	95.6	96.8	98.0	6 0.7
666	70	99.2										7 0.8
666	71		00.4	01.6	02.8	04.0	05.2	06.4	07.6	08.8	10.0	8 1.0
667	71	11.2	12.4	18.6	14.8	16.0	17.1	18.3	19.5	20.7	21.9	9 1.1
668	71	23.1	24.8	25.5	26.7	27.9	29.0	30.2	31.4	32.6	33.8	
669	71	85.0	36.2	87.4	38.6	89.8	40.9	42.1	43.3	44.5	45.7	
670	71	46.9	48.1	49.3	50.5	51.7	52.8	54.0	55.2	56.4	57.6	
671	71	58.8	60.0	61.2	62.8	63.5	64.7	65.9	67.1	68.2	69.4	
672	71	70.6	71.8	73.0	74.2	75.4	76.5	77.7	78.9	80.1	81.3	
678	71	82.5	83.7	84.9	86.0	87.2	88.4	89.6	90.8	91.9	93.1	
674 674	71 72	94.8	95.5	96.7	97.8	99.0	00.2	01.4	02.6	03.7	04.9	
675	72	06.1	07.8	08.5	09.6	10.8	12.0	13.2	14.4	15.5	16.7	
676	72	17.9	19.1	20.8	21.4	22.6	23.8	25.0	26.2	27.8	28.5	
677	72	29.7	80.9	32.0	88.2	84.4	35.5	36.7	87.9	39.1	40.2	
678	72	41.4	42.6	43.8	44.9	46.1	47.3	48.5	49.7	50.8	52.0	
679	72	53.2	54.4	55.5	56.7	57.9	59.0	60.2	61.4	62.6	68.7	
680	72	64.9	66.1	67.2	68.4	69.6	70.7	71.9	78.1	74.8	75.4	!
681	72	76.6	77.8	78.9	80.1	81.8	82-4	83.6	84.8	86.0	87.1	1 0.1
682	72	88.3	89.5	90.6	91.8	93.0	94.1	95.3	96.5	97.7	98.8	2 0.2
683	73	00.0	01.2	02.3	08.5	04.6	05.8	07.0	08.1	09.3	10.4	3 0.3
684	78	11.6	12.8	13.9	15.1	16.2	17.4	18.6	19.7	20.9	22.0	4 0.5
685	78	23.2	24.4	25.5	26.7	27.8	29.0	80.2	31.8	32.5	33.6	5 0.6
696	78	34.8	86.0	37.1	38-3	39.4	40.6	41.8	42.9	44.1	45.2	6 0.7
687	78	46.4	47.6	48.7	49.9	51.0	52.2	53.4	54.5	55.7	56.8	7 0.8
688	73	58.0	59.2	60.8	61.5	62.6	63.8	65.0	66.1	67.3	68.4	8 0.9
689	78	69.6	70.7	71.9	78.0	74.2	75.8	76.5	77.6	78.8	79.9	9 1.1
Barom- eter H or h.	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.

690 to 780---.

								_	_			
Barear eter H or b.	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01 mm.
Mau.	Metr.	Motres.	Metres.	Metres.	Metres.	Metres.	Motres.	Metres.	Metres.	Metres.	Metres.	Metr.
690	73	81.1	82.8	83.4	84.6	85.7	86.9	88.1	89.2	90.4	91.5	
691	78	92.7	93.8	95.0	96.1	97.8	98.4	99.6	35.2			
691	74			20.0		31.10	3012	-	00.7	01.9	03.0)
692	74	04.2	05.8	06.5	07.6	08.8	09.9	11.1	12.2	13.4	14.5	
698	74	15.7	16.8	18.0	19.1	20.8	21.4	22.6	28.7	24.9	26.0	
694	74	27.2	28.3	29.5	80.6	31.8	22.9	84.1	35.2	36.4	87.5	
695	74	38.7	39.8	41.0	42.1	48.8	44.4	45.5	46.7	47.8	49.0	
696	74	50.1	51.2	52.4	58-5	54.7	55.8	56.9	58.1	59.2	60.4	
697	74	61.5	62.6	68.8	64.9	66.1	67.2	68.8	69.5	70.6	71.8	
698	74	72.9	74.0	75.2	76.3	77.5	78.6	79.7	80.9	82.0	88.2] :
699	74	84.8	85.4	86.6	87.7	88.9	90.0	91.1	92.3	93.4	94.6	
555		1	00.4	50.0	J	00.0	50.0	J	02.0	20.4	54.0	
700	74	95.7	96.8	98.0	99.1							
700	75]	23.0	55.1	00.8	01.4	02.5	08.7	04.8	06.0]
701	75	07.1	08.2	09.4	10.5	11.6	12.7	13.9	15.0	16.1	17.3	
702	75	18.4	19.5	20.7	21.8	28.0	24.1	25.2	26.4	27.5	28.7	
708	75	29.8	80.9	32.1	33.2	84.8	35.4	36.6	87.7	88.8	40.0	
704	75	41.1	42.2	43.4	44.5	45.6	46.7	47.9	49.0	50.1	51.8	
705	75	52.4	53.5	54.7	55.8	56.9	58.0	59.2	60.3	61.4	62.6	
706	75	63.7	64.8	66.0	67.1	68.2	69.8	70.5	71.6	72.7	78.9	
707	75	75.0	76.1	77.2	78.4	79.5	80.6	81.7	82.8	84.0	85.1	
708	75	86.2	87.3	88.5	89.6	90.7	91.8	93.0	94.1	95.2	96.4	
709	75	97.5	98.6	99.7	00.0	55	51.0	00.0	0.1.1	55.2	55.5	
709	76	55	1 30.0	55.1	00.9	02.0	08.1	04.2	05.8	06.5	07.6	1
710	76	08.7	09.8	10.9	12.1	13.2	14.3	15.4	16.5	17.7	18.8	
711	76	19.9	21.0	22.1	23.3	24.4	25.5	26.6	27.7	28.9	30.0	!!!
712	76	81.1	82.2	83.8	34.4	35.5	36.6	37.8	38.9	40.0	41.1	1 (0.1
718	76	42.2	43.3	44.4	45.6	46.7	47.8	48.9	50.0	51.2	52.8	2 0.2
714	76	53.4	54.5	55.6	56.8	57.9	59.0	60.1	61.2	62.4	63.5	3 0.3
715	76	64.6	65.7	66.8	67.9	69.0	70.1	71.3	72.4	73.5	74.6	4 0.4
716	76	75.7	76.8	77.9	79.0	80.1	81.2	82.4	83.5	84.6	85.7	5 0.5
717	76	86.8	87.9	89.0	90.1	91.2	92.3	93.5	94.6	95.7	96.8	6 0.7
718	76	97.9	99.0									7 0.8
718	77		1	00.1	01.2	02.3	03.4	04.6	05.7	06.8	07.9	8 0.9
719	77	09.0	10.1	11.2	12.8	13.4	14.5	15.7	16.8	17.9	19.0	9 1.0
720	77	20.1	21.2	22.3	23.4	24.5	25.6	26.7	27.8	28.9	30.0	i
721	77	31.1	32.2	83.3	34.4	35.5	86.6	87.7	38.8	39.9	41.0	
722	77	42.1	43.2	44.3	45.4	46.5	47.6	48.7	49.8	50.9	52.0	
723	77	58.1	54.2	55.3	56.4	57.5	58.6	59.8	60.9	62.0	63.1	
724	77	64.2	65.3	66.4	67.5	68.6	69.6	70.7	71.8	72.9	74.0	
725	77	75.1	76.2	77.3	78.4	79.5	80.6	81.7	82.8	88.9	85.0	
726		86.1	87.2	88.8	89.4	90.5		92.7	93.8	94.9	96.0	
727	77	97.1	98.2	99.3	-5	23.0	91.6			2.200		
727	78		-3		00.4	01.5	02.5	03.6	04.7	05.8	06.9	
728	78	08.0	09.1	10.2	11.8	12.4	13.5	14.6	15.7	16.8	17.9	
729	78	19.0	20.1	21.2	22.3	23.4	24.4	25.5	26.6	27.7	28.8	ĺ
730	78	29.9	310	32.1	33.8	84.8	35.3	36.4	87.5	38.6	39.7	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0 01 mm.

781 to 770-.

					781	10 7	70					
Barom- eter H or h.	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm
Mini.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Motres.	Metres.	Motres.	Motres.	Metres.	Metr.
731	78	40.8	41.9	48.0	44.1	45.2	46.2	47.8	48.4	49.5	50.6	,
732	78	51.7	52.8	58.9	54.9	56.0	57.0	58.2	59.8	60.8	61.4	ł
788	78	62.5	63.6	64.7	65.8	66.9	67.9	69.0	70.1	71.2	72.8	1
734	78	78.4	74.5	75.6	76.6	77.7	78.8	79.9	81.0	82.0	83.1	·
735	78	84.2	85.3	86.4	87.5	88.6	89.6	90.7	91.8	92.9	94.0	i
736	78	95.1	96.2	97.3	98.2	99.4	1	İ		l		1
736	79		1	١			00.5	01.6	02.7	03.7	04.8	1
737	79	05.9	07.0	08.1	09.1	10.2	11.8	12.4	18.5	14.5	15.6	
738	79	16.7	17.8	18.9	19.9	21.0	22.1	28.2	24.3	25.3	26.4	ļ
739	79	27.5	28.6	29.6	80.7	31.8	33.8	88.9	35.0	26.1	87.1	ŀ
		eo 6	00.0	40.4		42.5	43.6	44.7	45.8	46.8	47.9	
740	79	88.2 49.0	89.8 50.1	51.1	41.4 52.2	58.8	54.8	55.4	56.5	57.6	58.6	
741	79 79	59.7	60.8	61.8	62.9	64.0	65.0	66.1	67.2	68.3	69.8	
742	79	70.4	71.5	72.6	78.6	74.7	75.8	76.9	78.0	79.0	80.1	
748	79	81.2	82.8	83.8	84.4	85.5	86.5	87.6	88.7	89.8	90.8	1
711	79	91.9	93.0	94.0	95.1	96.1	97.2	96.8	99.8	55.5	50.0	
745 745	80	31.5	30.0	54.5	00	30.2		55.5	00.0	00.4	01.4	
746	80	02.5	03.6	04.6	05.7	06.8	07.8	08.9	10.0	11.1	12.8	
740 747	80	13.2	14.8	15.8	16.4	17.4	18.5	19.6	20-6	21.7	22.7	Ì
748	80	23.8	24.9	25.9	27.0	28.0	29.1	80.2	31.2	32.8	33.8	
749	80	84.4	35.5	86.5	87.6	88.7	89.7	40.8	41.9	48.0	44.0	
					1		ì	1				
750	80	45.1	46.2	47.3	48.4	49.4	50.5	51.6	52-6	58.7	54.7	
751	80	55.7	56.8	57.8	58.9	59.9	61.0	62.1	63.1	64.2	65.2	
752	80	66.8	67.4	68.4	69.5	70.5	71.6	72.7	78.7	74.8	75.8	
753	80	76.9	78.0	79.0	80.1	81.1	82.2	83.8	84.3	85.4	86.4	
754	80	87.5	88.5	89.6	90.6	91.7	92.7	93.8	94-8	95.9	96.9	1 0.1
755	80	98.0	99.1									2 0.2
755	81			00.1	01.2	02.2	08.8	04.4	05.4	06.5	07.5	3 0.3
756	81	08.6	09.6	10.7	11.7	12.8	18.8	14.9	15.9	17.0	18.0	4 0.4
757	81	19.1	20.1	21.2	22.2	28.8	24.8 84.8	25.4 35.9	26.4 36.9	27.5 38.0	28.5 39.0	5 0.5
758	81	29.6	30.6	81.7 42.2	82.7	83.8	45.8	46.4	47.4	48.5	49.5	6 0.6
759	81	40.1	41.1	25.0	48.2	44.8	40.0	40.4	41.4	40.0	49.0	7 0.7 8 0.8
	81	50.6	51.6	52.7	58.7	54.8	55.8	56.9	57.9	59.0	60.0	9 0.9
760		61.1	62.1	63.2	64.2	65.8	66.8	67.3	68.4	69.4	70.5	# (V-3
761	81 81	71.5	72.5	78.6	74.6	75.7	76.7	77.8	78.8	79.9	80.9	
762 763	81	82.0	88.0	84.1	85.1	86.2	87.2	88.2	89.3	90.8	91.4	
764	81	92.4	93.4	94.5	95.5	96.6	97.6	98.6	99.7			
764	82		-5							00.7	01.8	
765	82	02.8	08.8	04.9	05.9	07.0	08.0	09.0	10.1	11.1	12.2	
766	82	18.2	14.2	15.8	16.3	17.4	18.4	19.4	20.5	21.5	22.6	
767	82	23.6	24.6	25.7	26.7	27.8	28.8	29.8	80.9	81.9	33.0	Ì
768	82	84.0	35.0	36.1	87.1	88.2	89.2	40.2	41.8	42.8	48.4	
769	82	44.4	45.4	46.5	47.5	48.5	49.5	50.6	51.6	52.6	58.7	
770	82	54.7	55.7	56.8	57.8	58.8	59.8	60.9	61.9	62.9	64.0	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01 mm
D	<u> </u>		<u> </u>			28		·				`

771 to 810 m.

Barom- eter H or h.	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Parts for eac 0.01mm
Milli.	Metr.	Motres.	Metres.	Motres.	Motres.	Motres.	Metres.	Motres.	Motres.	Metres.	Meiros.	Metr
771	82	65.0	66.0	67.1	68.1	69.2	70.2	71.2	72.8	73.3	74:4.	
772	82	75.4	76.4	77.5	78.5	79.5	80.5	81.6	82.6	83.6	84.7	'"
773	82	85.7	86.7	87.8	88.8	89.8	90.8	91.9	92.9	93.9	95.0	l
774	82	96.0	97.0	98.0	99.1					1	ŀ	
774	83	1	1	1		00.1	01.1	02.1	03.1	04.2	05.2	!
775	83	06.2	07.2	08.3	09.8	10.3	11.3	12.4	13.4	14.4	15.5	1
776	83	16.5	17.5	18.5	19.6	20.6	21.6	22.6	23.6	24.7	25.7	
777	83	26.7	27.7	28.8	29.8	30.8	31.8	32.9	83.9	84.9	36.0	
778	83	37.0	88.0	89.0	40.1	41.1	42.1	43.1	44.1	45.2	46.2	1
779	83	47.2	48.2	49.2	50.3	51.3	52.8	58.8	54.3	55.4	56.4	
780	82	57.4	58.4	59.4	60.5	61.5	62.5	63.5	64.5	65.6	66.6	
781	83	67.6	68.6	69.6	70.7	71.7	72.7	73.7	74.7	75.8	76.8	
782	83	77.8	78.8	79.8	80.9	81.9	82.9	88.9	84.9	86.0	87.0	
783	83	88.0	89.0	90.0	91.1	92.1	93.1	94.1	95.1	96.2	97.2	
784	83	98.2	99.2	50.0	31.1	74.1	80.1	34.1	80.1	DU. 2	81.2	
784	84	50.2	55.2	00.2	01.2	02.2	03.2	04.3	05.3	06.3	07.3	
785	84	06.8	09.3	10.3	11.4	12.4	13.4	14.4	15.4	16.5	17.5	
786	84	18.5	19.5	20.5	21.5	22.5	28.5	24.6	25.6	26.6	27.6	-
787	84	28.6	29.6	30.6	31.6	32.6	33.6	34.7	35.7	36.7	37.7	
788	84	28.7	39.7	40.7	41.7	42.7	43.7	44.8	45.8	46.8	47.8	
789	84	48.8	49.8	50.8	51.8	52.8	58.8	54.9	55.9	56.9	57.9	
790	84	58.9	59.9	60.9	61.9	62.9	63.9	65.0	66.0	67.0	68.0	
791	84	68.9	69.9	70.9	71.9	72.9	78.9	75.0	76.0	77.0	78.0	1 0.1
792	84	79.0	80.0	81.0	82.0	83.0	84.0	85.0	86.0	87.0	88.0	2 0.2
793	84	89.0	90.0	91.0	92.0	93.0	94.0	95.1	96.1	97.1	98.1	3 0.8
794	84	99.1			ŀ							4 0.4
794	85		00.1	01.1	02.1	03.1	04.1	05.1	06.1	07.1	08.1	5 0.0
795	85	09.1	10.1	11.1	12.1	13.1	14.1	15.1	16.1	17.1	18.1	6 0.6
796	85	19.1	20.1	21.1	22.1	23.1	24.1	25.1	26.1	27.1	28.1	7 0.7
797	85	29.1	80.1	31.1	32.1	33.1	34.1	35.1	36.1	37.1	38.1	8 0.8
798	85	89.1	40.1	41.1	42.1	48.1	44.1	45.1	46.1	47.1	48.1	9 0.8
799	85	49.1	50.1	51.1	52.0	58.0	54.1	55.0	56.0	57.0	58.0	
800	85	59.0	60.0	61.0	62.0	63.0	64.0	65.0	66.0	67.0	68.0	
801	85	69.0	70.0	70.9	71.9	72.9	78.9	74.9	75.9	76.9	77.9	
802	85	78.9	79.9	80.9	81.9	82.9	88.9	84.9	85.8	86.8	87.8	
808	85	88.8	89.8	90.8	91.8	92.8	93.8	94.8	95.8	96.7	97.7	l
804	85	98.7	99.7	_								
804	86			00.7	01.7	02.7	03.7	04.7	05.7	06.6	07.6	
805	86	08.6	09.6	10.6	11.6	12.6	13.6	14.6	15.5	16.5	17.5	1
806	86	18.5	19.5	20.5	21.5	22.5	28.4	24.4	25.4	26.4	27.4	l
807	86	28.4	29.4	80.4	81.8	32.3	33.3	34.3	35.3	36.3	87.3	1
808	86	38.3	39.2	40.2	41.2	42.2	48.2	44.2	45.1	46.1	47.1	
809	86	48.1	49.1	50.1	51.1	52.0	58.0	54.0	55.0	56.0	57.0	1
810	86	57.9	58.9	59.9	60.9	61.9	62.8	68. 8	64.8	65.8	66.8	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9	Parts for eac 0.01mm

BAROMETRICAL MEASUREMENT OF HEIGHTS. - DELCROS.

TABLE II. CORRECTION FOR DIFFERENCE OF TEMPERATURE OF ATTACHED THERMOMETERS.

Temperature of Barometers at Station $\begin{cases} Upper = T \\ Lower = T. \end{cases}$

	_				-	T		T	
_	Correct.	T' T	Correct.	T' — T	Correct.	TTT	Correct	T'-T	Correct.
Centig.	Metres.	Centigrade.	Metres.	Centigrade.	Metres.	Centigrade,	Metres.	Centigrade.	Metres.
0.0	0.0	8.0	10.3	16.0	20.6	24.0	80.9	32.0	41.3
0.2	0.8	8.2	10.6	16.2	20.9	24.2	31.2	32.2	41.5
0.4	0.5	8.4	10.8	16.4	21.1	24.4	31.5	82.4	41.8
0.6	0.8	8.6	11.1	16.6	21.4	24.6	31.7	32.6	42.0
0.8	1.0	8.8	11.3	16.8	21.7	24.8	32.0	32.8	42.3
1.0	1.3	9.0	11.6	17.0	21.9	25.0	32.2	83.0	42.5
1.2	1.5	9.2	11.9	17.2	22.2	25.2	32.5	33.2	42.8
1.4	1.8	9.4	12.1	17.4	22.4	25.4	82.7	83.4	43.1
1.6	2.1	9.6	12.4	17.6	22.7	25.6	83.0	83.6	45.3
1.8	2.3	9.8	12.6	17.8	22.9	25.8	83.8	33.8	43.6
2.0	2.6	10.0	12.9	18.0	23.2	26.0	83.5	84.0	43.8
2.2	2.8	10.2	18.1	18.2	23.5	26.2	33.8	34.2	44.1
2.4	3.1	10.4	18.4	18.4	23.7	26.4	84.0	84.4	44.3
2.6	3.4	10.6	18.7	18.6	24.0	26.6	34.3	34.6	44.6
2.8	8.6	10.8	18.9	18.8	24.2	26.8	84.6	84.8	44.9
3.0	3.9	11.0	14.2	19.0	24.5	27.0	84.8	85.0	45.1
3.2	4.1	11.2	14.5	19.2	24.8	27.2	35.1	35.2	45.4
8.4	4.4	11.4	14.7	19.4	25.0	27.4	85.8	35.4	45.6
3.6	4.6	11.6	15.0	19.6	25.8	27.6	35.6	85.6	45.9
8.8	4.9	11.8	15.2	19.8	25.5	27.8	85.8	35.8	46.2
40	5.2	12.0	15.5	20.0	25.8	28.0	86.1	36.0	46.4
4.2	5.4	12.2	15.8	20.2	26.0	28.2	86.4	36.2	46.7
4.4	5.7	12.4	16.0	20.4	26.3	28.4	86.6	36.4	46.9
4.6	5.9	12.6	16.3	20.6	26.6	28.6	86.9	36.6	47.2
4.8	6.2	12.8	16.5	20.8	26.8	28.8	87.1	36.8	47.4
5.0	6.4	13.0	16.8	21.0	27.1	29.0	37.4	37.0	47.7
5.2	6.7	13.2	17.0	21.2	27.8	29.2	87.6	37.2	48.0
5.4	7.0	13.4	17.8	21.4	27.6	29.4	87.9	87.4	48.2
5.6	7.2	13.6	17.5	21.6	27.8	29.6	88.2	37.6	48.5
58	7.5	13.8	17.8	21.8	28.1	29.8	88.4	37.8	48.7
6.0	7.7	14.0	18.0	22.0	28.4	80.0	88.7	38.0	49.0
6.2	8.0	14.2	18.3	22.2	28.6	30.2	88.9	88.2	49.2
6.4	8.8	14.4	18.5	22.4	28.9	30.4	89.2	38.4	49.5
6.6	8.5	14.6	18.8	22.6	29.1	80.6	39.5	38.6	49.8
6.8	8.8	14.8	19.0	22.8	29.4	80.8	89.7	38.8	50.0
7.0	9.0	15.0	19.3	23.0	29.7	81.0	40.0	39.0	50.3
7.2	9.3	15.2	19.6	23.2	29.9	81.2	40.2	39.2	50.5
7.4	9.5	15.4	198	23.4	30.2	31.4	40.5	89.4	50.8
7.6	9.8	15.6	20.1	23.6	80.4	31.6	40.7	39.6	51.1
7.8	10.1	15.8	20.3	23.8	30.7	31.8	41.0	89.8	51.3
8.0	10.3	16.0	20.6	24.0	30.9	32.0	41.8	40.0	51.6

This Table supposes the scale to be of brass from the top to the cistern. If it were of glass or of wood, the argument T'—T ought to be diminished at the ratio of 54 to 62.

In computing by the formula of Laplace, we begin by reducing the barometers to the same temperature by means of the following formula: $H = h' + h' \left(\frac{T' - T}{6196}\right)$. Table II. saves this trouble, and gives, in metres, the correction due to the difference of temperature of the barometers.

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TABLE III. CORRECTION FOR DEGREASE OF GRAVITATION IN LATITUDE.

 $\beta = (0.0028371 \text{ cosin. 2 L}). (A + a + \beta).$

The Argument is the Mean Latitude between the two Stations.

LATT	rude.				Co	rrection, in	metres, for			
Corre Added		1000	2000	3000	4000	5000	6000	7000	8000	9000
°	90	2.8	5.7	8.5	11.3	14.2	17.0	19.9	22.7	25.7
1	89	2.8	5.7	8.5	11.8	14.2	17.0	19.8	22.7	25.6
2	88	2.8	5.7	8.5	11.8	14.1	17.0	19.8	22.6	25.5
3	87	2.8	5.6	8.5	11.3	14.1	16.9	19.7	22.6	25.4
4	86	2.8	5.6	8.4	11.2	14.0	16.9	19.7	22.5	25.8
5	85	2.8	5.6	8.4	11.2	14.0	16.8	19.6	22.8	25.1
6	84	2.8	5.5	8.8	11.1	13.9	16.6	19.4	22.2	25.0
7	83	2.7	5.5	8.2	11.0	13.8	16.5	19.8	22.0	24.8
8 .	82	2.7	5.4	8.2	10.9	13.6	16.4	19.1	21.8	24.5
9	81	2.7	5.4	8.1	10.8	13.5	16.2	18.9	21.6	24.3
10	80	2.7	5.8	8.0	10.7	13.8	16.0	18.7	21.8	24.0
11	79	2.6	5.2	7.9	10.5	13.1	15.8	18.4	21.0	23.7
12	78	2.6	5.2	7.8	10.4	18.0	15.5	18.1	20.7	28.3
13	77	2.5	5.1	7.6	10.2	12.7	15.3	17.8	20.4	22.9
14	76	2.5	5.0	7.5	10.0	12.5	15.0	17.5	20.0	22.5
15	75	2.5	4.9	7.4	9.8	12.3	14.7	17.2	19.7	22.1
16	74	2.4	4.8	7.2	9.6	12.0	14.4	16.8	19.2	21.6
17	73	2.4	4.7	7.0	9.4	11.8	14.1	16.5	18.8	21.2
18	72	2.3	4.6	6.9	9.2	11.5	13.8	16.1	18.4	20.7
19	71	2.2	4.5	6.7	8.9	11.2	13.4	15.6	17.9	20.1
20	70	2.2	4.8	6.5	8.7	10.9	13.0	15.2	17.4	19.6
21	69	2.1	4.2	6.8	8.4	10.5	12.6	14.7	16.9	19.0
22	68	2.0	4.1	6.1	8.2	10.2	12.2	14.3	16.3	18.4
23	67	2.0	3.9	5.9	7.9	9.8	11.8	13.8	15.8	17.7
24	66	1.9	3.8	5.7	7.6	9.5	11.4	18.3	15.2	17.1
25	65	1.8	3.6	5.5	7.8	9.1	10.9	12.8	14.6	16.4
26	64	1.7	8.5	5.2	7.0	8.7	10.5	12.2	14.0	15.7
27	63	1.7	8.8	5.0	6.7	8.3	10.0	11.7	13.8	15.0
28	62	1.6	3.2	4.8	6.3	7.9	9.5	11.1	12.7	14.8
29	61	1.5	8.0	4.5	6.0	7.5	9.0	10.5	12.0	13.5
30	60 59	1.4	2.8	4.3	5.7	7.1	8.5 8.0	9.9	11.8	12.8 12.0
31	1 1	1.3	2.7	4.0	5.8 5.0	6.6 6.2		9.8 8.7	10.6	11.2
32 83	58 57	1.2 1.1	2.5 2.3	8.7 8.5	4.6	5.8	7.5 6.9	8.1	9.9 9.2	10.4
84	56	1.1	2.3	8.2	4.0	5.3	6.4	7.4	8.5	9.6
35	55	1.0	1.9	2.9	3.9	4.8	5.8	6.8	7.8	8.7
36	54	0.9	1.7	2.6	3.5	4.4	5.3	6.1	7.0	7.9
87	53	0.8	1.6	2.3	3.1	8.9	4.7	5.5	6.2	7.0
38	52	0.7	1.4	2.1	2.7	8.4	4.1	4.8	5.5	6.2
39	51	0.6	1.2	1.8	2.4	2.9	8.5	4.1	4.7	5.3
40 .	50	0.5	1.0	1.5	2.0	2.5	8.0	3.4	8.9	4.4
41	49	0.4	0.8	1.2	1.6	2.0	2.4	2.8	8.2	8.5
42	48	0.8	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7
43	47	0.2	0.4	0.6	0.8	1.0	1.2	1.4	1.6	1.8
44	46	0.1	0.2	0.8	0.4	0.5	0.6	0.7	0.8	0.9
45	45	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
						01	<u> </u>			!

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TABLE IV. CORRECTION FOR DECREASE OF GRAVITATION ON A VERTICAL LINE.

$$\mathfrak{d} = \left(\frac{\mathbb{A} + \alpha + \beta + \nu + 15396}{5366300}\right) \times \mathbb{A} \left(+ \alpha + \beta + \nu \right).$$

 $Argument = (A + a + \beta + v).$

Approximate Difference of Level.	Correspond. Correction Pusitive.	Approximate Difference of Level.	Correspond. Correction Positive.	Approximate Difference of Level.	Correspond. Correction Positive.	Approximate Difference of Level.	Correspond. Correction Positive.
Metres.	Metres.	Metres.	Metres.	Metres.	Motres.	Metres.	Metres.
100	0.2	2100	6.0	4100	12.9	6100	21.1
200	0.5	2200	6.3	4200	13.3	6200	21.6
300	0.8	2300	6.6	4800	18.7	6300	22.0
400	1.0	2400	6.9	4400	14.1	6400	22.5
500	1.3	2500	7.8	4500	14.5	6500	22.9
600	1.6	2600	7.6	4600	14.9	6600	23.4
700	1.8	2700	7.9	4700	15.8	6700	23.9
800	2.1	2800	8.3	4800	15.7	6800	24.3
900	2.4	2900	8.6	4900	16.1	6900	24.8
1000	2.7	8000	8.9	5000	16.5	7000	25.3
1100	2.9	8100	9.3	5100	16.9	7100	25.7
1200	8.2	8200	9.6	5200	17.8	7200	26.2
1800	8.5	8300	10.0	5300	17.7	7800	26.7
1400	8.8	8400	10.3	5400	18.1	7400	27.2
1500	4.1	8500	10.7	5500	18.5	7500	27.7
1600	44	8600	11.1	5600	19.0	7600	28.1
1700	4.7	8700	11.4	5700	19.4	7700	28.6
1800	5. 0	8800	11.8	5800	19.8	7800	29.1
1900	5.8	8900	12.2	5900	20.8	7900	29.6
2000	5.6	4000	12.5	6000	20.7	8000	30.1

TABLE V. CORRECTION FOR THE ELEVATION OF THE LOWER STATION ABOVE OCEAN.

Argument = Height of Barometer at Lower Station.

		He	ight of Barou	neter at Lowe	er Station in	Millimetres.		
Difference of Level.	400	450	500	550	600	650	700	750
Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres
1000	1.7	1.4	1.1	0.9	0.6	0.4	0.2	0.0
2000	8.4	2.8	2.2	1.7	1.8	0.8	0.4	0.1
8000	5.1	4.2	8.8	2.6	1.9,	1.8	0.7	0.1
4000	6.8	5.6	4.4	8.4	2.5	1.7	0.9	0.1
5000	8.5	6.9	5.5	4.3	8.1	2.1	1.1	0.1
6000	10.8	8-8	6.7	5.2	8.8	2.5	1.8	0.2
7000	12.0	9.7	7.8	6.0	4.4	2.9	1.5	0.2
8000	13.7	11.1	8.9	6.9	5.0	8.4	1.8	0.2
9000	15.4	12.5	10.0	7.7	5.7	3.8	2.0	0.3

TABLES

FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS. BY A. GUYOT.

Tables which, like the preceding ones by Delcros, in metrical measures, are sufficiently extensive to save the necessity of interpolations, relieve the computer of most of his trouble, and considerably reduce the chances of error in the computations. They thus render to science itself a real service, by inducing observers to determine a larger number of points, and to secure the accuracy of the results by repeating their observations at the same point in various atmospheric circumstances, both of which they can do without fear of being overwhelmed by the labor of the computation.

Similar tables are here offered to the observers who use instruments graduated to English measures. Like those of Delcros, the new tables are based on Laplace's formula, with a slight modification of only one constant. They dispense with the use of logarithms, and give the differences of level corresponding to every thousandth of an inch from 12 to 31 inches by means of the simplest arithmetical operations, so that the data being prepared and corrected, the computation of an elevation takes but a few minutes, and is done with scarcely any chance of error.

Laplace's formula and constants were adopted for the computation of the tables in preference to others found in the following sets for reasons which a few words will explain.

It has been remarked, page 9, that, in consequence of Laplace's constants having been retained in Gauss's, Schmidt's, and Baily's formulæ, they all give similar results; but that Bessel's formula differs in separating the correction due to the moisture of the air from that due to its temperature, while in Laplace's, and in the formulæ just mentioned, both are united. To introduce a separate correction for the expansion of aqueous vapor is, in the writer's view, a doubtful improvement. The laws of the distribution and transmission of moisture through the atmosphere are too little known, and its amount, especially in mountain regions, is too variable, and depends too much upon local winds and local condensation, to allow a reasonable hope of obtaining the mean humidity of the layer of air between the two stations by means of hygrometrical observations taken at each of them. These doubts are confirmed by the experience of the author and of many other observers, which shows that, on an average, Laplace's method works not only as well as the other, but more uniformly well. At any rate, the gain, if there is any, is not clear enough to compensate for the undesirable complication of the formula.

Though the several co-efficients of Laplace's formula need perhaps to be modified according to more recent and probably more accurate determinations of the physical constants on which they depend, as has been proposed by Plantamour, E. Ritter, and lately by the writer himself in a paper read before the American Association for the Advancement of Science at their meeting in Montreal, they have been retained in preparing the following tables, partly because it was found that the errors due to

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the various co-efficients nearly compensate each other; partly on the ground that, until a severe test, by means of actual comparative measurements made for the purpose, has shown the expediency of these modifications, it seemed desirable to adhere to the old constants, and thus to preserve a uniformity in the results with the tables of Oltmans, Delcros, Gauss, Baily, and others, which have already been extensively used. The substitution of the co-efficient 0.00260, expressing, according to Schmidt's computation (Mathem. und Physic. Geogr., II. p. 202), the variation of gravity in latitude, for the value 0.002837, does not sensibly alter the altitudes obtained.

The close agreement of the determinations furnished by Laplace's formula, in barometrical measurements carefully conducted, made in favorable circumstances, and during the warm season, with those obtained from repeated trigonometrical observations, or by the spirit-level, strongly testifies in favor of its general correctness. A few striking examples will suffice to show it.

The altitude of Mont Blanc, measured by the barometer, by MM. Bravais and Martins, on the 29th of August, 1844, and computed by Delcros, by means of nine corresponding stations situated on all sides of the mountain (see Annuaire Météorologique de France, for 1851, p. 274), was found to be 4810 metres. The altitude of the same point, being the mean of seven of the most elaborate and reliable geodetic measurements, which cost nearly twenty years of labor, is 4809.6 metres.

For smaller elevations the formula seems to answer equally well.

The barometrical measurement of Mount Washington, in New Hampshire, by the author, on the 8th and 9th of August, 1851, gave, by Delcros's Tables, for the mean of eight observations, taken at different hours of the day, 5466.7 English feet above Gorham, N. H., 6285.7 above high tide, and 6291.7 feet above the mean level of the ocean in Portland harbor. In August, 1852, W. A. Goodwin, Civil Engineer, starting from Gorham Railroad Station, found, by the spirit-level, Mount Washington to be 6285.5 feet above mean tide. In September, 1853, Captain T. J. Cram, of the Topographical Engineers, executed, in behalf of the Coast Survey, a careful measurement with the spirit-level, on the same line, for the purpose of testing the various methods of measuring altitudes, and found Mount Washington to be 6293 English feet above the mean level of the ocean.

In lower latitudes the formula showed equally good results. By a barometrical measurement in July, 1856, the altitude of the highest peak of the Black Mountain, North Carolina, about Lat. 36°, was found by the author to be 6701 English feet; and that of the highest Mountain House 5248 feet. In September, 1857, Major T. C. Turner, Chief Engineer of the Morganton Railroad, ran a line of levels from the same point which was used as the lower station for the barometrical measurement, to the top of the highest peak, and found its altitude to be 6711 English feet, and that of the Mountain House 5246 feet. Other points on the line agreed equally well.

Such an agreement, in so considerable elevations, is all that can be desired.

These figures show conclusively, that, when the errors which may arise from the great variability of the data furnished by the instruments have been removed by a repetition, in various states of the atmosphere, and by a proper combination of simultaneous observations at stations not too distant from each other, those which remain and may be attributed to the formula cannot be considerable. But, on the other

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hand, we have no right to expect such results from single observations, taken, perhaps, in unsettled weather, without paying any regard to the time of the day at which they were made, to the distance or the non-simultaneity of the corresponding observations, or to other unfavorable circumstances. It is too well known that in such cases large errors may and do actually occur; but for these the formula ought not to be held responsible.

ARRANGEMENT OF THE TABLES.

If we call

h = the observed height of the barometer τ = the temperature of the barometer t = the temperature of the air t = the observed height of the barometer t = the temperature of the barometer t = the temperature of the air

If we make, further,

Z = the difference of level between the two barometers;

L = the mean latitude between the two stations;

H == the height of the barometer at the upper station reduced to the temperature of the barometer at the lower station; or,

 $H = h' \{1 + 0.00008967 (\tau - \tau')\};$

The expansion of the mercurial column, measured by a brass scale, for 1° Fahrenheit = 0.00008967;

The increase of gravity from the equator to the poles = 0.00520048, or 0.00260 to the 45th degree of latitude;

The earth's mean radius = 20,886,860 English feet;

Then, Laplace's formula, reduced to English measures, reads as follows:

$$Z = \log \frac{h}{H} \times 60158.6 \text{ English feet} \left\{ egin{aligned} \left(1 + rac{t + t' - 64}{900}
ight). \ \left(1 + 0.00260\cos 2\ L\right). \ \left(1 + rac{z + 52252}{20886860} + rac{h}{10443430}
ight). \end{aligned}
ight.$$

Table I. gives, in English feet, the value of $\log H$ or $h \times 60158.6$ for every hundredth of an inch, from 12 to 31 inches in the barometer, together with the value of the additional thousandths, in a separate column. These values have been diminished by a constant, which does not alter the difference required.

Table II. gives the correction 2.343 feet \times $(\tau - \tau')$ for the difference of the temperatures of the barometers at the two stations, or $\tau - \tau'$. As the temperature at the upper station is generally lower, $\tau - \tau'$ is usually positive, and the correction negative. It becomes positive when the temperature of the upper barometer is higher, and $\tau - \tau'$ negative. When the heights of the barometers have been reduced to the same temperature, or to the freezing point, this table will not be used.

Table IV. shows the correction $D' \frac{z + 52252}{20886860}$ to be applied to the approximate altitude for the decrease of gravity on a vertical acting on the density of the mercurial column. It is always additive.

BAROMETRICAL MEASUREMENT OF HEIGHTS.

Table V. furnishes the small correction $\frac{\hbar}{10443430}$ for the decrease of gravity on a vertical acting on the density of the air; the height of the barometer \hbar at the lower station representing its approximate altitude. Like the preceding correction, it is always additive.

USE OF THE TABLES.

In Table I. find first the numbers corresponding to the observed heights of the barometer h and h'. Suppose, for instance, h = 29.345 in.; find in the first column on the left the number 29.3; on the same horizontal line, in the column headed .04, is given the number corresponding to 29.34 = 28121.7; in the last column but one on the right, we find for .005 = 4.5, or for 29.345 = 28126.2. Take likewise the value of h', and find the difference.

If the barometrical heights have not been previously reduced to the same temperature, or to the freezing point, apply to the difference the correction found in Table II. opposite the number representing r - r'; we thus obtain the approximate difference of level, D.

For computing the correction due to the expansion of the air according to its temperature, or $D \times {t+t'-64 \choose 900}$, make the sum of the temperatures, subtract from that sum 64; multiply the rest into the approximate difference D, and divide the product by 900. This correction is of the same sign as (t+t'-64). By applying it, we obtain a second approximate difference of level, D'.

In Table III., with D' and the mean latitude of the stations, find the correction for variation of gravity in latitude, and add it to D', paying due attention to the sign.

In Table IV. with D', and in Table V. with D' and the height of the barometer at the lower station, take the corrections for the decrease of gravity on a vertical, and add them to the approximate difference of level.

The sum thus found is the true difference of level between the two stations, or Z; by adding the elevation of the lower station above the level of the sea, when known, we obtain the *altitude* of the upper station.

The use of the small table, VI., by means of which approximate differences of level can be obtained by a single multiplication, is explained below, page 90.

Example 1.

Measurement of Mount Washington, New Hampshire, by A. Guyot, August 8th, 1851, 4 r.m.; the barometer at the lower station being at 825 English feet above the mean level of the sea; at the upper station at one foot below the summit.

The observation gave,

Gorham,
$$h = 29.272$$
 in. $r = 70^{\circ}.70$ F. $t = 72^{\circ}.05$ F. Mount Washington, $h' = 24.030$ " $t' = 54^{\circ}.52$ F. $t' = 50^{\circ}.54$ F. $t' = 64^{\circ}.59$ F. $t' = 64^{\circ}.59$ F. $t' = 64^{\circ}.59$ F. $t' = 64^{\circ}.59$ F. $t' = 64^{\circ}.59$ F. $t' = 64^{\circ}.59$ F.

BAROMETRICAL MEASUREMENT OF HEIGHTS,

	28,061.00 22,965,69
Difference, Table II. gives for $\tau - \tau' = 16^{\circ}.48$	5,155.40 — 37.64
Approximate difference of level, $D =$	5,117.76
$\frac{D \times (t + t' - 64)}{900} = \frac{5118 \times 58.6}{900} =$	333.19
Second approximate difference, $D'=$	5,450.95
Table III. gives for $D'=5450$ and Lat. 44°	0.50
Table IV. gives for $D'=5450$	14.94
Table V. gives for $h = 29.27$	0.00
Barometer below summit,	 1.00
Mount Washington above Gorham, or $Z =$	5,465.39
Barometer at Gorham above sea level	825.00
Mount Washington above the sea, or altitude,	6,290.39 Eng. ft.

Example 2.

Measurement of the highest peak of the Black Mountain, in North Carolina, July 11th, 1856, by A. Guyot.

By observation we have at,

	Deloment.	Attached Thermometer.	Temperature of Air.
Mountain House,	$\lambda = 24.934 \text{ in.}$	$\tau = 64^{\circ}.58 \text{ F}.$	$t = 61^{\circ}.34 \text{ F}.$
Highest Peak,	h' = 23.662 "	$\tau = 61^{\circ}.88 \text{ F.}$	$t' = 59^{\circ}.36 \text{ F}.$
	7-	$-r' = 2^{\circ}.70 \text{ F.}$	120°.70 F. 64°
		t + t' -	$64 = 56^{\circ}.7 \text{ F}.$
_			
Table II. give		5 0,	
		mate difference, D =	
	$\frac{D\times (t+r-6)}{900}$	$\frac{4)}{900} = \frac{1862 \times 56.7}{900} =$	= 85.8
	Second approxi	mate difference, D' :	= 1,447.5
Table III. give	es for $D'=1448$ as		. 1.2
_	es for $D'=1448$		3.8
•		and $h=25$.	. 0.7
Highest peak	above Mountain Ho	use, or Z :	= 1,453.2
Mountain Hou	se above the sea		5,248.4
Black Mounta	in, highest peak abo	ove the sea, or altitud	le, 6,701.6 Eng. fl

II.

TABLES

POR COMPUTING THE DIFFERENCE IN THE HEIGHT OF TWO PLACES FROM BAROMETRICAL OBSERVATIONS.

I. $D = 00158.53 \times \log H$ or A. Argument, the observed Height of the Barometer at either Station.

1	4	0	-:	61	<u>ئ</u>	7	ıd.	9	۲.	œ.	ei -	•	-	ci.	eś.	4
	A.	13	12	22	2	2	12.5	22	2	12	12	18.0	13	2	22	25
um od thu				į	2.1	4.2	6	8.8	10.4	12.5	14.6	16.6	18.7			
E E	о д				-	M	•	*	20	9	7	80	6			
	8	Eng. Fest. 4958.6	5178.8	6887.2	6699.0	5809.0	6017.4	6224.0	6429.2	6632.7	6884.5	7084.9	7233.8	7431.1	7627.0	7821.4
	80.	Eng. Feet.	5 152.4	6367.0	5578.9	5788.1	5996.6	6203.5	6408.8	6612.4	6814.4	7014.9	7213.9	7411,4	7607.4	7802.0
	.07	Eng. Fost.	6130.9	5344.7	5556.8	5767.3	6975.8	6182.8	6388.8	6592.1	6794.8	6995.0	7194.1	7891.8	7687.9	7782.6
	ş	Eng. Feet. 4898.7	5109.4	5823.4	5585.7	5746.2	5955.0	6162.2	6367.8	8211.8	6774.1	6975.0	7174.8	7872.1	7568.4	7768.2
of em Inch.	99.	Ebg. Fost. 4872.1	6.7808	5302.1	6614.5	5725.8	5934.2	6141.6	6847.8	6551.5	6754.0	6955.0	7154.4	7852.8	7548.8	7743.8
Hundredths of an Inch.	ş	Eng. Feet. 4850.4	5086.4	5280.7	5498.4	5704.8	6918.4	6120.9	6326.8	6531.1	6783.8	6934.9	7184.5	7882.6	7529.2	7724.4
		Eng. Fest. 4828.7	5044.9	5259.4	6472.2	5683.2	5892.6	6100.2	6306.3	6210.8	6718.6	6914.9	7114.6	7812.9	7509.6	1704.9
	8	Pr. Fort. 4806.9	5023.4	6238.0	6462.0	5662.2	5871.7	6079.6	6285.8	6490.4	6693.4	6894.8	7094.7	7293.1	7490.0	7685.4
	.01	Eng. Feet. 4785.2	8001.8	6216.6	5429.8	5641.2	6850.8	6058.8	6265.2	6470.0	6673.2	6874.7	7074.8	7278.8	7470.4	7666.0
	\$	Pp. Part. 4768.4	4980.3	5196.3	5408.5	5620.1	6839.9	6038.1	6214.6	6449.6	6652.9	6854.7	7054.9	7258.6	7450.8	7646.5
Barometer	Pre. Inst.	12.0	13.1	12.2	18.8	12.4	12.6	12.6	12.7	12.8	12.9	18.0	18.1	18.3	18.8	18.4

3	- inch	ļ .		۲.	œ,	e	d	-:	64	œi	•	ń	<u>.</u>	۲.	œ,	ف 	e.	-	esi	œ,	4	ند	9	<u>٠</u>	<u>من</u>	6
Barometer	Eng. Inch.	18.6	18.6	18.7	13.8	13.9	14.0	14.1	14.2	14.8	77.	14.6	14.6	14.7	14.8	14.9	15.0	16.1	16.2	16	16.4	*	15.6	. 15.7	15.8	15
Thousandths	i di		Feet.	1.9	8.8	9.9	7.5	9.4	11.8	18.2	16.0	17.0			1.7	8.7	6.1	8.8	8.5	10.2	11.9	13.6	16.8			
Tho				-	ea	æ		10	9	7	80	۵	_		_	ø	60	4	10	9	7	80	6			
	\$	Eng Feet. 8014.8	8206.9	8396.0	8284.8	8772.2	8958.3	9148.0	9326.5	9508.7	9.6896	8869.8	10047.8	10225.1	10401.2	10576.0	10749.6	10922.1	11093.5	11263.8	11433.0	11601.1	11768.2	11934.8	12099.2	12263.1
	9	Eng. Feet. 7995.1	8186.8	8377.1	82929	8753.5	8989.7	9124.6	9308.3	9490.5	9671.6	9851.4	10030.0	10207.4	10383.6	10558.6	10732.8	10904.9	11076.4	11246.8	11416.3	11584.4	11751.6	11917.7	12082.7	12246.7
	.07	Eng. Feet. 7975.8	8167.7	8858.1	8647.1	8784.8	8921.2	9106.3	9289.9	9472.8	9658.5	9833.5	10012.2	10189.7	10366.1	10541.2	10715.0	10887.7	11059.8	11229.8	11399.8	11567.6.	11784.9	11901.1	12066.3	12280.4
	8 .	Eng. Feet. 7956.6	8148.6	8339.1	8628.8	8716.1	8902.6	9087.8	9271.6	9454.2	9635.5	9815.6	9994.4	10172.0	10848.5	10528.7	10697.6	10870.5	11042.2	11212.8	11382.4	11650.8	11718.2	11884.6	12049.8	12214.0
Hundredths of an Inch.	.	Eng. Feet. 7937.8	8129.4	8320.1	8609.4	8697.4	8884.0	8.6906	9253.8	9436.0	9617.4	9.797.6	9976.5	10154.8	10330.9	10506.8	10680.3	10853.2	11025.1	11195.8	11365.5	11684.0	11701.6	11868.0	12033.8	12197.6
Handredth	70.	Eng. Feet. 7918.0	8110.8	8301.1	8490.6	8678.6	8865.4	80906	9234.9	9417.7	9599.8	9779.6	9968.7	10136.6	10313.3	10488.8	10662.9	10836.0	11008.0	11178.8	11348.6	11517.2	11684.8	11861.4	12016.9	12181.2
	8	Eng. Feet.	8091.1	8282.1	8471.7	8669.9	8846.8	9082.4	9216.6	9399.5	9581.3	9761.7	8940.9	10118.8	10295.7	10471.3	10645.6	10818.7	10990.8	11161.8	11831.6	11500.4	11668.1	11834.8	12000.4	12164.8
	.09	Eng. Feet.	8071.9	8263.1	8452.8	8641.1	8828.2	9018.9	9198.2	9381.3	9563.1	9743.7	9928.0	10101.1	10278.0	10458.8	10628.2	10801.5	10973.6	11144.7	11814.7	11483.6	11651.4	11818.2	11983.8	12148.4
	.01	Eng. Feet. 7860.1	8062.8	8244.0	8483.9	8622.3	8809.5	8995.4	9179.8	9963.0	9545.0	9725.7	9905.1	10083.8	10260.4	10486.8	10610.8	10784.1	10956.5	11127.7	11297.8	11466.7	11634.6	11801.6	11967.8	12132.0
	8.	Eng. Foot.	8033.6	8225.0	8416.0	9.8098	8790.8	8976.8	9161.4	9844.7	9626.8	9707.6	9887.3	10065.5	10242.7	10418.7	10693.4	10766.9	10939.8	11110.6	11280.8	11449.9	11617.9	11784.9	11950.8	12115.6
Barometer	E. Inob.	4 8 6	18.6	18.7	18.8	18.9	14.0	14.1	14.3	14.8	14.4	14.5	14.6	14.7	14.8	14.9	16.0	16.1	16.2	15.8	15.4	15.5	15.6	16.7	15.8	16.9

Barometer			·		Handredth	Hundredths of an Inch.					T C		Berometer
In Eng. 10ch	. 00	10.	.03	ۥ	70.	90 °	90.	40.	80.	8.		2 d	Br. Inch.
9	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Foet.	Eng. Feet.	Eng. Feet.	Eng Feet.	Eng. Feet.	Eng Feet.			0 81
16.1		12458.6	12474.8	12491.0	12507.2	12528.4	12539.6	12555.7	12671.9	12588.0		Je t	16.1
16.2		12620.8	12636.4	12652.5	12668.6	12684.7	12700.8	12716.8	12732.9	12748.9	-	9.6	16.2
16.8	12765.0	12781.0	12797.0	12818.0	12829.0	12845.0	12861.0	12876.9	12592.9	12906.8	69	8:	16.8
16.4	12924.8	12940.7	12956.6	12972.5	12988.4	18004.8	18020.2	13036.0	13051.9	13067.7	•	4.7	16.4
16.5	18083.6	18099.4	13115.2	18181.0	18146.8	18162.6	13178.4	13194.2	18210.0	18226.7	4	8.9	16.5
16.6	13241.5	18257.2	13272.9	18288.6	13304.8	18320.0	18335.7	18351.4	13367.1	18382.7	10	7.8	16.6
16.7	13396.4	18414.0	13429.6	18445.2	13.160.8	13476.4	18492.0	18507.6	13523.2	13538.7	9	9.4	16.7
16.8		13569.8	13586.4	18600.9	18616.4	18631.9	18647.4	13662.9	18678.4	13693.9	~	11.0	16.8
16.9	18709.4	18724.8	18740.8	13755.7	18771.1	18786.5	13801.9	13817.8	18832.7	18848.1	00	12.6	16.9
3 17.0	18963.5	18878.8	18894.2	13909.6	13924.9	18940.2	13955.6	18970.9	18986.2	14001.5	•	7	17.0
17.1	_	14032.0	14047.8	14062.6	14077.8	14093.0	14108.8	14128.6	14138.7	14153.9			17.1
17.3	14169.1	14184.3	14199.4	14214.6	14229.8	14244.9	14260.1	14275.8	14290.8	14305.5	_		17.2
17.8	14320.6	14335.7	14350.8	14365.8	14880.9	14896.0	14411.0	14426.1	14441.1	14456.2			17.8
17.4	14471.2	14486.2	14601.2	14516.2	14531.2	14546.1	14561.1	14676.1	14591.0	14605.9	-	1.6	17.4
17.6	14620.9	14635.8	14650.7	14665.6	14680.5	14695.4	14710.8	14726.2	14740.1	.14754.9	64	6.5	17.6
17.6	14769.8	14784.6	14799.4	14814.3	14829.1	14848.9	14858.7	14873.5	14888.2	14903.0	8	4.	17.6
17.7	14917.8	14932.5	14947.8	14962.0	14976.8	14991.5	15006.2	15020.9	16035.6	15050-8	4	8.8	17.7
17.8	15065.0	15079.6	15094.8	15109.0	16128.6	15138.2	15152.9	15167.8	15182.1	15196.7	10	7.8	17.8
17.9	15211.8	16225.9	15240.5	15255.0	15269.6	15284.2	15298.7	15318.8	16827.8	16842.4	9	هن هن	17.9
18.0	15856.8	15871.8	15385.8	16400.8	15414.8	15429.8	15448.7	15458.2	16472.7	15487.1	~	10.2	18.0
18.1	15501.5	15516.0	16530.4	16544.8	15559.2	15578.6	15588.0	15602.4	15616.8	15681.2	00	11.7	18.1
18.2		15659.9	15674.2	16688.5	15702.9	16717.3	15781.6	16745.8	15760.1	15774.4	6	18.1	18.2
18.8	16788.6	15802.9	15817.2	16831.4	15845.7	15859.9	16874.2	15888.4	15902.6	16916.8		***	18.8
18.4	16931.0	15945.2	15959.4	15978.6	15987.8	16001.9	16016.1	16030.2	16044.4	16058.5	- ; -	=	18.4

Berometer	Eng. Inch.	18.5	18.7	18.8	18.9 	19.0	19.1	19.3	19.3	19.4	19.5	9.6	19.7	19.8	19.9	0.02	20.1	87.02	20.3	7.02	20.5	20.6	20.7	8.02	6.02
	ğ	2 2	<u> </u>	~	~	~	=	=	<u> </u>	~	~	=	<u>=</u>	=	=	~	<u>~</u>	<u>~</u>	~	*			_	ă	× =
Thousandthe	luch.	, ž	1.4	2.7	7	6.4	.	8.1	9.5	10.9	12.2				1.3	2.6	6.8	2.	7.9	7.7	9.0	10.3	11.6		
			_	ed .	e9	*	10	9	7	60	6				_	61	••	4	10	9	-	80	6		
	8.	Eng. Foet. 16199.5 16339.6	16479.0	16617.8	16755.7	16892.8	17029.4	17165.2	17800.8	17484.6	17568.4	17701.4	17883.7	17965.4	18096.4	18226.8	18356.6	18485.7	18614.1	18741.9	18869.1	18995.7	19121.7	19247.0	19871.8
	80.	Eng. Feet. 16185.4 16325.7	16465.1	16603.9	16741.9	16879.2	17015.8	17151.6	17286.8	17421.2	17555.0	17688.1	17820.5	17952.2	18083.4	18213.8	18343.6	18472.8	18601.8	18729.1	18856.4	18983.1	19109.1	19284.5	19359.3
	.07	Eng. Foet. 16171.3 16311.7	16451.2	16590.0	16728.1	16865.5	17002.1	17138.1	17273.8	17407.8	17641.7	17671.8	17807.8	17939.1	18070.8	18200.8	18330.7	18459.9	18588.5	18716.4	18843.7	18970.5	19096.5	19222.0	19346.9
	90.	Eng. Fost. 16157.3 16297.7	16487.2	16576.2	16714.4	16851.8	16988.5	17124.5	17259.8	17894.4	17628.8	17661.5	17794.1	17926.0	18057.2	18187.8	18817.7	18447.0	18675.7	18708.6	18831.0	18957.8	19088.9	19209.5	19334.4
of an Inch.	.05	Eng. Feet. 16143.2 16283.7	16423.3	16562.8	16700.6	16888.1	16974.9	17110.9	17246.8	17380.9	17515.0	17648.2	17780.8	17912.8	18044.1	18174.8	18304.8	18434.1	18562.8	18690.9	18818.8	18946.2	19071.4	19196.9	19322.0
Hundredths of an Inch.	70°	Eng. Feet. 16129.1	16409.4	16548.5	16686.8	16824.8	16961.2	17097.4	17282.8	17867.5	17501.6	17635.0	17767.6	17899.6	18081.0	18161.7	18291.8	18421.2	18550.0	18678.1	18805.6	18932.5	19058.8	19184.4	19309.5
	80.	Eng. Feet. 16115.0	16895.4	16584.6	16673.0	16810.6	16947.5	17083.8	17219.8	17854.1	17488.2	17621.7	17754.4	17886.6	18017.9	18148.7	18278.8	18408.3	18537.1	18665.8	18792.9	18919.9	19046.2	19171.9	19297.1
	9.	Eng. Feet. 16100.9	16381.5	16520.7	16659.2	16796.9	16933.9	17070.2	17205.8	17340.6	17474.8	17608.8	17741.1	17873.8	18004.8	18135.6	18265.8	18395.4	18524.8	18652.5	18780.1	18907.2	19033.6	19159.3	19284.5
	.01	Eng. Feet. 16086.8	16367.5	16506.8	166-15-4	16788.2	16920.2	17056.6	17192.2	17327.2	17461.4	17595.0	17727.9	17860.1	17991.6	18122.6	18252.8	18382.5	18511.4	18639.7	18767.4	18894.5	19021.0	19146.8	19272.0
	8	Eng. Feet. 16072.6	16353.6	16492.9	16831.5	16769.4	16906.5	17048.0	17178.7	17313.7	17418.0	17581.7	17714.6	17846.9	17978.5	18109.5	18289.8	18369.5	18498.5	18626.9	18784.6	18881.8	19008.8	19184.2	19259.5
Barometer	in Rag. Inch.	18.5	18.7	18.8	18.9	19.0	19.1	19.2	19.8	19.4	19,61	19.6	19.7	19.8	19.9	20.0	20.1	20.3	20.8	20.4	20	20.6	20.7	80.8	20.9

Berometer					Hundredth	Hundredths of an Inch.					Thou		Berometer
In Inch.	8.	10.	.09	60.	.04	.05	96.	.07	80.	6	5 <i>A</i>	I do	Rog. Inch.
21.0	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Foot. 19446.4	Eng. Feet. 19458-8	Eng. Feet. 19471.2	Eng. Feet. 19483.6	Eng. Feet. 19496.0		ž	21.0
21.1	19508.4	19520.8	19533.1	19545.5	19557.9	19570.2	19582.6	19594.9	19607.8	19619.6	-	1.3	21.1
21.2	19632.0	19644.3	19656.6	19668.9	19681.2	19698.5	19705.8	19718.0	19730.8	19742.6	a	2.4	21.2
21.3	19754.9	19767.1	19779.4	19791.6	19803.9	19816.1	19828.4	19840.6	19852.8	19865.0	•	8.6	21.3
21.4	19877.8	19889.5	19901.7	19918.9	19926.0	19938.2	19950.4	19962.6	18974.7	19986.9	4	8.	21.4
21.5	19999.1	20011.3	20023.8	20035.5	20047.6	20069.7	20071.8	20063.9	20096.1	20108.2	10	0.9	21.5
21.6	20120.8	20132.8	20144.4	20156.5	20168.6	20180.7	20192.7	20204.8	20216.9	20228.9	9	7.2	21.6
21.7	20241.0	20253.0	20265.0	20277.0	20289.1	20301.1	20318.1	20825.1	20887.1	20349.1	7	8.4	21.7
21.8	20361.1	20378.0	20385.0	20897.0	20409.0	20420.9	20432.9	20444.8	20156.8	20468.7	90	9.7	21.8
21.9	20480.7	20192.6	20504.5	20616.4	20528.8	20540.2	20552.1	20664.0	20575.9	20587.8	6	10.9	21.9
99.0	90K90.7	20811.K	20628.4	90685.8	20847.1	20659.0	8.0670.8	20682.7	20694.5	20706.8			22.0
22.1	20718.2	20732.0	20741.8	20753.6	20765.4	20777.2	20739.0	20601.8	20812.6	20824.4			22.1
22.3	20836.2	20847.9	20859.7	20871.4	20883.2	20894.9	20906.7	20918.4	20930.1	20941.9			22.2
22.8	20953.6	20965.8	20977.0	20988.7	21000.4	21012.1	21028.8	21035.4	21047.1	21058-8	-	::	22.3
22.4	21070.5	21082.1	21093.8	21105.4	21117.1	21128.7	21140.4	21152.0	21163.6	21175.8	61	64	22.4
22.5	21186.9	21198.5	21210.1	21221.6	21283.2	21244.8	21256.4	21268.0	21279.5	21291.1	•	% 7.	22.5
22.6	21802.6	21814.2	21325.8	21837.8	21348.9	21860.4	21871.9	21888.5	21895.0	21406.5	4	4.6	22.6
22.7	21418.1	21429.6	21441.1	21452.5	21464.0	21475.5	21487.0	21498.5	21509.9	21521.4	20	6.7	22.7
22.8	21582.9	21544.8	21555.8	21567.2	21578.7	21590.1	21601.8	21613.0	21624.4	21685.8	8	6.8	22.8
22.9	21647.8	21658.7	21670.1	21681.4	21692.8	21704.2	21715.6	21727.0	21738.8	21749.7	7	8. 0.	22.9
28.0	21761.0	21772.4	21788.7	21795.1	21806.4	21817.7	21829.1	21840.4	21851.7	21868.0	80	9.1	28.0
23.1	21874.8	21885.6	21897.0	21908.8	21919.6	21930.8	21942.1	21953.4	21964.7	21976.0	6	10.2	28.1
23.2	21987.2	21998.5	22009.8	22021.0	22032.8	22013.6	22054.7	22066.0	22077.2	22088.4			28.2
28.8	22009.6	22110.8	22122.1	22183.8	22144.6	22155.6	22166.8	22178.0	22189.2	22200.4	_		23.8
23.4	22211.6	22222.7	22283.9	22245.0	22256.2	22267.8	22278.4	22289.6	22800.7	22311.8			28.4

Barometer					Hundredths of an Inch.	of an Inch.					Thou	andtha	Berometer
Ing. Inch.	8	10.	80.	8	9.	.05	96.	.07	80.	60.	8 4	lach.	Eng. Inch.
	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet. 2-2378.4	Eng Feet. 22889.5	Eng Feet.	Eng Feet 22411.7	Eng. Fost 22422.8			25.55
9 6	99789	92444 9	22166.0	22467.0	22478.1	22489.1	22500.2	22511.2	22522.8	22533.3			23.6
23.7	22544.3	22555.4	22566.4	22577.4	22588.4	22599.4	22610.4	22621.4	22682.4	22648.4	_	į	23.7
8	22654.8	22665.3	22676.3	22687.2	22698.2	22709.1	22720.1	22781.0	22742.0	22752.9	-	:	23.8
83.9	22763.8	22774.8	22785.7	22796.6	22807.5	22818.4	22829.4	22840.8	22861.3	22862.0	69	62	6:52
6	0.8486	99888.0	25894.7	22905.6	22916.5	22927.4	22938.2	22949.1	22960.0	22970.8	**	89	24.0
24.1	22981.7	22992.6	28003.8	23014.2	23025.0	28035.8	23046.6	23057.6	23068.8	28079.1	4	4.8	24.1
24.8	28089.9	23100.7	23111.4	23122.2	23133.0	23148.8	28154.5	23165.8	28176.1	23186.8	10	5.4	24.3
24.8	23197.6	28206.3	23219.1	28229.8	23240.5	23251.8	23262.0	23272.7	23283.4	28294.2	0	9.2	24.8
24.4	23304.9	23315.6	23326.3	23837.0	23347.6	23358.8	23369.0	28879.7	28890.8	28401.0	~	7.5	24.4
ž	2 11700	8 00700	0 60700	4 87786	98484.8	98464.9	2817K.R	98486.9	23496.8	23507.4	00	8	21.5
2. 2.	98618.1	22528.7	23539.8	23519.9	28560.5	28671.1	28581.7	23592.3	28602.9	28618.5	0	9.7	21.6
24.7	23624.1	23634.6	28645.3	23655.8	23666.8	23676.9	23687.5	23698.0	28708.6	28719.1			24.7
24.8	28729.7	28740.3	28750.7	28761.2	28771.7	28782.8	28792.8	28808.8	28818.3	23824.3			21.8
24.9	23834.8	23845.3	23855.7	23866.2	23876.7	23887.2	23897.7	23908.3	28918.6	23929.1	-	1.0	24.9
28.0	9.8090.K	98919.9	25960.4	8.026	23981.8	28991.7	24002.1	24012.5	24028.0	24033.4	61	 1.9	\$2.0
25.1	24018.8	24054.2	24064.6	24075.0	24065-4	24095.7	24106.1	24116.5	24126.9	24187.2	60	8.1	25.1
25.2	24147.6	24158-0	24169.8	24178.7	24189.0	24199.4	24209.7	24220.1	24280.4	24240.8	4	-	25.3
25.8	24251.1	24261.4	24271.8	24282.1	24292.4	24302.7	24318.0	24323.8	24383.6	24343.9	10	2	25.8
25.4	24854.2	24864.5	24374.7	24385.0	24895.8	24405.5	24415.8	24426.1	24186.8	24446.6	9	6.2	25.4
, X	24456.8	24467.0	24477.8	24187.5	24497.8	24508.0	24518.2	24528.4	24538.7	24548.9	~	7.2	25.5
26.6	24559.1	24569.3	24579.5	24589.7	24599.9	24610.0	24620.2	24680.4	2.16.40.6	24650.7	60	8.2	26.6
25.7	24660.9	24671.1	24681.2	24691.4	24701.6	24711.7	24721.8	24782.0	24742.1	24752.8	a	6	25.7
25.8	24762.4	24772.5	24782.6	24792.8	24802.9	24818.0	24823.1	24838.2	24843.8	24858.4			25.8
25.9	24863.5	24878.6	24883.7	24893.7	24908.8	24918.9	24924.0	21934.0	24944.1	24954.1		_	26.9

Barometer					Hundredth	Hundredths of an Inch.					Thom	andthe	Barometer
in Eng. Inch.	8.	10.	80.	e .	9.	.	9.	.0.	80.	8.	5.A 	94 14	in Eng. Inch.
26.0	Eng. Feet. 24964.2	Eng. Feet. 2-197-1.2	Eng. Feet. 24984.3	Eng. Feet. 24994.3	Eng. Feet. 25004.4	Eng. Feet. 25014.4	Eng. Feet. 25024.4	Eng. Feet. 25031.4	Eng. Feet. 25044.5	Eng. Feet. 25054.5		Ng t	26.0
26.1	25064.5	25074.5	25084.5	25094.5	25104.5	25114.5	25124.6	25134.6	25144.4	25154.4			26.1
26.2	25164.4	25174.4	25184.8	25194.3	25204.2	25214.2	25224.1	25234.1	25244.0	26254.0	-	1.0	26.2
26.8	25263.9	25273.8	25283.8	25293.7	25308.6	25313.5	25323.4	25383.8	25848.2	25353.1	61	2.0	26.3
26.4	25363.0	25872.9	25882-8	25392.7	25402.6	26412.4	25422.8	25432.3	25442.1	25451.9	•	6.	2 6. 4
26.5	25461.8	25471.7	25481.5	25491.4	25501.2	25511.0	25520.9	25580.7	25540.5	25550.4	•	6.8	26.5
26.6	25560.2	25570.0	26579.8	25389.7	25599.5	25609.8	25619.1	25628.9	25638.7	25648.5	10	6.7	26.6
26.7	25658.8	25668.1	25677.8	25687.6	25697.4	25707.1	25716.9	25726.7	25786.4	25746.3	9	6.9	28.7
26.8	25755.9	26765.6	25775.4	25785.1	25794.8	25804.6	25814.3	25824.0	25583.8	25843.5	7	6.9	26.8
26.9	25853.2	25862.9	25872.6	25882.3	25892.0	25901.7	25911.4	25921.1	25980.8	25940.5	80	7.8	56.9
3	PKOKO 9	PKOKO O	9.50.60 8	9.5070.9	9,096	9 2002 6	6 9000	94017 0	96097 K	96087.9	٠	œ	2
3 :	20000	96056 R	98088 1	2.07.02.0	PROPE O	9600K	96104.6	961149	96196	7 80170		3	: 5
27.5	26148.0	26152.6	26162.9	96171.8	26181.4	26191.0	28200.6	26210.2	26219.R	26229			5.00
87.28	26238.9	26248.5	26258.0	26267.6	26277.2	26286.7	26296.8	26305.8	26315.3	26324.9			84 85
27.4	26334.4	26344.0	26853.5	26363.0	26372.5	26382.1	26391.6	26401.1	26410.6	26420.1	-	6.0	27.4
27.5	26429.6	26439.1	26148.6	26458.1	26467.6	28477.1	26486.5	26496.0	26505.5	26514.9	69	1.9	27.5
27.6	26524.4	26533.9	26548.8	26552.8	26562.8	26571.7	26581.3	26590.6	26600.0	26609.5	**	89	27.6
27.7	26618.9	26628.4	26637.8	26647.2	26656.7	26666.1	26675.5	26684.9	26694.3	26708.7	4	7.00	27.72
27.8	26713.1	26722.5	26781.9	26741.8	26750.7	26760.1	26769.6	26778.8	26788.3	26797.6	9	4.7	87.8
27.9	26806.9	26916.3	26825.6	26835.0	268-14.8	26853.7	26863.0	26872.3	26881.7	26391.0	9	. 9.9	27.9
28.0	26900.4	26909.7	26919.0	26928.4	26937.7	26947.0	26956.8	26965.6	26975.0	26984.3	7	6.5	29.0
28.1	26998.6	27002.9	27012.2	27021.6	27080.7	27040.0	27049.8	27068.6	27067.8	27077.1	80	7.5	28.1
28.3	27086.4	27095.6	27104.9	27114.2	27123.4	27132.7	27141.9	27151.2	27160.4	27169.8	6	÷:0	28.3
28.3	27178.9	27188.1	27197.8	27206.5	27215.7	27226.0	27284.2	27248.4	27252.6	27261.8			28.3
28.4	27271.0	27280.2	27289.4	27298.6	27807.8	27817.0	27826.2	27885.8	27814.6	27858.7	_[=	28.4

Barometer					Hundredths of an Inch.	of an Inch.					<u>£</u>	Thousandthe	Barumeter
Ing. Inch.	90.	.01	80°	89	ş	.06	9	.00	.08	\$) A	वृ	Ā
88.5	Eng. Feet. 27862.9	Eng. Feet. 27872.0	Eng. Feet.	Eng. Feet. 27390.4	Eng. Feet. 27399.5	Eng. Feet. 27408.7	Eng. Fost. 27417.8	Eng. Feet. 27427.0	Eng. Feet. 27486.1	Eng. Feet. 27.145.2			28.5
88.6	27454.4	27463.5	27472.6	27481.8	27490.9	27500.0	27509.1	27518.2	27527.4	27586.5		T Set	28.6
28.7	27545.6	27554.7	27563.8	27572.9	27582.0	27591.1	27600.2	27609.3	27618.8	27627.4	-	6.0	28.7
28.8	27636.5	27645.5	27651.6	27663.7	27672.7	27681.8	27690.8	27699.9	27708.9	27717.9	æ	1.8	28.8
28.9	27727.0	27786.0	27746.1	27764.1	27768.1	27772.3	27781.2	27790.2	27199.3	27808.8	8	2.7	88.9
29.0	27817.3	27826.2	27885.2	27844.2	27853.2	27862.2	27871.2	27880.2	27889.1	27898.1	7	99	29.0
29.1	27907.1	27916.1	27925.0	27984.0	27948.0	27951.9	27960.9	27969.8	27978.8	27987.7	9	4.6	29.1
29.3	27996.7	28005.6	28014.6	28023.5	28032.4	28041.4	28050.3	28059.2	28068.3	28077.1	9	4.9	29.3
29.8	28086.0	28094.9	28103.8	28112.8	28121.7	28130.6	28139.6	28148.4	28157.3	28166.2	7	6.3	29.3
29.4	28175.1	28184.0	28192.9	28201.7	28210.6	28219.5	28228.4	28287.2	28246.1	28254.9	80	7.5	29.4
29.K	9,99,68	98979.6	28281.6	28290.3	28299.2	28308.0	28316.9	28825.7	28334.5	28343.4	6	8.1	29.6
29.6	28352.2	28361.0	28369.8	28878.7	28887.5	28396.3	28405.1	28413.9	28422.7	28481.5	_		29.6
29.7	28440.8	28449.1	28457.9	28466.7	28475.4	28484.2	28493.0	28501.8	28510.6	28519.3			29.7
29.8	28528.1	28586.9	28545.6	28554.4	28563.2	28571.9	28580.7	28589.4	28598.2	28606.9			29.8
29.9	28615.7	28624.4	28683.2	28641.9	28650.6	28659.3	28668.1	28676.8	28685.5	28694.3	_	8.6	29.9
80.0	28702.9	28711.6	28720.3	28729.0	28787.7	28746.4	28755.1	28763.8	28772.5	28781.1	63	1.7	\$0.0
80.1	28789.8	28798.5	28807.2	28815.9	28824.5	28883.2	28841.9	28850.6	28859.2	28867.9	80	8.8	80.1
80.3	28876.5	28885.3	28893.8	28902.5	28911.1	28919.8	28928.4	28987.0	28945.7	28954.3	•	8.4	80.2
80.8	28962.9	28971.5	28980.1	28988.8	28997.4	29006.0	29014.6	29023.2	29031.7	29040.8	10	4. 8	80.8
80.4	29048.9	29057.5	29066.1	29074.7	29083.8	29091.8	29100.4	29109.0	29117.6	29126.3	9	6	80.4
S	90184.7	90148.8	29151.9	29160.4	29169.0	29177.6	29186.1	29194.7	29203.3	29211.8	7	6.0	80.5
80.6	29220.8	29228.9	29237.4	29245.9	29254.4	29262.9	29271.5	29280.0	29288.5	29297.0	80	6.9	80.8
30.7	29305.5	29314.0	29822.6	29331.1	29339.6	29348.1	29856.6	29865.1	29373.5	29382.0	6	7.7	20.7
80.8	29390.5	29399.0	29407.5	29416.0	29121.4	29432.9	29441.4	29449-8	29458.8	29466.8			80.8
30.9	29476.2	29483.7	29492.1	29500.6	29509.0	29517.6	29525.9	29584.8	29542.8	29651.2	_		80.9

II. CORRECTION FOR 1-4', OR DIFFERENCE OF THE TEMPERATURE OF THE BAROMETERS AT THE TWO STATIONS.

This Correction is segative when the attached Thermometer at the Upper Station is lowest; positive, when the attached Thermometer at the Upper Station is highest.

		_					_		_				_	_			_			_	
Correction in The F.	218.2	214.8	215.5	216.7	217.9	219.0	220.3	221.4	222.6	223.7	224.9	226.1	227.2	228.4	229.6	9	230.7	281.9	288.1	234.8	235.4
Palita Palita	91.0	91.6	92.0	92.5	88.0	98.5	94.0	94.6	96.0	96.6	0.96	96.5	97.0	97.6	98.0		99	99.0	99.6	100.0	100.6
Correction in Eng.	189.7	190.9	192.1	193.3	194.4	195.6	196.8	197.9	199.1	200.8	201.6	202.6	208.8	206.0	206.1		207.3	208.2	209.7	210.8	212.0
7 — 7 Fahren besk.	81.0	81.5	82.0	82.5	83.0	88.5	84.0	84.5	86.0	86.5	86.0	86.5	87.0	87.5	88.0		88.5	89.0	89.5	90.0	90.8
Correction in Eng.	166.8	167.5	168.7	169.8	171.0	172.2	178.4	174.5	175.7	176.9	178.0	179.2	180.4	181.6	182.7		188.9	186.1	186.2	187.4	188.6
Patron Patron Daft.	1.0	71.5	72.0	72.5	73.0	73.5	74.0	74.6	75.0	75.5	76.0	78.5	77.0	77.5	78.0		78.5	79.0	79.6	80.0	80.5
Correction in Eng.	142.9	144.1	145.2	146.4	147.6	148.8	149.9	161.1	152.8	158.4	154.6	155.8	157.0	168.1	159.3	4	160.6	161.6	162.8	164.0	165.2
r — r Fahren- bedt.	61.0	61.5	62.0	62.5	63.0	63.5	64.0	64.5	66.0	65.5	0.99	96.5	67.0	67.8	68.0		2.5	0.69	69.5	20.0	70.6
Correction in Eng.	119.5	120.6	121.8	128.0	124.2	125.8	126.5	127.7	128.8	130.0	181.2	132.4	133.5	184.7	185.9	4	187.0	138.2	139.4	140.6	141.7
7 — 4 Fabrera Bodt.	°13	51.5	62.0	62.5	63.0	58.5	54.0	64.5	92.0	56.5	56.0	56.5	67.0	57.5	58.0		20. 20. 20.	29.0	59.5	60.0	60.5
Correction in Eng.	96.0	97.2	98.4	9.66	100.7	101.9	108.1	104.2	106.4	106.6	107.8	108.9	110.1	111.8	112.4		113.6	114.8	116.0	117.1	118.8
r — r' Pabren beit.	41.0	41.5	43.0	42.5	43.0	43.5	44.0	44.5	46.0	45.5	46.0	46.5	47.0	47.5	48.0		6.5	49.0	49.5	0.09	20.0
Correction in Rog.	72.6	78.8	75.0	76.1	77.3	78.5	79.6	80.8	82.0	88.2	8. 8.	85.6	86.7	87.8	89.0		20.00	91.4	92.2	98.7	94.9
Pabran Pabran Baft	8 1.0	31.5	82.0	82.6	83.0	88.5	34.6	34.5	86.0	85.5	86.0	86.5	87.0	37.5	38.0		9.9	89.0	89.5	40.0	40.5
Correction in Eng.	49.2	50.4	51.5	52.7	6.83	66.1	56.2	57.4	58.6	28.7	6.09	62.1	63.2	4.7	65.6		99	67.9	69.1	70.3	71.4
7 Tabrena- Pabrena- bosit.	21.0	21.5	22.0	22.5	23.0	28.5	24.0	24.5	25.0	25.5	26.0	26.5	27.0	27.5	28.0		28.5	29.0	29.5	80.0	80.5
Correction in Eng.	25.8	26.9	28.1	89.8	80.5	81.6	87.8	84.0	85.1	36.3	87.5	88.7	8.68	41.0	42.2		48. 8	44.5	46.7	46.9	48.0
7 — 7 Fabren- Bedt.	11.0	11.5	12.0	12.5	18.0	18.6	14.0	14.6	15.0	16.5	16.0	16.5	17.0	17.6	18.0		18.5	19.0	19.6	20.0	20.6
Correction in Eng.	2.8	3.5	4.7	6.9	7.0	8.5	9.4	10.5	11.7	12.9	14.1	15.2	16.4	17.6	18.7		19.9	21.1	22.8	28.4	24.6
r r' Pahren- bedt	0.1	1.5	2.0	2.5	3.0	8.5	4.0	4.5	5.0	6.5	6.0	6.5	7.0	7.6	8.0		20 20	0.6	9.2	10.0	10.6

CORRECTION FOR THE DIFFERENCE OF GRAVITY IN VARIOUS LATITUDES.

Ξ

Jorrection positive from Latitude 00 to 450.

Negative from 450 to 900

8000 8 800 14000 2000 17000 18000 9006 9000 22000 23000 24000 000 8 9 800 2000 2000 12000 18000 21000 900 Š 0 8: 1.4 2.1 8.5 5.2 7.7 4.1 6.2 0.5 6.9 10.4 8. 2.7 3.6 7 4.5 5.0 6.8 8.8 7.7 8.1 9.6 6.6 0.8 15.7 11.8 18.2 880 8.8 12.0 18.8 14.5 6: 10.1 10.7 12.6 16.1 18.5 14.5 15.3 16.9 17.7 19.3 4. 18.7 20.1 8.0 9.6 10.4 11.2 12.9 16.1 12.1 15.6 16.6 17.5 21.4 22.4 23.4 18.6 20.2 21.3 8.8 13.6 7.8 10.7 12.7 14.6 19.5 14.8 19.4 20.5 28.9 25.1 27.4 12.5 18.7 16.0 18.2 21.7 29.9 26.2 28.5 : 4.6 **6** 8.0 10.3 11.4 17.1 22.8 9.1 28.6 23.4 24.7 11.7 13.0 14.3 15.6 18.2 19.6 20.8 22.1 26.0 27.8 81.2 32.5 98 7.8 16.9 10.4 16.0 33.4 84.9 10.2 11.6 13.1 14.5 18.9 20.4 21.8 23.8 24.7 26.2 27.6 30.5 32.0 36.3 29.1 19.2 12.8 14.4 16.0 17.6 80.8 22.4 27.5 28.8 80.4 88.6 85.2 8.98 24.0 25.6 82.0 38.4 10.0 96 8.4 13.9 29.6 31.3 33.1 40.0 Letttade. 12.2 15.7 17.4 19.1 20.9 22.6 24.4 27.8 36.5 88.8 41.8 26.1 31.8 43.5 ÷ 700 6.2 7.0 8.7 20.6 16.8 18.7 24.8 28.1 81.8 33.7 36.5 41.1 43.0 15.0 29.9 89.3 44.9 46.8 18.1 13.9 16.9 17.9 23.9 25.9 11.9 19.9 21.9 27.9 33.9 82.8 87.8 41.8 43.8 45.8 47.8 29.9 81.9 39.8 8.0 10.0 တ 6 12.6 14.7 16.8 18.9 21.0 23.1 25.2 27.8 29.4 31.6 82.8 87.9 40.0 44.2 48.4 10.5 33.7 42.1 46.3 50.5 52.6 15.4 17.6 22.0 24.3 26.5 28.7 30.9 87.5 19.8 39.7 41.9 48.5 20.2 65.3 11.0 33.1 85.3 46.3 91 44.1 55.1 13.8 27.6 39.0 43.6 18.4 20.7 28.0 25.3 29.8 36.7 41.3 48.2 50.5 52.8 16.1 82.1 46.9 55.1 57.4 80.9 28.5 83.8 14.8 16.6 19.0 21.4 23.8 26.1 35.6 88.0 40.4 42.8 47.5 49.9 52.3 54.6 57.0 59.4 280 45.1 19.5 22.0 34.2 2.99 29.3 81.8 86.6 58.6 14.7 17.1 24.4 26.9 39.1 41.5 44.0 48.4 48.9 51.3 53.7 0.99 16.0 17.5 20.0 22.6 30.0 32.5 35.0 42.5 45.0 52.5 57.5 0.09 12.5 25.0 27.5 87.5 60.0 47.5 62.5 0.0 50.0 5.0 17.8 20.3 22.9 28.0 30.5 33.1 35.6 43.2 56.9 58.6 15.3 25.4 53.4 61.0 63.6 10.2 12.7 88.1 40.7 45.8 48.3 6.09 18.0 80.9 9.99 59.2 12.9 16.4 20.6 28.2 88.5 86.0 43.8 48.9 61.8 64.4 50.3 25.7 28.8 46.3 61.6 54.1 23.8 25.9 28.2 81.1 83.7 86.3 13.0 15.6 18.2 20.7 88.9 41.5 44.1 48.7 61.9 54.5 57.1 59.7 62.2 8.19 10.4 49.8 20.8 26.0 9.88 81.2 33.8 36.4 44.2 46.8 62.4 23.4 89.0 54.6 67.3 8.69 65.0 15.6 18.3 41.6 49.4 52.0 18.0 2000 900 800 0000 11000 12000 0008 14000 22000 25000 8 8 18000 21000 23000 24000 15000 16000 17000 00061 20000

VI V	Correction For	CTION		CORRECTION FOR LOWER STATIC	RRECTION FOR THE LOWER STATION	OR THE TION	E HEIG	Неисит ог Розітіге.	THE	VI. HB	HEIGHT OF A COLUMN OF OF AN INCH	OF A C	COLUMN OF OF AN INCH	OF A		R, CORRESPONDIN THE BAROMETER	NDING	70 0	TO ONE TENTE	NTH
Approxi- mate Dif-	Decrease of Gravity on a Vertical.	same of ty on a tical.	Ä	Height of the Barometer, in English Inches, at Lower Station.	he Barou Low	neter, in er Statio	English] n.	frobes, a		Barometer Reading			Tem	ersture (Temperature of the Air, Fahrenheit, being	r, Fahrei	abeit, be	9 4		
ference of Level.	•.	+200	16	18	96	8	24	98	88	in English Inches.	400	450	20 °	5 5°	09	99	30 °	75°	•	88.
Eng. Feet	1 8 6 4	Feet	Feet	W Set	Feet.	je je	Feet.	Feet	Feet.		ig ig	7 Set	, je	186	T S	ig ig	Pet	1	Ze L	Feet.
1000	2.5	8.9	1.6	1.3	1.0	8.0	9.0	0.4	0.2	18.5	144.6	146.1	147.7	149.3	150.9	152.5	154.0	156.7	157.2	158.8
2000	5.2	9.9	3.1	2.6	5.0	1.5	1.1	0.7	8.0	19.0	140.8	142.8	148.8	145.4	146.9	148.4	150.0	161.6	158.1	154.6
3000	7.9	9.3	4.7	8	3.0	2.3	1.7	1:1	0.5	19.5	137.1	138.6	140.1	141.6	143.1	144.6	146.1	147.6	149.1	150.6
4000	10.8	12.2	. 6.8	6.1	4.0	8.1	63	1.4	0.7	20.0	183.7	185.2	136.6	138.1	139.6	141.0	142.5	148.9	145.4	146.9
2000	13.7	15.2	7.8	6.4	2.0	8.8	8:8	1.8	9.0	20.2	130.5	131.9	133.8	134.7	136.1	137.6	139.0	140.4	141.8	148.3
0009	16.7	18.3	9.4	7.6	6.0	4.6	e:	2.1	1.0	21.0	127.8	128.7	130.1	181.5	132.9	134.3	135.7	187.0	188.4	139.8
7000	19.9	21.5	11.0	8.9	7:1	9.4	8.9	2.2	1.2	21.5	124.8	125.7	127.0	128.4	129.7	181.1	182.4	188.8	185.1	136.5
0008	23.1	24.7	12.5	10.2	8.1	6.2	4.4	89	8:	22.0	121.5	122.9	124.2	125.5	126.8	128.2	129.6	180.8	182.2	133.5
0006	26.4	28.1	14.1	11.4	9.1	6.9	2.0	89 64	1.5	22.5	118.8	120.1	121.4	122.7	124.0	125.8	126.6	127.9	129.2	130.5
10000	29.8	81.6	15.7	12.7	10.1	7.7	2.2		1.7	23.0	116.2	117.5	118.8	120.0	121.3	122.6	128.8	126.1	126.4	127.7
11000	.83.3	85.1	17.2	14.0	11.1	8.5	6.1	6.8	1.8	23.5	118.7	115.0	116.2	117.5	118.7	120.0	121.2	122.5	128.7	124.9
12000	86.9	88.7	18.8	15.8	12.1	9.3	9.9	4.2	2.0	24.0	111.8	112.6	113.8	115.0	116.2	117.4	118.6	119.9	121.1	122.3
13000	40.6	42.5	20.4	16.5	13.1	10.0	4.5	4.6	23	24.6	109.1	110.8	111.6	112.6	113.8	116.0	116.2	117.3	118.6	119.8
14000	44.4	46.8	21.9	17.8	14:1	10.8	7.7	4.9	2.8	25.0	106.9	108.1	109.3	110.4		112.8	118.9	116.1	116.8	117.4
15000	48.3	50.3	28.5	19.1	12.1	11.5	8,	S	2.5	25.5	104.8	105.9	102.1	108.2	109.3	110.5	111.6	112.8	113.9	116.1
16000	52.8	84.8	25.1	20.3	16.1	12.8	8.8	9.9	2.7	26.0	102.1	103.9	105.0	106.1		108.4	109.8	110.6	111.7	112.8
17000	56.4	58.4	26.6	21.6	17.1	13.1	9.4	6.0	8.8	26.5	100.9	102.0	103.1	104.2	105.3	106.4	107.6	108.6	109.7	110.8
18000	60.5	62.6	28.2	22.9	18.1	18.8	6.6	6.3	8.0	27.0	99.0	100.1	101.2	102.8	103.3	104.4	105.5	106,6	107.6	108.7
19000	64.8	67.0	89.8	24.1	19.2	14.6	10.5	6.7	8.2	27.5	97.2	88.3	8.66	100.8	101.4	102.5	108.6	104.6	105.6	106.7
20000	69.3	71.4	81.8	25.4	20.5	15.4	11.0	7.0	8 9	28.0	95.4	96.2	97.5	98.8	9.66	100.1	101.7	102.8	103.8	104.8
21000	78.6	6.94	82.9	26.7	21.2	16.1	9.11	7.4	8.5	28.5	93.8	94.8	95.8	6.96	97.9	98.9	6.66	100.9	101.9	103.0
22000	78.2	80.5	84.5	28.0	22.2	16.9	13.1	7.7	8.7	29.0	92.1	93.1	94.1	95.1	86.8	97.8	98.3	8.66	100.2	101.2
23000	82.9	85.3	86.0	29.3	23.2	17.7	12.7	8.1	80	29.6	90.6	91.6	93.6	93.6	94.6	96.5	96.8	97.2	98.5	99.2
21000	87.6	90.0	87.6	80.5	24.3	18.5	18.2	7.6	0.7	80.0	89.1	0.06	91.0	92.0	92.9	98.9	64.9	86.9	8.96	87.8
25000	93.0	# F.	89.1	81.8	25.2	19.2	13.8	8:8	4.1	30.0	87.6	88.0	0.89	100	41.4	85.3	93.3	94.2	96.2	96.1

III.

TABLE

TOR

COMPUTING THE DIFFERENCE IN THE HEIGHTS OF TWO PLACES BY MEANS OF

By PROF. ELIAS LOOMIS.

This table was computed from the formula of Laplace, modified in accordance with the results of more recent determinations.

Suppose that we have observed

At the lower station.
$$\begin{cases} H, \text{ the height of the barometer,} \\ T, \text{ the temperature of the barometer,} \\ t, \text{ the temperature of the air,} \end{cases}$$
 At the upper station.
$$\begin{cases} h', \text{ the height of the barometer,} \\ T', \text{ the temperature of the barometer,} \end{cases}$$

Represent by s the height of the lower station above the level of the sea, by L the lantude of the place, and by h the observed height h' reduced to the temperature T.

The difference of level x between the two stations is given by the formula,

$$x = 60158. 6 \text{ ft.} \times \log_{\frac{1}{h}} \times \left\{ \begin{array}{l} \left(1 + \frac{t + t' - 64}{900}\right) \\ \left(1 + 0.00265 \cos_{\frac{1}{h}} 2 \text{ L}\right) \\ \left(1 + \frac{t + 63961}{20399629} + \frac{t}{10444315}\right) \end{array} \right\}$$

But h represents the height h' reduced from the temperature T' to the temperature T. The expansion of mercury for 1° Fahr. is 0.0001000; that of the brass which forms the scale of the barometer is 0.0000104; the difference is 0.0000896. Hence we have h = h' {1 + 0.0000896 (T - T')}.

Therefore,

60158. 6 ft. log.
$$\frac{H}{h} = 60158.6$$
 ft. log. $\frac{H}{h'} = 2.3409$ ft. $(T - T')$.

Part I. of the accompanying Table furnishes in English feet the value of the expression 60158.6 log. H for heights of the barometer from 11 to 31 inches; only they have all been diminished by the constant 27541.5 feet which does not change the difference

Part II. furnishes the correction — 2.3409 (T — T') depending upon the difference T — T' of the temperatures of the barometers at the two stations. This cor-

TABLE FOR COMPUTING THE DIFFERENCE IN THE HEIGHTS

rection is generally negative. It would be positive if T - T' were negative; that is, if the temperature T' of the barometer at the upper station exceeded the temperature T at the lower station.

Part III. gives the correction $A \times 0.00265$ cos. 2 L, to be applied to the approximate altitude A, and which arises from the variation of gravity from the latitude of 45 degrees, to the latitude L of the place of observation. This correction has the same sign as cos. 2 L; that is, it is positive from the equator to 45 degrees, and negative from 45 degrees to the pole.

Part V. furnishes for the approximate difference of level A the small correction $A \times \frac{s}{10444315}$ corresponding to several values of the height s of the lower station. But in place of s there has been substituted as the argument of the table, the height H of the barometer at this station.

Method of Computation.

Take from Part I. the two numbers corresponding to the observed barometric heights H and h'. From their difference subtract the correction 2.3409 (T — T') found in Part II. with the difference T — T' of the thermometers attached to the barometers. We thus obtain an approximate altitude a.

We then calculate the correction $a t+t'-64 \over 900$ for the temperature of the air, by multiplying the nine-hundredth part of a by the sum of the temperatures t and t' diminished by 64. This correction is of the same sign as t+t'-64. We thus obtain a second approximate altitude A.

With A and the latitude of the place L, we seek in Part III. the correction A \times 0.00265 cos. 2 L arising from the variation of gravity with the latitude.

For the approximate height A, Part IV. gives the correction $A \times \frac{A + 52251}{30000000}$ arising from the diminution of gravity on a vertical. This correction is always additive.

Finally, when the height s of the lower station is considerable, the small correction $A \times \frac{e}{1004215}$ may be found in Part V. This correction is always additive.

Example 1.

M. Humboldt made the following observations on the mountain of Guanaxuato, in Mexico, in Latitude 21°, viz.

Thermometer in open air,	Upper station. t' = 70°.3	Lower station near the sea. $t = 77^{\circ}.5$
Thermometer to barometer,		$T = 77^{\circ}.5$
Barometer,	h' = 23.66	H = 30.046

Required the difference in the height of the two stations.

OF TWO PLACES BY MEANS OF THE BAROMETER.

$T_{\text{max}} = 0.046$ inches	27649.7
Part L gives $\begin{cases} \text{for H} = 30.046 \text{ inches} \\ \text{for } h = 23.66 \text{ inches} \end{cases}$	21406.9
Difference	6242.8
Part II. gives for $T - T' = 7^{\circ}.2$,	—16.9
Approximate altitude a ,	6225.9
$\frac{a}{900}(t+t'-64)=6.918\times83.8,$	+579.7
Second approximate altitude A,	6805.6
Part III. gives for $A = 6806$, and $L = 21^{\circ}$,	+13.3
Part IV. gives for 6806,	+19.3
Height above the sea,	6838.2 feet.

Example 2.

M. Gay Lussac in his celebrated balloon ascent in 1805, found his barometer to adicate 12.945 English inches, the temperature being 14°.9 Fahrenheit. The barometer at Paris at the same time indicated 30.145 English inches with a temperature of 87°.44 Fahrenheit. Required the elevation of the balloon above Paris.

$_{\rm max}$. (for $\rm H=30.145$ inches,	27735.6
Part I. gives $\begin{cases} \text{for H} = 30.145 \text{ inches,} \\ \text{for } h' = 12.945 \text{ inches,} \end{cases}$	5650.4
Difference,	22065.2
Part II. gives for $T - T' = 72^{\circ}.54$,	169.9
Approximate altitude a,	21915.3
$\frac{a}{900}(t+t'-64)=24.35\times38.34,$	+933.6
Second approximate altitude A,	22848.9
Part III. gives for $A = 22848$, and $L = 48^{\circ}$ 50'	8.2
Part IV. gives for 22848,	+82.1
Height of balloon above Paris,	22922.8 feet.

PART L Argument, the observed Height of the Barometer at either Station. Inches Jost. DMT. DIE. Inches. Joot. Diff. Inches. Feet. Diff. Inches Feet. 11.0 1396.9 16.0 11186.8 21.0 18291.0 26.0 22871.0 286.4 100.3 162.8 124.1 11.1 1633.3 16.1 11849.1 21.1 18415.1 26.1 28971.3 128.6 99.9 284.8 161.8 11.2 1867.6 11510.9 26.216.2 21.2 18538.7 24071.2 232.8 122.9 99.5 160.8 11.8 2099.9 16.8 11671.7 21.8 18661.6 26.8 24170.7 230.2 159.8 122.4 99.1 11.4 2380.1 16.4 11881.5 21.4 18784.0 26.4 24269.8 228.2 158.8 121.8 98.8 11.5 2558.3 11990.8 18905.8 26.5 24368.6 16.5 21.5 226.2 121.3 98.4 157.9 11:6 2784.5 16.6 12148.2 21.6 19027.0 26.6 24467.0 224.2 156.9 120.7 98.1 11.7 3008.7 16.7 12805.1 21.7 19147.7 26.7 24565.1 97.6 222.4 120.1 155.9 24662.7 11.8 8281.1 16.8 12461.0 21.8 19267.8 26.8 220.5 119.6 97.3 155.1 19887.4 24760.0 11.9 3451.6 12616.1 26.9 16.9 21.9 97.0 119.0 218.6154.1 12.0 8670.2 17.0 12770.2 22.0 19506.4 27.0 24857.0 96.6 216.8 118.5 158.8 12.1 8887.0 12923.5 22.1 19624.9 27.1 24953.6 17.1 96.2 215.0 152.3 118.0 12.2 4102.0 18075-8 22.2 27.2 25049.8 17.2 19742.9 218.3 117.4 95.9 151.5 5815.8 12.3 17.8 18227.8 22.8 19860.3 27.825145.7 211.6 150.6 116.9 95.5 12.4 4526.9 25241.2 17.4 18377.9 22.4 19977.2 27.4 209.8 149.7 116.4 95.2 25336.4 12.5 4736.7 17.5 18527.6 22.5 20098.6 27.5 208.2 115.8 94.8 148.9 12.6 4944.9 17.6 13676.5 22.6 20209.4 27.6 25431.2 206.5 94.5 148.0 115.4 12.7 5151.4 17.7 18824.5 22.720324.8 27.7 25525.7 205.0 114.8 94.2 147.2 12.8 5856.4 17.8 13971.7 22.8 20489.6 27.8 25619.9 203.3 93.8 146.8 114.4 12.9 5559.7 17.9 14118.0 22.9 20554.0 27.9 25713.7 93.4 201.7 118.8 145.6 18.0 5761.4 14268.6 28.0 20667.8 28.0 25807.1 18.0 93.2 200.2 144.7 118.3 25900.3 13.1 5961.6 18.1 14408-3 28.1 20781.1 28.1 198.7 92.8 144.0 112.9 18.2 6160.3 18.2 14552-8 23.2 20894.0 28.2 25998.1 92.5 197.2 143.1 112.4 13.8 6857.5 18.8 14695-4 28.8 21006.4 28.3 26085.6 195.7 142.4 111.9 92.1 18.4 6553.2 14837.8 28.4 28.4 18.4 21118.3 26177.7 91.9 194.8 141.6 111.4 18.5 6747.5 18.5 14979.4 23.5 21229.7 28.5 26269.6 140.9 91.5 192.8 110.9 18.6 6940.3 18.6 15120.8 23.6 21340.6 28.6 26361.1 91.2 191.4 140.0 110.5 18.7 7181.7 15260-8 23.7 28.7 26452.3 18.7 21451.1 190.0 139.4 110.0 90.9 13.8 7821.7 18.8 15899.7 23.8 21561.1 28.8 26543.2 90.5 188.6 188.6 109.5 18.9 7510.3 15538.3 28.9 26633.7 18.9 28.9 21670.6 187.3 187.9 109.1 90.3 26724.0 14.0 7697.6 19.0 15676-2 24.0 21779.7 29.0 89.9 186.0187.1 108.7 14.1 7888.6 19.1 15813.8 24.1 21888.4 29.1 26818.9 184.6 136.5 108.2 89.6 29.2 26903.5 14.2 8068.2 21996.6 19.2 15949.8 24.2 183.8 135.7 107.7 89.3 19.8 26992.8 14.8 8231.5 16085-5 24.3 22104.8 29.8 182.1 185.0 107.3 89.1 14.4 8483.6 19.4 16220-5 24.4 22211.6 29.4 27081.9 88.7 180.8 106.8 134.3 14.5 8614.4 19.5 16854-8 24.5 22318.4 29.5 27170.6 88.4 179.6 183.7 106.4 27259.0 14.6 8794.0 19.6 16488-5 24.6 22424.8 29.6 106.0 88.1 178.8 182.9 14.7 8972.8 19.7 16621-4 24.7 22530.8 29.7 27347.1 87.8 105.6 177.2 132.3 27484.9 14.8 9149.5 19.8 16758-7 24.8 22636.4 29.8 176.0 131.6 105.1 87.6 9825.5 16885-8 22741.5 29.9 27522.5 14.9 19.9 24.9 87.2 174.8 181.0 104.8 15.0 9500.3 20.0 17016-8 25-0 22846.3 30.0 27609.7 178.5130.3 104.8 86.9 15.1 20.1 80.1 27696.6 9678.8 25.1 22950.6 17146-6 86.7 172.4 129.7 108.8 15.2 9846.2 20.2 17276-8 25.2 28054.4 80.2 27783.3 171.8 129.0 103.5 86.4 10017.5 30.3 27869.7 15.8 20.8 17405-8 25.3 28157.9 84.0 103.1 170.2 128.4 15.4 10187.7 20.4 17588-7 26.4 23261.0 30.4 27955.7 85.8 169.1 127.7 102.6 15.5 10356.8 20.5 17661-4 25.5 28363.6 30.5 28041.5 85.6 168.0 127.2 102.8 15.6 10524.8 20.6 17788-6 25.6 23465.9 20.6 28127.1 85.2 167.0 126.5 101.8 15.7 10691.8 80.7 29212.3 20.7 25.7 28567.7 17915-1 85.0 165.9 125.9 101.5 15.8 10857.7 30.8 28297.3 20.8 18041.0 25.8 23669.2 125.8 101.1 84.7 164.8 15.9 11022.5 20.9 25.9 80.9 28382.0 18166-3 28770.8 84.4 163.8 124.7 100.7 16.0 11186.3 21.0 18291-0 26.0 23871.0 31.0 28466.4

PART II.

Correction due to T—T, or the Difference of the Temperatures of the Barometers at the two Stations.

This Correction is Negative when the Temperature at the Upper Station is lovest, and vice versi.

				2108		~				77			-,			
T-T.	Corre		-T .	Correction.	7	-T.	Correc- tion.	T-	T .	Correc- tion.	T -	T .	orrec- tion.	T -	T.	tion.
Pab't.	Too	·]	hh't.	Foot.	71	h't.	Foot.	Fab	78.	Foot.	Fah'	Pa.	Foot.	Pab	1 ⁷ 8.	Foot.
			-		7-	•			-		1	- -		1	-	
ĭ	2.	a l	14	32.8		27	68.2	40	- 1	93.6	58	- 1	124.1	6	-	154.5
2	4.	•	15	85.1		28	65.5	41		96.0	54		126.4	6	,	156.8
8	7.		16	87.5		29	67.9	4		96.8	56		128.7	6		159.2
4	9.		17	39.8		10		1	-	100.7	56	- 1	181.1	1 6		161.5
		- 1			1 1	1	70.2	_	1					_		
5	11.	•	18	42.1		81	72.6	44	- 1	108.0	57		133.4	70	1	163.9
6	14.		19	44.5		82	74.9	4.5	- 1	105.8	58		135.8	7	· i	166.2
7	16.		20	46.8		38	77.8	4		107.7	59		188.1	77		168.6
8	18.	7	21	49.2		84	79.6	43	7	110.0	60)	140.4	73	3	170.9
9	21.	_	22	51.5		85	81.9	45	3	112.4	61		142.8	74	4	173.8
10	23.	4	28	53.8	1 3	B6	84.8	45	•	114.7	62	1	145.1	71	5	175.6
11	25.	8	24	56.2	1	87	86.6	50)	117.0	68	3	147.5	70	8	177.9
12	28.	1	25	58.5	; ;	88	89.0	5	.	119.4	64	ı I	149.8	7	7	180.3
13	30.	4	26	60.9		89	91.8	5	2	121.7	65		152.2	72	3	182.6
						-						<u></u>		-	_	
1	١			ГШ	-		PAF	T			PA	RT	V .			
ll	Corn	from :	due to the Le	the Cha Litude o	ingo of	Grav-	IV	•	_		-					
11				Place of			COLLEGE		Com	nection:		the Ho Station		the L	OWEE	1 1
li				00 . نعبا			Decre					ye Pos				
II.	^	egano		Lat. 45	0 10 10	,,	of Gra	vity			Alter	ye ros	HVOT.			
1	00	100	200	tude.	400		Vertic	mL	H	ight of	Barom	eter a	Lower	Static	m.	
App.	900	800	700	600	500	450	Ahoo Posit	ior.	16 in.	18 in.	90 in.	22 in.	24 in.	26 in.	26 in.	APP.
1-	_			-		Foot.	Jee.			Free	Took.	Feet.	Foot.		Foot.	
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11						0	11				2.0			0.7	0.2	
2000	5.8	5.0	4.1	2.6	0.9	-	5.		8.1	2.5		1.5	1.1			2000
3000	7.9	7.5	6.1	4.0	1.4	0	7.		4.7	8.8	8.0	2.8	1.7	1.1	0.5	8000
4000	10.6	10.0		5.8	1.8	0	10.		6.8	5.1	4.0	8.1	2.2	1.4	0.7	4000
5000	13.2	12.4		6.6	2.3	0	13.	_	7.8	6.4	5.0	3.8	2.8	1.8	0.8	5000
6000	15.9	14.9	12.2	7.9	2.8	0	16.	7	9.4	7.6	6.0	4.6	8.8	2.1	1.0	6000
7000	18.5	17.4	14.2	9.2	8.2	0	19.	9	11.0	8.9	7.1	5.4	8.9	2.5	1.2	7000
8000	21.2	19.9	16.2	10.6	3.7	0	28.	1	12.5	10.2	8.1	6.2	4.4	2.8	1.8	8000
9000	28.8	22.4	18.3	11.9	4.1	0	26.	4	14.1	11.4	9.1	6.9	5.0	8.2	1.5	9000
10000	26.5	24.9	20.3	13.2	4.6	0	29.	8	15.7	12.7	10.1	7.7	5.5	3.5	1.7	10000
11000	29.1	27.4	22.8	14.6	5.1	0	88.	8	17.2	14.0	11.1	8.5	6.1	8.9	1.8	11000
12000	31.8	29.9		15.9	5.5	0	36.		18.8	15.8	12.1	9.2	6.6	4.2	2.0	12000
13000	34.4	82.4	1	17.2	6.0	o	40.	_	20.4	16.5	18.1	10.0	7.2	4.6	2.2	18000
14000	37.1	34.9	28.4	18.5	6.4	0	44,	- 1	21.9	17.8	14.1	10.8	7.7	4.9	2.8	14000
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15000	39.7	87.8	1	19.9	6.9	0	48.		23.5	19.1	15.1	11.5	8.3	5.8	2.5	15000
16000	42.4	39.8		21.2	7.4	0	52.	- 1	25.1	20.3	16.1	12.8	8.8	5.6	2.7	16000
17000	45.0	42.3			7.8	0	56.		26.6		17.1	18.1	9.4	6.0	2.8	17000
18000	47.7	44.8	1	28.8	8.3	0	60.	5	28.2	22.9	18.1	13.8	9.9	6.8	8.0	18000
18000	50.8	47.8	38.6	25.2	8.7	0	64.	8	29.8	24.1	19.2	14.6	10.5	6.7	8.2	19000
20000	53.0	49.8	40.6	26.5	9.2	0	69.	2	31.3	25.4	20.2	15.4	11.0	7.0	8.8	20000
21000	55.6	52.8	42.6	27.8	9.7	0	78.	6	82.9	26.7	21.2	16.1	11.6	7.4	3.5	21000
22000	58.3	54.8	44.7	29.1	10.1	0	78.	2	34.5	28.0	22.2	16.9	12.1	7.7	8.7	22000
23000	60.9	57.3	1	30.5	10.6	0	82.	- 4	36.0		28.2	17.7	12.7	8.1	3.8	23000
24000	63.6	59.8		1	11.0	0	87.	- 1	37.6		24.2	18.5	18.2	8.4	4.0	24000
25000						0	92.	- 1	39.1					l l		
II ZIMINI)	. 00.X	62.2	50.7	33.1	11.5	· U	B 372 .		35.1	31.8	25.2	19.2	13.8	8.8	4.1	25000

IV.

TABLES

FOR REDUCING BAROMETRICAL OBSERVATIONS TO THE LEVEL OF THE SEA, OR TO ANY OTHER LEVEL, AND FOR COMPUTING DIFFERENCES OF ELEVATION MEASURED BY THE BAROMETER, BY M. C. DIPPE.

The following tables, published by M. C. Dippe, in the Astronomische Nachrichten, No. 1056, November, 1856, are a modification and extension of Gauss's tables, published in Schumacher's Jahrbuch, for 1836 and the following years; which are based on the formula of Laplace. In this new form they answer a double purpose. They give the means of solving a problem which often occurs in Meteorology, viz.: The difference of elevation between two stations, and the temperature of the air at both, being known, to reduce the height of the barometer at one of the stations to the height it would have at the other. They are likewise adapted to the computation of heights from barometrical observations.

The formula of Laplace, which has been used, the Metres being reduced to Toises,

and the Centigrade degrees to degrees of Reaumur, reads as follows:

$$h = 9407.73 \left(1 + \frac{t + t'}{400}\right) \left(1 + a \cos 2 \phi\right) \left(1 + \frac{h}{r}\right) \left\{\log \frac{b}{b'} + 2 \log \left(1 + \frac{h}{r}\right)\right\}.$$

Where t and t' = the temperatures of the air, in degrees of Reaumur, at the lower and upper station,

b and b' = the height of the barometer, in any scale, reduced to the freezing point, at the lower and upper station,

h = the difference of level, in toises, between the two stations,

r = the distance, in toises, of the lower station to the centre of the Earth,

 ϕ = the latitude of the place of observation,

a = the increase of gravity from the equator to the poles.

Making, besides, m = the modulus of the common logarithms, the formula becomes, with sufficient accuracy,

$$\log b - \log b' = h \left\{ \frac{1}{9407.73} \cdot \frac{1}{1 + \frac{t+d}{400}} - \frac{2m}{r} \right\} \cdot \frac{1}{1 + a \cos 2\phi} \cdot \frac{1}{1 + \frac{h}{r}}.$$

Assuming r, or the radius of the Earth, at 45° latitude = 3266631 toises, and $\alpha = 0.002595$, instead of 0.002845 adopted in Gauss's tables, and making

$$u = \log b - \log b',$$

$$a = \log \left(\frac{1}{9407.78} \cdot \frac{1}{1 + \frac{t+\theta}{400}} - \frac{2m}{r} \right),$$

$$c = -m a \cos 2\phi,$$

$$c' = -\frac{mh}{r},$$

then the reduction of the height of the barometer to another level is given by the formula,

1.
$$\log u = \log h + a + c + c';$$

2. $\log b = \log b' + u.$

Table I. contains the values of a for the argument t+t'; 10 units are to be subtracted from the characteristic.

Table II. gives the values of c for the argument ϕ , or the correction for the change of gravity in latitude, which is negative from 0° to 45°, positive from 45° to 90°.

Table III. furnishes the values of c' for the argument h in toises, or the correction for the decrease of gravity on the vertical. Both in Tables II. and III. the values of c and c' are given in units of the fifth decimal place.

The difference of elevation of the two stations is given by the formula,

1.
$$u = \log b - \log b'$$
,
2. $\log h = \log u + \Lambda + c + c'$,

in which A is the arithmetical complement of a, and the corrections c and c' receive contrary signs. For the sake of convenience, the values of A have been placed in Table I., and in Table III. the correction for A is found in another column, with the more convenient argument $v = \log u + A$.

If the heights of the barometers have not been reduced to the freezing point, then, B and B' being the unreduced heights of the barometers, and T and T' the temperature of the attached thermometer in degrees of Reaumur,

$$b:b'=\frac{B}{1+\frac{T}{440}}:\frac{B'}{1+\frac{T}{440}},$$

and making $\frac{m}{4440} = \beta$,

$$\mathbf{z} = \log b - \log b' = (\log \mathbf{B} - \beta \mathbf{T}) - (\log \mathbf{B}' - \beta \mathbf{T}').$$

Instead of $\beta = 0.000098$, we can write with sufficient accuracy 0.00010.

USE OF THE TABLES.

These tables can be used in any latitude, and for any barometrical scale; but the indications of the barometers must be reduced to the freezing point; and the temperatures of the air must be given in degrees of Reaumur. The tables suppose the use of logarithms with 5 decimals, such as those of Lalande, and give the results in toises.

I. For Reducing Barometrical Observations to another Level.

Given h in toises, t, t', ϕ , and b or b'. To find b or b'.

In Table I. with the argument t + t', take a,

In Table II. with the argument ϕ , take c,

In Table III. with the argument h, take c',

the last two corrections being given in units of the fifth decimal, making

$$\log h + a + c + c' - 10$$
 (whole units) = $\log u$.

Then we have

for a level lower by
$$h$$
 toises, $\log b = \log b' + u$; for a level higher by h toises, $\log b' = \log b - u$.

If h, or the difference of elevation, is given in metres, take c', which is always negative, from Table III. (for A) with the argument $v = \log h + 9.71$, and write

$$\log u = 9.71018 + \log h + a + c + c' - 10$$
 (whole units).

Then again is $\log b = \log b' + u$.

Example 1.

Suppose the height of the barometer, reduced to the freezing point, to be b'=295.39 Paris lines; the temperature of the air $t' = 11^{\circ}.8$ Reaumur, and the latitude $\phi = 51^{\circ} 48'$; the increase of heat downwards being 1° Reaumur for 100 toises. What is the height of the barometer, reduced to the freezing point, at a station lower by h = 498.2 toises?

In the case
$$t = t' + 4^{\circ}.98 = 16^{\circ}.78$$
, and $t + t' = 28^{\circ}.58$.

Then

Table I. for 28°.58 gives
$$a = 5.99538$$
Table II. for 51° 48′ gives $c = +0.00026$
Table III. for 498 toises gives $c' = -0.00007$

$$\log u = 8.69297 - 10$$

$$u = 0.04931$$

$$\log b = 2.47040$$

$$\log b = 2.51971$$
Barometer at the lower station $b = 330.90$ Paris lines.

Example 2.

Suppose the reduced barometer b' = 598.6 millimetres; the temperature of the air $t' = 18^{\circ}.0$ Centigrade = 14°.4 Reaumur; the difference of elevation h = 2217metres; $\phi = 3^{\circ}$. The temperature of the air at the lower station $t = 27^{\circ}.5$ Centigrade = 22°.0 Reaumur, and t + t' = 36°.4 Reaumur.

Then
$$\log \lambda = \begin{cases} \log 2217 = 3.34577 \\ + 9.71018 \\ \hline 3.05595 \end{cases}$$
 $v = 3.06$

$$a = 5.98750$$

$$c = -0.00112$$

$$c' = -0.00015$$

$$\log u = 9.04218 - 10$$

$$u = 0.11020$$

$$\log b' = 9.77714$$

$$\log b = 9.88734$$
Barometer at the lower station $b = 771.5$ millimetres.

For Computing Differences of Elevation from Barometrical Observations.

Given the unreduced height of the barometer at the lower and upper station, B and B'; the temperatures of the attached thermometers, T and T'; the temperatures of the air, t and t'; and the latitude, ϕ .

To find h, or the difference of elevation between the two stations.

Subtract (log B' — 10 T') from (log B — 10 T), paying due attention to the nature of the signs of T and T', and taking the numbers 10 T and 10 T' as units of the fifth decimal. Calling then $(\log B - 10 T) - (\log B' - 10 T') = u$, or if the heights of the Barometers are reduced to the freezing point, $\log b - \log b' = v$ take,

In Table I., A with the argument t + t', and make $v = \log u + A$. In Table II., with the argument ϕ , take c reversing the sign. D

In Table III., for A, with the argument v, take c', which, in this case, is always positive; then, remembering that the values of c and c' are given in units of the fifth decimal, we have,

$$v + c + c'$$
 = log h in toises,
 $v + c + c' + 0.28982 = \log h$ in metres,
 $v + c + c' + 0.80584 = \log h$ in English feet.

Example 1.

L. station B = 329.013 Paris lines; T = +15.88 R.;
$$t = +$$
 15.96 R.; $\phi = 45$ 32. U. station B' = 268.215 Paris lines; T' = + 8.40 R.; $t = +$ 7.92 R. $t + t' = 23.88$ R.
$$\log B = 2.51722 - 10 \times 15.88 = 2.51563$$
$$\log B' = 2.42848 - 10 \times 8.4 = 2.42764$$
$$u = 0.08799$$
$$\log u = 8.94443$$
$$A = 3.99982$$
$$v = 2.94425$$
$$c = -0.00002$$
$$c' = + 0.00012$$
$$\log h = 2.94435$$
$$h = 879.74 \text{ toises.}$$

Example 2.

L. station B = 763.15 millimetres; T =
$$t$$
 = 25.3 Cent. = 20.24 R.; ϕ = 21. U. station B' = 600.95 millimetres; T' = t' = 21.3 Cent. = 17.04 R. $t + t'$ = 37.28 R. $t + t'$ = 37.28 R. $t + t'$ = 37.28 R. $t + t'$ = 37.28 R. $t + t'$ = 0.10345 $t + t'$ = 0.10345 $t + t'$ = 0.10345 $t + t'$ = 0.10345 $t + t'$ = 0.10345 $t + t'$ = 0.10345 $t + t'$ = 0.00084 $t + t'$ = 0.00014 $t + t'$ = 0.00014 $t + t'$ = 0.00014 $t + t'$ = 0.00014 $t + t'$ = 0.009882 $t + t'$ = 0.28982 $t + t'$ = 0.28982 $t + t'$ = 0.30584 $t + t'$ = 0.30584 $t + t'$ = 0.30584 $t + t'$ = 0.30584 $t + t'$ = 0.69.3 toises = 2084.0 metres = 6837.9 English feet.

I. ARGUMENT: SUM OF THE TEMPERATURES OF THE AIR IN DEGREES OF REAUMUR.

t+t		6.09489		1+1		Correction for	
kesumur.	а	Difference.	A	Resumur.	a	Difference.	A
-60°	6.09617		3.90888	-20°	6.04776		3.95224
-59	6.09489		8.90511	-19	6.04661	115	8.95339
-58	6.09362		8.90688	-18	6.04547	114	3.95453
-57	6.09235	197	8.90765	-17	6.04484	118	3.95366
-56	6.09106	197 196	8.90892	-16	6.04220	114	3.95680
-55	6.08982	196	8.91018	-15	6.01207	112	8.95793
-54	6.08856	126	8.91144	-14	6.04094	113	8.95906
-53	6.08730	196	8.91270	-18	6.03981	112	8.96 019
-52	6.08605	125	3.91395	-12	6.03869	112	3.96131
-51	6.08480	194	8.91520	-11	6.03757	112	8.96243
-50	6.08856	126	8.91644	-10	6.03645	112	8.96355
-49	6.08281	128	3.91769	- 9	6.03532	. 111	3.96467
-48	6.08108	194	8.91892	- 8	6.03422	111	8.96578
-17	6.07984	198	3.92 016	-7	6.03311	110	3.966 99
-46	6.07861	128	8.92189	- 6	6.03201	111	8.96799
-45	6.07788		3.92262	- 5	6.03090		8.96910
-44	6.07616	199	3.92384	-4	6.02980	110	8.97020
-43	6.07494	199	8.92506	- 8	6.02871	109	3.97129
-42	6.07372	199	8.92628	- 2	6.02761	110	8.97239
-41	6.07250	199	8.92750	- 1	6.02652	109	8.97348
-40	6.07129	120	8.92871	0	6.02543	109	8.97457
-39	6.07009	121	3.92991	+1	6.02434	106	8.97566
-88	6.06588	120	8.93112	2	6.02326	109	8.97674
-37	6.06768	190	8.93282	8	6.02217	108	8.97783
-36	6.06648	119	3.98352	4	6.02109	107	8.97891
-35	6.06529	119	3.98471	5	6.02002	107	3.979 98
-84	6.06410	119	8.98590	6	6.01895	108	3.98105
-83	6.06291	118	8.98709	7	6.01787	107	8.96213
-32	6.06178	118	3.93827	8	6.01680	106	8 98320
-31	6.06055	116	8.93945	9	6.01574	106	8.98426
-80	6.05987	116	8.94068	10	6.01468	106	3.98532
-29	6.05819	116	3.94181	11	6.01362	106	3.9 9 63 9
-28	6.05702	117	3.94298	12	6.01256	106	3.98744
-27	6.05585	116	3.94415	18	6.01150	105	3.98 850
-26	6.05469	117	8.94581	14	6.01045	105	8.98955
-25	6.05852	,,,	3.94648	15	6.00940		8.99060
-24	6.05286	116	3.94764	16	6.00835	106	3.99165
-23	6.05121	115	8.94879	17	6.00781	104	8.99269
-22	6.05005	116	3.94995	18	6.00626	105	3.99374
-21	6.04890	116	8.95110	19	6.00522	104	8.99478
-20	6.04776	114	3.95224	+20	6.00418	104	2.99582

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TABLES

FOR REDUCING BAROMETRICAL OBSERVATIONS TO ANOTHER LEVEL, AND FOR COMPUTING DIFFERENCES OF ELEVATION MEASURED BY THE BAROMETER, BY M. C. DIPPE.

In No. 1088 of the Astronomische Nachrichten, published in June, 1857, Dr. DIFFE gives the following set of Tables for reducing barometrical observations to another level, and for computing heights. These tables, being based, as the preceding ones (IV.), on the formula of Laplace, and computed with the same constants, give results nearly identical, but dispense with the use of logarithms.

USE OF THE TABLES.

The tables suppose the height of the barometer to be expressed in French inches or Paris lines, and the temperature in degrees of Reaumur; they give the differences of level in French toises.

The signs used have the following signification: --

At Lower Station. $\begin{cases} B = \text{Observed Height of Barometer in Paris lines.} \\ T = \text{Attached Thermometer in degrees of Reaumur.} \\ b = \text{Barometer reduced to the freezing point.} \\ t = \text{Temperature of the air, detached Thermometer.}$

At Upper Station. $\begin{cases} B' = \text{Observed Height of Barometer.} \\ T' = \text{Attached Thermometer.} \\ b' = \text{Barometer at the freezing point.} \\ t' = \text{Temperature of the air.} \end{cases}$

 $\phi =$ Latitude of the place.

h = Difference of elevation between the two stations.

I. For Reducing Barometrical Observations to another Level.

Given, h in toises, t, t', ϕ , and b or b'. To find b or b.

Make first
$$2\tau = \frac{t+t}{2}$$
 and τ , and

In Table I., with the argument 2τ , take τ' ; In Table III., with the arguments h and \(\tau_1 \), take C; In Table IV., with the arguments A and ϕ , take C';

Make, further,

$$u = h + C + C'$$
 and $\frac{u}{100}$ r' ;

And if b' be given, and b required,

In Table II., with the argument b, take H;

thèn is

$$H = H' + (u - \frac{u}{100}\tau'),$$

and the height of the barometer, in Table II., due to H, is b required.

If b be given, and b' required for a level higher by h toises, then,

In Table II., with the argument b, take H'.

Make, further,

$$H' = H - (u - \frac{u}{100} r'),$$

and b' is the height of the barometer in Table II., corresponding to H'.

Beample 1.

Suppose the height of the barometer reduced to the freezing point to be b'=295.39 Paris lines; the temperature of the air $t'=11^{\circ}.8$ Reaumur; and the latitude $\phi = 51^{\circ}.48$; the increase of heat downwards being 1° Reaumur for 100 toises. What is the height of the barometer reduced to the freezing point, at a station lower by h = 498.2 to ses?

In this case,
$$t' = 11^{\circ}.8$$
; $t = 11^{\circ}.8 + 4^{\circ}.98$; $t + t' = 28^{\circ}.58$; $2\tau = \frac{t+t}{2} = 14^{\circ}.29$; $\tau = 7^{\circ}.15$;

and according to Table I.

cording to Table I.
$$r' = +6.67$$
.

With
$$h$$
 and τ , in Table III., we find $C = -1.4$
With h and ϕ , in Table IV., we find $C' = +0.3$
We add $h = 498.2$
and we have $u = 497.1$; $\frac{u}{100}$
 $\tau' = -33.15$

With
$$b'$$
, in Table II., we find $H' = \frac{367.86}{831.81}$

$$\begin{array}{c} \frac{w}{100} = & 4.971 \\ \tau' = + 6.67 \\ 29.88 \\ 2.96 \\ .24 \\ \hline \frac{w}{100} \tau' = + 88.15 \end{array}$$

Finally, with H, in Table II., we find b = 330.91 Paris lines, which is the required height of the barometer at the lower station. Gauss's tables (IV.) would give b =330.90 lines.

Example 2.

Suppose b'=330.46 Paris lines; $t'=-12^{\circ}.3$ Reaumur; h'=92.7 toises; $\phi = 62^{\circ}$.

In this case, assuming t = t',

$$2\tau = \frac{t+t'}{2} = -12^{\circ}.3; \ \tau = -6.15;$$

and according to Table I.

$$\tau' = -6.55$$
.

With h and τ , in Table III., take C = -0.2

With h and ϕ , in Table IV., take C' = + 0.1

Add
$$h = 92.7$$

We have $u = 92.6$
 $-\frac{u}{100} \tau' = +6.07$
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 0.0

924.89

With b', in Table II., take H' =H =

With H, in Table II., we find b = 338.53 Paris lines. Gauss's tables (IV.) would give b = 338.54 lines.

II. For Computing Differences of Elevation from Barometrical Observations.

Suppose to be given B, B', T, T', t, t', ϕ ; required h.

Make first
$$\tau = \frac{t+\ell}{4}$$
 and $T - T'$.

Then in Table II., with the argument B take H, B' take H',

and make

$$u = (H - H') + \frac{H - H'}{100} \tau - (T - T'),$$

in which each full degree of T - T' corresponds to a toise.

Further, in Table III., with u and r, take C reversing the sign;

in Table IV., with u and ϕ , take C' reversing the sign;

in Table V., with T - T' and τ , take C' with the signs of T - T.

Then the difference of elevation required is

$$h = u + C + C' + C''.$$

If the heights of the barometer, reduced to the freezing point, or b and b', are given,

then in Table II., with the argument, $\begin{cases} b \text{ take H} \\ b' \text{ take H}' \end{cases}$

and make

$$u = H - H' + \frac{H - H'}{100} \tau$$

Further, in Table III., take C reversing the sign; in Table IV., take C' reversing the sign;

and

$$h = u + C + C'.$$

Example 1.

B = 333.6 Paris lines; T = + 17°.0 Reaumur;
$$t = +$$
 19°.0 R.; $\phi = 48^\circ$. B' = 289.9 Paris lines; T' = + $\frac{16^\circ}{.3}$ Reaumur; $t' = + \frac{15^\circ}{.2}$ R. T - T' = $\frac{16^\circ}{.7}$ $t + t' = + \frac{34^\circ}{.2}$ $\tau = + 8.55$

In Table II. with B take H = 864.9
" with B' take H' = 291.2
H - H' = 573.7
$$\frac{H - H'}{100} = 5.787$$

 $\frac{H - H'}{100} = 49.06$ $\frac{H - H'}{100} = 5.787$
 $\frac{H - H'}{100} = 0.7$
 $\frac{H - H'}{100} = 0.7$
 $\frac{H - H'}{100} = 0.7$
 $\frac{H - H'}{100} = 0.7$

In Table III., with u and τ , take C = +1.8In Table IV., with u and ϕ , take C' = -0.2In Table V., with T - T' and τ take C'' = 0.0

Difference of elevation, or h = 623.66 toises. Gauss's Tables give 623.64 toises.

Example 2.

Suppose to be given,

$$b = 342.68$$
 Paris lines; $t = -10^{\circ}.38$ Reaumur; $\phi = 65^{\circ}.$

b' = 285.47 Paris lines; $t' = -14^{\circ}.94$ Reaumur; $T - T' = 0^{\circ}.$ R.

$$t + t' = -\frac{25^{\circ}.32}{6.33}$$

$$\begin{array}{c} H - H' = \overline{746.30} \\ \frac{H - H'}{100} \tau = -47.24 \end{array}$$

In Table III., with
$$u$$
 and τ , take $C = +1.8$
In Table IV., with u and ϕ , take $C' = -1.2$

$$h = 699.66$$

u = 699.06

Gauss's Tables give h = 699.72 toises.

TABLES

FOR REDUCING BAROMETRICAL OBSERVATIONS TO ANOTHER LEVEL, AND FOR COMPUTING DIFFERENCES OF ELEVATION, BY M. C. DIPPE.

TABLE I. - Argument, the observed Height of the Barometer at either Station.

	1				Tenths (of a Line.				
Barom- eter in Paris Lines.	0	1	9	8	4	5	6	7	8	9
B or B		<u> </u>	<u>!</u>	<u> </u>	■ or H' is	Tolses —		!	<u> </u>	<u> </u>
270	0.7	2.2	8.7	5.2	6.7	8.2	9.7	11.2	12.8	14.3
271	15.8	17.8	18.8	20.3	21.8	23.8	24.8	26.3	27.8	29.3
272	30.8	82.8	88.8	35.8	36.8	38.3	39.8	41.8	42.8	41.3
278	45.8	47.8	48.8	50.8	51.8	53.3	54.8	56.8	57.8	59.3
274	60.8	62.2	63.7	65.2	66.7	68.2	69.7	71.2	72.7	74.1
273	75.6	77.1	78.6	80.1	81.6	83.1	84.5	86.0	87.5	89.0
93 Inch.	1	i	1	l		l		ì	ļ	1
276	90.5	91.9	98.4	94.9	96.4	97.9	99.8	100.8	102.8	103.8
277	105.2	106.7	108.2	109.7	111.1	112.6	114.1	115.6	117.0	118.5
278 279	120.0	121.4	122.9	124.4	125.8	127.3	128.8	130.2	131.7	133.2
280	184.6 149.8	136.1 150.7	187.6 152.2	139.0 153.6	140.5 155.1	142.0 156.5	148.4 158.0	144.9 159.5	146.3 160.9	147.8
281	163.8	165.3	166.7	168.2	169.6	171.1	172.5	174.0	175.4	176.9
201	100.0	100.0	200	100.2	100.0	*****	112.0	11110	1.0.1	1
282	178.3	179.8	181.2	182.7	184.1	185.6	187.0	189.5	189.9	191.4
283	192.8	194.2	195.7	197.1	198.6	200.0	201.4	202.9	204.8	205.8
284	207.2	208.6	210.1	211.5	213.0	214.4	215.8	217.8	218.7	220.1
285	221.6	223.0	221.4	225.9	227.8	228.7	230.2	231.6	233.0	211.5
286	235.9	237.8	238.7	240.2	241.6	243.0	244.4	245.9	247-8	248.7
287	230.1	251.6	258.0	254.4	255.8	257.8	258.7	260.1	261.5	262.9
94 Inch. 288	264.4	263.8	267.2	268.6	270.0	271.4	272.9	274.3	275.7	277.1
289	278.5	279.9	281.3	282.8	284.2	285.6	287.0	288.4	289.8	291.2
290	292.6	294.0	295.4	296.8	298.3	299.7	801.1	302.5	803.9	305.3
291	306.7	808.1	809.5	310.9	312.3	318.7	315.1	316.5	317.9	319.3
292	320.7	822.1	823.5	324.9	326.8	827.7	329.1	330.5	331.9	. 333.3
293	334.7	836.1	337.5	888.9	340.2	341.6	843.0	811.1	345.8	817.2
		ŀ						Ì		1
294	848.6	350.0	851.4	852.8	854.2	355.5	356.9	358.8	359.7	361.1
295	862.5	363.9	365.2	866.6	868.0	369.4	370.8	372.2	878-5	374.9
296 297	376.3 390.1	877.7 391.5	379.1 392.8	880.4 894.2	881.8 895.6	888.2 897.0	384.6 398.3	385.9 399.7	\$87.3 401.1	388.7 402.4
297	403.8	405.2	406.5	407.9	409.3	410.7	412.0	418.4	414.8	416.1
299	417.5	418.9	420.2	421.6	428.0	424.8	425.7	427.1	428.4	429.8
95 Inch										
800	481.1	482.5	483.9	435.2	486.6	487.9	439.8	440.7	442.0	448.4
801	444.7	446.1	447.5	448.8	450.2	451.5	452.9	454.2	455.6	456.9
302	458.3	459.6	461.0	462.3	468.7	465.0	466.4	467.8	469.1	470.5
808	471.8	478.1	474.5	475.8	477.2	478.5	479.9	491.2	492.6	493.9
804	485.3	486.6	487.9	489.3	490.6	492.0	498.3	494.7	496.0	497.8
805	498.7	500.0	501.4	502.7	504.0	505.4	506.7	508.0	509.4	510.7
306	512.0	518.4	514.7	516.0	517.4	518.7	520.1	521.4	522.7	524.0

TABLE I. Continued.

arom-					Tenths (of a Line.				
Paris ines.	0	1	2	8	4	5	6	7	8	9
806	512.0	513.4	514.7	516.0	517.4	518.7	520.1	521.4	522.7	524.0
307	525.4	526.7	528.0	529.4	530.7	582.0	538.4	534.7	536.0	537.4
308	538.7	540.0	541.3	542.6	544.0	545.8	546.6	547.9	549.3	550.6
309	551.9	553.2	554.6	555.9	557.2	568.5	559.8	561.2	562.5	563.8
810	565.1	566.4	567.8	569.1	570.4	571.7	578.0	574.3	575.6	576.9
B11	578.8	579.6	580.9	582.2	588.5	584.8	586.1	587.5	588.8	590.1
Inch.			7040							
812	591.4	592.7	594.0	595.8	596.6	597.9	599.2	600.6	601.9	608.2
818	604.5	605.8	607.1	608.4	609.7	611.0	612.3	618.6	614.9	616.2
B14	617.5	618.8	620.1	621.4	622.7	624.0	625.3	626.6	627.9	629.2
B15	630.5	681.8	633.1	684.4	635.7	687.0	638.3	689.5	640.8	642.1
B16	643.4	644.7	646.0	647.8	648.6	649.9	651.2	652.5	688.8	655.1
B17	656.3	657.6	658.9	660.2	661.5	662.8	664.1	665.4	666.6	667.9
818	669.2	670.5	671.8	678.1	674.3	675.6	676.9	678.2	679.5	680.8
319	682.0	693.8	684.6	685.9	687.2	688.4	699.7	691.0	692.3	693.6
320	694.8	696.1	697.4	698.7	699.9	701.2	702.5	708.8	705.0	706.3
321	707.6	708.9	710.1	711.4	712.7	713.9	715.2	716.5	717.7	719.0
322	720.8	721.6	722.8	724.1	725.4	726.6	727.9	729.2	730.4	731.7
B23	733.0	784.2	733.5	786.7	738.0	789.8	740.5	741.8	748.1	744.9
Inch.									1	
B24	745.6	746.8	748.1	749.4	750.6	751.9	758.2	754.4	755.7	736.9
B25	758.2	759.4	760.7	761.9	763.2	764.5	765.7	767.0	768.2	769.5
326	770.7	772.0	778.2	774.5	775.7	777.0	778.2	779.5	780.7	782.0
B27	783.2	784.5	785.7	787.0	788.2	789.5	790.7	792.0	798.2	794.0
328	795.7	797.0	798.2	799.4	800.7	801.9	808.2	804.4	805.7	806.9
B29	808.2	809.4	810.6	811.9	813.1	814.4	815.6	816.8	818.1	819.
E30	820.6	821.8	823.0	824.8	825.5	826.7	828.0	829.2	880.4	831.7
331	832.9	834.2	835.4	836.6	837.9	839.1	840.3	841.6	842.8	844.0
B32	845.2	846.5	847.7	848.9	850.2	851.4	852.6	853.9	855.1	856.1
323	857.5	858.8	860.0	861.2	862.4	863.7	864.9	866.1	867.8	868.6
834	869.8	871.0	872,2	878.4	874.7	875.9	877.1	878.8	879.6	880.8
835	882.0	888.2	884.4	885.7	886.9	888.1	889.3	890.5	891.7	893.0
Inch.										
B 36	894.2	893.4	896.6	897.8	899.0	900.8	901.5	902.7	903.9	905.1
837	906.8	907.5	908.7	909.9	911.2	912.4	913.6	914.8	916.0	917.2
338	918.4	919.6	920.8	922.0	928.3	924.5	925.7	926.9	928.1	929.1
239	930.5	931.7	982.9	934.1	935.8	936.5	937.7	938.9	940.1	941.5
340	942.5	943.7	944.9	946.1	947.8	948.5	949.7	950.9	952.1	953.8
841	954.5	955.7	956.9	958-1	959.3	960.5	961.7	962.9	964.1	965.8
342	966.5	967.7	968.9	970-1	971.3	972 5	973.7	974.8	976.0	977.2
843	978.4	979.6	980.8	982.0	983.2	984.4	985.6	996.8	987.9	989.1
844	990.8	991.5	992.7	993.9	995.1	996.2	997.4	998.6	999.8	1001.0
845	1002.2	1008.4	1004.5	1005.7	1006.9	1008.1	1009.3	1010.5	1011.6	1012.8
846	1014.0	1015.2	1016.4	1017-5	1018.7	1019.9	1021.1	1022.8	1023.4	1024.6
847	1025.8	1027.0	1028.1	1029.8	1030.5	1031.7	1032.8	1084.0	1035.2	1036.4
Inch 348	1037.5	1038.7	1039.9	1041.1	****	1043.4	10000	10.00	1046 9	1048.1

TABLE II.

CORRECTION FOR THE TEMPERATURE OF THE AIR.

Argument, $2\tau = \frac{t+t'}{2}$.

2 τ	71	Diff.	2 τ	71	Diff.	2 τ	7'	Diff.	2 τ	T [†]	Diff.
-25 -24 -23 -22 -21 -20 -19 -18 -17 -16	-14.29 -18.64 -18.00 -12.86 -11.78 -11.11 -10.50 -9.89 -9.29 -8.70 -8.11 -7.58	0.65 0.64 0.64 0.63 0.62 0.61 0.60 0.59 0.39	-12 -11 -10 - 9 - 8 - 7 - 6 - 5 - 4 - 3	-6.38 -5.82 -5.26 -4.71 -4.17 -8.63 -3.09 -2.56 -2.04 -1.52 -1.01 -0.50	0.56 0.56 0.55 0.54 0.54 0.54 0.58 0.69 0.53	+ 1 2 3 4 4 5 6 7 8 9 10 11 12	+0.50 0.99 1.48 1.96 2.44 2.91 8.38 8.85 4.31 4.76 5.21 5.66	0.49 0.49 0.46 0.48 0.47 0.47 0.47 0.46 0.45	+14 15 16 17 18 19 20 21 22 23 24 25	+ 6.54 6.99 7.41 7.83 8.26 8.68 9.09 9.50 9.91 10.31	0.44 0.43 0.42 0.43 0.43 0.41 0.41 0.41 0.40
-13 -12	- 6.95 - 6.38	0.58	0 + 1	0.00 +0.50	0.50	18 +14	6.10 +6.54	0.44 0.44	26 +27	11.50 +11.89	0.39

TABLE III. FOR C.

ARGUMENTS, h and r.

In computing Heights reverse the signs of C. — Arguments, τ and u.

À, (#)	H			τ, in Deg	grees of Re	aumur —			
Toises.	-16°	-12°	-8°	-4°	0 0	+40	+8°	+12°	+16
50	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1
100	0.2	0.2	0.2	0.2	0.8	0.3	0.8	0.8	0.3
150	0.3	0.8	0.4	0.4	0.4	0.4	0.4	0.4	0.4
200	0.4	0.5	0.5	0.5	0.5	0.5	0.6	0.6	0.6
250	0.5	0.6	0.6	0.6	0.6	0.7	0.7	0.7	0.7
300	0.7	0.7	0.7	0.7	0.8	0.8	0.8	0.9	0.9
850	0.8	0.8	0.8	0.9	0.9	0.9	1.0	1.0	1.1
400	0.9	0.9	1.0	1.0	1.0	1.1	1.1	1.2	1.2
450	1.0	1.1	1.1	1.1	1.2	1.2	1.8	1.8	1.4
500	1.1	1.2	1.2	1.3	1.8	1.4	1.4	1.5	1.5
550	1.2	1.3	1.4	1.4	1.5	1.5	1.6	1.6	1.7
600	1.4	1.4	1.5	1.6	1.6	1.7	1.7	1.8	1.9
650	1.5	1.6	1.6	1.7	1.8	1.8	1.9	1.9	2.0
700	1.6	1.7	1.8	1.8	1.9	2.0	2.0	2.1	2.2
750	1.7	1.8	1.9	2.0	2.0	2.1	2.2	2.3	2.3
800	1.9	2.0	2.0	2.1	2.2	2.3	2.4	2.4	2.5
850	2.0	2.1	2.2	2.3	2.3	2.4	2.5	2.6	2.7
900	2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9
950	2.8	2.4	2.5	2.6	2.7	2.7	2.9	3.0	3.1
1000	2.4	2.5	2.6	2.7	2.8	2.9	3.1	8.2	3.3

In computing Heights, reverse the signs of C'. Arguments φ and u.

Lati	tude.	ļi													
_	+	100	200	800	400	500	600	700	800	900	1000				
0	90	0.8	0.5	0.8	1.0	1.3	1.6	1.8	2.1	2.3	2.6				
5	85	0.8	0.5	0.8	1.0	1.3	1.5	1.8	2.0	2.3	2.6				
10	80	0.2	0.5	0.7	1.0	1.2	1.5	1.7	2.0	2.2	2.4				
15	75	0.2	0.4	0.7	0.9	1.1	1.8	1.6	1.8	2.0	2.8				
20	70	0.2	0.4	0.6	0.8	1.0	1.2	1.4	1.6	1.8	2.0				
25	65	0.2	0.8	0.5	0.7	0.8	1.0	1.2	1.8	1.5	1.7				
30	60	0.1	0.8	0.4	0.5	0.6	0.8	0.9	1.0	1.2	1.8				
35	53	0.1	0.2	0.3	0.4	0.4	0.5	0.6	0.7	0.8	0.9				
36	54	0.1	0.2	0.2	0.8	0.4	0.5	0.6	0.6	0.7	0.8				
37	53	0.1	0.1	0.2	0.8	0.4	0.5	0.5	0.6	0.6	0.7				
88	52	0.1	0.1	0.2	0.8	0.8	0.4	0.4	0.5	0.6	0.6				
3 9	51	0.1	0.1	0.2	0.2	0.8	0.8	0.4	0.4	0.5	0.5				
40	50	0.1	0.1	0.1	0.2	0.2	0.8	0.8	0.4	0.4	0.5				
41	49	0.0	0.1	0.1	0.1	0.2	0.2	0.8	0.8	0.3	0.4				
42	48	0.0	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.8				
43	47	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.2	0.2				
44	46	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1				
45	45	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				

TABLE V. FOR C".

ARGUMENTS τ and T — T. To be used only in computing Heights.

T-T	1	•	Correction	on for T-	T, in Tol	see, with t	be same s	dgn; τ 🕳		
Resumur.	-19 °	-10°	-80	-6 °	-4°	_2°	00	+2°	+40	+69
0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.0
2	0.4	0.8	0.8	0.8	0.2	0.2	0.2	0.1	0.1	0.0
3	0.6	0.5	0.5	0.4	0.4	0.8	0.2	0.2	0.1	0.1
4	0.8	0.7	0.6	0.5	0.5	0.4	0.8	0.2	0.2	0.1
5	1.0	09	0.8	0.7	0.6	0.5	04	0.3	0.2	0.1
6	1.1	1.0	0.9	0.8	0.7	0.6	0.5	0.4	0.8	0.1
7	1.8	1.2	1.1	0.9	0.8	0.7	0.6	0.4	0.8	0.2
8	1.5	1.4	1.2	1.1	0.9	0.8	0.6	0.5	0.8	0.2
9	1.7	1.6	1.4	1.2	1.1	0.9	0.7	0.6	0.4	0.2
10	1.9	1.7	1.5	1.4	1.2	1.0	0.8	0.6	0.4	0.2

Correction for T - T with contrary sign; -

T-F	+8°	+10°	+13°	+14°	T — T'	+8°	+100	+120	+14°
1	0.0	0.0	0.0	0.0	6	0.0	0.1	0.2	0.8
2	0.0	0.0	0.1	0.1	7	0.0	0.1	0.2	0.8
8	0.0	0.0	0.1	0.1	8	0.0	0.1	0.2	0.4
4	0.0	0.0	0.1	0.2	9	0.0	0.1	0.2	0.4
5	0.0	0.1	0.2	0.2	10	0.0	0.1	0.8	0.4

LAPLACE'S FORMULA FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS, MODIFIED BY BABINET.

In the Comptes Rendus de l'Académie des Sciences for March, 1851, M. Babinet proposes the following modification of Laplace's formula, the object of which is to dispense both with the use of logarithms and with tables of any kind.

Laplace's formula is,

$$z = 18393$$
 metres (log H — log h) $\left[1 + \frac{2(T+t)}{1000}\right]$,

z being the difference of level between the two stations,

H, the height of barometer at the lower station,

h, the height of barometer at the upper station,

T, temperature of air at the lower station,

t, temperature of air at the upper station.

The two barometers are supposed to be reduced to the same temperature. The small correction for the latitude is omitted.

For elevations less than 1000 metres, and even for much greater elevations, if approximate results only are needed, the formula may be transformed into the following:

 $z = 16000 \text{ metres } \frac{H - h}{H + h} \left[1 + \frac{2(T + t)}{1000} \right].$

Example 1.

Suppose,

at lower station, barometer at zero Cent. = 755^{mm}; temperature of air 15° Cent. at upper station, barometer at zero Cent. = 745^{mm}; temperature of air 10° Cent.

$$H - h = 10^{ma}$$
. $T + t = 25^{\circ}$ Cent. $H + h = 1500^{mm}$. $2 (T + t) = \frac{1}{18} \frac{1}{18} \frac{1}{18} = .05$.

Then

 $z = 16000_{1180} \times (1.05) = 112$ metres.

Laplace's formula, by Delcros's tables, would give 111.6 metres.

Example 2.

Suppose,

at lower station, barometer at zero Cent. = 730^{mm} ; temperature of air 20° Cent. at upper station, barometer at zero Cent. = 635^{mm} ; temperature of air 15° Cent.

$$H - h = 95^{mm}$$
 $T + t = 35^{\circ}$ Cent.
 $H + h = 1365^{mm}$ $2 (T + t) = 758 = .07$.

Then

 $z = 16000_{1\frac{9}{5}\frac{5}{65}} \times (1.07) = 1191.5$ metres.

Laplace's formula, by Delcros's tables, would give 1191.1 metres.

For greater elevations an intermediate station may be supposed.

Babinet's formula reduced to English measures becomes,

$$z = 52494$$
 English feet $\frac{H-h}{H+h} \left[1 + \frac{(T+t-64)}{900} \right];$

but as, in this form, it loses the simplicity of its coefficient, it will be found, on trial, that its use requires rather more computing than the author's tables (II.), p. 38, which give more accurate results.

VII.

TABLES

FOR COMPUTING THE DIFFRENCE IN THE HEIGHTS OF TWO PLACES BY MEANS OF THE BAROMETER. - BAILY.

Bally, in his Astronomical Tables and Formulæ, page 111, gives the following final formula:

Where ϕ = the latitude of the place,

 β = the height of the barometer,

τ = the temperature, Fahrenheit, of the mercury, t = the temperature, Fahrenheit, of the air,

at the lower station.

 β' = the height of the barometer,

 τ' = the temperature, Fahrenheit, of the mercury, station. t' = the temperature, Fahrenheit, of the air.

The numerical values assumed are as follows: -

The constant barometrical coefficient = 60158.53 English feet.

The expansion of moist air for 1° Fahrenheit = .0022222.

The expansion of mercury for 1° Fahrenheit = .0001001.

The increase of gravitation from Equator to Poles = .00539.

The radius of the Earth at ϕ = 20898240 English feet.

The height of lower station assumed = 4000 English feet.

Make A = the log of the first term, in English feet.

B = the log of 1 + .0001 (r - r').

C = the log of the last term.

 $D = \log \beta - (\log \beta' + B).$

Then, by the tables which follow, the logarithm of the difference of altitude in English feet

 $= A + C + \log D.$

Baily's Tables have been recomputed and extended by Downes, for Lee's Collection of Tables and Formulæ (2d edit. pp. 84, 85). These new tables are given here as revised by Mr. Downes for this volume.

_				_	
1.	THERMOMETERS	IN	THE	()PRN	AIR.

+ "	A	t + t*	A	t + t'	A	t + t'	A	t+t'	A
٧٩	4.74913	87	4.76742	o 78	4.78497	109	4.80183	° 145	4.81807
2	4.74965	38	4.76791	74	4.78544	110	4.80229	146	4.81831
8	4.75016	89	4.76841	75	4.78592	111	4.80275	147	4.81896
4	4.75068	40	4.76891	76	4.78640	112	4.80321	148	4.81940
5	4.75120	41	4.76940	77	4.78687	118	4.80367	149	4.81964
6	4.75171	42	4.76990	78	4.78785	114	4.80418	150	4.82028
7	4.75228	48	4.77089	79	4.78782	115	4.80458	151	4.82072
8	4.75274	44	4 77089	80	4.78880	116	4.80504	152	4.82116
9	4.75326	45	4.77189	81	4.78877	117	4.80550	153	4.82160
10	4.75877	46	4.77187	82	4.78225	118	4.80595	154	4.82204
11	4.75429	47	4.77286	83	4.78972	119	4.90641	155	4.82248
12	4.75480	48	4.77285	84	4.79019	120	4.80686	156	4.82291
18	4.75581	49	4.77335	85	4.79066	121	4.80731	157	4.82335
14	4 75582	50	4.77884	86	4.79113	122	4.80777	158	4.62379
15	4.75623	51	4.77488	87	4.79100	128	4.80622	159	4.82423
16	4.75684	52	4.77482	88	4.79207	124	4.80867	160	4.82466
17	4.75785	58	4.77580	89	4.79254	125	4.80918	161	4.82510
18	4.75786	54	4.77579	90	4.79801	126	4.80958	162	4.82553
19 20	4.75887 4.75888	55 56	4.77628 4.77677	91 92	4.79848 4.79395	127 128	4.8100 8 4.81048	163 164	4.8 25 97 4.8 26 40
21	4.75938	57	4.77725	98	4 79442	129	4.81096	165	4,82684
22	4.75989	58	4.77774	94	4.79489	180	4.81138	166	4.82727
23	4.76040	59	4.77823	95	4.79585	181	4.81188	167	4-82770
24	4.76090	60	4.77871	96	4.79582	132	4.81228	168	4.82814
25	4.76141	61	4.77919	97	4.79628	188	4.81278	169	4.82857
26	4.76191	62	4.77968	98	4.79675	134	4.81817	170	4.82900
27	4.76241	63	4.78016	99	4.79721	185	4.81862	171	4.82943
28	4.76292	64	4.78065	100	4.79768	136	4.81407	172	4.82984
29	4.76342	63	4.78118	101	4.79814	187	4-81452	173	4.93029
30	4.76892	66	4.78161	102	4.79861	138	4.81496	174	4.83072
81	4.76412	67	4.78209	108	4.79907	139	4.81541	175	4.83116
82	4.76492	68	4.78257	104	4.79953	140	4.81585	176	4.83158
83	4.76542	69	4.78305	105	4.79999	141	4.81630	177	4.83201
84	4.76592	70	4.78353	106	4.80045	142	4.81674	178	4.83244
85	4.76612	71	4.78401	107	4.80091	148	4.81719 4.81763	179 180	4-83297
86	4.76692	72	4.78149	106	4.80187	144	4.01.109	190	4.88330

	п.	Аттасны	D THERMON	ETER.			ATITUDE OF
т—т'	В	T-T'	В	τ-τ'	В	ф	c
°	0.00000	20	0.00087	0 40	0.00174	ô	0.60117
1	0.00004	21	0.00087	41	0.00174	5	0.00117
2	0.00002	22	0.00091	42	0.00178	10	0.00110
3	0.00018	22	0.00100	43	0.00187	15	0.00110
4	0.00018	24	0.00100	44	0.00191	20	0.00001
•	0.00027		0.00104		0.00131		0.00050
5	0.00022	25	0.00109	45	0.00195	25	0.00075
6	0.00026	26	0.00118	46	0.00200	80	0.00058
7	0.0000	27	0.00117	47	0.00204	85	0.00040
8	0.00085	28	0.00122	48	0.00206	40	0.00020
9	0.00089	29	0.00126	49	0.00212	45	0.00000
10	0.00043	30	0.00180	50	0.00217	50	9.99980
11	0.00048	31	0.00185	51	0.00221	55	9.99960
12	0.00052	32 .	0.00189	52	0.00225	60	9.99942
18	0.00056	88	0.00148	53	0.00230	65	9.99925
14	0.00031	84	0.00148	54	0.00284	70	9.99910
15	0.00065	35	0.00152	55	0.00288	75	9.99900
16	0.00069	36	0.00156	56	0.00248	80	9.99890
17	0.00074	87	0.00161	57	0.00247	85	9.99885
18	0.00078	88	0.00165	58	0.00251	90	9.99888
19	0.00083	39	0.00169	59	0.00256	1	

EXAMPLE.

	Upper Station.	Lower Station.
Thermometer in open air,	t'=70.4,	t = 77.6.
Attached Thermometer,	r = 70.4	$\tau = 77.6$.
Barometer,	$\beta' = 23.66$ inches,	$\beta = 30.05$ inches.
Latitude of the place	$\phi=21^{\circ}.$	•
B = 0.00031	$\log D = 9.0$	1502
$\log \beta' = 1.37401$	C = 0.0	00087
1.37432	$\Lambda = 4.6$	91940
$\log\beta=1.47784$	3.0	83529
D = 0.10352	= 68	43.7 English feet.

VIII.

TABLES

FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS,

BASED ON BESSEL'S FORMULA.

By E. PLANTAMOUR.

[These Tables, computed by Professor E. Plantamour, Director of the Observatory at Geneva, Switzerland, are found in Vol., XIII. Part 1, of the Mémoires de la Société de Physique, &c. de Genère, p. 63, together with the following explanations.]

In No. 356 of the Astronomische Nachrichten, Bessel published a paper on the measurement of heights by means of the barometer, in which he deduces a formula which contains a factor depending on the humidity of the air. This formula is:

$$\log \frac{P}{P} = \frac{(g) \cdot H' - H}{L(1 + KT)} \left[1 - a \frac{0.002561}{\sqrt{PP'}} \cdot 10^{-0.0279712} T - 0.0000625826 T^{2} \right],$$

where the various quantities have the following signification: -

h being the elevation of the lower station, and

h' the elevation of the upper station above the level of the sea,

a = the radius of the Earth,

$$H=\frac{ah}{a+h},$$

$$H' = \frac{a h'}{a + h'};$$

P = the weight of the atmosphere at the lower station,

P' = the weight of the atmosphere at the upper station,
 the unit of weight assumed being the pressure of a column of mercury

of 336.905 Paris lines, at the temperature of the freezing point, or zero-Reaumur, and under the 45th degree of latitude.

(g) = the gravity, at the level of the sea, in the mean latitude between the two places of observation.

Therefore, calling ϕ the latitude,

 $(g) = 1 - 0.0026257 \cos \phi,$

L = the constant barometrical coefficient depending on the relative density of the mercury and of the air,

K = the coefficient of the expansion of the air,

T = the mean temperature of the layer of air between the lower and upper station,

a = the fraction of saturation of the same layer.

The second term in the parenthesis, destined to take into account the aqueous vapor in the air, was obtained by assuming that the elastic force of vapor for a temperature T is represented, in unit of weight, by the expression,

$$p = 0.0067407 \times 10^{-0.0279712} \text{ T} - 0.0000625826 \text{ T}^2$$
.

Multiplying the second member by 336.905 we find the expression of the elastic force of vapor that Laplace deduced from Dalton's experiments. Substituting, in the computation, Regnault's results, the numerical value of these coefficients is somewhat changed, and we find then

$$v = 0.0060527 \times 10^{-0.0301975} \text{ T} - 0.000080170 \text{ T}$$

Bessel's tables give the difference of elevation in toises. The logarithm of the difference is obtained by the sum of four logarithms. The same form is preserved in the following tables; but the differences of elevation are given in metres.

The term due to the expansion of the air is computed in Bessel's tables for two values of the coefficient, viz. that of Gay-Lussac, 0.00375, and that of Rudberg, 0.003648; in the new tables it is only computed for that of Regnault, 0.003665.

The relative density of dry air at the freezing point, under a barometrical pressure of 0^m·.76, and at the 45th degree of latitude, and of mercury in the same circumstances, adopted by Bessel, is that determined by the experiments of Biot and Arago, viz.

The value of that constant derived from Regnault's experiments has been substituted. Regnault found the weight of a litre of dry air, at zero Centigrade, under a pressure of 0°.76, and at the latitude of Paris, to be 1.293187 grammes, which, reduced to the gravity of the 45th degree of latitude, becomes 1.292732 grammes. The weight of a litre of mercury, at zero Centigrade, he found to be 13596 grammes; the ratio is thus:

$$D = \frac{1}{10517.8}$$

or about χ_{08} smaller than the value adopted by Bessel. If the constant coefficient L is expressed by $L = \frac{0^{\infty}.76}{D \cdot \mu}$, μ being the modulus of the common logarithms, its numerical value becomes

$$L = 18404^{-1}.8.$$

In order to reduce the formula into tables, Bessel caused it to undergo several modifications, which we have followed, introducing the values of the constants above mentioned.

Let b and b' be the heights of the barometer, expressed in the metrical scale, at the two stations; t and t', the temperatures of the mercury measured with a brass scale; we have,

$$P = \frac{b}{0-.76} \cdot (g) \cdot \left(\frac{a}{a+h}\right)^{1} \frac{(1+0.00001879 t)}{(1+0.00018018 t)^{2}}$$

and

$$P' = \frac{b'}{0 - .76} \cdot (g) \cdot \left(\frac{a}{a + b'}\right)^{3} \frac{(1 + 0.00001879 f)}{(1 + 0.00018018 f)}.$$

Therefore,

$$\log P = \log b + \log (g) - \log 0^{-.76} - \frac{2 H \mu}{a} - \mu t [0.00018018 - 0.00001879],$$

$$\log P' = \log b' + \log (g) - \log 0^{m}.76 - \frac{2 R' \mu}{a} - \mu t' [0.00018018 - 0.00001879].$$

If we call B, B' the heights of the barometer reduced to the freezing point, which we obtain by making

$$\log B = \log b - t \cdot 0.000070095$$
; $\log B' = \log b' - t' \cdot 0.000070095$,

$$\log \frac{P}{P'} = \log B - \log B' + \frac{H' - H}{7829755}$$

and with sufficient accuracy.

$$\checkmark P P' = \frac{\checkmark B B'}{0^{m} \cdot 76}$$

Substituting these expressions in the formula, it becomes,

$$\log B - \log B' = \frac{(g) \cdot H' - H}{L(1 + KT)} \left[1 - \frac{L(1 + KT)}{(g) \cdot 7829755} - \frac{a \cdot 0.001748}{\sqrt{BB'}} \cdot 10^{0.0301975} T - 0.000080170 T^{3} \right].$$

If we set instead of a the half sum $\frac{a+a}{2}$ of the fraction of saturation observed at both stations, we find, after some transformations,

$$\log B - \log B' = \frac{(g) (H' - H) (397.25 - KT)}{398.25 \cdot L (1 + KT)} \times \left[1 - \frac{(\alpha + \alpha') \cdot 0.34807}{(397.25 - KT) \sqrt{BB'}} \cdot 10^{0.0301975 T} - 0.000080170 T^{2}\right].$$

Making further,

$$V = \frac{398.25}{397.25 - KT} L (1 + KT),$$

$$W = \frac{0.34807}{397.25 - KT} \cdot 10^{0.0301975 T - 0.000080170 T^2},$$

we shall have for the logarithm of the approximate difference of level between the two stations H' — H,

$$\log (H' - H) = \log [\log B - \log B'] + \log V + \log \frac{1}{1 - W \frac{a + a'}{\sqrt{B B'}}} + \log \frac{(g)}{1}.$$

Table I. gives the values of log V and log W, both of which only depend on the temperature; the argument is the sum of the temperature of the air, τ and τ' , observed at both stations, supposing $\tau + \tau' = 2 T$.

Table IL gives the factor depending on the humidity of the air; with the argument

W.
$$\log \frac{(a+a)}{\sqrt{BB'}}$$
,

we obtain

$$\log \frac{1}{1 - W \frac{(\alpha + \alpha')}{\sqrt{B B'}}} = \log V'.$$

Table III. gives the factor depending on the latitude for every degree, viz.

$$\log G' = \log \frac{1}{(g)}.$$

The logarithm of the approximate difference is thus given by the sum of four logarithms. To obtain the exact elevation, the small correction found in Table IV. must be added to the number corresponding to that logarithm. For we have, with the necessary accuracy,

$$h' - h = H' - H + \frac{H'^2}{a} - \frac{H^2}{a}$$

Table IV. gives, for every 200 metres, the quantity $\frac{H^s}{a}$; the number in the table corresponding to $\frac{H'^s}{a}$ must be added to the approximate elevation; and the number corresponding to $\frac{H^s}{a}$ must be subtracted from the same.

USE OF THE TABLES.

Reduce first the observed height of the barometer at both stations to the freezing point by means of the usual tables, or by the logarithmic formula,

$$\log B = \log b - t \cdot 0.00007$$
, $\log B' = \log b' - t' \cdot 0.00007$;

b and b' being, in fractions of metre, the observed heights at the temperatures t and t' marked by the attached thermometers; and B and B' the reduced height at the lower and upper station.

Take the difference of log B and log B', and find, in the tables of the common logarithms, the logarithm of that difference, viz. log (log B — log B'); find also the logarithm of the product \checkmark B B', or

$$\log \checkmark B B' = \frac{\log B + \log B'}{2}.$$

Make further the sum $\tau + \tau'$ of the temperature of the air at both stations, and likewise the sum of a + a' of the fraction of saturation.

Then, in Table I., with argument r + r', take log V and log W; further, to log W add log (a + a'), and subtract log $\checkmark BB'$; and with the logarithm thus obtained as argument, take in Table II. log V'.

Table III. with the mean latitude of the stations gives log G'.

H' — H being the approximate difference of level between the two stations, we have

$$\log (H' - H) = \log (\log B - \log B') + \log V + \log V' + \log G'.$$

The altitude of the lower station being known, we deduce from H' - H the approximate altitude, H', of the upper station; h', the exact altitude, or h' - h, the difference of elevation, is given by the formula,

$$h' - h = H' - H + \frac{H'^{\circ}}{a} - \frac{H^{\circ}}{a}$$

Table IV. gives the values of $\frac{H'^*}{a}$ and $\frac{H^*}{a}$ for the values of H' or H for every 200 metres.

Example 1.

Computing the height of St. Bernard, taking Geneva, 407 metres above the level of the sea, as the lower station. The observation gives,

$$\log \left[\log B - \log B'\right] = 9.04215$$
In Table I. argt. $\tau + \tau' = +7.08$, $\log V = 4.27164$
In Table II. argt. 7.4409, $\log V' = 0.00120$
In Table III. argt. 46°, $\log G' = -0.00004$

$$\log (H' - H) = 3.31495$$

$$H' - H = 2065.1 \text{ metres.}$$
In Table IV. $\frac{H'^s}{a} - \frac{H^s}{a} = +0.9$

$$h' - h = 2066.0$$
Geneva altitude $h = 407.0$
St. Bernard above the level of the sea $h' = 2473.0$ metres.

Example 2.

Computing the height of Mont Blanc from the observations of Bravais and Martins, on the 29th of August, 1844, taking St. Bernard (2473.0 metres) as the lower station. The observation gives,

h = 2473.0

Mont Blanc above the sea, h' = 4811.7 metres.

St. Bernard altitude,

			···	TABLE					TABLE IV.	
		Arge	ment =	7 + 11. Cax	tigrade De	press.			Arg*t. =	Height.
7+71.	log. V.	log. W.	T+T.	log. V.	log. W.	T + T'.	log. V.	log. W.	H'. H.	<u> </u> ±
	4.04044		٥			٥			Metres.	
-24 -28	4.24644	6.5862 6.5441	+15 +16	4.27783 4.27861	7.1692 7.1889	+54	4.30711 4.30784	7.7038 7.7160	200 400	0.01
-22	4.24811	6.5620	+17	4.27988	7.1985	+56	4.80856	7.7287	600	0.06
-21	4.24894	6.5797	+18	4.28016	7.2181	+57	4.30929	7.7413	800	0.10
-20	4.24977	6.5974	+19	4.28098	7.2275	+58	4.81001	7.7589	1000	0.16
1 1)			1
-19	4.25059	6.6157	+20	4.28170	7.2420	+59	4.31073	7.7664	1200	0.23
-18 -17	4.25142	6.6841 6.6521	+21	4.28247	7.2564	+60 +61	4.81145	7.7789	1400	0.31
-17 -16	4.25225	6.6700	+22	4.28828	7.2708 7.2850	+62	4.81217	7.7914 7.8038	1600 1800	0.40
-15 -15	4.25889	6.6879	+24	4.28477	7.2993	+63	4.81360	7.8161	2000	0.63
-										
-14	4.25471	6.7057	+25	4.28558	7.3135	+64	4.81482	7.8285	2200	0.76
-18	4.25558	6.7232	+26	4.28629	7.8276	+65	4.81503	7.8407	2400	0.90
-12	4.25684	6.7407	+27	4.28705	7.8417	+66	4.31574	7.8580	2600	1.06
-11	4.25716	6.7581	+28	4.28781	7.8557			ļ	2800	1.28
-10	4.25797	6.7755	729	4.28857	7.8697			l	3000	1.41
- 9	4.25878	6.7926	+80	4.28988	7.8887			1	8200	1.61
- 8	4.25959	6.8096	+81	4.29006	7.8975				3400	1.82
- 7	4.26040	6.8266	+82	4.29084	7.4114	i	•	Ì	3600	2.04
- 6	4.26121	6.8486	+88	4.29159	7.4252			ŀ	3800	2.27
- 5	4.26202	6.8608	+84	4.29284	7.4889			1	4000	2.51
- 4	4.26282	6.8770	+85	4.29819	- 4700	ŀ		,	4200	2.77
- 8	4.26862	6.8985	+86	4.29819	7.4526 7.4662			}	4400	3.04
- 2	4.26448	6.9100	+87	4.29459	7.4798			1	4600	3.32
- 1	4.26528	6.9268	+38	4.29534	7.4983			ĺ	4800	3.62
0	4.26603	6.9426	+39	4.29608	7.5068	1		1	5000	3.93
									H	
+ 1	4.26682	6.9581	+40	4.29683	7.5202		,		5200	4.25
+ 2 + 8	4.26762 4.26841	6.9736	+41	4.29757 4.29831	7.5886			}	5400 5600	4.58
+ 4	4.26921	7.0048	+48	4.29881	7.5470 7.5602			ĺ	5800	4.93 5.28
+ 5	4.27000	7.0195	+44	4.29979	7.5785			1	6000	5.65
								ł	1	
+ 6	4.27079	7.0847	+45	4.30058	7.5867		-]	6200	6.04
+ 7	4.27157	7.0499	+46	4.80127	7.5999				6400	6.48
+ 8	4.27236	7.0650	+47	4.30200	7.6180				6600	6.84
+ 9 + 10	4.27815 4.27393	7.0800	+48	4.80278	7.6260				6800	7.26
110	4.2/398	7.0900	+49	4.80847	7.6390				7000	7.70
+11	4.27471	7.1099	+50	4.30420	7.6519				7200	8.14
+12	4.27550	7.1248	+51	4.80493	7.6648				7400	8.60
+18	4.27628	7.1397	+52	4.80566	7.6777				ll	
+14	4.27705	7.1545	+53	4.30639	7.6905				l	
+15	4.27788	7.1692	+54	4.30711	7.7083					1
<u></u>									<u> </u>	

		TAB	LE IL	** 			TABL	R II	r.
	An		og. W. (a + 1	*') y .			Argument		-
Argum't.	log. ₹¹.	Argum't.	log. V'.	Argum't.	log. ₹′.	٠.	log. G ⁱ .	•-	log. G'.
6.5	0.00014	7.70	0.00218	8.09	0.00588	°	+0.00114	40	+0.00020
6.6	0.00017	7.71	0.00218	8.10	0.00550	1	+0.00114	41	+0.00020
6.7	0.00022	7.72	0.00229	8.11	0.00568	2	+0.00114	42	+0.00010
6.8	0.00027	7.78	0.00234	8.12	0.00576	8	+0.00114	43	+0.00008
6.9	0.00034	7.74	0.00289	8.18	0.00590	4	+0.00118	44	+0.00004
7.0	0.00043	7.75	0.00245	8.14	0.00604	5	10.00110	45	0.00000
7.1	0.00045	7.76	0.00243	8.15	0.00618	6	+0.00112	46	0.00000 -0.00004
7.2	0.00069	7.77	0.00256	8.16		7	+0.00112	47	-0.00004
7.8	0.00087	7.78	0.00262	8.17	0.00647	8	+0.00111	48	-0.00012
7.4	0.00109	7.79	0.00269	8.18	0.00662	9	+0.00110	49	-0.00012
7.41	0.00112	7.80	0.00275	8.19	0.00678	10	+0.00107	50	-0.00020
7.42	0.00114	7.81	0.00281	8.20	0.00694	11	+0.00106	51	-0.00024
7.48	0.00117	7.82	0.00288	8.21	0.00710	12	+0.00104	52	-0.00028
7.44 7.45	0.00120 0.00128	7.88 7.84	0.00295	8.22 8.23	0.00727	18	+0.00108	58	-0.00081
7.20	0.00128	7.04	0.00302	5.40	0.00744	14	+0.00101	54	-0.00085
7.46	0.00125	7.85	0.00309	8.24	0.00761	15	+0.00099	55	-0.00089
7.47	0.00128	7.86	0.00316	8.25	0.00779	16	+0.00097	56	-0.00048
7.48	0.00181	7.87	0.00823	8.26	0.00798	17	+0.00095	57	-0.00046
7.49	0.00134	7.88	0.00881	8.27	0.00616	18	+0.00092	58	-0.00050
7.50	0.00188	7.89	0.00888	8.28	0.00835	19	+0.00090	59	-0.00054
7.51	0.00141	7.90	0.00846	8.29	0.00855	20	+0.00087	60	-0.00057
7.52	0.00144	7.91	0.00854	8.80	0.00875	21	+0.00085	61	-0.00060
7.53	0.00147	7.92	0.00363	8.81	0.00896	22	+0.00082	62	-0.00064
7.54	0.00151	7.98	0.00871	8.32	0.00917	23	+0.00079	63	0.00067
7.55	0.00154	7.94	0.00880	8.33	0.00989	24	+0.00076	64	-0.00070
7.56	0.00158	7.95	0.00389	8.34	0.00961	25	+0.00078	65	-0.00078
7.57	0.00162	7.96	0.00398	8.85	0.00988	26	+0.00070	66	-0.00076
7.58	0.00165	7.97	0.00407			27	+0.00067	67	-0.00079
7.59	0.00169	7.98	0.00417			28	+0.00064	6 8	-0.00082
7.60	0.00178	7.99	0.00427			29	+0.00060	69	-0.00085
7.61	0.00177	8.00	0.00437			80	+0.00057	70	-0.00087
7.62	0.00181	8.01	0.00447			81	+0.00054	71	-0.00090
7.68	0.00186	8.02	0.00457	'		82	+0.00050	72	-0.00092
7.64	0.00190	8.03	0.00468			83	+0.00046	78	-0.00094
7.65	0.00194	8.04	0.00479			84	+0.00048	74	-0.00097
7.66	0.00199	8.05	0.00490			85	+0.00089	75	-0.00099
7.67	0.00204	8.06	0.00502			86	+0.00085	76	-0.00101
7.68	0.00208	8.07	0.00518			87	+0.00081	77	-0.00101
7.69	0.00218	8.08	0.00525			88	+0.00028	78	-0.00104
7.70	0.00218	8.09	0.00588			89	+0.00034	79	-0.00106
		l				40	+0.00020	80	-0.00107

CORRECTION

FOR THE HOUR OF THE DAY AND THE SEASON OF THE YEAR AT WHICH THE OBSERVATIONS HAVE BEEN TAKEN.

In all the preceding tables, the mean temperature of the layer of air between the two stations is assumed to be given by the half-sum of the temperatures observed at each station, or by $\frac{t+t'}{2}$. Experience, however, has proved that this assumption is not true under all meteorological circumstances, and that, not to speak of more irregular influences, the temperature expressed by $\frac{t+t'}{2}$ differs in + or - from the true mean temperature by a quantity which considerably varies with the hour of the day, the season of the year, and the elevation at which the observations are taken. The amount of the correction for the temperature of the air, as given by the various formulas, thus needs to be modified accordingly. In the absence of the data necessary for establishing the law of the decrease of heat on the vertical in the various layers of the atmosphere, at the different periods of the day and of the year, and in different latitudes, which alone would furnish the means of determining the true value of this correction in these various circumstances, the following empirical tables enable us to form a judgment of the importance of that correction.

Tables IX. and X. are taken from Berghaus, Grundriss der Geographie, p. 91, and in the Tables accompanying the same work, p. 71. The correction to be applied for the hour of the day at which the observations have been taken, is found by multiplying the approximate height obtained by the factors in Table IX., giving to the correction the sign of the factor. This table and the following are calculated to be used in the climate of Germany, and for elevations not much exceeding 5,000 feet. The influence of the seasons on the correction is not taken into the account; judging from Table X., the correction may be, perhaps, too small for the summer months, and may better answer for the autumn. Using these factors, we obtain for the differences of level, in toises, placed at the head of each column, in Table X., the correction corresponding to each hour, from 6 A. M. to 10 P. M.

TABLE IX.

Hour.	Factor,	Hour.	Factor.	Hour.	Factor.
A. M. 6	+0.0075 +0.0050	Noon. P. M. 1	-0.0054 -0.0057	P. M. 5	-0.0011 +0.001 3
. 8	+0.0025	2	-0.0059	7	+0.0023
9	0.0005	8	-0.0045	8	+0.0032
10	-0.0085	4	-0.0081	9	+0.0048
11	-0.0044	5	-0.0011	10	+0.0054

TABLE X.

CORRECTION FOR THE HOUR OF THE DAY.

ARGUMENT, THE HOUR, AND THE APPROXIMATE HEIGHT IN TOISES.

				Correct	ion, in To	vises, for				
Hour.	100	200	300	400	500	600	700	800	900	Hour.
A. M. 6	+0.7	+1.5	+2.2	+8.0	+8.7	+4.5	+5.2	+6.0	+6.7	6 A. M.
7	+0.5	+1.0	+1.5	+2.0	+2.5	+8.0	+8.5	+4.0	+4.5	7
8	+0.2	+0.5	+0.7	+1.0	+1.2	+1.5	+1.8	+2.0	+2.8	8
9	-0.0	-0.1	-0.1	-0.2	-0.2	-0.8	-0.8	-0.4	-0.4	9
10	-0.8	-0.7	-1.0	-1.4	-2.1	-2.4	-2.8	-8.1	-8.5	10
11	-0.4	-0.9	-1.8	-1.8	-2.2	-2.7	-8.1	-8.6	-4.0	11
Noon.	-0.5	-1.1	-1.6	-2.2	-2.7	-3.3	-8.8	-4.4	-4.9	Noon.
P. M. 1	-0.6	-1.1	-1.7	-2.8	-2.8	-8.4	-4.0	-4.5	-5.1	1 P. M.
2	-0.6	-1.2	-1.8	-2.4	-8.0	-8.5	-4.1	-4.7	-5.8	2
8	-0.4	-0.9	-1.3	-1.8	-2.2	-2.7	-8.1	-8.6	-4.0	8
4	-0.8	-0.6	-0.9	-1.2	-1.5	-1.8	-2.1	-2.4	-2.7	4
5	-0.1	-0.2	-0.8	-0.4	-0.5	-0.6	-0.7	-0.8	-0.9	5
6	+0.1	+0.2	+0.4	+0.5	+0.5	+0.8	+0.9	+1.0	+1.1	6
7	+0.2	+0.4	+0.7	+0.9	+1.1	+1.3	+1.6	+1.8	+2.0	7
8	+0.3	+0.6	+0.9	+1.8	+1.6	+1.9	+2.2	+2.5	+2.9	8
9	+0.4	+0.8	+1.8	+1.7	+2.1	+2.6	+8.0	+8.4	+3.8	9
10	+0.5	+1.1	+1.6	+2.1	+2.7	+8.2	+2.8	+4.8	+4.8	10

Table XI. is found in the Résumé des Observations Thermométrique et Barométriques faites à Genève et au Grand St. Bernard pendant les dix années 1841 à 1850, a very elaborate paper by Professor E. Plantamour, Director of the Observatory at Geneva, published in Vol. XIII. of the Mémoires de la Société de Physique de Genève. The author, after having determined the difference of elevation between Geneva (407.0 metres above the level of the sea) and the Great St. Bernard, by means of the corresponding observations, made during these 10 years, and using his own tables given above, reversed the problem. Assuming the difference of level thus found, viz. 2066 metres, to be the true height of the layer of air between the two stations, and its weight being given by the barometrical observations, he deduced from these data its mean density, and from the density its mean temperature at every even hour in every month of the year. Comparing these mean temperatures with those given at the same hours by the half-sum of the temperatures taken at the upper and the lower station, he found the differences contained in Table XI., which are the corrections to be applied to the half-sums of the temperatures to obtain, in this particular case, the true mean temperatures. The second part of the table has been computed by multiplying each temperature in the first by 7.5 metres, in order to show the value of that correction in barometrical measurements.

TABLE XI.

CORRECTION TO BE APPLIED TO THE HALF-BUMS OF THE TEMPERATURES OF THE AIR, OBSERVED AT GENEVA AND AT THE GREAT ST. BERNARD, TO OBTAIN THE TRUE MEAN TEMPERATURE OF THE AIR BETWEEN THE TWO STATIONS.

Correction, in Centigrade Degrees, Sec													
Hour.	Jan.	Peb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year
Noon.	-0.5	° -1.7	-8.0	-8.9	° -4.1	° -4.4	° -4.4	-3.8	-2.7	° -1.6	-0.4	+0.7	° -2.
2	-0.2	-1.5	-2.8	-8.7	-4.0	-4.4	-4.4	-3.8	-2.6	-1.5	-0.2	+0.7	-2.
4	+0.4	-0.6	-1.6	-2.5	-2.7	-8.4	-8.6	-2.9	-1.7	-0.7	+0.4	+1.3	-1.
6	+1.2	+0.7	-0.2	-0.9	-1.8	-2.1	-2.2	-1.6	-0.5	+0.4	+1.3	+2.1	-0.
8	+1.5	+1.4	+0.6	0.0	0.0	-0.6	-0.7	-0.5	+0.3	+1.8	+1.7	+2.6	+0.
10	+1.7	+1.5	+1.2	+0.6	+0.7	+0.5	-0.1	+0.1	+0.8	+1.7	+1.8	+2.6	+1.
Mid-	+1.9	+1.8	+1.9	+1.8	+1.8	+1.6	+0.9	+1.2	+1.8	+2.3	+2.1	+2.5	+1.
night. 2	+2.0	+2.2	+2.5	+1.9	+2.2	+2.0	+1.5	+2.0	+1.9	+2.5	+2.4	+2.6	+2.
4	+2.8	+2.5	+2.6	+1.8	+1.7	+1.4	+1.1	+1.8	+2.1	+2.5	+2.7	+2.9	+2.
6	+2.0	+2.0	+1.7	+0.7	+0.4	+0.1	0.0	+0.7	+1.5	+1.7	+2.3	+2.9	+1.
8	+1.5	+1.1	0.0	-1.8	-2.0	-2.2	-2.4	-1.7	-0.4	+0.6	+1.7	+2.5	-0:
10	+0.4	-0.4	-2.0	-8.1	-8.5	-8.8	-3.7	-8.1	-2.0	-1.0	+0.8	+1.3	-1.
	+1.2	+0.8	+0.1	-0.8	-0.9	-1.2	-1.5	-0.9	-0.2	+0.7	+1.3	+2.1	0.0
Mean,				0.0	1			<u> </u>			<u> </u>		
Mean,		10.0			 	rection, I	<u> </u>						
Hour.	Jan.	Feb.	March.	April.	 		<u> </u>		Sept.	Oct.	Nov.	Dec.	Yee
Hour.	Jan.	Peb.	March.	April.	Cor	June.	July.	Aug.	Sept.			!	
Hour.	Jan 8.7	Feb12.7	March.	April.	May. -80.7	June.	July.	Aug.	Sept20.2	-12.0	- 3.0	+ 5.2	<u>-18</u>
Hour.	Jan 8.7 - 1.5	Feb12.7 -11.2	March22.5 -21.0	April29.2 -27.7	May80.7	June83.0	July83.0	Aug28.5 -28.5	Sept20.2 -19.5	-12.0 -11.2	- 8.0 - 1.5	+ 5.2 + 5.2	-18. -17.
Hour. Noon. 2	Jan 8.7 - 1.5 + 3.0	Feb12.7 -11.2 - 4.5	March22.5 -21.0 -12.0	April29.2 -27.7 -18.7	May80.7 -30.0	June83.0 -38.0 -25.5	July83.0 -27.0	Aug28.5 -28.5 -21.7	Sept20.2 -19.5 -12.7	-12.0 -11.2 - 5.2	- 8.0 - 1.5 + 8.0	+ 5.2 + 5.2 + 9.7	-18 -17 -11
Hour. Noon. 2 4	Jan 8.7 - 1.5	Feb12.7 -11.2	March22.5 -21.0 -12.0	April29.2 -27.7 -18.7 - 6.7	May80.7	June83.0 -38.0	July83.0	Aug28.5 -28.5 -21.7 -12.0	Sept20.2 -19.5	-12.0 -11.2 - 5.2	- \$.0 - 1.5 + \$.0 + 9.7	+ 5.2 + 5.2 + 9.7 +15.7	-18 -17 -11 - 2
Hour. Noon. 2	Jan 3.7 - 1.5 + 3.0 + 9.0	Feb12.7 -11.2 - 4.5 + 5.2 +10.5	March22.5 -21.0 -12.0 - 1.5 + 4.5	April29.2 -27.7 -18.7	May80.7 -30.0 -20.2 - 9.7	June33.0 -38.0 -25.5 -15.7	July83.0 -27.0 -16.5 - 5.2	Aug28.5 -28.5 -21.7	Sept. -20.2 -19.5 -12.7 - 3.7	-12.0 -11.2 - 5.2 + 8.0 + 9.7	- 3.0 - 1.5 + 3.0 + 9.7 +12.7	+ 5.2 + 5.2 + 9.7	-18. -17. -11. - 2. + 4.
Hour. Noon. 2 4 6 8 10	Jan 8.7 - 1.5 + 3.0 + 9.0 +11.2 +12.7	Feb12.7 -11.2 - 4.5 + 5.2 +10.5 +11.2	March22.5 -21.0 -12.0 - 1.5 + 4.5 + 9.0	April29.2 -27.7 -18.7 - 6.7 0.0 + 4.5	May. -80.7 -30.0 -20.2 - 9.7 0.0 + 5.2	June. -33.0 -33.0 -25.5 -15.7 - 4.5 + 3.7	July83.0 -83.0 -27.0 -16.5 - 5.2 - 0.7	Aug28.5 -28.5 -21.7 -12.0 - 8.7 + 0.7	Sept. -20.2 -19.5 -12.7 - 3.7 + 2.2 + 6.0	-12.0 -11.2 - 5.2 + 8.0 + 9.7 +12.7	- 8.0 - 1.5 + 8.0 + 9.7 +12.7 +13.5	+ 5.2 + 5.2 + 9.7 +15.7 +19.5 +19.5	-18 -17 -11 - 2 + 4 + 8
Hour. Noon. 2 4 6 8 10 Midnight.	Jan 8.7 - 1.5 + 8.0 + 9.0 +11.2 +12.7	Feb12.7 -11.2 - 4.5 + 5.2 +10.5 +11.2	March22.5 -21.0 -12.0 - 1.5 + 4.5 + 9.0	April29.2 -27.7 -18.7 - 6.7 0.0 + 4.5	May. -80.7 -30.0 -20.2 - 9.7 0.0 + 5.2	June33.0 -33.0 -25.5 -15.7 - 4.5 + 3.7	July83.0 -83.0 -27.0 -16.5 - 5.2 - 0.7 + 6.7	Aug28.5 -28.5 -21.7 -12.0 - 8.7 + 9.0	Sept20.2 -19.5 -12.7 - 3.7 + 2.2 + 6.0 + 9.7	-12.0 -11.2 - 5.2 + 8.0 + 9.7 +12.7	- 3.0 - 1.5 + 3.0 + 9.7 +12.7 +13.5	+ 5.2 + 5.2 + 9.7 +15.7 +19.5 +19.5	-18 -17 -11 - 2 + 4 + 8
Hour. Noon. 2 4 6 8 10 Midnight.	Jan 8.7 - 1.5 + 8.0 + 9.0 + 11.2 + 12.7 + 14.5	Feb12.7 -11.2 - 4.5 + 5.2 +10.5 +11.2 +18.5	March22.5 -21.0 -12.0 - 1.5 + 4.5 + 9.0 +14.5 +18.7	April29.2 -27.7 -18.7 - 6.7 0.0 + 4.5 + 9.7 +14.2	May. -80.7 -30.0 -20.2 - 9.7 0.0 + 5.2 +18.5 +16.5	June. -83.0 -83.0 -25.5 -15.7 - 4.5 + 8.7	July83.0 -83.0 -27.0 -16.5 - 5.2 - 0.7 + 6.7 +11.2	Aug28.5 -28.5 -21.7 -12.0 - 8.7 + 0.7 + 9.0 +15.0	Sept. -20.2 -19.5 -12.7 - 8.7 + 2.2 + 6.0 + 9.7 +14.2	-12.0 -11.2 - 5.2 + 8.0 + 9.7 +12.7 +17.2	- 8.0 - 1.5 + 8.0 + 9.7 +12.7 +13.5 +15.7	+ 5.2 + 5.2 + 5.2 + 9.7 +15.7 +19.5 +19.5	-18. -17. -11. - 2. + 4. + 8. +12.
Hour. Noon. 2 4 6 8 10 Midnight. 2	Jan 8.7 - 1.5 + 8.0 + 9.0 + 11.2 + 12.7 + 14.5 + 15.0 + 17.2	Feb12.7 -11.2 - 4.5 + 5.2 +10.5 +11.2 +18.5 +16.5	March22.5 -21.0 -12.0 - 1.5 + 4.5 + 9.0 +14.5 +18.7	April29.2 -27.7 -18.7 - 6.7 0.0 + 4.5 + 9.7 +14.2 +13.5	Cor May. -80.7 -30.0 -20.2 - 9.7 0.0 + 5.2 +18.5 +16.5 +12.7	June. -83.0 -83.0 -25.5 -15.7 - 4.5 + 8.7 +12.0 +15.0 +10.5	July83.0 -83.0 -27.0 -16.5 - 5.2 - 0.7 + 6.7 + 11.2 + 8.2	Aug28.5 -28.5 -21.7 -12.0 - 8.7 + 0.7 + 9.0 +15.0 +13.5	Sept. -20.2 -19.5 -12.7 - 8.7 + 2.2 + 6.0 + 9.7 +14.2 +15.7	-12.0 -11.2 - 5.2 + 8.0 + 9.7 +12.7 +17.2 +18.7 +18.7	- 8.0 - 1.5 + 8.0 + 9.7 +12.7 +18.5 +15.7 +18.0 +20.2	+ 5.2 + 5.2 + 9.7 +15.7 +19.5 +19.5 +19.5 +21.7	-18. -17. -11. - 2. + 4. + 8. +12. +16. +15.
Hour. Noon. 2 4 6 8 10 Mid-night. 2 4 6	Jan. - 8.7 - 1.5 + 3.0 + 9.0 + 11.2 + 12.7 + 14.5 + 15.0 + 17.2 + 16.0	Feb. -12.7 -11.2 - 4.5 + 5.2 +10.5 +11.2 +18.5 +16.5	March22.5 -21.0 -12.0 - 1.5 + 4.5 + 9.0 +14.5 +18.7 +19.5	April29.2 -27.7 -18.7 - 6.7 0.0 + 4.5 + 9.7 +14.2 +13.5 + 5.2	Cor May. -80.7 -30.0 -20.2 - 9.7 0.0 + 5.2 +18.5 +16.5 +12.7 + 3.0	June. -33.0 -33.0 -25.5 -15.7 - 4.5 + 3.7 +12.0 +15.0 + 10.5 + 0.7	July33.0 -33.0 -27.0 -16.5 - 5.2 - 0.7 + 6.7 + 11.2 + 8.2 0.0	Aug. -28.5 -28.5 -21.7 -12.0 - 8.7 + 0.7 + 9.0 +15.0 +13.5 + 5.2	Sept. -20.2 -19.5 -12.7 - 3.7 + 2.2 + 6.0 + 9.7 +14.2 +15.7 +11.2	-12.0 -11.2 - 5.2 + 8.0 + 9.7 +12.7 +17.2 +18.7 +18.7 +12.7	- 3.0 - 1.5 + 3.0 + 9.7 +12.7 +13.5 +15.7 +18.0 +20.2 +17.2	+ 5.2 + 5.2 + 9.7 +15.7 +19.5 +19.5 +18.7 +19.5 +21.7	-18 -17 -11 - 2 + 4 + 8 +12 +16 +15 + 9
Hour. Noon. 2 4 6 8 10 Midnight. 2	Jan 8.7 - 1.5 + 8.0 + 9.0 + 11.2 + 12.7 + 14.5 + 15.0 + 17.2	Feb12.7 -11.2 - 4.5 + 5.2 +10.5 +11.2 +18.5 +16.5	March22.5 -21.0 -12.0 - 1.5 + 4.5 + 9.0 +14.5 +18.7 +19.5	April29.2 -27.7 -18.7 - 6.7 0.0 + 4.5 + 9.7 +14.2 +13.5 + 5.2	Cor May. -80.7 -30.0 -20.2 - 9.7 0.0 + 5.2 +13.5 +16.5 +12.7 + 3.0 -15.0	June. -83.0 -83.0 -25.5 -15.7 - 4.5 + 8.7 +12.0 +15.0 +10.5	July83.0 -83.0 -27.0 -16.5 - 5.2 - 0.7 + 6.7 + 11.2 + 8.2	Aug. -28.5 -28.5 -21.7 -1.2.0 -1.7 + 0.7 + 9.0 +15.0 +13.5 + 5.2 -12.7	Sept. -20.2 -19.5 -12.7 - 8.7 + 2.2 + 6.0 + 9.7 +14.2 +15.7	-12.0 -11.2 - 5.2 + 8.0 + 9.7 +12.7 +17.2 +18.7 +18.7 +18.7 + 4.5	- 3.0 - 1.5 + 3.0 + 9.7 +12.7 +13.5 +15.7 +18.0 +20.2 +17.2	+ 5.2 + 5.2 + 9.7 +15.7 +19.5 +19.5 +18.7 +19.5 +21.7 +21.7	-18 -17 -11 - 2 + 4 + 8 +12 +16 +15 + 9

THE elevation of a place in the interior of a continent where regular meteorological observations are made, may be ascertained by taking the yearly means of the barometer reduced to the freezing point, and of the temperature of the air, as data for the upper station, and the yearly means of the reduced barometer and of the free thermometer at the level of the sea, as the data for the lower station. The Hypsometric Tables then will give the difference of level. As observation, however, has shown that the mean height of the barometer at the level of the sea is not the same in all latitudes, it is necessary to take for such a comparison the mean height of the barometer which belongs to the latitude of the station the elevation of which is to be computed, or that which is nearest to it.

Table XII., published by Schouw, in Poggendorf's Annalen, and in the Comptes Rendus de l'Académie des Sciences, Tom. III. p. 573, gives in Paris lines the mean height of the barometer in various latitudes. The reduction into millimetres is from Martins's French translation of Kaemtz's Meteorology, p. 278; the corresponding values in English inches, and the new stations, Savannah, Ga., Philadelphia, Pa., and Cambridge, Mass., have been added. The mean heights last mentioned have been derived from three years of observations at Savannah, by Dr. John F. Posey, from June, 1853, to June, 1856, published in the American Almanac; from four years of hourly observations at Girard College, Philadelphia, by Prof. A. D. Bache; and from ten years of observations at Cambridge Observatory. They have been reduced to a common absolute standard and to mean tide-water at the respective places.

These mean barometric heights, corrected for the variation of gravity in latitude, according to the proposition of Poggendorf, by the formula b=b 45 (1 — 0.0025935 cos 2 ϕ), where b is the height of the barometer in latitude ϕ , and b 45 the corresponding height at the forty-fifth degree of latitude, are found in another column. For computing the elevations, the uncorrected heights are to be used.

The mean barometric pressure, as shown by Table XIII. from Kaemtz's *Précis de Météorologie*, French translation, p. 281, is not the same in all seasons, and the monthly means differ by a quantity which also varies with the latitude. If, therefore, the height of an inland station is to be ascertained from the barometrical means of one or more months only, the computation must be made with the mean pressure in the corresponding months at the level of the sea; or if this is not known, the yearly means taken from Table XII. must be corrected for the difference between the monthly means of the given month, or months, and the annual mean in the same latitude, as derived from the comparison of the numbers in Table XIII.

Example.

Suppose an inland station, in latitude 40° N.; the mean barometric pressure for July is 26.30 inches, and its elevation is to be computed from it.

Table XII. gives for latitude 40°, at Philadelphia, reduced to the level of the sea, 30.053 inches. Table XIII. gives as the mean for July, at the same place, 759.80 millimetres, and for the year, 760.25 millimetres (both not reduced to the level of the sea), difference — 0.45 millimetres = — 0.017 English inches, which is to be subtracted from the annual mean, 30.053, to reduce it to the mean of July; or

n

30.053 - 0.017 = 30.036. This last number is to be used in the computation, with the mean temperature of July at both stations.

Towards the tropical regions, the irregular or non-periodic variations of the barometer, which in high and middle latitudes are so considerable as to render simultaneous observations indispensable for the measurement of heights, gradually decrease and nearly cease to exist, while the monthly and daily periodic variations, which are small in high latitudes, considerably increase. Within the tropics, therefore, the oscillations of the barometer being far more uniform, observations made during a short period of time, or even single observations, may be used for computing heights, without corresponding observations, by referring them to the mean pressure at the level of the sea as to a constant, provided this last has been corrected for the monthly and daily periodic variation at the place.

Table XIII. furnishes the means of applying the correction for the monthly variation, as described above. Table XIV., which gives the mean height of the barometer at all hours of the day in various latitudes, enables the observer to correct the data according to the hour at which the observations have been taken. This table is from Kaemtz's Vorlesungen über Meteorologie, French translation, p. 249. The column Bossekop is from the observations of the French Scientific Expedition in the North; the column Philadelphia, from the observations at Girard College, has been added.

The correction for the hourly variation is found by taking the difference between the mean of the hour of observation and the daily mean, and correcting accordingly, with due regard to the signs, either the yearly mean at the sea level, or the observation at the upper station.

Example.

The barometer at Caracas, latitude 10° 30' N., on the 20th of August, at 4 o'clock P. M., reads 680.57 millimetres.

which is the number to be used for the computation of the height of Caracas. In this case, however, the monthly correction, being derived from a higher latitude, may be too small. Both corrections can of course be applied, with contrary signs, to the observation at Caracas, leaving then the mean height at the level of the sea as a constant.

TABLE XII.

MEAN HEIGHT OF THE BAROMETER,

IN VARIOUS LATITUDES, REDUCED TO THE LEVEL OF THE SEA, AND TO THE FREEZING POINT.

		In Mill	metres.	In Englis	h Inches.	In Par	is Lipes.
Places.	Latitude.	Observed.	Corrected for Gravity.	Observed.	Corrected for Gravity.	Observed.	Corrected for Gravity.
Cape of Good Hope,	o , 33 S.	763.01	762.20	30.041	20.006	388.24	337.88
Rio Janeiro, Brazil,	23 8.	764.03	762.65	80.080	80.026	338.69	238.08
Christiansborg, Guinea,	5 80N.	760.10	758.16	29.925	29.850	886.95	836.09
La Guayra, Venezuela,	10	760.17	758.22	29,928	29.855	386.98	836.16
St. Thomas, W. Indies,	19	760.51	758.95	29.942	29.881	837 18	886.44
Macao, China,	28	762.99	761.61	80.040	29.986	888.23	837.62
Teneriffe, Canary Isles,	28	764.21	763.10	80.087	80.044	838.77	838.28
Savannah, Georgia,	32	764.59	763.74	30.102	80.070	838.93	888.57
Funchal, Madeira,	82 30	765.18	764.34	80.126	30.093	839.20	338.88
Tripoli, Northern Africa,	28	767.41	766.60	30.214	80.182	840.19	889.88
Palermo, Sicily,	38	762.95	762.47	30.088	30.019	338.21	388.00
Philadelphia, Penn.	40	763.35	763.00	80.053	80.040	338.38	338.23
Naples, Italy,	41	762.84	762.06	80.014	80.008	387.94	337.82
Cambridge, Mass.	42	762.44	762.24	80.018	80.010	3 37.99	337.90
Florence, Italy,	48 80	761.98	761.81	29.997	29.998	837.76	837.71
Avignon, France,	44	762.02	761.95	30.001	29.998	837.80	837.77
Bologna, Italy,	44 30	762.18	762.13	30.007	30.003	837.87	887.85
Padua, Italy,	45	762.18	762.18	30.007	30.007	337.87	\$37.87
Paris, France,	49	761.41	761.68	29.978	29.988	837.53	337.65
London, England,	51 80	760.96	761.41	29.960	29.978	337.33	387.53
Altona, Denmark,	58 30	760.42	761.01	29.988	29.961	8 37.09	337.35
Dantxig, Prussia,	54 80	760.10	760.76	29.925	29.952	386.95	837.24
Königsberg, Prussia,	54 80	760.49	761.14	29.941	29.967	837.12	387.41
Apenrade, Denmark,	55	759.58	760.71	29.906	29.950	836.72	837.22
Edinburgh, Scotland,	56	758.25	759.00	29.853	29.882	886.13	836.46
Christiania, Norway,	60	758.64	759.63	29.868	29.908	336.30	836.74
Hardanger, Norway,	60	756.94	757.04	29.801	29.841	335.55	335.99
Bergen, Norway,	60	757.01	758.00	29.804	29.844	385.58	836.02
Reikiavig, Iceland,	64	752.00	753.20	29.607	29.654	\$83.36	333.89
Godthaab, S. Greenland,	64	751.94	753.13	29.603	29.651	833.88	333.86
Eyafiord, Iceland,	66	758.58	754.89	29.669	29.721	334.06	834.64
Godhavn, Disco, Greenl.	68	753.76	755.16	29.677	29.731	884.14	834.76
Upernavik, N. Greenl.	78	755.18	756.80	29.782	29.796	831.77	335.49
Melville Isl., Arct. Amer.	74 80	757.08	758.75	29.807	29.872	835.61	836.85
Spitzbergen,	75 80	756.76	758.48	29.794	29.862	335.47	836.28

XIII. MEAN HEIGHT OF THE BAROMETER, IN ALL MONTHS OF THE YEAR, IN VARIOUS LATITUDES.

Not reduced to the Level of the Sea.

Places,	HAVANA.	CAL- CUTTA.	MACAO.	CAIRO.	BA- VANNAM.	PHILA- DELPHIA.	CAM- BRIDGE.	PARIS.	St. Pr- trassurg
Latitude,	230 9/	220 33/	22° 11′	30° 2′	320 5'	39° 58′	42° 23′	48° 50'	590 56'
		<u>'</u>							
Jan.	765.24	764.57	767.93	762.40	762.80	760.97	761.87	758.86	762.54
Feb.	760-15	758.86	767.01	66	763.76	759.63	760.90	759.09	763.10
March,	760.98	756.24	766.08	759.43	763.05	760.51	759.09	756.83	760.76
April,	759.58	753.83	761.93	760.10	763.10	760.05	759.37	755.18	761.19
May,	758.19	750.81	761.64	758.28	763.39	759.09	759.63	755.61	760.94
June,	760.67	748.10	757.81	754.42	764.87	759.22	758.91	757.28	759.63
July,	760.67	747.54	757.91	753.90	764.02	759.80	760.84	756.52	758.25
Aug.	757.33	748.53	757.91	754.06	765.54	760.54	761.11	756.74	759.94
Sept.	757.46	751.88	762.22	756.70	763.36	761.25	761.83	756.61	761.19
Oct.	758.19	755.25	763.87	759.70	763.13	760.68	761.07	754.42	760.92
Nov.	761.25	758.37	766.17	760.76	763.41	760.49	760.85	755.75	758.05
Dec.	763.62	760.59	768.65	761.82	761.12	760-82	760.80	755.09	760.22
Year,	760.28	754.54	768.18	758.82	763.41	760.25	760.44	756.46	760.57

XIV. MEAN HEIGHT OF THE BAROMETER, AT ALL HOURS OF THE DAY, IN VARIOUS LATITUDES.

Not reduced to the Level of the Sea.

Places,	Pacific Ocean.	CUMARA.	LA GUAYRA.	CAL- CUTTA.	PHILADEL-	PADUA.	HALLE.	St. Pr-	Boserkor
Latitude,	00 0'	10° 28'n.	10° 36′#.	22° 35′n.	39° 58'n.	45° 24'n.	51° 29'n.	59° 56'n.	69° 58'x
Observers,	Horner.	Hum- boldt.	Boussin- gault.	Belfour.	Bache.	Ciminello.	Kaemts.	Kupffer.	Bravais.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Milling.
Midnight,	752.47	756.86	759.64	756.80	760.49	757.01	753.23	759.35	754.90
1	752.20	756.53	759.34	758.62	760.46	756.90	758.14	"	66
2	731.77	756.21	759.05	758.57	760.41	756.84	758.05	759.32	754.79
8	751.63	755.89	758.81	758.49	760.34	756.78	752.99	"	66
4	751.32	755.66	758.68	758.47	760.39	756.74	752.99	759.32	754.70
5	751.65	755.79	758.85	758.44	760.49	756.75	753.84	66	44
6	751.95	756.18	759.82	758.68	760.75	756.79	753.12	759.39	754.68
7	752.48	756.58	759.94	759.16	761.00	756.89	753.24	66	44
8	752.95	756.98	760.50	759.88	761.15	757.01	753.37	759.49	754.75
9	753.16	757.31	759.63	760.11	761.22	757.08	758.44	66	66
10	753.15	757.32	760.50	760.19	761.17	757.14	753.46	759.51	754.96
11	752.80	757.01	759.99	760.09	760.97	757.07	753.40	46	66
Noon,	752.85	756.57	759.41	759.61	760.56	757.02	753.29	759.47	755.01
1	751.87	755.99	758.91	759.22	760.13	756.85	753.11	**	64
2	751.55	755.47	758.41	758.89	759.83	756.67	752.99	759.38	754.96
3	751.15	755.14	758.12	758.12	759.65	756.54	752.89	66	"
4	751.02	754.96	758.05	757.91	739.65	756.47	753.84	759.82	754.82
5	751.81	755.14	758.10	757.98	759.70	756.46	752-86	66	46
6	751.71	755.41	758.40	758.01	759.85	756.50	752.91	759.31	754.87
7	731.93	755.81	758.90	758.02	760.08	756.63	753.02	66	66
8	752.85	756.21	759.19	758.54	760.31	756.79	758.14	759.32	754.99
9	752.74	756.59	759.69	759.24	760.49	756.92	758.24	46	66
10	752.85	756.87	759.93	759.33	760.59	757.02	753.81	759.36	754.92
11	752.86	757.15	759.98	759.09	760.72	757.02	758.29		66
Mean,	752.18	756.83	759.22	758.87	760.43	756.83	758.19	759.38	754.85

Table XIV. shows that, after all irregular variations of the barometer have been eliminated, there remains a double period of rise and fall within the twenty-four hours, and that the amplitude of these daily oscillations is greatest within the tropics, and goes on diminishing towards the polar regions.

According to Kaemtz, the mean time of the daily maxima and minima, or the mean tropic hours for the northern hemisphere, are as follows:—

The minimum of the afternoon is reached at The maximum of the evening is reached at The minimum of the night is reached at The maximum of the morning is reached at The maximum of the morning is reached at The maximum of the morning is reached at The maximum of the morning is reached at The maximum of the morning is reached at The maximum of the morning is reached at The maximum of the afternoon is reached at The maximum of the afternoon is reached at The maximum of the evening is reached at The maximum of the maximum of the morning is reached at The maximum of the evening is reached at The maximum of the maximum o

Even in temperate and high latitudes these diurnal variations, though small, must be taken into account, if great accuracy is required, in reducing corresponding observations made at a somewhat different hour to the time of the observation at the station the height of which is to be determined. But in so doing, it must be remembered that the times of the minima and maxima change with the seasons, as is shown by Table XV. from Kaemtz, p. 251 of the French translation.

XV. TROPIC HOURS OF THE DAILY VARIATION OF THE BAROMETER AT HALLE.

LAT. 51° 80' N.

Month.	Minimum, P. M.	Maximum, P. M.	Minimum, A. M.	Maximum, A. M.	Month.	Minimum, P. M.	Maximum, P. M.	Minimum, A. M.	Maximum, A. M.
	b.	h.	ь.	h.		h.	h.	h.	h.
Jan.	2.81	9.17	4.91	9.91	July,	5.21	11.04	8.04	8.78
Feb.	3.43	9.46	3.86	. 9.66	Aug.	4.86	10.66	3.06	8.96
March,	3.82	9.80	8.87	10.10	Sept.	4.55	10.45	3.45	9.71
April,	4.46	10.27	3.53	9.53	Oct.	4.17	10.24	3.97	10.07
May,	5.43	10.93	8.08	9.13	Nov.	8.52	9.85	4.68	10.08
June,	5.20	10.93	2.83	8.78	Dec.	8.15	9.11	4.91	10.18

This shifting of the times of maxima and minima with the seasons diminishes with the latitude, and tends to disappear towards the equator, with the inequality of the days and nights. The elevation above the level of the sea also causes a change in the tropic hours of the daily variation which is not yet sufficiently studied.

Table XIV. gives evidence that the amplitude of the hourly oscillation is greatest under the equator, and gradually decreases towards the pole. Kaemtz computes its mean value in various latitudes and at the level of the sea, as follows:—

XV'. AMPLITUDE OF DAILY VARIATIONS IN VARIOUS LATITUDES.

Latitude.	Variation.	Latitude.	Variation.	Latitude.	Variation.	Latitude	Variation.
° 0	Millim. 2.28	28 55	Millim. 1.80	0 / 89 4	Millim. 1.13	52 88	Millm. 0.45
5 26 N.	2.26	29 28	1.58	48 84	0.90	57 17	0.23
17 52	2.03	34 26	1.85	48 1	0.67	62 25	0.00

The amplitude also decreases with the elevation, at least in our latitudes; it was found to be on the Faulhorn, in Switzerland, 9000 feet above the sea level, 0.27 millimetres, while it was 0.90 millimetres at Geneva.

TABLES

FOR REDUCING BAROMETRICAL OBSERVATIONS TO THE LEVEL OF THE SEA, OR TO ANOTHER LEVEL.

To reduce barometric means taken at a given elevation to the height they would have if taken at the level of the sea, or barometric observations made at different elevations to a common level, in order to eliminate the influence of altitude in the comparison of barometric pressures, is a problem, the solution of which is often needed in meteorology.

For a complete and accurate reduction, embracing all cases, Tables IV. and V., by Dippe, given above, pages 54 et seq., may be used. But when the difference of height between the two stations, or above the sea-level, does not exceed a few hundred feet, the small tables XVI. to XIX., in three different scales, will be found more convenient.

Tables XVI. and XVII. have been computed from the constants of Laplace's formula, the barometric coefficient, including the correction for the decrease of gravity on a vertical, being respectively 60,345.51 English feet and 56,621.83 Paris feet; and the coefficient for expansion of moist air 0.00222 and 0.005.

In Table XVIII. the coefficient 18,420 metres, deduced from Regnault's experiments (see *Proceedings of the Amer. Assoc. for Adv. of Science*, 1857), and his coefficient for expansion of dry air, 0.003665, increased to 0.0039, in order to include the effect of moisture, have been used.

USE OF THE TABLES.

The correction for reducing the barometer to the level of the sea is found by the formula

$$C = \frac{f}{N} \times \frac{h'}{\lambda},$$

where C is the correction required; f, the elevation of the station; N, the number in the tables; h', the reading of the barometer; h, the normal height of barometer at the sea-level.

Example.

At Cambridge Observatory, Massachusetts, at 71.34 English feet above mean tide, the mean barometer is = 29.939 inches; the mean temperature 47°.3 Fahrenheit; what would be the height at the level of the sea?

In Table XVI. we take for $47^{\circ}.3 = 90.49$, or, in order to get the correction in a fraction of an inch, 904.9.

Then

$$C = \frac{71.34}{904.9} \times \frac{29.939}{30} = 0.079$$
, correction required;

and

29.939 + 0.079 = 30.018 inches, height of the barometer at the level of the sea.

It will be seen that the quantity represented by the second member can be neglected without causing a sensible error in the correction. In this case the error does not amount to .001; it scarcely would reach .002 for 250 feet of elevation; so that the reduction can be made in most cases by a simple division; viz. $\frac{f}{N}$.

EVI. HEIGHT, IN ENGLISH FEET, OF A COLUMN OF AIR CORRESPONDING TO A TENTH OF AN ENGLISH INCH IN THE BAROMETER, AT TEMPERATURES BETWEEN 32° AND 100° FAHRENHEIT,

The Barometric Pressure at the Lower Station being = 30 English Inches.

Temper- ature of Air, Fahren.	Height in English Feet.	Temper- ature of Air, Fahren.	Height in English Feet.	Temper- ature of Air, Fahren.	Height in English Feet.	Temper- ature of Air, Fahren.	Height in English Feet.	Temper- ature of Air, Fahren.	Height in English Feet.
32°	87.51	46°	90.28	60°	92.95	74°	95.67	87°	98.20
23	87.70	47	90.42	61	98.15	75	95.87	88	98.40
34	87.90	48	90.62	62	98.84	76	96.06	89	98.59
83	88.09	49	90.81	68	98.58	77	96.26	90	98.79
36	88.28	50	91.01	64	98.73	78	96.45	91	98.98
87	88.48	51	91.20	65	98.92	79	96.65	92	99.17
88	88.67	52	91.40	66	94.12	80	96.84	98	99.87
39	88.87	53	91.59	67	94.81	81	97.04	94	99.56
40	89.06	54	91.78	68	94.51	82	97.28	95	99.76
41	89.26	55	91.98	69	94.70	88	97.42	96	99.95
42	89.45	56	92.17	70	94.90	84	97.62	97	100.15
48	89.65	57	92.87	71	95.09	85	97.81	98	100.34
44	89.84	58	92.56	72	95.29	86	98.01	99	100.54
45	90.08	59	92.76	73	95.48	87	98.20	100	100.73

XVIL HEIGHT, IN FRENCH PEET, OF A COLUMN OF AIR COERESPONDING TO A PARIS LINE IN THE BAROMETER, AT TEMPERATURES OF THE AIR BETWEEN 0° AND 34° REAUMUR,

The Barometric Pressure at the Lower Station being = 887 Paris Lines.

Temper- ature of Air, Resumur.	Height in French Feet.	Temper- ature of Air, Resumur.	Height in French Feet.	Temper- ature of Air, Reaumur.	Height in French Foot.	Temper- ature of Air, Resumur.	Height in French Feet.	Temper- ature of Air, Resumur.	Height in French Feet.
	78.08	7°	75.68	14°	78.19	21°	80.75	28°	88.81
1	78.44	8	76.00	15	78.56	22	81.11	29	83.67
2	78.81	9	76.36	16	78.92	23	81.48	80	84.04
8	74.17	10	76.78	17	79.29	24	81.85	81	84.40
4	74.54	11	77.10	18	79.65	25	82.21	82	84.77
5	74.90	12	77.46	19	80.02	26	82.58	. 88	85.13
6	75.27	18	77.83	20	80.88	27	82.94	84	85.50

EVIII. HEIGHT, IN METRES, OF A COLUMN OF AIR CORRESPONDING TO A MILLIMETRE IN THE BAROMETER, AT TEMPERATURES BETWEEN 0° AND 89° CENTIGRADE,

The Berometric Pressure at the Lower Station being = 760 Millimetres.

Temper- ature of Air, Centigr	Height in Metres.	Temper- ature of Air, Centigr.	Height in Metres	Temper- ature of Air, Centigr.	Height in Metres.	Temper- ature of Air, Centigr.	Height in Metres.	Temper- ature of Air, Centigr.	Height in Metres.
0°	10.54	8°	10.86	16°	11.19	24°	11.52	32°	11.85
1	10.58	9	10.91	17	11.28	25	11.56	88	11.89
2	10.62	10	10.95	18	11.28	26	11.60	34	11.93
3	10.66	11	10.99	19	11.82	27	11.64	85	11.97
4	10.70	12	11.08	20	11.86	28	11.69	86	12.01
5	10.74	18	11.07	21	11.40	29	11.78	87	12.06
6	10.78	14	11.11	22	11.44	80	11.77	38	12.10
7	10.82	15	11.15	23	11.48	81	11.81	89	12.14

BARONETRICAL MEASUREMENT OF HEIGHTS.

Table XIX. gives, in metrical measure, the values of a millimetre in the barometer at different elevations and Centigrade temperatures. The values are derived from Laplace's constants, as in Tables XVI. and XVII.

This table may be used, as the preceding ones, for reducing barometrical observations to the level of the sea, and also to any other level by a similar process.

Example.

Suppose the barometer to read 700 millimetres at the altitude of 750 metres, the temperature of air being = 16° Centigrade; what would be the reading at a station lower by 350 metres, assuming the temperature of the air downwards to increase at the rate of 1° Centigrade for 185 metres?

The temperature of air at lower station will be $16^{\circ} + 1^{\circ}.9 = 17^{\circ}.9$

The approximate height of barometer about 73 centimetres.

Then, in Table XIX. we find for 16° and 70 centimetres,
" for 17°.9 and 73 centimetres,
11.73

Mean 11.94

And

D

 $\frac{350}{11.94}$ = 29.31, or barometer at lower station 700 + 29.31 = 729.31 millimetres.

Delcros's tables, with these data, would give for the difference of level 349.76, instead of 350 metres; the corresponding error in the height of the barometrical column does not exceed 0.08 millimetre, and thus remains within the limits of error which may be expected in an ordinary observation.

The principal object of this table, however, is to furnish the scientific traveller with the means of readily computing on the spot approximate differences of level, by simply multiplying the difference between the readings of the barometer at each station by the half sum of the numbers in the table corresponding to the data given by the observations.

Example.

Suppose the barometer at the lower station to read 732.5, and at the upper station 703.2 millimetres; the temperature of the air being respectively 18° and 16° Centigrade.

The difference of the barometers, supposed to be reduced to the same temperature, is 29.3 millimetres.

Then, Table XIX. gives for 18° Centigrade and 73 centimetres, 11.73

" for 16° Centigrade and 70 centimetres, 12.15

Half sum, or mean, 11.94

And, $29.3 \times 11.94 = 349.8$ metres = difference of level required.

By the large tables of Delcros, we find for the same data 350.1 metres.

This table can be considered as a complement to Delcros's tables, and may save the traveller the trouble of carrying the larger tables.

A similar table in English measures is found above, at the end of the author's larger tables (Table VI.), page 48 of this series, and another, more extensive one, below, page 92, the use of which is explained by the examples just given.

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XIX. HEIGHT, IN METRES, OF A COLUMN OF AIR, CORRESPONDING TO A MILLIMETRE IN THE BARONETER, AT DIFFERENT TEMPERATURES AND ELEVATIONS.

Temper- sture of			Barome	eter at the	Lower Sta	tion, Readi	ing in Cont	imetres.		
Air, Centig.	76	75	74	78	79	71	70	69	68	67
•	Motres.	Metres.	Metres.	Metres.	Metres.	Metres.	Motres.	Metres.	Motres.	Metre
0	10.52	10.66	10.80	10.94	11.10	11.26	11.42	11.59	11.75	11.9
2	10.60	10.74	10.89	11.08	11.19	11.85	11.51	11.68	11.85	12.0
4	10.69	10.88	10.97	11.12	11.28	11.44	11.60	11.77	11.94	12.1
6	10.77	10.91	11.06	11.20	11.87	11.53	11.69	11.86	12.04	12.2
8	10.85	11.00	11.15	11.29	11.46	11.62	11.78	11.96	12.18	12.9
10	10.94	11.08	11.23	11.88	11.55	11.71	11.87	12.05	12.22	12.4
12	11.02	11.17	11.82	11.47	11.63	11.80	11.97	12.14	12.82	12.5
14	11.11	11.25	11.41	11.55	11.72	11.89	12.06	12.23	12.41	12.6
16	11.19	11.34	11.49	11.64	11.81	11.98	12.15	12.83	12.51	12.7
18	11.27	11.48	11.58	11.78	11.90	12.07	12.24	12.42	12.60	12.7
20	11.86	11.51	11.67	11.82	11.99	12.16	12.88	12.51	12.69	12.8
22	11.44	11.60	11.75	11.90	12.08	12.25	12.42	12.61	12.79	12.9
24	11.58	11.68	11.84	11.99	12.17	12.34	12.51	12.70	12.88	13.0
26	11.61	11.77	11.98	12.08	12.26	12.48	12.61	12.79	12.98	13.1
28	11.70	11.85	12.01	12.17	12.35	12.52	12.70	12.88	18.07	13.2
80	11.78	11.94	12.10	12.25	12.48	12.61	12.79	12.98	13.16	18.3
32	11.86	12.02	12.18	12.84	12.52	12.70	12.88	13.07	13.26	13.4
84	11.95	12.11	12.27	12.43	12.61	12.79	12.97	13.16	13.35	13.5
86	12.03	12.19	12.86	12.52	12.70	12.88	18.06	18.25	13.45	13.6
38	12.12	12.28	12.44	12.60	12.79	12.97	13.15	13.33	13.54	13.7
emper-				Ba	rometer in	Centimetr	te.			
ture of										1
Centig.	66	65	64	68	62	61	60	59	58	57
•	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metre
.0	12.11	12.80	12.49	12.69	12.89	13.10	13.32	13.55	18.78	14.0
2	12.21	12.40	12.59	12.79	13.00	13.21	13.43	13.66	13.89	14.1
4	12.31	12.50	12.69	12.89	13.10	18.31	13.54	18.77	14.00	14.2
6	12.40	12.60	12.79	13.00	13.20	18.42	13.64	13.88	14.11	14-8
8	12.50	12.69	12.89	13.10	13.81	13.52	18.75	18.99	14.22	14.4
10	12.60	12.79	12.99	13.20	13.41	13.68	18.86	14.09	14.84	14.5
12	12.69	12.89	18.09	13.30	18.51	13.73	13.96	14.20	14.45	14.7
14	12.79	12.99	18.19	13.40	13.62	18.84	14.07	14.81	14.56	14.8
16	12.89	13.09	18.29	18.50	18.72	18.94	14.18	14.42	14.67	14.9
13	12.98	13.19	13.89	13.61	18.82	14.05	14.28	14.53	14.78	15.0
20	13.08	18.28	18.49	18.71	18.98	14.15	14.89	14.68	14.89	25.1
22	13.18	13.88	18.59	18.81	14.08	14.26	14.50	14.74	15.00	15.2
24	18.27	18.48	13.69	18.91	14.18	14.86	14.60	14.85	15.11	15.3
26	18.87	13.59	18.79	14.01	14.24	14.47	14.71	14.96	15.22	15.4
28	18.47	13.68	13.89	14.11	14.84	14.57	14.82	15.07	15.33	15.6
80	13.57	18.78	13.99	14.22	14.44	14.68	14.92	15.18	15.44	15.7
82	13.66	13.87	14.09	14.32	14.55	14.78	15.08	15.28	15.55	15.8
34	13.76	13.97	14.19	14.44	14.65	14.89	15.14	15.89	15.66	15.9

XIX'. HEIGHT, IN ENGLISH FEET, OF A COLUMN OF AIR, CORRESPONDING TO A TENTH OF AN INCH IN THE BAROMETER, AT DIFFERENT TEMPERATURES AND ELEVATIONS.

Berometer				Tea	peratur	of the	lir, Fahr	enheit, b	eing			
Reading in English Inches.	40 °	450	500	550	600	650	700	750	800	850	900	950
22.0	121.5	122.8	124.2	125.5	126.8	128.2	129.5	180.8	182.1	133.5	184.8	126.1
22.2	120.4	121.7	128.1	124 4	125.7	127.0	128.3	129.6	180.9	132.2	138.6	184.9
22.4	119.8	120.6	121.9	128.2	124.6	125.9	127.2	128.5	129.8	181.1	132.4	133.7
22.6	118.2	119.5	120.8	122.1	128.4	124.7	1 26 .0	127.8	128.6	129.9	181.2	182.4
22.8	117.2	118.5	119.8	121.1	122.8	123.6	124-9	126.2	127.5	128.8	180.0	131.3
23.0	116.2	117.5	118.7	120.0	121.8	122.6	123.8	125.1	126.4	127.6	129.9	130.2
28.2	115.2	116.5	117.7	119.0		121.5	122.7		125.3		127.8	129.0
23.4	114.2	115.5	116.7	118.0	119.2	120.5	121.7	128.0	124.2	125.4	126.7	127.9
28.6 23.8	118 2	114.4	115.7	116.9	118.1	119.4	120.6	121.8	128.1	124.8	125.5	126.8
24.5	112.3	118.5	114.8	116.0	117.2	118.4	119.7	120.9	122.1	123.3	124.6	125.8
24.0	111.4	112.6	118.8	115.0	116.2	117.4	118.7	119.9	121.1	122.8	123.5	124.7
24.2	110.5	111.7	112.9	114.1	115.8	116.5	117.7	118.9	120.1	121.3	122.5	123.7
24.4	109.5	110.7	111.9	118.1	114.8	115.5	116.7	117.9	119.1	i	121.5	122.7
24.6	108.6	109.8	111.0	112.2	118.4	114.6	115.8	116.9	118.1	i	120.5	121.7
24.8	107.8	108.9	110.1	111.8	112.5	118.7	114-8	116.0	117.2	118.4	119.5	120.7
25.0	106.9	108.1	109.2	110.4	111.6	112.7	118.9	115.1	116.2	117.4	118.6	119.7
25.2	106.0	107.2	108.4	109.5	110.7	111.8	118.0	114.1	115.3	116.5	117.6	118.8
25.4	105.2	106.4	107.5	108.7	109.8	111.0	112.1	113.8	114.4	115.6	116.7	117.9
25.6	104.4	105.5	106.7	107.8	108.9	110.1	111.2	112.4	113.5	114.6	115.8	116.9
25.8	103.6	104.7	105.8	107.0	108.1	109.2	110.4	111.5	112.6	118.8	114.9	116.0
26.0	102.8	103.9	105.0	106.1	107.8	108.4	109.5	110.6	111.8	112.9	114.0	115.1
26.2	102.0	103.1	104.2	105.3	106.5	107.6	108.7	109.8	110.9	112.0	118.1	114.2
26.4	101.2	102.8	108.4	104.6	105.7	106.8	107.9	109.0	110.1	111.2	112-3	113.4
26.6	100.5	101.6	102.7	103.8	104.9	106.0	107.1	108.2	109.8	110.4	111.4	112.5
26.8	99.7	100.8	101.9	103.0	104.1	105.2	106.8	107.4	108.5	109.5	110.6	111.7
27_0	99.0	100.1	101.2	102.2	103.8	104.4	105.5	106.6	107.6	108.7	109.8	110.9
27.2	98.3	99.3	100.4	101.5	102.6	108.6	104.7	105.8	106.8	107.9	109.0	110.1
27.4	97.5	98.6	99.7	100.7	101.8	102.9	103.9	105.0	106.1	107.1	106.2	109.3
27.6	96.8	97.9	98.9	100.0	101.1	102.1	103.2	104.2	105.8	106.8	107.4	108.5
27.8	96.1	97.2	98.2	99.8	100.8	101.4	102.4	103.5	104.5	105.6	106.6	107.7
28.0	95.4	96.5	97.5	98.6	99.6	100.6	101.7	102.7	103.8	104.8	105.9	106.9
28.2	94.8	95.8	96.8	97.9	98.9	99.9	101.0	i02.0	108.0	104.1	105.1	106.1
28.4	94.1	95.1	96.1	97.2	96.2	99.2	100.2	101.8	102.8	108.3	104.8	105.4
28.6	:98.4	94.4	95.5	96.5	97.5	98.5	99.5	100.6	101.6	102.6	103.6	104.6
28.8	92.8	93.8	94.8	95.8	96.8	97.8	98.8	99.8	100.8	101.8	102.8	103.8
29.0	92.1	93.1	94.1	95.1	96.2	97.2	98.2	99.2	100.2	101.2	102.2	103.2
29.2	91.5	92.5	93.5	94.5	95.5	96.5	97.5	98.5	99.5	100.5	101.5	102.5
29.4	90.9	91.9	92.9	98.9	94.8	95.8	96.8	97.8	98.8	99.8	100.8	101.8
29.6	90.3	91.3	92.2	98.2	94.2	95.2	96.2	97.2	98.2	99.1	100.1	101.1 100.4
29.8	89.7	90.6	91.6	92.6	98.6	94.5	95.5	96.5	97.5	98.5	99.4	100.4
30.0	89.1	90.0	91.0	92.0	92.9	93.9	94.9	95.9	96.8	97.8	98.8	99.7
30.2	88.5	89.4	90.4	91.4	92.3	98.8	94.3	95.2	96.2	97.2	98.1	99.1
80.4	87.9	88.8	89.8	90.8	91.7	92.7	93.6	94.6	95.6	96.5	97.5	98.4

REDUCING TO THE TRUE MEAN BAROMETRIC PRESSURE.

When the Barometrical means to be used have been derived from observations taken at such hours of the day as, if combined, do not give the true mean pressure, they must be reduced to the true means by using the Tables XX. and XXI. These tables give the corrections to be applied to the hourly means, in each month, for reducing them to the means which would have been given by observations made at each of the twenty-four hours. The correction for any given set of hours is found by taking the mean of the corrections due to each of the combined hours, paying due attention to the signs. Table XX. has been computed from the hourly observations made under the superintendence of Professor A. D. Bache, at Girard College, Philadelphia. Table XXI. is from the Greenwich Observations, by Glaisher.

XX.

NORTH AMERICA. — PHILADELPHIA. Lat. 39° 58' N. Long. 75° 11' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Barometric Pressure of the respective Days, Months, and of the Year.

Barometer in English Inches.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	Inch.	Inch.		Inch.		Inch.		Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
Midnight													0024
1													+.0007
2									1			1	+.0080
8	008	+.002	+.009	+.005	+.007	+.007	+.003	+.005	+.009	+.011	+.007	014	+.0086
4	003	+.008	+.009	+.002	+.008	+.002	.000	+.004	+.005	+.007	+.008	010	+.0038
5	008	.000	+.002	007	0 06	007	010	005	006	003	006	008	0050
6	009	004	011	020	019	022	019	017	016	012	012	015	0147
7	021	013	020	029	026	024	025	023	023	021	019	023	0222
8	032	023	028	034	031	029	028	026	029	080	028	029	0290
9	040	026	028	085	028	027	027	033	031	029	084	080	0307
10	041	026	025	038	021	025	026	030	029	026	038	082	0296
11	02 3	019	016	023	018	019	019	022	021	014	017	011	0185
Noon.	+.006	004	002	008	006	010	012	012	009	+.001	+.006	+.005	0037
1							1	1	ı				+.0107
2			1 1				ı		1			l .	+.0240
8	+.034	+.034	+.034	+.034	+.028	+.019	+.020	+.022	+.024	+.028	+.033	+.034	+.0287
4	+.031	+.032	+.034	+.042	+.082	+.027	+.027	+.027	+.030	+.028	+.027	+.080	+.0806
5		1					1						+.0267
6	1				1		1	•				1	+.0202
7			1.					ı			1		+.0128
8	+.003	.000	003	+.009	+.002	+.010	+.014	+.008	+.007	009	006	+.013	+.0010
9					1								0027
10				l .			f						0065
11		l .	1	l .	1	1	ł	•			į.	1	0064
į													
6, 2, 10													
7, 2, 9													
9, 12, 8, 9	.000	001	 001	002	004	004	004	004	004	003	001	+.003	- .002

XXI. England. — Greenwich. Lat. 51° 29' N.; Long. 0° 0'.

Corrections to be applied to the Means of the Hours of Observation, or Sets of Hours, to obtain the true Mean Barometric Pressure for the respective Months. — Glaisher.

English Inches.

									. —				
Hours.	Jan.	Feb.	March	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Duc.	Moan.
	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch	Inch.	Inch.	Inch.	Inch.	inch.	Inch.
Midn	.000	001	002	008	005	.000	006	010	005	005	011	004	005
1	.001	.004	.018	.000	.002	.004	.000	.000	.000	.004	005	.001	.002
2	.002	.008	.020	.007	.004	.005	.003	.007	.005	.010	.003	.006	.007
8	.005	.012	.028	.010	.005	.004	.003	.011	-010	.015	.006	.010	.009
4	.011	.014	.022	.011	.003	.001	.005	.014	.012	.020	.013	.012	.012
5	.015	.015	.019	.011	,006	002	.006	.011	.014	.022	-016	.014	.012
6	.015	.012	.012	.006	.006	006	.002	.005	.010	.018	.015	.011	.009
7	.010	.007	.005	003	.006	010	004	.000	.001	.008	.010	.006	.003
• •	.010		1000	.000	,000	.020	.004		.001	••••	.010		
8	.008	.000	004	008	.003	012	008	007	006	003	.008	.004	003
9	008	008	010	011	007	012	010	008	011	009	005	010	009
10	010	015	015	014	009	011	010	009	013	014	007	015	012
11	014	016	015	011	006	009	009	008	010	014	005	015	011
Noon	005	012	010	008	002	006	006	005	005	010	.002	009	006
Noon 1	.002	006	005	004	.000	003	003	.000	.000	003	.002	.003	001
2	-005	.008	.000	.003	.003	.003	.001	.003	.004	.004	.011	.008	.004
			003	.009		.003	.005	ŧ .		ł	1	ľ	1
8	.004	.006	003	.009	.006	.007	.000	.005	.006	.005	.010	.010	.006
4	.002	.008	.005	.004	.010	.018	.009	.009	.010	.003	.008	.009	.007
5	.000	.006	.004	.014	.014	.017	.013	.011	.011	.000	.004	.006	.008
6	003	.002	.000	.011	.015	.017	.013	.011	.006	005	.000	.002	.006
7	005	004	006	007	.010	.014	.010	.005	.000	008	006	003	.000
											1		
8	006	006	012	005	.000	.008	.004	005	005	011		006	
9	007	008	015	009	006	.003	001	010	009	~014	017	 0^9	008
10	005	007	012	012	008	002	003	015	011	012	019	010	010
.11	004	005	010	012	008	002	012	015	011	009	017	009	009
6. 6	.006	.007	.006	1	.011	.005	.008	.008	.008	.006	.007	.006	.008
7. 7	.002	.002	.000	005	.008	.002	.003	.002	.000	.000	.002	.002	.001
8. 8	002	003	008	006	.002	002	002	006	006	007	004	001	004
9. 9	007	00 8	018	010	006	004	005	009	010	012	011	009	009
10.10	007	011	014	013	009	006	007	1	l .	013	013	012	011
7. 2. 9	.003	.001			.001	001	001	i .	1	001	.001	.002	.001
						600	5000						
6. 2. 8	.005	.003	.000	.001	.008	.002	.002	.001	.008	.004	.005	.004	.003
6. 2.10	.005	.008	.000	001	.000	i	001	002	.001	.003	.002	.003	.001
6. 2. 6	-006	.006	.004	.007	.008	005	.005	.006	.007	.006	.009	.007	.006
7. 2	.007	.005	.003	.000	.004	001	001	.002	.002	.006	.010	.007	.003
8. 2	.004	.002	002	002	.008	004	003	002	001	.000	.007	.006	.001
8. 1	.002	003	004	006	.001	007	006	003	003	003	.005	.003	002
7. 1	.006	-001	.000	003	.003	006	003	.000	.000	.002	.008	.004	.001
9.12.3.9	004	005	008	005	002	002	003	004	004	007	002	004	004

BAROMETRICAL MEASUREMENT OF HEIGHTS.

XXII. TABLE TO REDUCE, BY INTERPOLATION,

THE OBSERVATIONS TO THE SAME ABSOLUTE TIME.

DECIMALS OF AN HOUR.

Min.	Decimal.	Min.	Decimal.	Min.	Decimal.	Min.	Decimal.	Min.	Decimal.	Min.	Decimal.
1	.017	11	.188	21	.850	81	.517	41	.683	51	.850
2	.033	12	.200	22	.367	32	.588	42	.700	52	.867
8	.050	18	.217	28	.888	88	.550	43	.717	58	.888
4	.067	14	.233	24	.400	84	.567	44	.788	54	.900
5	.093	15	.250	25	.417	85	.588	45	.750	55	.917
6	.100	16	.267	26	.483	36	.600	46	.767	56	.933
7	.117	17	.283	27	-450	87	.617	47	.783	57	.930
8	.133	18	.800	28	.467	88	.633	48	.800	58	.967
9	.150	19	.817	29	.483	89	.650	49	.817	59	.983
10	.167	20	.333	80	.500	40	.667	50	.833	60	1.000

TABLE FOR CORRECTION OF CURVATURE AND REFRACTION.

From a mountain, when furnished with a barometer, or with an apparatus for determining the temperature of boiling water, and a pocket level, an observer can find the elevations of distant points, which are in sight, but lower than the mountain itself on which he stands. He has only to seek, with the level, the point on the slope of the mountain which corresponds to the point at a distance that he wishes to determine, and to take there a barometrical, or a boiling point observation. This observation is to be calculated in the usual way, but the result must be corrected for the curvature of the surface of the globe, and for the atmospheric refraction, by means of the following Table.

This method, which furnishes the means of multiplying, without much trouble, the measurements of heights, gives approximations which are sufficient for most of the purposes of Physical Geography. It may even seem preferable to direct measurements for determining the mean elevation of certain physical lines, which are best estimated when seen from a distance; such as the upper limit of the growth of trees, the limits of different kinds of vegetation, that of permanent snow, that of the mean elevation of the crest of a mountain range, &c.

Table XXIII. is taken from Captain Lee's Collection of Tables and Formulæ, 2d edit., page 81.

XXIII. CORRECTIONS FOR CURVATURE AND REFRACTION.

Showing the Difference of the Apparent and True Level, in fast and decimals, for Distances in fast and miles.

Distances For Care			or the Appare			0	orrection in Fe	et.
Fee Fee Fee Fee Fee Refraction. Fee Refraction. Fee Refraction. Refraction. Refraction. Refraction. Fee Curvatura.								
Fee	Distances				1 1	İ	1	B A
150	in Feet.			ture and	in Miles.			ture and
150	100	00024	.00004	.00020		-0417	.0060	.0357
200 .00094 .00018 .00082 \$.2752 .0586 .3216 .2019 .00021 .00128 1 .6670 .0953 .5717 .2000 .00215 .00091 .00184 1 1 .5008 .2144 1 .3264 .2000 .20082 .00082 .00082 .20082 .2 .4 .1688 .5965 .8.5733 .5000 .00588 .00085 .0058 .00618 .2 .4 .1688 .5965 .5.733 .5000 .00598 .00085 .00618 .2 .6 .1008 .1673 .7 .0025 .5000 .00598 .00085 .00618 .2 .6 .1708 .1.673 .7 .0025 .5000 .00698 .00085 .00618 .2 .6 .1708 .1.673 .7 .0025 .5000 .00086 .00012 .00086 .5 .5 .1699 .2821 .1.2299 .5 .0000 .001172 .00167 .01006 .5 .5 .1799 .2821 .1.2299 .01173 .00167 .01006 .5 .5 .1799 .2821 .1.2293 .01153 .00192 .01153 .00192 .01153 .00192 .01153 .00219 .01812 .00318 .00277 .01661 .7 .25 .6830 .46890 .28.0143 .00289 .00287 .01661 .7 .27 .5180 .2821 .2881 .00287 .01661 .7 .27 .5180 .28824 .41.3066 .02838 .00277 .01661 .7 .27 .5180 .28824 .41.3066 .02838 .00269 .0 .48.1910 .8844 .41.3066 .02838 .00877 .02261 .02848 .08440 .03788 .00847 .02481 .00482 .02588 .00877 .02261 .003788 .00378 .00364 .00482 .00268 .00865 .00866 .00878 .03465 .00866 .00868 .00878 .00866 .00868 .00879 .04614 .00408 .00878 .00865 .00866 .00868 .00879 .04614 .00868 .00878 .00865 .00878 .04614 .00888 .00872 .00872 .04811 .00888 .00872					i	IL .		1
250						l		1 1
100292					n - 1	.6670	.0953	.5717
100	800	.00215	.00091	.00184	1	1.5008	.2144	1.2864
1.60	350	.00298	.00042	.00251	1 2	2.6680	.3 811	2.2869
1.60	400	.00888	.00055	.00328	24	4.1688	-5955	8.5783
B50	450	.00484	.00069	.00415		6.0080	.8561	5.1469
100	500	.00598	.00085	.00518	84	8.1708	1.1673	7.0085
100	550	.00724	-00103	.00621	4	10.6720	1.5246	9.1474
100	600	.00861	.00128	.00738	ایتہ∥	13.5468	1.9295	11.5778
TOO					11 ~ 1		2.8821	14.2929
T50					54		2.8824	17.2945
S50	750		.00192	.01158	,	24.0120	8.4808	20.5817
900 01938	800	.01581	.00219	.01812	6	28.1809	4.0258	24.1551
100					D - I			
1000 102892 100382 102069 8½ 48.1910 6.8844 41.3066 1060 102688 100377 102261 9 54.0270 7.7181 46.3089 1100 102895 100414 102481 9½ 60.1971 8.5996 51.5975 1150 103164 100452 102712 10 66.7000 9.5286 57.1714 1200 103445 100492 .02958 11 80.7070 11.5296 69.1774 1250 103738 100584 .08204 12 96.0480 13.7211 82.3269 1800 104048 100578 103465 13 112.7230 16.1033 96.6197 1350 .04861 100623 103738 14 130.7820 18.6760 112.0560 1400 104689 100670 10419 15 150.0750 21.4393 146.3589 1500 105883 100769 104811 16 170.7520 24.3931					n - 1			r 11
1060 .02638 .00377 .02261 9 54.0270 7.7181 46.3089 1100 102895 .00414 .02481 91 60.1971 5.5996 51.5975 1150 103164 .00452 .02712 10 66.7000 9.5286 57.1714 1200 .03445 .00492 .02958 11 80.7070 11.5296 69.1774 1250 .03738 .00584 .08204 12 96.0480 13.7211 82.3269 1800 .04048 .00578 .03465 13 112.7230 16.1033 96.6197 1850 .04361 .00623 .03738 14 130.7820 18.6760 112.0560 1400 .04889 .00670 .04019 15 150.0750 21.4393 146.3589 1500 .05883 .00799 .04811 16 170.7520 24.3931 146.3589 1500 .05748 .00821 .04927 18 216.1086 30.8727<					H - I			
1100 102895 100414 102481 91/2 60.1971 8.5996 51.5975 1150 103164 100452 102712 10 66.7000 9.5286 57.1714 1200 103445 100492 102958 11 80.7070 11.5296 69.1774 1250 103738 100584 108204 12 96.0480 13.7211 82.3269 1800 104048 100578 103465 13 112.7230 16.1033 96.6197 1350 104361 100623 103738 14 130.7820 18.6760 112.0560 1400 104889 100670 104019 15 150.0750 21.4393 128.6357 1450 105030 100719 104311 16 170.7520 24.3931 146.3589 1500 105883 100769 104614 17 192.7630 27.5876 165.2254 1550 106125 100875 105250 19 240.7870 84								1
1150 103164 100452 102712 10 66.7000 9.5286 57.1714 1200 103445 100492 .02958 11 80.7070 11.5296 69.1774 1250 103738 100584 .08204 12 96.0480 13.7211 82.5269 1800 104048 100578 .08465 13 112.7230 16.1033 96.6197 1350 .04361 100623 103788 14 130.7820 15.6760 112.0560 1400 104689 100670 104019 15 150.0750 21.4393 128.6357 1450 105030 100719 104311 16 170.7520 24.3931 146.3589 1500 105883 100769 104614 17 192.7630 27.5876 165.2254 1550 106748 100827 18 240.7870 84.3981 206.3889 1650 1.06514 10098 1.05926 240.7870 84.3981 228.6857 <	1050	.02638	.00877	.02261	9	54.0270	7.7181	46.3069
1200 103445 100492 102958 11 80.7070 11.5296 69.1774 1250 103738 100584 .08204 12 96.0480 13.7211 82.5269 1800 104048 100578 .08465 13 112.7230 16.1033 96.6197 1850 .04361 100623 .08788 14 130.7820 18.6760 112.0560 1400 .04689 100670 .04019 15 150.0750 21.4393 128.6357 1450 .05030 .00719 .04811 16 170.7520 24.3931 146.3589 1500 .05883 .00769 .04614 17 192.7630 27.5876 165.2254 1550 .06748 .00821 .04927 18 216.1086 30.8727 185.2359 1600 .06125 .00875 .05250 19 240.7870 34.3981 206.3889 1750 .07327 .01047 .06845 20 266.8000 <t< th=""><th>1100</th><th>.02895</th><th>.00414</th><th>.02481</th><th>94</th><th>60.1971</th><th>8.5996</th><th>51.5975</th></t<>	1100	.02895	.00414	.02481	94	60.1971	8.5996	51.5975
1250 .03788 .00584 .03204 12 96.0480 13.7211 82.3269 1800 .04048 .00578 .03465 13 112.7230 16.1033 96.6197 1350 .04361 .00623 .08788 14 130.7820 18.6760 112.0560 1400 .04689 .00670 .04019 15 150.0750 21.4393 128.6357 1450 .05030 .00719 .04811 16 170.7520 24.3931 146.3589 1500 .05383 .00769 .04614 17 192.7630 27.5876 165.2254 1560 .05748 .00821 .04927 18 216.1086 30.8727 188.2359 1600 .06125 .00875 .05250 19 240.7870 34.3981 206.3889 1650 .06514 .00981 .05926 20 266.8000 38.1143 228.6857 1850 .08188 .01170 .06645 .070845 .070845	1150	.03164	.00452	.02712	10	66.7000	9.5286	57.1714
1800 .04048 .00578 .03465 13 112.7230 16.1033 96.6197 1850 .04361 .00623 .08788 14 130.7820 18.6760 112.0560 1400 .04689 .00670 .04019 15 150.0750 21.4393 128.6357 1450 .05030 .00719 .04811 16 170.7520 24.3931 146.3589 1500 .05383 .00769 .04614 17 192.7630 27.5876 165.2254 1550 .05748 .00821 .04927 18 216.1086 30.8727 188.2339 1600 .06125 .00875 .05250 19 240.7870 34.3981 206.3889 1650 .06514 .00981 .05926 240.7870 34.3981 228.6857 1700 .06914 .00988 .05926 266.8000 28.1143 228.6857 1850 .08188 .01170 .06645 .070845 .06687 .01234 .07403<	1200	.03445	.00492	.02958	11	80-7070	11.5296	
1350 .04361 .00623 .08788 14 130.7820 15.6760 112.0560 1400 .04689 .00670 .04019 15 150.0750 21.4393 128.6357 1450 .05030 .00719 .04811 16 170.7520 24.3931 146.3589 1500 .05883 .00769 .04614 17 192.7630 27.5876 165.2254 1550 .05748 .00821 .04927 18 216.1086 30.8727 185.2359 1600 .06125 .00875 .05250 19 240.7870 84.3981 206.3889 1650 .06514 .00981 .05926 20 266.8000 28.1148 228.6857 1750 .07327 .01047 .06280 20 266.8000 28.1148 228.6857 1850 .08188 .01170 .07018 .07403 .09098 .01300 .07798 .07798 .07798	1250	.03738	.00584	.08204		96.0480		1 ' 1
1400 .04889 .00670 .04019 15 150.0750 21.4393 128.6357 1450 .05030 .00719 .04811 16 170.7520 24.3931 146.3589 1500 .05883 .00769 .04614 17 192.7630 27.5876 165.2254 1550 .05748 .00821 .04927 18 216.1066 30.8727 185.2359 1600 .06125 .00675 .05250 19 240.7870 34.3981 206.3889 1650 .06514 .00931 .05583 20 266.8000 38.1143 228.6857 1700 .06914 .00988 .05926 .0107 .06645 38.1143 228.6857 1850 .08188 .01170 .07018 .07403 .09098 .01300 .07798	1800	.04048	.00578	.08465	18,	112.7280	16.1033	96.6197
1450 .05030 .00719 .04811 16 170.7520 24.3931 146.3589 1500 .05883 .00769 .04614 17 192.7630 27.5876 165.2254 1550 .05748 .00821 .04927 18 216.1086 30.8727 185.2359 1600 .06125 .00875 .05250 19 240.7870 34.3981 206.2889 1650 .06514 .00931 .05583 20 266.8000 38.1143 228.6857 1700 .06914 .00988 .05926 .05926 .01047 .06280 .0170 .06645 .07752 .01107 .06645 .07018 .08188 .01170 .07018 .07403 .09098 .01300 .07798 .07798 .01300 .07798 .07798 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000	1850	.04361	.00623	.08788	14	130.7820	18.6760	112.0560
1500 .05883 .00769 .04614 17 192.7630 27.5876 165.2254 1550 .05748 .00821 .04927 18 216.1086 30.8727 185.2359 1600 .06125 .00875 .05250 19 240.7870 34.3981 206.2889 1650 .06514 .00931 .05583 20 266.8000 38.1143 228.6857 1700 .06914 .00988 .05926 .06280 .01702 .06645 .07752 .01107 .06645 .07018 .08188 .01170 .07018 .07403 .09098 .01300 .07798 .07798 .01300 .07798 .07798 .000000 .000000 .000000 .00000	1400	.04689	.00670	.04019	15	150.0750	21.4393	
1550 .05748 .00821 .04927 18 216.1086 30.8727 185.2359 1600 .06125 .00875 .05250 19 240.7870 34.3981 206.2889 1650 .06514 .00931 .05583 20 266.8000 38.1143 228.6857 1700 .06914 .00988 .05926 .01750 .06280 .0170 .06645 .0170 .06645 .0170 .06645 .0170 .07018 .07403 .09098 .01300 .07798 .07798 .0170 .07798 .0170 .07798 .0170 .07798 .0170 .07798 .0170 .07798 .0170 .07798 .0170 .07798 .0170 .07798 .0170 .07798 .0170 .07798 .0170	1450	.05030	.00719	.04811	16	1	I.	
1600 1.06125 1.00675 1.05250 19 240.7870 34.3981 206.3889 1650 1.06514 1.00931 1.05583 20 266.8000 38.1143 228.6857 1700 1.06914 1.00988 1.05926 1.07327 1.01047 1.06280 1.07752 1.01107 1.06645 1850 1.08188 1.01170 1.07018 1.06645 1.01234 1.07403 1.09098 1.01300 1.07798					U H	{		
1650 .06514 .00981 .06583 20 266.8000 28.1143 228.6857 1700 .06914 .00988 .05926 1750 .07327 .01047 .06280 1800 .07752 .01107 .06645 1850 .08188 .01170 .07018 1900 .08687 .01234 .07403 1950 .09098 .01300 .07798	1550	.05748	.00821	.04927	18	216.1066	30.8727	185.2359
1700	1600	.06125	.00875	.05250	19	240.7870	84.8981	
1750	1650	.06514	.00981	.05588	20	266-8000	88-1148	228.6857
1800		.06914		1				
1850		1			j l	1	1	1
1900 .08637 .01234 .07403 1950 .09098 .01300 .07798	1800	.07752	.01107	.06645			1	
1950 .09098 .01300 .07798	1850	.08188	.01170	.07018	 	1		[
	1900	.08637	.01234	.07403		f		[
2000 109570 101367 108208	1950	.09098	.01300	.07798		I	t	1 (
	2000	.09570	.01367	.08208			1	

THERMOMETRICAL

MEASUREMENT OF HEIGHTS,

OR

TABLES

FOR DEDUCING DIFFERENCES OF LEVEL FROM OBSERVATIONS OF THE TEMPERATURE OF BOILING WATER.

THERMOMETRICAL MEASUREMENT OF HEIGHTS.

TABLES

FOR DEDUCING DIFFERENCES OF LEVEL FROM THE TEMPERATURE OF THE BOILING POINT OF WATER.

When water is heated in the open air, the elastic force of the vapors produced from it gradually increases, until it becomes equal to the incumbent weight of the atmosphere. Then, the pressure of the atmosphere being overcome, the steam escapes rapidly in large bubbles, and the water boils. The temperature at which, in the open air, water boils, thus depends upon the weight of the atmospheric column above it, and under a less barometric pressure the water will boil at a lower temperature than under a greater pressure. Now, as the weight of the atmosphere decreases with the elevation, it is obvious that, in ascending a mountain, the kigker the station where an observation is taken, the lower the temperature at which water boils at that station will be.

The difference of elevation between two places, therefore, can be deduced from the temperature of boiling water observed at each station. It is only necessary to find the barometric pressures which correspond to those temperatures, and, the atmospheric pressures at both places being known, to compute the difference of level by a formula, or by the tables given above for computing heights from barometrical observations.

From the above, it may be seen that the heights determined by means of the temperature of boiling water are less reliable than those deduced from barometrical observations. Both derive the difference of altitude from the difference of atmospheric pressure. But the temperature of boiling water gives only indirectly the atmospheric pressure, which is given directly by the barometer. This method is thus liable to all the chances of error which may affect the measurements by means of the barometer, besides adding to them new ones peculiar to itself, the principal of which, not to speak of the differences exhibited in the various tables of the force of vapor, is the difficulty of ascertaining with the necessary accuracy the true temperature of boiling water. In the present state of thermometry it would hardly be safe, indeed, to answer, in the most favorable circumstances, for quantities so small as hundredths of degrees, even when the thermometer has been constructed with the utmost care; moreover, the quality of the glass of the instrument, the form and the substance of the vessel containing the water, the nature of the water itself, the place at which the bulb of the thermometer is placed, whether in the current of steam or in the water, - all these circumstances cause no inconsiderable variations to take place in the indications of thermometers observed under the same atmospheric

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THERMOMETRICAL MEASUREMENT OF HEIGHTS.

pressure. Owing to these various causes, an observation of the boiling point, differing by one tenth of a degree from the true temperature, ought to be still admitted as a good one. Now, as the tables show, an error of one tenth of a degree Centigrade in the temperature of boiling water would cause an error of 2 millimetres in the barometric pressure, or of from 70 to 80 feet in the final result, while with a good barometer the error of pressure will hardly ever exceed one tenth of a millimetre, making a difference of 3 feet in altitude.

Notwithstanding these imperfections, the hypsometric thermometer, or thermobarometer, is of the greatest utility to travellers traversing distant or rough countries, on account of its being more conveniently transported, and much less liable to accidents than the mercurial barometer. The best form for it is that contrived and described by Regnault in the *Annales de Chimie et de Physique*, Tom. XIV. p. 202. It consists of an accurate thermometer with long degrees, subdivided into tenths, whose bulb is placed, about 2 or 3 centimetres above the surface of the water, in the steam arising from distilled water in a cylindrical vessel, the water being made to boil by a spirit-lamp. The whole instrument when closed is about 6 inches long; when drawn out for observation, about 14 inches.

Table XXIV. of barometric pressures corresponding to temperatures of boiling water, has been calculated by Regnault from his Tables of Forces of Vapor, and published in the *Annales de Chimie et de Physique*, Tom. XIV. p. 206. It gives, in millimetres of mercury, the barometric pressures corresponding to every tenth of a Centigrade degree; for greater convenience, the values for every hundredth have been added.

The accuracy of this table has been tested by direct observation by Mr. Wisse, a traveller competent in such matters, who noted down simultaneously the temperatures of the boiling point of water and the height of the barometer, in various parts of the Andes, up to the summit of the volcano of Pichincha, including in his observations barometrical pressures ranging from 752 to 430 millimetres of mercury. The agreement between the barometric pressures given here by Regnault and those found by Wisse are very satisfactory, the differences never exceeding a few tenths of a millimetre. See *Annales de Chimie et de Physique*, Tom. XXVIII. p. 123.

Table XXV. is the same table, revised by A. Moritz, who, in a communication to the Académie des Sciences, in October, 1856, called the attention to some slight errors of computation in Regnault's table, and gave the corrected numbers for every whole degree from 40° to 102° Centigrade. Those numbers are given here from 80° upwards, as published in the *Journal de l'Institut*; the values for every tenth of a degree, and their differences, have been computed to fit the table for practical use. The comparison of the two tables will show that the corrections mostly amount to a few hundredths, and never exceed one tenth of a millimetre.

Table XXVI. is table XXV. reduced to English measures.

Centig.				R	undredthe	of a Degree				
Sogroos.	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.
•	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
85.0	488.04	483.21	488.88	488.55	488.72	488.89	434.07	484.24	484.41	434.5
85.1	484.75	434.92	485.09	435.26	435.43	435.60	485.78	485.95	486.12	436.2
85.2	436.46	436.68	436.80	486.97	437.14	437.81	487.49	437.66	487.83	438.0
85.8	489.17	488.84	488.51	438.69	438.86	489.03	439.20	439.87	489.55	439.7
85.4	439.89	440.06	440.28	440.41	440.58	440.75	440.98	441.10	441.27	441.4
85.5	441.62	441.79	441.97	442.14	442.81	442.48	442.66	442.83	443.00	443.1
85.6	443.35	443.52	448.70	448.87	444.05	444.22	444.89	444.57	444.74	444.9
85.7	445.09	445.26	445.44	445.61	445.79	445.96	446.14	446.81	446.49	446.8
85.8	446.84	447.01	447.19	447.86	447.54	447.71	447.89	448.06	448.24	448.4
85.9	448.59	448.76	448.94	449.11	449.29	449.46	449.64	449.81	449.99	450.1
86.0	450.84	450.52	450.69	450.87	451.04	451.22	451.40	451.57	451-75	451.9
86.1	452.10	452.28	452.45	452.68	452.81	452.98	453.16	453.84	453.52	453.6
86.2	458.87	454.05	454.22	454.40	454.58	454.75	454.93	455.11	455.29	455.4
86.8	455.64	455.82	456.00	456.17	456.85	456-53	456.71	456.89	457.06	457.2
86.4	457.42	457.60	457.78	457.96	458.14	458.81	458.49	458.67	458.85	459.0
86.5	459.21	459.89	459.57	459.75	459.93	460.10	460.28	460.46	460-64	460.8
86.6	461.00	461.18	461.86	461.54	461.72	461.90	462.08	462.26	462.44	462.6
86.7	462.80	462 98	468.16	468.84	463.52	463.70	468.88	464.06	461.24	464.4
86.8	464.60	464.78	464.96	465.14	465.82	465.50	465.69	465.87	466.05	466.2
86.9	466.41	466.59	466.77	466.95	467.18	467.81	467.50	467.68	467.86	468.0
87.0	468.22	468.40	468.58	468.77	468.95	469.13	469.31	469.49	469.68	469.8
87.1	470.04	470.22	470.41	470.59	470.77	470.95	471.14	471.32	471.50	471.6
87.2	471.87	472.05	472.24	472.42	472.60	472.78	472.97	478.15	478.83	478.5
87.8	478.70	478.88	474.07	474.25	474.44	474.62	474.80	474.99	475.17	475.3
87.4	475.54	475.72	475.91	476.09	476.28	476.46	476.64	476.83	477.01	477.5
					480 10	478.80	478.49	478.67	478.86	479.0
87.5	477.88	477.56	477.75	477.98 479.78	478.12	480.15	480.84	480.52	480.71	480.5
87.6	479/23	479.41	479.60			482.01	482.20	482.38	482.57	482.7
87.7	481.08	481.27	481.45	481.64 488.50	481.82 483.69	488.87	484.06	484.25	484.44	484.6
87.8 87.9	482.94 484.81	483.18 485.00	488.81 485.19	485.87	485.56	485.75	485.94	486.13	486.81	486.5
								400.01	400 10	488.3
88.0	486.69	486.88	487.07	487.25	487.44	487.63	487-82	488.01	488.19	490.2
88.1	488.57	488.76	488.95	489.18	489.82	489.51	489.70	489.89 491.77	490.07 491.96	492.1
88.2	490.45	490.64	490.83	491.02	491.21	491.89	491.58	491.77	493.86	494.0
88.8 88.4	492.34 494.24	492.58 494.48	492.72 494.62	492.91 494.81	498.10 495.00	493.29 495.19	493.48 495.89	495.58	495.77	495.9
	l I			}						
89.5	496.15	496.84	496.58	496.72	496.91		497.80	497.49	497.68	497-8
88.6	498.06	498.25	498.44	498.64	498.83	499.02	499.21	499.40	499.60	499.7
88.7	499.98	500.17	500.36	500.56	500.75	500.94	501.13	501.82	501.52	501.7
88.8	501.90	502.09	502.28	502.48	502.67	502.86	508.05	508.24	503.44	503.6 506.5
88.9	503.82	504.01	504.21	504.40	504.60	504.79	504.98	505.18	505.87	
	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.

Centig.				B	undredths	of a Degre	10.			
Degrees.	0.	1.	9.	8.	4.	4.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
89.0	505.76	505.95	506.15	506.84	506.54	506.73	506.92	507.12	507.31	507.51
89.1	507.70 509.65	507.89	508.09	508.28	508-48	508.67 510.62	508.87 510.82	509.06	509.26	509.45 511.40
89.2 89.3	511.60	509-84 511-80	510.04 511.99	510.23 512.19	510.43 512.88	512.58	512.78	511.01 512.97	511.21 513.17	518.36
89.4	513.56	518.76	518.95	514.15	514.85	514.54	514.74	514.94	515.14	515.33
55.4	0.0.00	0200	010.00	0,4.10	D14-00	012.00	024	0,100	0.0.24	220.00
89.5	515.53	515.73	515.92	516.12	516-82	516.51	516.71	516.91	517.11	517.80
89.6	517-50	517.70	517.90	518.09	518.29	518.49	518.69	518.89	519.08	519.28
89.7	519.48	519.68	519.88	520.07	520.27	520.47	520.67	520.87	521.06	521.26
89.8	521.46	521.66	521.86	522.06	522.26	522.46	522.66	522.86	523.05	523.25
89.9	523.45	523.65	528.85	524.05	524.25	524.45	524.65	524.85	525.05	525.25
		-	-							
90.0	525-45	525.65	525.85	526.05	526.25	526.45	526.65	526.85	527.05	527.25
90.1	527-45	527.65	527.85	528.05	528.25 530.27	528.45	528.66 530.67	528.86	529.06	529.26
90.2 90.8	529.46 581.48	529.66 531.68	529.86 531.88	580.07 532.09	532.29	530.47 532.49	532.69	530.87 532.89	531.08 533.10	531.28 533.80
90.4	533.50	588.70	533.91	584.11	584.31	584.51	534.72	584.92	585.12	585.88
	000.00	500.70	900.41	002.11	Define	503.01	004.12	907.02	000.12	500.00
90.5	535.53	535.78	585.94	586.14	536.35	536.55	586.75	586.96	587.16	587.87
90.6	537.57	587.77	537.98	538.18	588.39	538.59	538.79	589.00	589.20	589.41
90.7	539.61	539.81	540.02	540.22	540.43	540.63	540.84	541.04	541.25	541.45
90.8	541.66	541.87	542.07	542.28	542.48	542.69	542.90	543.10	543.31	543.51
90.9	548.72	548.98	544.18	544.84	544.54	544.75	544.96	545.16	545.37	545.57
									_	
91.0	545.78	545.99	546.19	546.40	546.61	546.81	547.08	547.28	547.44	647.64
91.1	547.85	548.06	548.26	548.47	548.68	548.88	549.09	549.80	549.51	549.71
91.2	549.92 552.00	550.13 552.21	550.84	550.54 552.63	550.75	550.96 558.04	551.17 558.25	551.88 558.46	551.58	551.79
91.8 91.4	554.09	554.80	552.42 554.51	554.72	552.84 554.93	555.14	555.85	555.56	558.67 555.77	553.88 555.98
71.1	004.09	004.00	004.01	004.12	004.50	900.14	000.00	900.90	000.77	000.80
91.5	556.19	556.40	556.61	556.82	557.03	557.24	557.45	557.66	557.87	558.08
91.6	558.29	558.50	558.71	558.92	559.13	559.84	559.55	559.76	559.97	560.18
91.7	560.89	560.60	560.81	561.08	561.24	561.45	561.66	561.87	562.09	562.30
91.8	562.51	562.72	562.98	568.15	568.26	563.57	563.78	563.99	564.21	564.42
91.9	564.63	564.86	565.06	565.27	565.48	565.69	565.91	566.12	566.23	566.55
92.0	566.76	566.97	587.19	567.40	567.61	567.85	568.04	568.25	568.46	569.68
92.1	568.89	569.10	569.82	569.53	569.75	569.96	570.17	570.39	570.60	570.82
92.2	571.08	571.24	571.46	571.67	571.89	572.10	572.82	572.53	572.75	572.96
92.8 92.4	578.18 575.34	573.40 575.56	578.61 575.77	573.83 575.99	574.04 576.20	574.26 576-42	574.48 576.64	574.69 576.85	574.91 577.07	575.12 577.28
74-4	010.04	010.00	010.11	010.88	370.50	3/0-42	310.04	310-50	311.01	401-60
92.5	577.50	577.72	577.93	578.15	578.87	578.58	578.80	579.02	579-24	579-43
92.6	579.67	579.89	580.10	580.32	580.54	580.75	580.97	581.19	581.41	581-62
92.7	581.84	582.06	582.28	582.49	582.71	582.93	588.15	588.37	583.58	563.80
92.8	584.02	584.24	584.46	584.68	584.90	585.11	585.88	585-55	585.77	585.99
92.9	586.21	586.48	586.65	586.87	587.09	587.81	587.53	587.75	587.97	588.19
	0.	1.	9.	3.	4.	5.	6.	7.	ş.	9.

Contig.				H	lundredthe	of a Degre	10.			
Dogress.	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim. 589.29	Millim.	Millim. 589.73	Millim. 589.95	Millim. 590.17	Millim. 590.39
93.0	588.41	588.68	588.85	589.07		589.51	591.94	592.16	592.38	592.60
93.1	590.61 592.82	590.83 598.04	591.05 598.26	591.27 593.49	591.49 598.71	591.71 593.93	594.15	594.87	594.60	594-82
93.2 93.8	595.04	595.26	595.48	595.71	595.98	596.15	596.37	596 59	596.82	597.04
93.4	597.26	597.48	597.71	597.98	598.15	598.37	598.60	598.82	599.04	599.27
93.5	599.49	599.71	599.94	600.16	600.28	600.60	600.88	601.05	601.27	601.50
93.6	601.72	601.94	602.17	602.29	602.62	602.84	608.07	603.29	603.52	603.74
93.7	603.97	604.19	604.42	604.64	604-87	605.09	605.82	605.54	605.77	605.99
93.8	606.22	606.45	606.67	606.90	607.12	607.85	607.58	607.80	608.03	608.25
93.9	608.48	608.71	608.93	609.16	609.88	609-61	609.84	610.06	610.29	610.51
94.0	610.74	610.97	611.19	611.42	611.65	611.87	612.10	612.23	612.56	612-79
94.1	618.01	613.24	618.47	613.69	613.92	614.15	614.88	614.61	614.83	615.06
94.2	615.29	615.52	615.75	615.97	616.21	616.48	616.66	616-89	617.12	617.35
94.8	617.58	617.81	618.04	618.27	618.50	618.72	618.96	619.18	619.41	619.64
94.4	619.87	620.10	620.83	620.56	620.79	621.02	621.25	621.48	621.71	621.94
94.5	622.17	622.40	622.68	622.86	628.09	623.32	623.56	623.79	624.02	634.25
94.6	624.48	624.71	624.94	625.17	625.40	625.68	625.87	626.10	626.33	626.56
94.7	626.79	627.02	627.25	627.49	627.72	627.95	628.18	628.41	628.65	62 8.88
94.8	629.11	629.84	629.58	629.81	680.04	630.27	630.51	630.74	630.97	681.21
94.9	681.44	631.67	681.91	682.14	682.88	632.61	632.84	633.06	683.31	633. 55
95.0	633.78	634.01	634.25	634.48	684.72	634.95	635.18	635.42	685.65	635.89
95.1	636.12	636.85	686.59	686.82	637.06	637.29	637.53	637.76	638.00	638.23
95.2	688.47	638.71	638.94	639.18	689.41	639.65	639.89	640.12	640.86	640.59
95.3	640.83	641.07	641.80	641.54	641.77	642.01	642.25	642.48	642.72	642.9
95.4	643.19	643.48	648.67	648.90	644-14	644.88	644.62	644.86	645.09	645.33
95.5	645.57	645.81	646.05	646.28	646.52	646.76	647.00	647-24	647.47	647.7
95.6	647.95	648.19	648.48	648.67	648.91	649.14	649.88	649.62	649.86	650.1
95.7	650.34	650.58	650.82	651.06	651.30	651.53	651.77	652.01	652.25	652.4
95.8	652.78	652.97	653.21	658.45	658.69	653.93	654.17	654.41	654.65	654.8
95.9	655.18	655.87	655.61	655.85	656.09	656.33	656.5 8	656.82	657.06	657.3
96.0	657.54	657.78	658.02	658.26	658.50	658.74	658.99	659.23	659.47	659.7
96-1	659.95	660.19	660.48	660.68	660.92	661.16	661.40	661.64	661.89	662.1
96.2	662.87	662.61	662.86	663.10	668-34	663.58	668.83	664.07	664.31	664.5
96.3	664.80	665.04	665. 29	665.58	665.78	666.02	666.26	666.51	666.75	667.0
96.4	667.24	667.48	667.78	667.97	668.22	668.46	668.71	668.95	669.20	669.4
96.5	669.69	669.93	670.18	670.42	670.67		671.16	671.40	671.65	671.9
96.6	672.14	672.89	672.63	672.88	678.12		673.62	673.86	674.11	674.3
96.7	674.60	674.85	675.09	675.34	675.59		676.08	676.33	676.58	676.8
96.8	677.07	677.32	677.57	677.81	678.06	678.31	678.56	678.81	679.05	679.3
96.9	679.55	679.80	680.05	680.29	680.54	680.79	681.04	681.29	681.53	681.7
	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.

Centig.	Hundreckhe of a Degree. 9. 1. 2. 8. 4. 5. 6. 7. 8. 9.												
Degrees.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.			
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.			
97.0	682.08	682.28	682.53	682.78	683.08	683.27	683.52	683.77	684.02	684.27			
97.1	684.52	684.77	685.02	685.27	685.52	685.77	686.02	686.27	686.52	686.77			
97.2	687.02	687.27	687.52	687.77	688.02	688.27	688.58	688.78	689.03	689.28			
97.3	689.53	689.78	690.08	690.28	690.53	690.78	691.04	691.29	691.54	691.79			
97.4	692.04	692.29	692.54	692.80	698.05	693.80	693.55	698.80	694.06	694.31			
97.5	694.56	694.81	695.06	695.82	695.57	695.82	696.07	696.32	696.58	696.83			
97.6	697.08	697.88	697.59	697.84	698.09	698.84	698.60	698.85	699.10	699.36			
97.7	699.61	699.86	700.12	700.37	700.68	700.88	701.18	701.39	701.64	701.90			
97.8	702.15	702.40	702.66	702.91	708.17	703.42	703.68	703.93	704.19	704.44			
97.9	704.70	704.96	705.21	705.47	705.72	705.98	706.24	706.49	706.75	707.00			
98.0	707.26	707.52	707.77	708.03	708.28	708.54	708.80	709.05	709.81	709.56			
98.1	709.82	710.08	710.88	710.59	710.85	711.10	711.36	711.62	711.88	712.18			
98.2	712.89	712.65	712.91	718.16	713.42	718.68	713.94	714.20	714.45	714.71			
98.3	714.97	715.22	715.49	715.75	716.01	716.26	716.52	716.78	717.04 719.68	717.80			
98.4	717.56	717.82	718.08	718.84	718.60	718.85	719.11	719.87		719.89			
98.5	720.15	720.41	720.67	720.98	721.19	721.45	721.71	721.97	722.23	722.49			
98.6	722.75	723.01	723.27	723.58	728.79	724.05	724.81	724.57	724.83	725.09			
98.7	725.35	725.61	725.87	726.13	726.39	726.65	726.92	727.18	727.44	727.70			
98.8	727.96	728.22	728.48	728.75	729.01	729.27	729.58	729.79	730.06	780.82			
98.9	730.58	780.84	781.11	781.37	781.63	781.89	782.16	782.42	782.68	782.95			
99.0	733.21	788.47	783.74	734.00	734.27	784.58	734.79	735.06	735.32	735.59			
99.1	785.85	786.11	786.88	786.64	736.91	787.17	787.44	737.70	787.97	788.23			
99.2	788.50	788.77	789.03	789.80	739.56	739.83	740.10	740.36	740.68	740.89			
99.8	741.16	741.48	741.69	741.96	742.23	742.49	742.76	743.03	748.30	743.56			
99.4	748.88	744.10	744.86	744.68	744.90	745.16	745.48	745.70	745.97	746.23			
99.5	746.50	746.77	747.04	747.80	747.57	747.84	748.11	748.88	748.64	748.91			
99.6	749.18	749.45	749.72	749.99	750.26	750.52	750.79	751.06	751.33	751.60			
99.7	751.87	752.14	752.41	752.68	752.95	758.22	758.49	753.76	754.08	754.30			
99.8	754.57	754.84	755.11	755.88	755.65	755.92	756.20	756.47	756.74	757.01			
99.9	757.28	757.55	757.82	758.10	758.37	758.64	758.91	759.18	759.46	759.73			
100.0	760.00	760.27	760.55	760.82	761.09	761.86	761.64	761.91	762.18	762.46			
100.1	762.73	768.00	763.28	763.55	763.82	764.09	764.37	764.64	764.91	765.19			
160.2	765-46	765.73	766.01	766.28	766.56	766.83	767.10	767.88	767.65	767.93			
100.8	768.20	768.47	768.75	769.02	769.30	769.57	769.85	770.12	770.40	770.67			
100.4	770.95	771.28	771.50	771.78	772.05	772.83	772.61	772.88	778.16	773.43			
100.5	778.71	778.99	774.26	774.54		775.09	775.37	775.65	775.98	776.20			
100.6	776.48	776.76	777.04	777.81	777.59	777.87	778.15	778.43	778.70	778.98			
100.7	779.26	779.54	779.82	780.09	780.37	780.65	780.98	781.21	781.48	781.76			
100.8	782.04	782.32	782.60	782.88	783.16	783.43	788.71	783.99	784.27	784.55			
100.9 101.0	781.88 787.63	785.11 787.91	785.39 788.19	785.67 788.47	785.95 788.75	786.28 789.03	786.51 789.31	786.79 789.59	787.07 789.87	787.85 790.15			
101.0	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.			
	•	4.	~.	٠.	780	J.	—		9.				

TABLE XXV.

BAROMETRIC PRESSURES CORRESPONDING TO TEMPERATURES OF THE BOILING POINT OF WATER,

EXPRESSED IN MILLIMETRES OF MERCURY FOR CENTIGRADE TEMPERATURES.

By REGRAULT, REVISED BY MORITS.

Bolling Point, Centigrade.	Berometer in Millimetres.	Differ- ence.	Boiling Point, Centigrade.	Barometer in Millimetres.	Differ-	Boiling Point, Centigrade.	Barometer in Millimetres.	Differ-
80.0	854.62		83.0	400.07		86.0	450.30	
80.1	856.06	1.44	83.1	401.66	1.60	86.1	452.06	1.76
80.2	857.50	1.45	88.2	403.26	1.60	86.2	458.83	1.77
80.8	858.96	1.45	88.8	404.87	1.61	86.3	455.60	1.77
80.4	860.41	1.46	83.4	406.48	1.61	86.4	457.38	1.78
		1.46		,55555	1.62			1.78
80.5	861.87		88.5	406.10	1	86.5	459.17	
80.6	863.34	1.47	88.6	409.72	1.62	86.6	460.96	1.79
80.7	364.81	1.47	88.7	411.85	1.63	86.7	462.75	1.80
80.8	866.29	1.48	88.8	412.98	1.68	86.8	464.55	1.50
80.9	867.77	1.48	83.9	414.62	1.64	86.9	466.36	1.61
		1.40			1.64	1	1200100	1-81
81.0	369.26		84.0	416.26	!	87.0	468.17	1
81.1	370.75	1.49	84.1	417.91	1-65	87.1	469.99	1.82
81.2	872.25	1.60	84.2	419.57	1.56	87.2	471.82	1.63
81.3	878.75	1.50	84.8	421.28	1.66	87.8	478.65	1.83
81.4	875.25	1.51	84.4	422.89	1.67	87.4	475.49	1.84
		1.51		422.00	1.67		210.00	1.64
81.5	876.77		84.5	424.56	1	87.5	477.83	l
81.6	878.28	1.53	84.6	426.24	1.68	87.6	479.18	1.83
81.7	879.81	1.52	84.7	427.92	1.68	87.7	481.04	1.86
81.8	881.38	1.58	84.8	429.61	1.69	87.8	482.90	1.96
81.9	882.87	1.58	84.9	431.80	1.69	87.9	484.76	1.67
****	000.01	1.54	04.0	301.00	1.70	07.50	404.10	1.87
82.0	284.40		85.0	433.00		88.0	486.64	
82.1	885.95	1.54	85.1	484.71	1.70	88.1	488.52	1.88
82.2	387.49	1.55	85.2	436.42	1.71	88.2	490.40	1.89
32.8	889.05	1.55	85.8	438.18	1.78	88.3	492.29	1.89
82.4	890.61	1-56	85.4	439.85	1.72	88.4	494.19	1.90
	200.01	1.56	00.4	400.00	1.73	00.4	454.13	1.90
82.5	892.17		85.5	441.58	l	88.5	496.09	ĺ
82.6	898.74	1.57	85.6	448.31	1.78	88.6	498.00	1.91
82.7	895.31	1.57	85.7	445.05	1.74	88.7	500.92	1.93
82.8	396.89	1.48	85.8	446.80	1.74	88.8	500.92 501.94	1.93
82.9	89 8.48	1.56	85.9	448.55	1.76	1		1.93
83.0	400.07	1.59	86.0	448.55	1.76	88.9	503.77	1.93

Boiling Point, Centigrade.	Barometer in Millimetres.	Differ- ezace.	Boiling Point, Centigrade.	Barometer in Millimetres.	Differ- ence.	Boiling Point, Centigrade.	Barometer in Millimetres.	Differ- ence.
89.0	505.70		o 9 3 .0	588.88		97.0	681.98	
89.1	507.65	1.94	93.1	590.58	2-90	97.1	684.42	2.49
89.2	509.59	3.96	98.2	592.74	9.91	97.2	686.92	2.60
89.3	511.54	1.95	93.8	594.96	2.32	97.8	689.42	2.51
89.4	518.50	1.96	98.4	597.18	2.22	97.4	691.94	2.51
	010.00	1:97	55.7	507.10	2:36		001.04	2.52
89.5	515.47		93.5	599.41		97.5	694,46	
89.6	517.44	1.97	93.6	601.65	2.94	97.6	696.98	2.53
89.7	519.42	1.96	93.7	603.89	2.94	97.7	699.52	2.64
89.8	521.40	1.98	93.8	606.14	2.25	97.8	702.06	2.54
89.9	523.89	1.99	93.9	608.40	2.26	97.9	704.62	2.55
1 33.3		2.00	00.0	400.40	2.26		104.02	2.56
90.0	525.39		94.0	610.66		98.0	707.17	
90.1	527.40	2.00	94.1	612.98	2-27	98.1	707.17	2.57
90.2	529.41	2.01	94.2	615.21	2.28	98.2	712.81	2.67
90.3	531.42	2.03	94.8	617.50	2.29	98.3	714.90	2.58
90.4	533.44	2-03	94.4	619.79	2.29	98.4	717.49	2.59
00.2	555.71	2.08	04.4	010.10	3-80	2017	111.20	2.60
90.5	585.47		94.5	622.09		98.5	720.08	
90.6	587.51	2.04	94.6	624.39	2.31	98.6	722.69	2.61
90.7	539.55	2.04	94.7	626.71	2.81	98.7	725.30	2.61
90.8	541.60	2.08	94.8	629.98	2.32	98.8	727.93	2.62
90.9	518.65	2.06	94.9	631.36	2.83	98.9	780.55	2.68
	010.00	2.06	04.0	001.00	2.83	00.0	100.00	2.64
91.0	545.71		95.0	633.69		99.0	733.19	
91.1	547.78	2.07	95.1	636.08	2.84	99.1	735.84	2.64
91.2	549.86	2.07	95.2	638.38	2.35	99.2	788.49	2.65
91.8	551.94	2.08	95.8	640.74	2.36	99.8	741.15	2.66
91.4	554.08	2.09	95.4	648.10	2.86	99.4	748.82	2.67
		2.09			2.87			2.68
91.5	556.12		95.5	645.48		99.5	746.50	
91.6	558.22	2.10	95.6	647.86	2,88	99.6	749.15	2.68
91.7	560.38	2.11	95.7	650.24	2.39	99.7	751.87	2.69
91.8	562.44	9.11	95.8	652.68	2.89	99.8	754.57	2.70
91.9	564.56	2.12	95.9	655.04	2.40	99.9	757.28	9.71
		2.12			2.41			2.72
92.0	566.69		96.0	657.44		100.0	760.00	
92.1	568.82	9.18	96.1	659.86	2.42	100.1	762.73	2.72
92.2	570.96	2.14	96.2	662.28	2.49	100.2	765.46	2.73
92.8	578.11	2.15	96.3	664.71	2.48	100.8	768.20	2.74
92.4	575.27	2.15	96.4	667.15	2.44	100.4	770.95	2.75
		9.16			9-44			2.76
92.5	577.48		96.5	669.59		100.5	778.71	
92.6	579.5 9	2.17	96.6	672.05	2.48	100.6	776.47	2.77
92.7	581.77	2.17	96.7	674.51	2.46	100.7	779.25	2.77
92.8	598.95	2.18	96.8	676.97	9.47	100.8	782.08	2.76
92.9	596.14	2.19	96.9	679.45	2.47	100.9	784.82	2.79
93.0	588.38	2.19	97.0	681.98	2.48	101.0	787.62	2.60
1		1			1			1

TABLE XXVI.

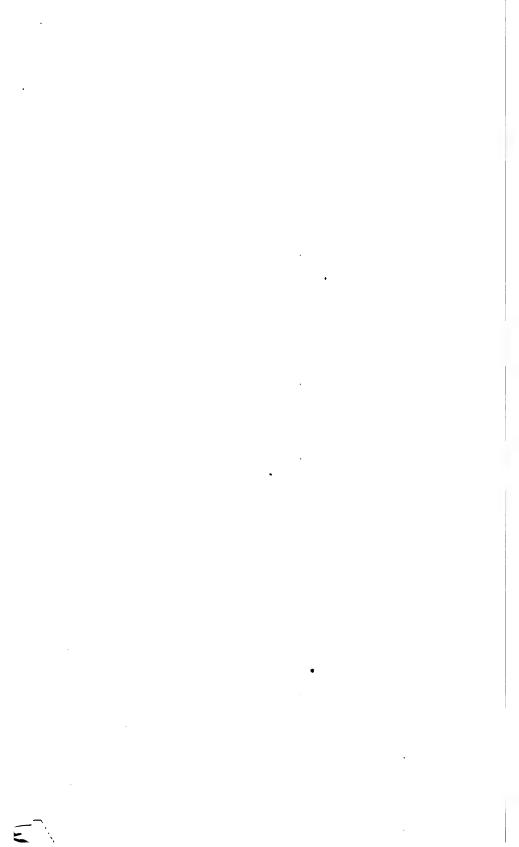
BAROMETRIC PRESSURES CORRESPONDING TO TEMPERATURES OF THE BOILING POINT OF WATER,

EXPRESSED IN ENGLISH INCHES FOR TEMPERATURES OF FAHRENHRIT.

REDUCED FROM RESEAULT'S TABLE, REVISED BY MORITE.

Boiling Point, Fahren.	Barom- etar in English Inches.	Differ- ence.	Boiling Point, Fahren.	Barom- eter in English Inches.	Differ-	Boiling Point, Fahren.	Barom- eter in English Inches.	Difference.	Boiling Point, Fahren.	Barom- eter in English Inches.	Differ-
0 185.0 185.1 185.2 185.3 185.4	17.048 17.085 17.122 17.160 17.197	0.037 .037 .037 .037	188.0 188.1 188.2 188.8 188.4	18.195 18.235 18.274 18.314 18.358	0.039 1039 1089 -040	0 191.0 191.1 191.2 191.3 191.4	19.407 19.448 19.490 19.532 19.578	0.042 .043 .042 .048	0 194.0 194.1 194.2 194.3 194.4	20.685 20.729 20.773 20.817 20.861	110.0 110. 110. 110.
183.5 183.6 183.7 185.8 185.9	17.285 17.272 17.310 17.348 17.355	.038 .038 .038 .038	188.5 188.6 188.7 188.8 188.9	18.893 18.432 18.472 18.512 18.552	.040 .040 .040 .040	191.5 191.6 191.7 191.8 191.9	19.615 19.657 19.699 19.741 19.783	.042 .043 .043 .042	194.5 194.6 194.7 194.8 194.9	20.905 20.949 20.993 21.038 21.082	110. 110. 110. 110.
186.0 186.1 186.2 186.3 186.4	17.423 17.461 17.499 17.537 17.575	.038 .038 .038 .038	189.0 189.1 189.2 189.3 189.4	18.592 18.632 18.672 18.712 18.753	1040 1040 1040 1040	192.0 192.1 192.2 192.3 192.4	19.825 19.868 19.910 19.952 19.995	.042 .043 .043 .043	195.0 195.1 195.2 195.3 195.4	21.126 21.171 21.216 21.260 21.305	.045 .045 .045 .045
196.5 186.6 186.7 186.9	17.614 17.652 17.690 17.729 17.767	.038 .038 .038 .038	189.5 189.6 189.7 189.8 189.9	18.798 18.883 18.874 18.914 18.955	.040 .040 .041 .041	192.5 192.6 192.7 192.8 192.9	20.087 20.060 20.128 20.166 20.208	.043 :043 :043 :043 :043	195.5 195.6 195.7 195.8 195.9	21.850 21.895 21.440 21.485 21.530	.045 .045 .045 .045
187.0 187.1 187.2 187.8 187.4	17.896 17.844 17.883 17.922 17.961	.039 .039 .039 .039	190.0 190.1 190.2 190.3 190.4	18.996 19.036 19.077 19.118 19.159	.041 .041 .041 .041	198.0 193.1 193.2 193.3 193.4	20.251 20.294 20.888 20.881 20.424	.048 .048 .048 .048	196.0 196.1 196.2 196.8 196.4	21.576 21.621 21.666 21.712 21.758	.045 .045 .046 .046
187.5 187.6 187.7 187.8 187.9 188.0	18.000 18.089 18.078 18.117 18.156 18.195	.039 .039 .039 .039	190.5 190.6 190.7 190.8 190.9 191.0	19.200 19.241 19.283 19.824 19.865 19.407	.041 .041 .041 .041 0.041	193.5 193.6 193.7 193.8 193.9 194.0	20.467 20.511 20.554 20.598 20.641 20.685	.048 .048 .044 .044 0.044	196.5 196.6 196.7 196.8 196.9 197.0	21.803 21.849 21.895 21.941 21.967 22.033	.046. 046. 046. 046.

Boiling Point, Fahren.	Barom- eter in English Inches.	Difference.	Boiling Point, Fahren.	Barom- eter in English Inches.	Difference.	Boiling Point, Fahren.	Barom- eter in English Inches.	Differ- ence.	Boiling Point, Fahren.	Barom- eter in English Inches.	Difference.
0	00.000		0			0			0		
197.0	22.033	0.046	201.0	28.948	0.049	205.0	25.990	0.058	209.0	28.180	0.087
197.1 197.2	22.079 22.125	.046	201.1	28.993 24.042	-040	205.1	26.048	-068	209.1	28.287 28.293	.067
197.2	22.172	-046	201.2	24.092	.060	205.8	26.096 26.149	.052	209.2	28.350	.057
197.4	22.218	.046	201.4	24.142	-050	205.4	26.149	.063	209.4	28.407	.057
151.4	22.210	.046	201.4	24.172	.080	200.4	20.202	.058	200.9	28.407	-067
197.5	22.264		201.5	24.191	000	205.5	26.255		209.5	28.464	
197.6	22.811	.047 .047	201.6	24.241	.080	205.6	26.309	.083	209.6	28.521	-057
197.7	22.358	-047	201.7	24.291	.060	205.7	26.362	.054	209.7	28.579	.057
197.8	22.404	.047	201.8	24.841	.050	205.8	26.416	.054	209.8	28.686	.087
197.9	22.451	.047	201.9	24.891	-050	205.9	26.470	.054	209.9	28.698	.058
\(\frac{1}{2} = \frac{1}{2} =								1000			1000
198.0	22.498	-047	202.0	24.443	-050	206.0	26.528	.054	210.0	28.751	.088
198.1	22.545	-047	202.1	24.492	-050	206.1	26.577	.054	210.1	28.809	.048
198.2	22.592	.047	202.2	24.542	.080	206.2	26.681	.054	210.2	28.866	.058
198.3	22.639	.047	202.8	24.598	.051	206.3	26.685	.054	210.8	28.924	.068
198.4	22.686	-047	202.4	24.644	.051	206.4	26.740	-054	210.4	28.982	.058
198.5	22.784		202.5	24.694		206.5	26.794		210.5	29.040	
198.6	22.781	-047	202.6	24.745	-051	206.6	26.848	-084	210.6	29.098	.088
198.7	22.829	.047	202.7	24.796	-081	206.7	26.908	-054	210.7	29.156	.058
198.8	22.876	.048	202.8	24.847	.051	206.8	26.957	-055	210.8	29.215	.048
198.9	22.924	.048	202.9	24.898	-051	206.9	27.012	-056	210.9	29.278	.058
1		.048			-051			.066		ĺ	.059
199.0	22.971	040	203.0	24.949		207.0	27.066		211.0	29.831	
199.1	23.019	.048	203.1	25.000	.051 -051	207.1	27.121	-055	211.1	29.390	.059
199.2	23.067	.048	203.2	25.051	.061	207.2	27.176	-055	211.2	29.449	.059
199.3	23.115	.048	203.3	23.103	.051	207.8	27.281	.058	211.8	29.508	.059
199.4	28.168	.049	203.4	25.154	.052	207.4	27.286	.055	211.4	29.566	.059
100 -	00 011		000 5	0.5 000							
199.5	28.211 28.259	.048	203.5 203.6	25.206	.052	207.5	27.841	.085	211.5	29.625	.089
199.5	23.209	.048	203.6	25.257 25.809	.052	207.6	27.397 27.452	.066	211.6	29.684	.059
199.8	23.356	-048	203.7	25.361	.052	207.7	27.452	.055	211.7 211.8	29.711 29.803	-069
199.9	23.405	.048	203.9	25.418	-083	207.9	27.568	-086	211.9	29.862	.089
-33.3		-049		20.110	.052		2	-056		20-002	.059
200.0	28.458	_	204.0	25.465		208.0	27.618		212.0	29.922	
200.1	28.502	.049	204.1	25.517	.052	208.1	27.674	.056	212.1	29.981	.060
200.2	28.550	-049	204.2	25.569	-062	208.2	27.780	.056	212.2	30.041	.060
200.3	23.599	-049	204.3	25.621	.052	208.8	27.786	.056	212.3	30.101	.060
200.4	23.648	-049 -049	204.4	25.674	.052	208.4	27.842	.066	212.4	30.161	-060
		.049			1002			.036		1	-060
200.5	23.697	.049	204.5	25.726	.052	208.5	27.898	.056	212.5	80.221	-060
200.6	23.746	.049	204.6	25.779	.058	208.6	27.954	.086	212.6	80.281	.060
200.7	23.795	-049	204.7	25.881	.053	208.7	28.011	.056	212.7	30.341	.060
200.8	28.845	.049	204.8	25.884	.058	208.8	28.067	.056	212.8	30.401	.060
200.9	23.894	0.049	204.9	25.937	0.053	208.9	28.128	0.067	212.9	80.461	0.060
201.0	28.943		205.0	25.990		209.0	28.180		218.0	30.522	
<u> </u>	<u> </u>	<u> </u>	1			1			t		

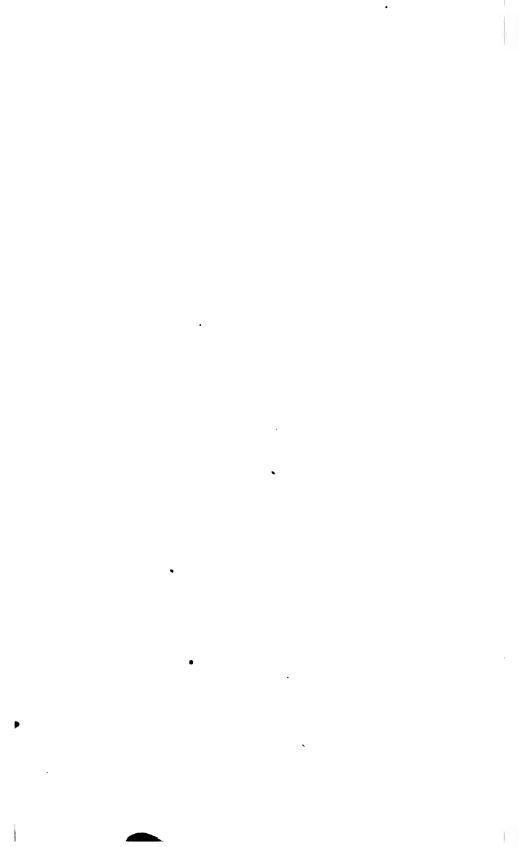


APPENDIX

30

THE HYPSOMETRICAL TABLES.

COMPARISON OF THE DIFFERENT MEASURES OF LENGTH MOST GENERALLY USER FOR INDICATING ALTITUDES.



COMPARISON

OF THE MEASURES OF LENGTH MOST GENERALLY USED FOR INDICATING ALTITUDES.

It is too well known that the measures used in scientific researches among civilized nations are not uniform, as the convenience of all would require. In France the metre is employed; in England and North America, the yard and its third part, the English foot; in Germany, most commonly, the Old French or Paris foot, the sixth part of the French toise called the *Toise du Pérou*; at the same time, however, though not so extensively, the Rhine foot, in Denmark and Holland, and especially in Prussia, where it has been declared, under the name of Prussian foot, the legal measure in that kingdom; in Austria, the klaster of Vienna and its sixth part, the foot of Vienna; in Switzerland, the Swiss or federal foot, which has been adjusted to the metrical system, and is three tenths of a metre; and so on.

The numerous altitudes ascertained, either by private efforts, or in connection with the public works, and quite especially with the extensive geodetic operations carried on by the governments of these various countries for the survey of a regular map, are expressed in the measures respectively adopted by each of them. These heights, however, before they can be compared, require to be uniformly reduced to any one of these measures. Their relation to each other, therefore, is given here, together with numerous reduction tables, designed to save both the useless expenditure of time and the almost unavoidable errors arising from so numerous reductions.

The exact relation of the standard measures above mentioned is not easily ascertained, and the numbers given by the best authorities by no means always agree; for the manufacture of exact copies of a standard scale, and the accurate comparison of it, require considerable skill, and belong to the most delicate operations of physics. The numbers used for computing the following tables have been adopted, after a careful review of the authorities, as the most reliable. A few words on the most important original legal standards of measures may not be unwelcome. For further details on the subject the reader is referred principally to Dove's work, *Maas und Messen*, 2d edition, Berlin, 1835.

The principal original, legal standards are the following: -

1. The Toise du Pérou, the old French standard, made in 1735, in Paris, by Langlois, under the direction of Godin, is a bar of iron which has its standard length at the temperature of 13° Reaumur. It is known as the Toise du Pérou, because it was used by the French Academicians Bouguer and La Condamine in their measurement

of an arc of the meridian in Peru. What follows will show that it may almost be called the only common standard, to which all the others are referred for comparison.

- 2. The Metre is a standard bar of platina, made by Lenoir in Paris, which has its normal length at the temperature of zero Centigrade, or the freezing point. Its length is intended to make it a natural standard, and to represent the ten-millionth part of the terrestrial arc comprised between the equator and the pole, or of a quarter of the meridian. The length of this arc given by the measurement ordered for the purpose by the Assemblée Nationale, of the arc of the meridian between Barcelona, through France, to Dunkirk, combined with the measurements previously made in Peru and in Lapland, gave for the distance of the equator from the pole 5,130,740 toises, with an ellipticity of $\frac{1}{334}$, and for the length of the metre 443.29596 lines of the toise du Perou, assumed to be 443.296 lines, or 3 feet 11.296 lines. This last quantity was declared in 1799 to be the length of the legal metre, and vrai et définitif, and is the length of Lenoir's platina standard. Later and more extensive measurements in various parts of the globe, however, seem to indicate that this quantity is somewhat too small. The latest and most exact results we now possess, combined and computed by Bessel, would make the quarter of the meridian 10,000,856 metres, and the metre = 443.29979 Paris lines; Schmidt's computation would make it 443.29977 lines, and both numbers are confirmed by Airy's results. The legal metre is thus, in fact, as Dove remarks, a legalized part of the toise du Pérou, and this last remains the primitive standard. But it must be added that a natural standard, in the absolute sense of the word, is a utopian one, which ever-changing Nature never will give us. The metre is, for all practical purposes, what it was intended to be, a natural standard; though it must be confessed that, in practice, the question is not whether and how far a standard is a natural or a conventional one, but how readily and accurately it can be obtained, or recovered when lost.
- 3. The English Standard Yard is a brass bar, made by Bird in 1760, which was declared, by act of Parliament, 1st May, 1825, the legal measure of length when at the temperature of 62° Fahrenheit, under the name of Imperial Standard. Another standard, sometimes also called Parliamentary Standard, was made by Bird in 1758. Sir George Shuckburgh found both to be nearly identical, at least within 0.0002 of an inch. (Philos. Trans. for 1798, p. 170.)

Another scale of brass, however, made by Troughton for Sir George Shuckburgh, described in the *Philosophical Transactions for* 1798, and known as Shuckburgh's scale, obtained among scientific men, perhaps, a higher degree of authority, on account of the great accuracy of its division, and of its apparatus, devised by Troughton, for delicate comparisons. That scale was used by Captain Kater, in 1818, in his researches for determining the length of the pendulum beating a second at London, and also the length of the metre, expressed in English inches of the imperial standard. (*Phil. Trans. for* 1818.)

Numerous attempts to determine the relation between the English and the French measures show no inconsiderable discrepancies in their results. Omitting the older comparisons with the toise, we give here the value of the metre in English imperial inches, as resulting from the most reliable comparisons.

A standard scale made and divided by Troughton, and in all particulars identical

USED FOR INDICATING ALTITUDES.

with Shuckburgh's scale, was brought to France in 1801 by Pictet. The comparison of it with the standard metre, made by Prony, Legendre, and Méchain, gave, after due reduction of the two standards to their respective normal temperatures,

1 metre at 32° Fahr. = 39.371 English imperial inches at 62° Fahr.

This determination was adopted for all reductions in Kelly's *Universal Cambist*, and in the French translation of the work, published in Paris in 1823.

A new comparison was made with great care by Captain H. Kater, in 1818. (See *Philos. Trans. for* 1818, p. 103.) The standards used were a brass scale metre, by Fortin, terminated with parallel planes (*mètre à bouts*), and a bar of platina on which the length of the metre was marked by two very fine lines (*mètre à traits*). Both were compared with Shuckburgh's scale, and a double series of experiments gave as the mean result:

Brass metre at 32° Fahr. = 39.37076 inches of Shuckburgh's scale at 62° Fahr.

On this value of the metre are based the reduction tables by Matthieu, published yearly in the *Annuaire du Bureau des Longitudes*; and it has come into general use, both in Europe and in this country.

Captain Kater gives besides, in the same paper, p. 109, note, the value of the metre compared with Bird's Parliamentary standard as being

1 metre at 32° F. = 39.37062 imp. inches of Bird's Parliamentary standard at 62° F. This value has been adopted by Dove, as being the legal one, in his reduction tables in his work, *Maas und Messen*, p. 175, &c., and by many German authorities.

According to Baily's experiments, made in 1835, when engaged in constructing a new standard for the Royal Astronomical Society (*Memoirs R. Ast. Soc.*, Vol. IX.), the value of the metre is (Lee, Collection of Tables and Formula, p. 62)

1 metre at 32° F. = 39.370092 imperial standard inches at 62° F.

The original legal standards having been lost in the fire which destroyed, several years ago, the Parliament Houses, an act of Parliament provided for the construction of new ones; but as the report of the committee having charge of the construction of the new British standard has not yet been published, the discussion of the subject must be postponed.

The value adopted in the following tables, is that determined by Captain Kater, viz. 1 metre = 39.37079 English inches.

It may not be out of place to remark that Schumacher, in the first edition of his Sammlung von Hülfstafeln, used the value 1 metre = 39.3827 English inches, as given in the Base du Système Métrique; but this number, which expresses the relation of both standards when at the freezing point, becomes 39.37079 when they are respectively reduced to their normal temperatures. Schumacher's tables, therefore, must be corrected accordingly.

4. The actual standard of length of the United States is a brass scale of eighty-two inches in length, prepared for the Coast Survey of the United States, by Troughton of London, meant to be identical with the English Imperial Standard, and deposited in the office of weights and measures. The temperature at which it is a standard is 62° Fahrenheit, and the yard measure is between the 27th and 63d inches of the

scale. (See Report on the Construction and Distribution of Weights and Measures, by Prof. A. D. Bache, 1857.)

Hassler, first Superintendent of the United States Coast Survey, made an elaborate comparison of eleven different standard metres with the brass scale of eighty-two inches, by Troughton. Three of the standard metres, certified to be correct by high authorities, seem to deserve especial confidence: — 1. An iron metre, presented to Mr. Hassler by Tralles, which was one of the three that Tralles had made by Lenoir at the same time with those distributed to the committee on the weights and measures.

2. Another metre of iron, also by Lenoir, verified by Bouvard and Arago, and declared by them to be identical with the original.

3. A platina standard by Portin, verified by Arago, and found to be $\frac{1}{1000}$ of a millimetre too long, for which error allowance was made. Their comparison with the Troughton scale at the temperature of the freezing point gave:

- 1. Iron metre of Tralles = 39.3809171 inches of the Troughton scale.
- 2. Iron metre of Lenoir = 39.3799487 " "
- 3. Platina metre of Fortin = 39.3804194 " "

Or, correcting for expansion, and reducing them to their respective standard temperatures:

- 1. Iron metre of Tralles at 32° F. = 39.36850 2. Iron metre of Lenoir at 32° F. = 39.36754 2. Plating water of Faction 4 20° F. = 39.36754 2. Plating water of Faction 4 20° F. = 39.36850 2. Plating water of Faction 4 20° F. = 39.36850
- 3. Platina metre of Fortin at 32° F. = 39.36789) ton scale of 82 inches at 62° F

Hassler, in his Report to Congress on Weights and Measures, in 1832, adopts the first value, viz.:

1 metre at 32° F. = 39.3809171 inches of the Troughton scale at 32° F; and the Troughton scale was declared the United States standard, from which copies were to be made.

This value materially differs from those given by other careful comparisons, while, on the other hand, the close accordance of the numbers corresponding to the various standard metres proves the accuracy of Hassler's method and comparison. It is, therefore, difficult not to ascribe, with Baily, this discrepancy to some inaccuracy in the length of the Troughton scale of 82 inches. But as that scale has been declared the standard of length of the United States, it seems better to call it, as is done in the Coast Survey Reports, the American yard, and its subdivisions the American foot and inch, and to consider it as a new standard, similar to, but not identical with, the English imperial standard. The value of the metre expressed in American standard inches is given in the Coast Survey Report for 1853, as

1 metre at 32° F. = 39.36850535 United States standard inches at 62° F.

We learn from the Report on Weights and Measures, by Prof. A. D. Bache, 1857, p. 18, that two copies of the new British standards, now in progress of construction, viz. a bronze standard, No. 11, and a malleable iron standard, No. 57, have been presented by the British government to the United States. A series of careful comparisons, made in 1856, by Mr. Saxton, under the direction of Prof. A. D. Bache, of the British bronze standard, No. 11, with the Troughton scale of eighty-two inches, showed that the British bronze standard yard is shorter than the American yard by 0.00087 inch.

USED FOR INDICATING ALTITUDES.

Comparisons of the American standards with new French standards, recently presented to the United States by the French government, are still in progress.

For the present, however, it seems best to adhere to the value of the metre, expressed in American standard inches, adopted by the Coast Survey as given above. From this value the separate tables, which will be found below, for the reduction of the American yard and foot, were computed.

- 5. The Klaster of Vienna is a silver line let into a prismatic bar of iron, on which the length of the klaster was engraved by Voigtländer. It has its normal length at 13° Reaumur, and was declared by law, in 1816, the standard Klaster of Vienna. On the same silver line the French toise is marked, from the standard toise sent, in 1760, by La Caille and La Condamine to the Observatory of Vienna. According to a recent and very careful comparison by Struve (Mem. of the Austrian Acad., Vol. V., I. p. 117), the value of the klaster of Vienna is 0.9730317 toise du Pérou.
- 6. The *Prussian Foot* is marked on a standard iron bar, 3 feet long, made by Pistor in Berlin; it is a standard at the temperature of 13° Reaumur. The length of the Prussian foot was declared by law to be = 139.13 lines of the toise du Pérou.
- 7. A Mexican Vara, the standard length, brought from Mexico at the close of the war, by Major Turnbull of the Topographical Engineers, was presented to the Office of Weights and Measures. This standard was made by soldering sheet-brass upon the tinned surface of an iron bar. A careful comparison of its length with the American standard was made under the direction of Prof. Bache, which gave its length to be = 32.9682 inches at 58°.7 Fahrenheit, or 32.9680 when reduced to 62° Fahrenheit.

The relation of that particular Mexican standard to the Spanish standard not being known, it was thought better to adopt, for the present, the value of the Spanish Vara, and of its third part, the Castilian foot, found in Thionville, Traité des Poids et Mesures, &c., in Balbi's Abrégé de Géographie, viz. 1 vara = 0.847965 metre.

From the fundamental equations indicated above have been derived all those which have been used for computing the reduction tables given in the Appendix. At the head of each table will be found the value from which it was computed.

The tables are so arranged as to give directly the reduction of any whole number not exceeding three or four figures, and larger numbers within the limits needed for altitudes, by means of a single addition.

Example.

Reduce 25,351 English feet into metres.

In Table XVI., on the line beginning with 25,000 and in the column headed 300, take for 25,300 = 7711.30 metres.

In the second part of the table, on the line beginning with 50, and in column headed 1, take for

51 = 15.54 "

English feet 25,351 = 7726.84

The fractions, which seldom occur, are treated as whole numbers, taking care only properly to move the decimal point.

Tables XL. to XLIV. will be found convenient for converting fractional parts of a toise or of a foot into each other.

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TO CONVERT

FRENCH TOISES

INTO DIFFERENT MEASURES OF LENGTH.

I, CONVERSION OF FRENCH TOISES INTO METRES.

1 Toise = 1.94909631 Metre.

Toines.					Un	ite.				
Tens.	0.	1.	2.	8.	4,	5.	ß.	7.	8.	9.
	Motres.	Metres.	Motres.	Motres.	Motres.	Motres.	Metros.	Motres.	Motres.	Metres.
0	0.000	1.949	3.898	5.847	7.796	9.745	11.694	18.648	15.592	17.541
10	19.490	21.439	23.388	25.887	27.287	29.286	81.185	33.124	85.078	37.0 2 2
20	88.981	40.980	42.879	44.828	46.777	48.726	50.675	52.624	54.578	56.522
80	58.471	60.420	62.369	64.318	66.267	68.216	70.165	72.114	74.068	76.912
40	77.961	79.911	81.860	88.809	85.758	87.707	89.656	91.605	93.554	95.503
50	97.452	99.401	101.850	108.299	105.248	107.197	109.146	111.095	113.044	114.993
60	116.942	118.991	120.840	122.789	124.788	126.687	128.686	180.585	182.534	184.484
70	186.433	188.882	140.881	142.280	144.229	146.178	148.127	150.076	152.025	153.974
80	155.928	157.872	159.821	161.770	168.719	165.668	167.617	169.566	171.515	173.464
90	175.418	177.862	179.311	181.260	183.209	185.158	187.108	189.057	191.006	192.955
					Hun	freds.				
Thousands.	0.	100.	200.	200.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	0.00	194.90	889.81	584.71	779.61	974.52	1169.42	1864.83	1559.23	1754-13
1000	1949.04	2143.94	2338.84	2588.75	2728.65	2923.55	3118.46	3312.36	3507.27	3702.17
2000	3898.07	4092.98	4287.88	4482.78	4677.69	4872.59	5067.50	5262.40	5457.30	5652.21
8000	5847.11	6042.01	6286.92	6481.82	6626.72	6821.63	7016.53	7211.44	7406.34	7601-24
4000	7796.15	7991.05	8185.95	8880.66	8575.76	8770.66	8965.57	9160.47	9355.38	9550.28
5000	9745.18	9940.09	10185.0	10829.9	10524-8	10719.7	10914.6	11109.5	11804.4	11499.3
	II. Co	NVERSI	ON OF		INTO FI	RENCH (R PARI	S PEET	•	
Toises.					Un	its.				_
Tens.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Par Feet	Par. Feet.	Par. Feet.	Par.Feet.	Par. Feet.	Par Foot.	Par.Foot.	Par. Foot.	Par Foot	Par Feet
0	0.00	6	12	18	24	80	86	42	48	54
10	60	66	72	78	84	90	96	102	108	114
20	120	126	182	188	144	150	156	162	168	174
80	180	186	192	198	204	210	216	222	228	234
40	240	246	252	258	264	270	276	282	288	294
50	800	806	812	818	324	880	836	842	848	354
60	860	866	872	878	384	890	396	402	408	414
70	420	426	482	488	444	450	456	462	468	474
80	480	486	492	498	504	510	516	522	528	534
90	840	546	552	558	564	570	576	582	588	594

III. CONVERSION OF FRENCH TOISES INTO ENGLISH FEET AND DECIMALS.

1 Toke - 6.8945916 English Feet.

Toises.		Units.											
Tons.	0.	1.	2.	8.	4.	5,	6.	7.	s.	9.			
		1 -			Eng. feet.		_						
0	0.000	1			1				51.157				
10	63.946				89.524		102.313	1	1	ľ			
20	11	l .	ł	ł .	158.470		166.259		1				
3 0					217.416		280.205						
40	255.784	262.178	268.573	274.967	281. 86 2	287.757	294.151	300.546	806.940	318.83			
50	319.729	826.124	332.519	838.918	345.308	351.702	859.097	364.492	370.886	877.28			
60	383.675	390.070	396.465	402.859	409.254	415.648	422.048	428.438	484.832	441.22			
70	11	1	l	(473.200		485.989	4		1			
80	i	1	Į.	i e	537.146								
90	11	•)	1	601.091		1	1	i				
Thousands.					Hund	reds.							
	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.			
0	Eng. feet. 0.0				Eng. feet. 2557.8		Eng feet. 3836.8		Eng feet. 5115.7				
1000	6394.6	1	l	1	8952.4		10231.3		ì				
2000				1	15347.0		1	1	i	1			
8000	41			1	21741.6		l	1	1				
4000	Я			ł									
5000	R .				29136.2		1		1				
J-000	110101210	02012.4	99701.9	88891.8	34580.5	85170.2	30809.7	36149.2	37038.6	37728.			
			N OF F	RENCH	TOISES	INTO A	MERICA			37728.			
2000			N OF F	RENCH	TOISES	INTO A	MERICA			37728.			
Toless.	IV. COI	(VERSIO	N OF F	RENCH	TOISES 942206 Ame	INTO A	MERICA	N FEET	•				
			N OF F	RENCH	TOISES	INTO A	MERICA			9.			
Toises. Tens.	O. Am. Feet.	T. Am. Feet	N OF F	RENCH oise — 6.8	TOISES 042206 Ame	INTO A srican Feet its. 5. Am. Feet	MERICA 6.	7.	S. Am Feet.	9.			
Toises. Tens.	O. Am. Feet. 0.000	1. Am. Feet 6.394	2. Am Feet. 12.788	RENCH cise — 6.8 3. Am Feet. 19.183	TOISES 942206 Ame Un 44. Am. Feet 25.577	INTO A prican Feet its. 5. Am. Feet 31.971	G. Am Feet 38.365	7. Am Feet. 44.760	Am. Feet. 51.154	9. Am.Fee 57.54			
Toises. Tens. 0 10	IV. COI	1. Am.Feet 6.394 70.336	2. Am. Feet. 12.788 76.731	RENCH cise = 6.8 3. Am Feet. 19.183 83.125	TOISES 942905 Ame Un 4 Am. Feet 25.577 89.519	INTO A srican Feet its. 5. Am. Feet 31.971 95.918	6. Am. Feet 38.365	7. Am Feet. 44.760 108.702	Am. Feet. 51.154	9. Am.Fee 57.54 121.49			
Tolses. Tens. 0 10 20	O. Am. Feet. 0.000 63.942 127.884	1. Am. Feet 6.394 70.336 184.279	2. Am Feet. 12.788 76.731 140.678	3. Am. Feet. 19.183 83.125 147.067	TOISES 42905 Ame Un Am. Feet 25.577 89.519 153.461	INTO A prican Feet its. 5. Am. Feet 31.971 95.918 159.855	MERICA Am Feet 38.865 102.808 166.250	7. Am Feet. 44.760 108.702 172.644	Am. Feet. 51.154 115.096 179.038	9. Am.Fee 57.54 121.49 185.43			
Tolses. Tens. 0 10 20 80	O.000 68.942 127.884 191.827	1. Am. Feet 6.394 70.336 134.279 198.221	2. Am Feet. 12.788 76.731 140.673 204.615	3. Am Feet. 19:183 83.125 147.067 211.009	TOISES 942205 Ame Un Am. Feet 25.577 89.519 153.461 217.403	INTO A srican Feet its. 5. Am. Feet 31.971 95.918 159.855 228.798	6. Am Feet 38.365 102.308 166.250 230.192	7. Am Feet. 44.760 108.702 172.644 286.586	S. Am. Feet. 51.154 115.096 179.038 242.980	9. Am. Fee 57.54 121.49 185.43 249.37			
Toises. Tens. 0 10 20	O.000 68.942 127.884 191.827	1. Am. Feet 6.394 70.336 134.279 198.221	2. Am Feet. 12.788 76.731 140.673 204.615	3. Am Feet. 19:183 83.125 147.067 211.009	TOISES 42905 Ame Un Am. Feet 25.577 89.519 153.461	INTO A srican Feet its. 5. Am. Feet 31.971 95.918 159.855 228.798	MERICA Am Feet 38.865 102.808 166.250	7. Am Feet. 44.760 108.702 172.644 286.586	S. Am. Feet. 51.154 115.096 179.038 242.980	9. Am. Fee 57.54 121.49 185.43 249.37			
Tolses. Tens. 0 10 20 80	0.000 68.942 127.884 1291.827 255.769	1. Am. Feet 6.394 70.336 134.279 196.221 262.163	2. Am Feet 12.788 76.731 140.673 204.615 268.557	RENCH oise = 6.8 Am Feet. 19.183 83.125 147.067 211.009 274.951	TOISES 942205 Ame Un Am. Feet 25.577 89.519 153.461 217.403	INTO A prican Feet its. 5. Am. Feet 31.971 95.918 159.855 223.798 287.740	6. Am Feet 38.365 102.308 166.250 230.192	7. Am Feet. 44.760 108.702 172.644 236.586 300.528	S. Am Feet. 51.154 115.096 179.038 242.980 306.923	9. Am. Fee 57.54 121.49 185.43 249.37 813.31			
Toises. Tens. 0 10 20 30 40	0. Am. Feet. 0.000 63.942 127.884 191.827 265.769 819.711	1. Am. Feet 6.394 70.336 134.279 198.221 262.163 326.105	2. Am. Feet. 12.788 76.731 140.673 204.615 268.557 832.499	RENCH oise = 6.8 3. Am Feet. 19.183 83.125 147.067 211.009 274.951 388.894	TOISES 942906 Ame Un 4. Am. Feet 25.577 89.519 153.461 217.403 281.346	INTO A prican Feet its. 5. Am. Feet 31.971 95.918 159.855 228.798 287.740 851.682	MERICA Am Feet 38.365 102.308 166.250 230.192 294.134 858.076	7. Am Feet. 44.760 108.702 172.644 286.586 800.528	S. Am Feet. 51.154 115.096 179.038 242.980 306.923 370.865	9. Am.Fee 57.54 121.49 185.43 249.37 313.31			
Toises. Tens. 0 10 20 30 40	0. Am. Feet. 0.000 63.942 127.884 191.827 255.769 319.711 383.653	1. Am.Feet 6.394 70.336 134.279 198.221 262.163 326.105 390.047	2. Am. Feet. 12.788 76.731 140.673 204.615 268.557 352.499 896.442	RENCH oise = 6.8 3. Am Feet 19.183 83.125 147.067 211.009 274.951 388.894 402.886	TOISES 942906 American United States 1	INTO A rican Feet its. 5. Am. Feet 31.971 95.918 159.855 228.798 287.740 851.682 415.624	MERICA Am Feet 38.365 102.308 166.250 230.192 294.134 858.076	7. Am Feet. 44.760 108.702 172.644 286.586 800.528 364.470 428.413	S. Am Feet. 51.154 115.096 179.038 242.980 306.923 370.865 484.807	9. Am.Fee 57.54 121.49 185.43 249.37 813.31 377.25 441.20			
Toines. Tens. 0 10 20 80 40 50 60	0. Am. Feet. 0.000 63.942 127.884 191.827 255.769 319.711 383.653 447.595	1. Am.Feet 6.394 70.336 134.279 198.221 262.163 326.105 390.047 453.990	2. Am. Feet. 12.788 76.731 140.673 204.615 268.557 352.499 896.442 460.384	RENCH oise = 6.8 3. Am Feet 19:183 83:125 147.067 214.951 388.894 402.836 466.778	TOISES 942906 Ame 4a. Am. Feet 25.577 89.519 153.461 217.403 281.346 345.288 409.280 473.172	INTO A rican Feet its. 5. Am. Feet 31.971 95.918 159.855 228.798 287.740 851.682 415.624 479.566	MERICA 38.365 102.308 166.250 230.192 294.184 358.076 422.018 485.961	7. Am Feet. 44.760 108.702 172.644 286.586 800.528 364.470 428.413 492.355	S. Am Feet. 51.154 115.096 179.038 242.980 306.923 370.865 484.907 498.749	9. Am.Fee 57.54 121.49 185.43 249.37 813.31 377.25 441.20 505.14			
Toises. Tuns. 0 10 20 30 40 50 60 70	1V. COI 	1. Am.Feet 6.394 70.336 134.279 198.221 262.168 326.105 390.047 453.990 517.932	2. Am. Feet. 12.788 76.731 140.673 204.615 268.557 382.499 396.442 460.384 524.326	RENCH oise = 6.8 3. Am. Feet. 19.183 83.125 147.067 211.009 274.951 388.894 402.836 466.778 530.720	TOISES 942906 Ame 4a. Am. Feet 25.577 89.519 153.461 217.403 281.346 345.288 409.230	INTO A rican Feet its. 5. Am. Feet 31.971 95.918 159.855 2287.740 851.682 415.624 479.566 543.509	MERICA 38.365 102.308 166.250 230.192 294.134 358.076 422.018 485.961 549.003	7. Am Feet. 44.760 108.702 172.644 236.586 300.528 364.470 428.413 492.355 556.297	8. Am. Feet. 51.154 115.096 179.038 242.980 306.923 370.865 484.807 498.749 562.691	9. Am. Fee 57.54 121.49 185.43 249.37 313.31 377.25 441.20 505.14 569.08			
Toises. Tens. 0 10 20 30 40 50 60 70 80 90	1V. COI	1. Am. Feet 6.394 70.336 134.279 198.221 262.163 826.105 890.047 453.990 517.932 581.874	2. Am. Feet. 12.788 76.731 140.673 204.615 268.557 332.499 396.442 460.384 524.326 88.268	RENCH coise = 6.8 Am. Feet. 19.183 83.125 147.067 211.009 274.951 388.894 402.836 466.778 530.720 594.662	TOISES 942906 Ame Un 44. Am. Feet 25.577 89.519 153.461 217.403 281.346 345.288 409.230 473.172 537.114 601.057 Hune	INTO A rican Feet its. 5. Am. Feet 31.971 95.918 159.855 2287.740 851.682 415.624 479.566 543.509 607.451 ireds.	MERICA 38.365 102.308 166.250 230.192 294.134 858.076 422.018 485.961 549.003 613.845	7. Am Feet. 44.760 108.702 172.644 236.586 300.528 364.470 428.413 492.855 562.297 620.289	Am. Feet. 51.15.96 179.038 242.980 306.923 370.865 484.807 498.749 562.691 626.633	9. Am.Fee 57.54 121.49 185.43 249.37 813.31 377.26 441.20 505.14 569.08 683.02			
Toises. Tens. 0 10 20 30 40 50 60 70 80	1V. COI 	1. Am. Feet 6.394 70.336 134.279 198.221 262.163 826.105 890.047 453.990 517.932 581.874	2. Am. Feet. 12.788 76.731 140.673 204.615 268.557 332.499 396.442 460.384 524.326 88.268	RENCH oise = 6.8 3. Am. Feet. 19.183 83.125 147.067 211.009 274.951 388.894 402.836 466.778 530.720	TOISES 942906 Ame Un 44. Am. Feet 25.577 89.519 153.461 217.403 281.346 345.288 409.230 473.172 537.114 601.057 Hune	INTO A prican Feet its. 5. Am. Feet 31.971 95.918 159.855 228.798 287.740 851.682 415.624 479.566 543.509 607.451	MERICA 38.365 102.308 166.250 230.192 294.134 858.076 422.018 485.961 549.003 613.845	7. Am Feet. 44.760 108.702 172.644 236.586 300.528 364.470 428.413 492.355 556.297	Am. Feet. 51.15.96 179.038 242.980 306.923 370.865 484.807 498.749 562.691 626.633	9. Am.Fee 57.54 121.49 185.43 249.37 813.31 377.26 441.20 505.14 569.08 683.02			
Toises. Tens. 0 10 20 80 40 50 60 70 80 90	1V. COI	1. Am. Feet 6.394 70.336 134.279 198.221 262.163 826.105 890.047 453.990 517.932 681.874	2. Am. Feet. 12.788 76.731 140.673 204.615 268.557 382.499 396.442 460.384 524.326 588.268	RENCH cise = 6.8 Am. Feet. 19.183 83.125 147.067 211.009 274.951 388.894 402.836 466.778 530.720 594.662	TOISES 042906 Ame Un Am. Feet 25.5.77 89.519 153.461 217.403 281.346 345.288 409.280 473.172 537.114 601.057 Hune 4.00. Am. Feet.	5. Am. Feet 31.971 95.918 159.855 223.798 287.740 851.682 415.624 479.566 543.509 607.451 ireds. Am Feet	MERICA Am Feet 38.365 102.308 166.250 230.192 294.134 358.076 422.018 485.961 549.003 613.845 600. Am Feet	7. Am Feet. 44.760 108.702 172.644 286.586 300.528 364.470 428.413 492.855 556.297 620.239	8. Am. Feet. 51.154 115.096 179.038 242.980 306.923 370.865 484.807 498.749 562.691 626.683	9. Am. Fee 57.54: 121.49: 185.43: 249.37: 313.31: 377.25: 441.20 505.14: 569.08: 653.02:			
Toises. Tens. 0 10 20 80 40 50 60 70 80 90 Thousands.	1V. COI Am. Feet. 0.000 63.942 127.884 191.927 255.769 819.711 883.653 447.595 511.538 575.480 0.	1. Am. Feet 6.394 70.336 134.279 198.221 262.163 826.105 890.047 453.990 517.932 581.874	20. Am. Feet. 12.788 76.731 140.673 204.615 268.557 382.499 396.442 460.384 524.326 588.268 200. Am Feet. 1278.8	RENCH cise = 6.8 Am. Feet. 19.183 83.125 147.067 211.009 274.951 388.894 402.836 466.778 530.720 594.662 \$00. Am. Feet. 1918.8	TOISES 042906 Ame Un Am. Feet 25.5.77 Am. Feet 25.5.77 Language 4.0.230 473.172 537.114 601.057 Hunc Am. Feet 2557.7	INTO A krican Feet its. 5. Am. Feet 31.971 159.855 223.798 287.740 851.682 415.624 479.566 543.509 607.451 lreds. 500. Am Feet 8197.1	MERICA Am Feet 38.365 102.808 166.250 230.192 294.134 858.076 422.018 485.961 549.03 613.845 600. Am Feet 8836.5	7. Am Feet. 44.760 108.702 172.644 236.586 300.528 364.470 428.413 492.355 566.297 620.289 700. Am Feet. 4476.0	S. Am. Feet. 51.154 115.096 179.038 242.980 306.923 370.865 484.807 498.749 562.691 626.638 SOO. Am Feet. 5115.4	9. Am. Fee 57.54 121.49 185.43 249.37 313.31 377.25 441.20 505.14 569.08 683.02			
Toises. Tens. 0 10 20 30 40 50 60 70 80 90 Thousands.	1V. COI	1. Am. Feet 6.394 70.336 134.279 198.221 262.163 826.105 890.047 453.990 517.932 581.874 100. Am Feet 639.4 7033.6	2. Am. Feet. 12.788 76.731 140.673 204.615 268.557 332.499 396.442 460.384 524.326 588.268 200. Am Feet 1278.8 7673.1	RENCH coise — 6.81 Am. Feet. 19.183 83.125 147.067 2114.009 274.951 388.894 402.836 466.778 530.720 594.662 300. Am. Feet. 1918.3 8312.5	TOISES 4206 Ame Un 4. Am. Feet 25.577 89.519 153.461 217.403 281.346 345.288 409.230 473.172 537.114 601.057 Hunc 400. Am. Feet 2557.7 8951.9	INTO A prican Feet its. 5. Am. Feet 31.971 95.918 159.855 2287.740 851.682 415.624 479.566 543.509 607.451 ireds. 500. Am Feet 3197.1 9591.3	MERICA Am. Feet 38.3655 102.308 102.308 166.250 230.192 294.134 858.076 422.018 485.961 549.903 613.845 6000. Am. Feet 3836.5 10230.8	7. Am Feet. 44.760 108.702 172.644 236.586 300.528 364.470 428.413 492.355 562.297 620.289 700. Am Feet. 4476.0 10870.2	S. Am. Feet. 51.15.96 179.038 242.980 306.923 370.865 484.807 498.749 562.691 626.633 SOO. Am Feet. 5115.4 11509.6	9. Am. Fee 57.54 121.19 185.43 249.37 813.31 377.26 441.20 505.14 569.08 683.02 900. Am. Fee 5754.1 12149.6			
Toises. Tens. 0 10 20 30 40 50 60 70 80 90 Thousands.	1V. COI 1V. COI 10. 10. 10. 10. 10. 10. 10. 10	1. Am. Feet 6.394 70.336 134.279 198.221 262.163 826.105 890.047 453.990 517.932 581.874 100. Am Feet 639.4 7033.6 18427.9	2. Am. Feet. 12.788 76.731 140.673 204.615 268.557 332.499 396.442 460.384 524.326 588.268 200. Am Feet 1278.8 7673.1 14067.3	RENCH coise — 6.8 Am. Feet. 19.183 83.125 147.067 211.009 274.951 388.894 402.836 466.778 530.720 594.662 \$60. Am. Feet. 1918.3 8312.5 14706.7	TOISES 42906 Ame Un 4. Am. Feet 25.577 89.519 153.461 217.403 281.346 345.288 409.230 473.172 537.114 601.057 Hunc 400. Am. Feet. 2557.7 8951.9 15846.1	INTO A prican Feet its. 5. Am. Feet 31.971 95.918 159.855 2287.740 851.682 415.624 479.566 543.509 607.451 ireds. 500. Am Feet 3197.1 9591.3 15985.5	MERICA Am. Feet 38.365 102.308 166.250 2394.134 858.076 422.018 485.961 549.803 613.845 600. Am. Feet 8836.5 10230.8 16625.0	7. Am Feet. 44.760 108.702 172.644 236.586 300.528 364.470 428.413 492.855 560.297 620.239 700. Am Feet. 4476.0 10870.2 17264.4	S. Am. Feet. 51.154 115.096 179.038 242.980 306.923 370.865 434.807 498.749 562.691 626.633 SOO. Am. Feet. 5115.4 11509.6 17903.8	9. Am. Fee 57.54 121.49 185.43 249.37 313.31 377.25 441.20 505.14 569.08 633.02 4m. Fee 5754.1 12149.4 18543.1			
Toises. Tens. 0 10 20 30 40 50 60 70 80 90 Thousands.	1V. COI 1. Am. Feet. 0.000 63.942 127.884 191.827 255.769 819.711 983.653 447.595 511.538 575.480 0. 6394.2 12788.4 19182.7	1. Am. Feet 6.394 70.336 134.279 198.221 262.168 326.105 390.047 453.990 517.932 581.874 100. Am Feet 639.4 7033.6 18427.9 19822.1	2. Am. Feet. 12.788 76.731 140.673 204.615 268.557 332.499 896.442 460.384 524.326 588.268 200. Am. Feet. 1278.8 7673.1 14067.3 20461.5	RENCH oise = 6.8 3. Am Feet. 19.183 83.125 147.067 211.009 274.951 388.894 402.886 466.778 530.720 594.662 \$00. Am Feet. 1918.3 8312.5 14706.7 21100.9	TOISES 4206 Ame Un 4. Am. Feet 25.577 89.519 153.461 217.403 281.346 345.288 409.230 473.172 537.114 601.057 Hunc 400. Am. Feet 2557.7 8951.9	INTO A rican Feet its. 5. Am. Feet 31.971 95.913 159.855 228.798 287.740 851.682 415.624 479.566 543.509 607.451 ireds. 500. Am Feet 3197.1 9591.3 15985.5 22379.8	MERICA Am. Feet 38.365 102.308 166.250 230.192 294.184 858.076 422.018 485.961 549.003 613.845 600. Am. Feet 3886.5 10230.8 16625.0 23019.2	7. Am Feet. 44.760 108.702 172.644 286.586 300.528 364.470 428.413 492.355 556.297 620.239 700. Am Feet. 4476.0 10870.2 17264.4 23658.6	S. Am Feet. 51.154 115.096 179.038 242.980 306.923 370.865 434.907 498.749 562.691 626.638 SOO. Am Feet. 5115.4 11509.6 17903.8 24298.0	9. Am. Fee- 57.54 121.49 185.43 249.37 377.25 441.20 505.14 569.08 633.02			

TO CONVERT

METRES

INTO DIFFERENT MEASURES OF LENGTH.

1 LEGAL METRE = 448.296 FRENCH OR PARIS LINES.

V. CONVERSION OF METRES INTO TOISES AND DECIMALS.

1 Metre = 0.518074074 Toise.

Motres.					Hund	ireds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Tolees.	Toises.	Toises.	Toless.	Toleas.	Toises.	Tolses	Toises.	Toises.	Toless.
0	0.00	51.81		153.92	205.23		4	859.15	410.46	461.77
1000	513.07	564.88	615.69	667.00	718.30	769.61	820.92	872.23	923.53	974.8
2000	1026.15	1077.46	1128.76	1180.07	1231.88	1282.69	1838.99	1385.30	1436.61	1487.9
8000	1539.22	1590.58	1641.84	1698.14	1744.45	1795.76	1847.07	1898 37	1949.68	2000.9
4000	2052.80	2108.60	2154.91	2206.22	2257.53	2308.83	2360.14	2411.45	2462.76	2514.0
5000	2565.37	2616.68	2667.98	2719.29	2770.60	2821.91	2878.21	2924.52	2975.83	3027.1
6000	8078.44	3129.75	8181.06	8282.87	8288.67	3834.98	3886.29	3437.60	3488.90	3540.2
7000	3591.52	3642.83	8694.18	8745.44	3796.75	8848.06	3899.36	8950.67	4001.98	4053.2
8000	4104.59	4155.90	4207.21	4258.51	4309.82	4861.18	4412.44	4463.74	4515.05	4566.3
9000	4617.67	4668.97	4720.28	4771.59	4822.90	4874.20	4925.51	4976.82	5028.13	5079.4
Motres. Tens.	0.	1.	2.	8.	Un	5.	6.	7.	8.	9.
•	Toises.	Toless. 0.513	Toless.	Toises. 1.589	Tolses. 2.052	Toless. 2.565	Toises. 8.078	Toless.	Tolses	Tolers. 4.618
10	5.131	5.644	6.157	6.670	7-188	7.696	8.209	8.722	9.235	9.748
20	10.261	10.775	11.288	11.801	12.314	12.827	18.840	13.853	14.366	14.879
30	15.392	15.905	16.418	16.981	17.445	17.958	18.471	18.984	19.497	20.010
40	20.528	21.036	21.549	22.062	22.575	23.088	28.601	24.114	24.628	25.141
50	25.654	26.167	26.680	27.198	27.706	28.219	28.732	29.245	29.758	30.271
60	30.784	31.298	81.811	82.824	82.837	83.850	33.863	34.876	34.889	35.4 02
70	85.915	86.428	86.941	37.454	87.967	88.481	38.994	89.507	40.020	40.563
80	41.046	41.559	42.072	42.585	43.098	48.611	44.124	44.637	45.151	45.664
90	46.177	46.690	47.208	47.716	48.229	48.742	49.255	49.768	50.281	50.794

1 Metre = 8.078644 Paris Feet.

Motres.					Motres.	Units.	•			
Tuns.	0. .	1.	9.	8.	4.	5.	6.	7.	8.	9.
	Fr. Post.	Fr. Foot.	Fr. Feet.	Fr. Foot.	Fr. Foot.	Fr. Feet.	Fr. Feet.	Fr. Feet.	Fr. Feet.	Fr. Feet.
0	0.00	8.08	6.16	9.24	12.81	15.39	18.47	21.55	24.63	27.71
10	30.78	23.86	26.94	40.03	43.10	46.18	49.26	52.38	55.41	58.49
20	61.57	64.65	67.78	70.80	78.88	76.96	80.04	83.12	86.20	89.27
80	92.85	95.48	98.51	101.59	104.67	107.75			116.98	120.06
40	123.14	126.22	129.29	182.87	185.45	138.58	141.61	144.69	147.77	150.84
50	153.92	157.00	160.08	163.16	166.24	169.81	172.39	175.47	178.55	181.63
€0	184.71	187.79	190.86	193.94	197.02	200.10	203.18	206.26	209.83	212.41
70	215.49	218.57	221.65	224.78	227.80	230.88	288.96	287.04	240.12	248.20
80	246.28	249.35	252.48	255.51	258.59	261.67	264.75	267.82	270.90	273.98
90	277.06	280.14	288.22	286.30	289.37	292.45	295.53	298.61	301.69	804.77
100	807.84	810.92	814.00	817.08	32 0.16	828.34	326.82	329.89	882.47	885.55
110	838.63	841.71	844.79	347.86	350.94	854.08	857.10	860.18	363.26	866.83
120	369.41	872.49	375.57		881.78	884.81	387.88	290.96	894.04	897 .12
130	400.20	403.28	406.85	409.48	412.51	415.59	418.67	421.75	424.88	427.90
140	430.98	484.06	487.14	440.22	448.30	446.37	449.45	452.58	455.61	458.69
150	461.77	464.85	467.92	471.00	474.08	477.18	480.24	483.32	486.39	489.47
160	492.55	495.68	498.71	501.79	504.86	507.94	511.02	514.10	517.18	520.26
170	523.84	526.41	529.49	532.57	535.65	538.73	541.81	544.88	547.96	551.04
180	554.12	557.20	560.28	563.36	566.43	569.51	572.59	575.67	578.75	581.88
190	584.90	587.98	591.06	594.14	597.22	600.80	608.88	606.45	609.53	612.61
200	615.69	618.77	621.85	624.92	628.00	631.08	684.16	637.24	640.82	648.89
210	646.47	649.55	652.68	655.71	658.79	661.87	664.94	668.02	671.10	674.18
220	677.26	680.34	683.41	686.49	699.57	692.65	695.78	698.81	701.89	704.96
280	708.04	711.12	714.20		720.86	728.48	726.51	729.59	732.67	785.75
240	738.83	741.90	744.98	748.06	751.14	754.22	757.80	760.38	768.45	766.58
250	769.61	772.69	775.77	778.85	781.92	785.00	788.08	791.16	794.24	797.82
260	800.40	803.47	806.55	809.68	812.71	815.79	818.87	821.94	825.02	828.1 0
270	881.18	634.26	887.84		843.49	846.57	849.65		855.81	858.89
280	861.96	865.04		871.20	874.28	877.86	880.48	883.51	1	889.67
290	892.75	895.88	898.91	901.98	905.06	908.14	911.22	914.30	917.88	920.45
300	923.58	926.61	929.69	932.77	935.85	938.98	942.00	945.08	948.16	951.24
310	954.82	957.40	960.47	963.55	966.68					
820	985.10							1006.65		
830						1031.28				
340	1046.67	1049.75	1052.83	1055.91	1058.98	1062.06	1065.14	1068.22	1071.80	1074.38
850						1092.85				
360	11			1	1	1123.63				
370	11	i		1	1151.84		1	1160.57	t	1
380			1	1	1182.12			1191.36	L.	1
390	1200.59	1208.67	1206.75	1209.88	1212.91	1215.99	1219.06	1222.14	1225.22	1228.80
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

1 Metre = 8.078444 Paris Feet.

Metres.		9. 1. 2. 3. 4. 5. 6. 7. 8. 9.											
Tens.	0.	1.	2.	8.	4.	5.	6.	7.	6.	9.			
						Fr. Feet.							
400	11 1		1	ı		1246.77	ž.			ì			
410	11 (1	1		1277.55		•	ľ				
420	1292.95	1296.02	1299.10	1302.18	1805.26	1308.34	1811.42	1314.50	1817.57	1320.6			
430	1823.73	1326.81	1329.89	1382.97	1886.04	1339.12	1342.20	1345.28	1348.36	1851.4			
440	1854.52	1857.59	1360.67	1368.75	1866.83	1369.91	1372.99	1376.06	1379.14	1382.7			
450	1885.30	1388.38	1891.46	1894.54	1397.61	1400.69	1403.77	1406.85	1409.93	1413.0			
460	1416-08	1419.16	1422.24	1425.82	1428.40	1431.48	1434.55	1437.63	1440.71	1443.7			
470	1446.87	1449.95	1453.03	1456.10	1459.18	1462.26	1465.34	1468.42	1471.50	1474.5			
480	1477.65	1480.78	1488.81	1486.89	1489.97	1493.05	1496.12	1499.20	1502.28	1505.2			
490	1508.44	1511.52	1514.59	1517.67	1520.75	1523.83	1526.91	1529. 9 9	1533.07	1536.1			
500	1539.22	1542.80	1545.88	1548.46	1551.54	1554.61	1557.69	1560.77	1563.85	1566.9			
510	11)	1585.40	1 1			ŀ			
520	11 1				1	1616.18		1		1			
580						1646.97				4			
540				l		1677.75				1			
550	1693.14	1696.22	1699.80	1702.88	1705.46	1708.54	1711.61	1714 69	1717.77	1720			
560	II I				1	1789.82				1			
570	11 1		1	1	1	1770.11							
						1800.89							
580 590				1		1881.67							
000	1010.20	1010.00	1000111	1020.02	1020.00	1001101	1001110	1001100	1010101	10 20.			
600	1847.07	1850.14	1853.22	1856.80	1859.38	1862.46	1865.54	1868.62	1871.69	1874.7			
610	1877.85	1880.93	1884.01	1887.09	1890.16	18 93.2 4	1896.32	1899.40	1902.48	1905.			
620	1908.64	1911.71	1914.79	1917.87	19 2 0.95	1924.03	1927.11	1980.18	1933.26	1936.			
630	1939.42	1942.50	1945.58	1948.66	1951.78	1954.81	1957.89	1960.97	1964.05	1967.			
640	1970.20	1978.28	1976.36	1979.44	1982.52	1985.60	1988.67	1991.75	1994.83	1997.			
650	2000.99	2004.07	2007.15	2010.22	2013.80	2016.38	2019.46	2022.54	2025.62	2028.			
660	2031.77	2084.85	2037.98	2041.01	2014.09	2047.17	2050.24	2053.32	2056.40	2059.			
670	2062.56	2065.64	2068.71	2071.79	2074.87	2077.95	2081.03	2084.11	2087.19	2090.			
680	2093.34	2096.42	2099.50	2102.58	2105.66	2108.73	2111.81	2114.89	2117.97	2121.			
690	11		1	1		2139.52				ı			
700	2154.91	2157.99	2161.07	2164.15	2167.22	2170.80	2173.88	2176.46	2179.54	2182.0			
710	11					2201.09			i	1			
720	н			1	I	2231.87	1						
730				1		2262.66		. 1					
740				1	1	2293.44							
750	2308.88	2811.91	2314.99	2818.07	2321.15	2824.28	2827.30	2380.38	2333.46	2336.			
760			1	ı		2355.01				1			
770				l .		2885.79							
780						2416.58							
790	13	1		1	1	2447.36	1	1		ı			
	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.			

1 Metre = 8.078444 Paris Feet.

_	M -4		7			Metres.	Units,				
	Motres. Tens.	· 0.	1.	2,	3.	L	5.	6.	7.	8.	9.
-				Fr. Foot.				Fr. Feet.		Fr Foot.	Fr. Feet.
	800					2475.07		2481.28	1		
	810					2505.85		2512.01			
1	820					2536.64		2542.79			
١	830	1			2564.34			2578.58			
	840	2585.89	2588.97	2592.05	2595.18	2598.21	2601.29	2604.86	2607.44	2610.52	2618.60
1	850	2616.68	2619.76	2622.88	2625.91	2628.99	2682.07	2635.15	2638.23	2641.80	2644.88
1	860	2647.46	2650.54	2653.62	2656.70	2659.78	2662.85	2665.98	2669.01	2672.09	2675.17
1	870	2678.25	2681.32	2684.40	2687.48	2690.56	2698.64	2696.72	2699.80	2702.87	2705.95
1	880	2709.03	2712.11	2715.19	2718.27	2721.34	2724.42	2727.50	2730.58	2733.66	2786.74
	890	2789.62	2742.89	2745.97	2749.05	2752.18	2755.21	2758.29	2761.36	2764.44	2767.52
	900	2770.60	2778.68	2776.76	2779.83	2782.91	2785.99	2789.07	2792.15	2795.28	2798.81
!	910	1				2813.70		2819.85	2822.93	2826.01	2829.09
H	920	2832.17	2885.75	2838.33	2841.40	2844.48	2847.56	2850.64	2853.72	2856.80	2859.87
	930	2862.95	2866.03	2869.11	2872.19	2875.27	2878.35	2881.42	2884.50	2887.58	2890.66
1	940	2898.74	2896.82	2899.89	2902.97	2906.05	2909. 13	2912.21	2915.29	2918. 3 6	2921.44
	950	2924.52	2927.60	2930.68	2933.76	2936.84	2939.91	2942.99	2946.07	2949.15	2952.23
1	960	2955.81	2958.38	2961.46	2964.54	2967.62	2970.70	2978.78	2976.86	2979.98	2983.01
il	970	2986.09	2989.17	2992.25	2995.83	2998.40	8001.48	8004.56	3007.61	3010.72	3013.80
	980	8016.88	3019.95	8023.03	3026.11	3029.19	8032.27	3085.85	3038.42	8041.50	3044.58
	990	3047.66	3050.74	8053.82	8056.89	8059.97	8063.05	8066.18	3069.21	3072.29	8075.87
	Motres.	French 1	Poot. 16	letres.	rench Fee	i. Motr	us. Fre	nch Feet.	Metro	ı. Fren	ch Feet.
11-	1000	3078		5000	15892.22	90	00	7706.00	1300	100	19.78
H	2000	6156.	4		18470.67			0784.44	1400		98.22
H	3000	9235	11 -		21549.11			3862.89	1500		76.67
	4000	12313	- 1	1	24627.56	- 11		8941.38	1600		55.11
						Decim	otres.				
	Metres,	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
		Fr. Feet.	Fr Feet.		Fr. Foot.	Fr. Feet.	Fr. Feet	Fr. Post.	Fr. Feet.	Fr.Feet.	
	0	0.0000	0.3078		0.9285	1.2314	1.5392		2.1549		2.7706
-	1	3.0784			4.0020	4.3098	4.6177			5.5412	l .
-	2	6.1569	6.4647	1		7.3883	7.6961	1		8.6196	8.9275
∦	8	9.2353	9.5432					11.0824		11.6981	
	4	12.3138	12.6216	12.9295	18.2373	13.5452	18.8580	14.1608	14.4687	14.7765	15.0844
-	5	15.8922	15.7001	16.0079	16.3158	16.6286	16.9814	17.2393	17.5471	17.8550	18.1628
	6					19.7020	1				1 1
il	7				1	22.7805		1	1		
il	8	24.6276	24.9354	25.2482	25.5511	25.8589	26.1668	26.4746	26.7825	27.0903	27.3982

1 Motre == 3.98989917 English Feet.

	1 Matres 2.2035017 English Feet. Matres. (Units.) 9. 1. 2. 3. 4. 5. 6. 7. 8. 9.													
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
0	Eng.Feet.	Eng. Feet.	Eng.Fost. 6.56	Eng. Fost. 9.84	Eag.Feet. 13.12	Eng.Feet. 16.40	Eng Feet. 19.69	Eng. Feet. 22.97	Eng Feet. 26.25	Eng. Fert 29.53				
10	32.81	36.09	89.37	42.65	45.98	49.21	52.49	55.78	59.06	62.34				
20	65.62	68.90	72.18	75.46	78.74	82.02	85.30	88.58	91.87	95.15				
30	98.43	101.71	104.99	108.27	111.55	114.83	118.11	4	124.67					
40	131.24	134.52	137.80	141.08	144.86	147.64	150.92	154.20	157.48	1 6 0.76				
50	164.04	167.33	170.61	178.89	177.17	180.45	188.78	187.01	190.29	193.57				
60	196.85	200.18	203.42	206.70	209.98	218.26	216.54	219.82	223.10	226.3 8				
70	229.66	232.94	296.22	239.51	242.79	246.07	249.35	252.68	255.91	259 .19				
80	262.47	265.75	209 .08	272.81	275.60	278.88	2 82.16	285.44	288.72	292. 00				
90	295.28	298.56	801.84	305.12	308.40	811.69	814.97	318.25	821.53	324. 81				
100	328.09	831.87	884.65	887.98	841.21		847.78	351.06	854.34	357.62				
110	860.90	864.18	867-46	870.74	374.02		360.58	888.87	887.15	390.43				
120	893.71	896.99	400.27	408.55	406.83	410.11	413.89	416.67	419.96	423.24				
180 140	426.52 459.88	429.80 462.61	465.89	496.36 469.17	489.64 472.45	442.92 475.78	446.20 479.01	449.48 482.29	452.78 485.57	456.01 488.85				
150	492.13	495.42	498.70	501.98	505.26	508.54	511.82	515.10	518.38	521.66				
160	524.94	528.22	581.51	584.79	588.07	541.35	544.63	547.91	551.19	551.47				
170	557.75	561.08	564.31	567.60	570.88		577.44	580.72	584.00	587.25				
180	590.56	593.84	597.12	600.40	608.69		610.25	613.53	616.81	620. 09				
190	623.87	626.65	629.93	633.21	636.49	689.7 8	648.06	646.34	649.62	652.90				
200	656.18	659.46	662.74	666.02	669.30	672. 58	675.87	679.15	682.43	685.71				
210	688. 99	692.27	695.55	698.83	702.11	705.39	708.67		715.24	718.52				
220	721.80	725.08	728.36	731.64	784.92	738.20	741.48	744.76	748.05	751.33				
230	754.61	757.89	761.17	764.45	767.73	771.01	774.29	777.57	780.85	784.13				
240	787.42	790.70	793.98	797.26	800.54	. 803.82	807.10	810.38	813.66	816-94				
250	820.22	823.51	826.79	880.07	833.35	l I	839.91	843.19	846.47	849.75				
260	853.03	856.31	859.60	862.88	866.16	869.44	872.72	876.00	879.28	882.56				
270	885.84	889.12	892.40	895.69	898.97	l 1	905.53	908.81	912.09	915.37				
280	918.65	921.93	925.21	928.49	931.78		938.84	941.62	944.90	948.18				
290	951.46	954.74	958.02	961.80	964.58	967-87	971.15	974.48	977.71	980.99				
300	984.27			994.11			1003.96							
310	1017.08	1020.36	1023.64	1026.92					1043.83					
320	1049.89		1056.45			1066.29			1076.13					
330	1082.70	1085.98	1089.26	1092.54	1095.82	1099.10	1102.88	1105.66	1108.94	1112.22				
340	1115.51	1118.79	1122.07	1125.35	1128.63	1181.91	1185.19	1138.47	1141.75	1145.03				
350	1148.81	1151.60	1154.88	1158.16	1161.44	1164.72	1168.00	1171.28	1174.56	1177.84				
360							1200.81							
370							1283.62 1266.43							
380 390							1299.24							
	0.	1.	9.	s.	4.	5.	6.	7.	8.	9.				

400 to 799.

Motres.	- Metres. (Units.)									
	•.	1.	2.	8,	4.	5.	6.	7.	8.	9.
400		Eng. Feet.								1 -
400		1315.64		ı	1	1828.76			1388.61	1
410	II	1348.45				1361.57		ſ	1871.42	
420		1381.26	i e		1	1394.38		l .	1404.22	1
430	1410.79	1414.07	1417.85		1		1480.47		1437.08	1
440	1443.60	1446.88	1450.16	1403.44	1456.72	1460.00	1463.28	1466.56	1469.84	1478.
450	1	1479.69						1499.37	1502.65	1505.9
460		1512.49			1		9	1532.18	1585.46	1538.7
470		1545.30		1	1			1564.99	1568.27	1571.5
480	11	1578.11				1591.28		1597.80	1601.08	1604.8
490	1607.64	1610.92	1614.20	1617.48	1620.76	1624.05	1627.33	1630.61	1688.89	1687.1
500	1640.45	1648.73	1647.01	1650.29	1653.57	1656.85	1660.13	1663.42	1666.70	1669.9
510	1673.26	1676.54	1679.82	1683.10	1686.38	1689.66	1692.94	1696.22	1699.51	1702.7
520	1706.07	1709.35	1712.63	1715.91	1719.19	1722.47	1725.75	1729.08	1732.81	1785.6
580	1738-88	1742.16	1745.44	1748.72	1752.00	1755.28	1758.56	1761.84	1765.12	1768.4
540	1771.69	1774.97	1778.25	1781.53	1784.81	1788.09	1791.37	1794.65	1797.93	1801.2
550	1804.49	1807.78	1811.06	1814.84	1817.62	1820.90	1824.18	1827.46	1890.74	1834.0
560	1837.80	1840.58	1848.87	1847.15	1850.48	1858.71	1856.99	1860.27	1863.55	1866.8
570	1870.11	1873.39	1876.67	1879.96	1883.24	1886.52	1889.80	1898.08	1896.36	1899.6
580	1902.92	1906 20	1909.48	1912.76	1916.05	1919.88	1922.61	1925.89	1929.17	1982.4
590	1935.73	1939.01	1942.29	1945.57	1948.85	1952.18	1955.42	1958.70	1961.98	1965.2
600	1968.54	1971.82	1975.10	1978.88	1981.66	1984.94	1988.22	1991.51	1994.79	1998.0
610	2001.85		2007.91		2014.47	1	2021.08		1	2030.8
620	2034.16	2037.44	2040.72	2044.00	2047.28	2050.56	2053.84	2057.12	2060.40	2063.6
630	2066.97	2070.25	2078.53	2076.81	2080.09	2083.87	2086.65	2089.98	2093.21	2096.4
640	2099.78	2103.06	2106.34	2109.62	211 2.9 0	2116.1 8	2119.46	2122.74	2126.02	2129.8
630	2132.58	2135.87	2189.15	2142.43	2145.71	2148.99	2152.27	2135.55	2159.83	21 62 .1
660	1	2168.67				2181.80				
670	1	2201.48			2211.33		2217.89	,		2227.7
680	2231.01	2234.29	2237.57	2240.85	2244.13	2247.42	2250.70	2253.98	2257.26	2260.5
690	2263 .82	2267.10	2270.38	2273.66	2276.94	2280.22	2288.51	2286.79	2290.07	2296.3
700	2296.63	2299.91	2303.19	2808.17	2309.75	2318.03	2316.21	2819.60	2322.88	2326.1
710	1	2382.72			2342.56		2849.12	1		
720			2368.81		1 1	2378.65				
730		2396.34				2411.46				2424.5
740		2481.15							2454-11	2457.3
750	2180 87	2468.96	2487.24	2470 59	2172 80	2177.08	3180°88	2488.64	2486.92	2490.2
760		2496.76								
770		2529.57					2545.98			
780		2562.38					2578.79			
790		2595.19								
	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.

1 Metre = 3.98089917 English Feet.

Metres.	Metres. (Units.)									
	0.	1.	2.	8.	4.	8.	6.	7.	8.	9.
_		Eng. Feet.	Eng. Fost.					1 -		
0	0.0	3.28	6.56	9.84	13.12	ı	19.69	22.97	26.25	29.53
10	82.81	36.09	89.87	42.65	45.93	l .	52.49	55.78	59.06	62.34
20 30	65.62 98.43	68.90	72.18 104.99	75.46 108.27	78.74			88.58	91.87	95.15
40	131.24		187.80	141.08	111.55 144.36		118.11 150.92	121.39		127.96
40	131.24	104.02	107.50	141.06	144.00	147.04	150.82	154.20	157.48	1 6 0.76
50	164.04	167.38	170.61	173.89	177.17	180.45	183.78	187.01	190.29	193.57
60	196.85	1	203.42	206.70	209.98	1	216.54	219.82	223.10	226.38
70	229.66	282.94	286.22	239.51	242.79		249.35	252.63	255.91	259.19
80	262.47	265.75	269.03	272.31	275.60	278.88	282.16	285.44	288.72	292.00
90	295.28	298.56	301.84	305.12	308.40	311.69	814.97	818.25	321.53	324.81
100	328.09		884.65	887.93	841.21		847.78	351.06	354.34	\$57.62
110	860.90	364.18	867-46	870.74	874.02	877.30	8 80.58	383.87	287.15	59 0.43
120	893.71	896.99	400.27	408.55	406.83	410.11	413.39	416.67	419.96	423.24
130	426.52	429.80	483.08	486.36	489.64	442.92	446.20	449.48	452.78	456.01
140	459.33	462.61	465.89	469.17	472.45	475.78	479.01	482.29	485.57	488.85
150	400 10	495-42	498.70	501.98	505.26	508.54	K11 00	K1K 10	E10 90	E91 cc
150 160	492.13 524.94	528.22	581.51	584.79	588.07		511.82 544.63	515.10 547.91	518.38 551.19	521.66 554.47
170	557.75	561.08	564.31	567.60	570.88	574.16	577.44	580.72	584.00	587.25
180	590.56	593.84	597.12	600.40	608.69		610.25	618.53	616.81	620.09
190	623.87	626.65	629.93	633.21	686.49	689.78	648.06	646.34	649.62	652.90
		0.000	1.00					0.0.0.2	0.0.02	
200	656.18	659.46	662.74	666.02	669.30	672.58	675.87	679.15	682.43	685.7 1
210	688.99	692.27	695.55	698-83	702.11	705.39	708.67	711.96	715.24	718.52
220	721.80	725.08	728.36	731.64	784.92	738.20	741.48	744.76	748.05	751.33
230	754.61	757.89	761.17	764.45	767.73	771.01	774.29	777.57	780.85	784.1 3
240	787.42	790.70	793.98	797.26	800.54	803.82	807.10	810.38	813.66	816-9 4
250	820.22	828.51	826.79	880.07	833.35	836.68	839.91	843.19	846.47	849.75
260	853.03		859.60	862.88	866.16	1. 1	872.72	876.00	879.28	882.56
270	885.84	889.12	892-40	895.69	898.97		905.53	908.81	912.09	915.37
280	918.65	921.93	925.21	928.49	931.78	1 1	938.34	941.62	944.90	948.18
290	951.46	954.74	958.02	961.30	964.58	967.87	971.15	974.48	977.71	980.99
				4-						_
800	984.27		990.83				1003.96			1013.80
310	1017.08			1026.92		1033.48	1036.76			1046.61
320	1049.89		1056.45	: 1		1066.29			1076.18	
330	1032.70		1089.26		1095.82				1108.94	
840	1115.51	1115.79	1122.07	1120.35	1125.63	1121.91	1185.19	1185.47	1141.75	1145.03
350							1168.00			
360							1200.81			
370							1288.62			
880							1266.43			
390	1279.55	1282.83	1286.11	1289.39	1292.67	1295.96	1299.24	1302.52	1305.80	1309.08
	0.	1.	9.	g.	4.	5.	6.	7.	8.	9.

1900 to 1599.

					Metre.	(Units.)				
Motres.						1	r	T T	i	, -
	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.
1200	Eng. Feet. 3937.08	Eng. Feet. 3940.36	Eng. Feet. 3943.64			Eng.Feet. 3953.48	Eng.Feet. 3956.76	Eng. Feet. 8960.05	Eng.Feet. 3963.38	Eng. Feet. 3966.61
1210	3969.89	3978.17	3976.45	3979.73	3983.01	3986.29	3989.57	3992.85	8996.14	3999.42
1220	4002.70	4005.98	4009.26	4012.54	4015.82	4019.10	4022.88	4025.66	4028.94	4032.23
1230	4035.51	4038.79	4042.07	4045.85	4048.63	4051.91	4055.19	4058.47	4061.73	4065.03
1240	4068.31	4071.60	4074.88	4078.16	4081.44	4084.72	4088.00	4091.28	4094.56	4097.84
1250	4101.12		4107.69			4117.58	1		4127.37	4130.65
1260	4133.93	4137.21	4140.49	4148.78			4153.62	4156.90	4160.18	4163.46
1270	4166.74	4170.02	4173.80	4176.58			4186.43	4189.71	4192.99	4196.27
1280	4199.55	4202.88	4206.11	4209.89	4212.67		4219.24		4225.80	4229.08
1290	1232.36	4235.64	4288.92	4242.20	4245.48	4248.76	4252.05	4255.88	4258.61	4261.89
1300	4265.17	4268.45	4271.73	4275.01	4278.29	4281.57	4284.85	4288.14	4291.42	4294.70
1310	4297.98	4301.26	4304.54	4307.82	4811.10	4314.88	4817.66	4320.94	4324.23	4327.51
1320	4330.79	4334.07	4337.35	4840.63	4343.91		4350.47	4853.75	4357.08	4360.31
1330	4363.60	4366.88	4370.16	4373.44	4376.72		4383.28		4389.84	4398.12
1340	4396.40	4399.69	4402.97	4406.25	4409.58	4412.81	4416.09	4419.87	4422.65	4425.98
1350	4429.21	4432.49	4435.78	4439.06	4442.84	4445.62	4448.90	4452.18	4435.46	4458.74
1360	4462.02	4465.30	4468.58	4471.87	4475.15	4478.43	4481.71	4484.99	4488.27	4491.55
1370	4494.83	4498.11	4501.39	4504.67	4507.96	4511.24	4514.52	4517.80	4521.08	4524.86
1380	4527.64	4580.92	4534.20	4587.48	4540.76	4544.05	4547.88	4550.61	4553.89	4557.17
1390	4560.45	4563.73	4567.01	4570.29	4378.57	4576.85	4580.14	4583.42	4586.70	4589.98
1400	4593.26	4596.54	4599.82	4603.10	4606.38	4609.66	4612.94	4616.23	4619.51	4622.79
1410	4626.07	4629.35	4682.63	4635.91	4639.19	4642.47	4645.75	4649.03	4652.81	4655. 6 0
1420	4658.88	4662.16	4665.44	4668.72	4672.00	4675.28	4678.56	4681.84	4685.12	4688.40
1430	4691.69	4694.97	4698.25	4701.58	4704.81	4708.09	4711.37	4714.65	4717.98	4721.21
1440	4724.49	4727.78	4781.06	4734.84	4787.62	4740.90	4744.18	4747.46	4750.74	4754.02
1450	4757.80	4760.58	4763.87	4767.15	4770.48	4778.71	4776.99	4780.27	4788.55	4786.83
1460	4790.11	4793.39	4796.67	4799.96	4803.24	4806.52	4809.80	4813.08	4816.86	4819.64
1470	4822.92	4826.20	4829.48	4832.76	4886.05	4839.83	4842.61	4845.89	4849.17	4852.45
1480	4855.73	4859.01	4862.29	4865.57	4868.85	4872.14	4875.42	4878.70	4881.98	4885.26
1490	4888.54	4891.82	4895.10	4898.38	4901.66	4904.94	4908.28	4911.51	4914.79	4918.07
1500	4921.35	4924.63	4927.91	4981.19	4984.47	4937.75	4941.08	4944.81	4947.60	4950.88
1510	4954.16	4957.44	4960.72	4964.00	4967.28	4970.56	4973.84	4977.12	4980.40	4983.69
1520	4986.97	4990.25	4993.53	4996.81	5000.09	5003.37	5006.65	5009.93	5013.21	5016.49
1530	5019.78	5023.06	5026.34	5029.62	5082.90	5036.18	5039.46	5042.74	5046.02	5049.30
1540	5032.58	5055.87	5059.15	5062.43	5065.71	5068.99	5072.27	5075.55	5078.83	5082.11
1550		ı	5091.96					1		
1360			5124.76							
1570			5157.57							
1580								l .	1	5213.35
1590										5246.16
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

1600 to 2000.

1600 52: 1610 52: 1620 53: 1630 53: 1640 53: 1640 53: 1650 541 1660 544 1670 557 1710 561 1720 567 1740 577 1770 580 1780 587 1790 587 1810 593 1820 597 1830 600 1840 603: 1850 616: 1870 613: 1880 616: 1890 620: 1910 623: 1910 626: 1930 633: 1940 636	249.44 282.25 315.06 847.87 880.67 413.48 446.29 479.10	ing.Feet. Er 249.44 52 282.25 52 315.06 58 847.87 58 880.67 58	259.72 52 285.58 52 318.84 53 351.15 51	256.00 288.91 321.62 854.48 887.24	Eng.Feet. 5259.28 5292.09 5324.90 5857.71	4. Eng.Feet 5262.56 5295.37		6. Eng.Fest.	7.	8.	9.
1600 521 1620 531 1630 541 1650 541 1660 544 1670 547 1700 567 1710 561 1720 564 1740 570 1750 584 1790 587 1830 600 1810 1820 1850 6161 1850 6161 1850 6161 1850 6261 1920 6281 1940 636	249.44 282.25 315.06 847.87 880.67 413.48 446.29 479.10	249.44 52 282.25 52 315.06 58 847.87 58 880.67 58	259.72 52 285.58 52 318.84 53 351.15 51	236.00 288.91 321.62 354.48	5259.28 5292.09 5824.90	5262.56		Eng Fort			
1610 522 1620 531 1630 544 1660 544 1670 554 1700 557 1710 561 1720 564 1730 567 1770 580 1780 587 1780 584 1790 587 1830 600 1810 1820 1820 1830 600 1850 616 1870 613 1880 616 1870 613 1890 620 1910 623 1940 636 636 1940 636 636 1940 1940 636 1940 1940 636 1940 1940 636 1940 194	282.25 315.06 847.87 880.67 413.48 446.29 479.10 511.91	282.25 52 315.06 58 847.87 58 880.67 58	285.58 53 318.34 53 351.15 51	288.81 821.62 854.48	5292.09 5 324. 90			, -			1 -
1620 531 1630 584 1640 586 1640 586 1640 586 1660 544 1670 547 1680 551 1700 557 1710 561 1720 567 1740 577 1780 584 1790 587 1890 590 1810 593 1820 597 1830 600 1840 603 1850 666 1870 613 1880 616 1870 613 1880 616 1890 620 1910 6236 1910 6269 1930 633 1940 636	815.06 847.87 880.67 413.48 446.29 479.10 511.91	315.06 53 847.87 53 880.67 58 413.48 54	318.34 53 351.15 51	321.62 354.48	5324.9 0	15295.X7				5275.69	
1680 581 1640 586 1640 544 1670 541 1680 561 1690 554 1700 557 1710 561 1720 564 1780 577 1770 580 1780 584 1790 587 1800 590 1810 593 1820 597 1830 600 1840 603 1850 616 1870 613 1880 616 1890 620 1910 623 1910 6269 1930 633 1940 636	847.87 880.67 413.48 446.29 479.10 311.91	847.87 58 880.67 58 413.48 54	351.15 51	854.48		ı		5301.93	5805.21	5308.49	5311.78
1640 588 1650 541 1660 544 1670 547 1680 551 1690 557 1710 561 1720 567 1740 577 1770 580 1810 593 1820 597 1830 600 1840 603 1850 610 1870 613 1880 616 1890 620 1910 623 1910 626 1930 633 1940 636	880.67 413.48 446.29 479.10 311.91	880.67 58 413.48 54	1	1	0807.71	5828.18	ſ	5884.74	5338.02	5841.30	5344.58
1650 541 1660 544 1670 547 1680 551 1690 557 1710 561 1720 564 1780 577 1770 580 1770 580 1810 593 1820 597 1830 600 1840 603 1850 606 1870 613 1880 616 1890 620 1910 623 1910 626 1930 633 1940 636	413.48 446.29 479.10 311.91	413.48 54	888.96 00	587.24		5860.99		5867.55	5870.83	5874.11	5377.39
1660 544 1670 547 1680 551 1690 553 1700 567 1710 561 1720 564 1730 567 1740 577 1770 580 1780 587 1800 590 1810 593 1820 597 1830 600 1840 603 1850 606 1870 613 1880 616 1890 620 1900 623: 1910 6266 1920 629: 1930 636	446.29 479.10 311.91				5390.52	5898.80	5897.08	5400.86	5403.64	5406.92	5410.20
1670 547 1680 551 1700 557 1710 561 1720 567 1760 577 1770 580 1810 593 1820 597 1830 600 1850 616 1870 613 1880 616 1890 626 1920 629 1940 636 63	479.10 311.91	446.29 54	416.76 54	420.05	5423.88	5426.61	5429.89	5483.17	5436.4 5	5489.78	5443.01
1680 581 1700 557 1710 561 1720 564 1780 577 1760 577 1770 580 1810 593 1820 597 1830 600 1850 616 1870 613 1880 616 1890 626 1920 628 1940 636 63	311.91	- 10120 37	449.57 54	452.85	5456.14	5459.42	5462.70	5465.98	5469.26	5472.54	5475.82
1690 554 1700 557 1710 561 1720 564 1730 567 1740 570 1750 574 1760 577 1770 580 1810 593 1820 597 1830 600 1840 603 1850 606 1870 613 1880 616 1890 620 1910 626 1920 629 1930 636		479.10 54	482.88 54	485.66	5488.94	5492-2 8	5495.51	5498.79	5502.07	5505.35	5506.63
1700 557 1710 561 1720 564 1730 567 1740 570 1750 577 1770 580 1770 584 1790 597 1810 593 1820 597 1830 600 1840 603 1850 606 1870 613 1880 616 1890 620 1910 626 1920 629 1930 636 1940 636	544.72	511.91 55	515.19 55	518.47	5521.75	5525.03	5528.32	5531.60	5534.88	5538.16	5541.44
1710 561 1720 564 1730 567 1740 570 1750 574 1760 577 1770 580 1790 584 1790 593 1810 593 1820 597 1830 600 1840 603 1850 616 1870 613 1880 616 1890 620 1910 623 1910 623 1940 636		544.72 55	548.00 55	551.28	5554.56	5557.84	5561.12	5564.40	5567.69	5570.97	5574.25
1710 561 1720 564 1730 567 1740 570 1750 574 1760 577 1770 580 1790 584 1790 593 1810 593 1820 597 1830 600 1840 603 1850 616 1870 613 1880 616 1890 620 1910 623 1910 623 1940 636	577.58	577.58 55	580.81 55	584.09	5587.87	5590.65	5598.98	5597.21	5600.49	5603.78	5607.06
1720 564 1780 577 1780 584 1790 587 1810 593 1820 597 1830 600 1870 613 1880 616 1890 6226 1910 6236 1940 636 1940 1940 636 1940					5620.18	5628.46	5626.74	5630.02	5638.80	5636.58	5639.87
1780 567 1740 570 1760 574 1770 580 1770 581 1790 587 1800 590 1810 593 1820 597 1830 600 1840 603 1850 610 1870 613 1880 616 1890 620 1910 623 1910 623 1910 623 1920 629 1930 633 1940 636				1	5652.99	5656.27	5659.55	5662.83	5666.11	5669.89	5672.67
1740 570 1750 574 1760 577 1770 580 1780 584 1790 587 1800 590 1810 593 1820 597 1830 600 1840 603 1850 606 1860 610 1870 613 1880 616 1890 620 1900 623: 1910 626 1920 629: 1930 636					5685.80	5689.08	5692.86	5695-64	5698,92	5702.20	5705.48
1760 577 1770 580 1780 584 1790 587 1810 593 1820 597 1830 600 1840 608 1850 616 1870 613 1880 616 1890 620 1900 623 1910 623 1920 629 1930 636	08.76	708.76 57	712.05 57	15.88	5718.61	5721.89	5725.17	5728.45	5781.78	5735.01	5738.29
1760 577 1770 580 1780 584 1790 587 1810 593 1820 597 1830 600 1840 608 1850 616 1870 613 1880 616 1890 620 1900 623 1910 623 1920 629 1930 636	41 57	747 57 87	744.85 57	48.14	5751.42	5754.70	E757 00	5761. 2 6	5764.54	5767-82	5771.10
1770 580 1780 584 1790 587 1800 590 1810 593 1820 597 1830 600 1840 603 1850 610 1870 613 1880 616 1890 620 1900 623 1910 626 1920 629 1930 633 1940 636				1	5784.28	5787.51	5790.79	5794.07	5797.85	5800.63	5803.91
1780 584 1790 587 1800 590 1810 593 1820 597 1830 600 1840 608 1850 616 1870 613 1880 616 1890 620 1900 623 1910 626 1920 629 1930 636					5817.08	5820.82	58 23.6 0		5880.16	5883.44	5836.72
1790 587 1800 590 1810 593 1820 597 1830 600 1840 603 1850 616 1870 613 1880 616 1890 620 1900 623 1910 623 1920 629 1930 633 1940 636		1			5849.84		5856.40	5859.69		5866.25	5869.53
1800 590 1810 593 1820 597 1830 600 1840 603 1850 616 1870 613 1880 616 1890 620 1900 623: 1910 626 1920 629: 1930 633: 1940 636					5882.65	5885.93	5889.21			5899.06	5902.34
1810 593 1820 597 1830 600 1840 603 1850 610 1870 613 1880 6161 1890 620 1900 623 1910 626 1920 629 1930 633 1940 636			370.00			0000.03	0000.21	5052.15		0033.00	0302.04
1820 597 1830 600 1840 603 1850 610 1870 613 1880 616 1890 620 1900 623 1910 626 1920 629 1930 633 1940 636	05.62	05.62 59	908.90 59	12.18	5915.46	5918.74	5922.02	5925.30	5928-58	5931.87	5935.15
1880 600 1840 608 1850 610 1870 613 1880 616 1890 620 1900 623 1910 626 1920 629 1930 633 1940 636	38.43	38.43 59	41.71 59	44.99	5948.27	5951.55	5954.83	5958.11	5961.39	5964.67	5967.96
1840 608 1850 606 1860 610 1870 613 1880 616 1890 620 1900 623 1910 626 1920 629 1930 633 1940 636	71.24	71.24 59	74.52 59	77.80	5981.08	5984.36	5987.64	5990.92	5994.20	5997.48	6000-76
1850 606 1860 610 1870 613 1880 616 1890 620 1900 623 1910 626 1920 629 1930 633 1940 636	04.05	04.05 60	007.88 60	10.61	6013.89	6017.17	6020.45	6023.73	6027.01	6030.29	6033.57
1860 610 1870 613 1880 616 1890 620 1900 623 1910 626 1920 629 1930 633 1940 636	36.85	86.85 60	40.14 60	43.42	8046.70	6049.98	6053.26	6056.54	6059.82	6063.10	6066.3 8
1870 613 1880 616 1890 620 1900 623 1910 626 1920 629 1930 633 1940 636	69.66	69.66 60	72.94 60	76.23	6079.51	6062.79	6086.07	6089.35	6092.63	6095.91	6099.19
1880 616 1890 620 1900 623 1910 626 1920 629 1930 633 1940 636	02.47	02.47 610	03.75 61	09.03	6112.32	6115.60	6118.88	6122.16	6125.44	6128.72	6132.00
1890 6200 1900 623 1910 626 1920 629 1930 633 1940 636	35.28	35.28 613	38.56 61	41.84	6145.12	6148.40	6151.69	6154.97	6158.25	6161.53	6164.81
1890 6200 1900 623 1910 626 1920 629 1930 633 1940 636	68.09	68.09 613	71.37 61			6181.21	1	6187.78	6191.06		6197.62
1910 626 1920 629 1930 633 1940 636	00.90	00.90 620	04.18 62	07.46	8210.74	6214.02	6217.3 0	6220.58	6223.87	6227.15	6230.43
1910 626 1920 629 1930 633 1940 636	33.71	33.71 623	36.99 62	40.27	8248.55	6246.83	6250.11	6253.39	6256.67	6259.96	6263.24
1920 1980 1940 636											6296.05
1930 633 1940 636											6328.85
1940 636	- 1										6861.66
1050 690						6378.07					6394.47
בהסוו טפעו	97.75	97.75 640	01.08 64	04.82	6407.60	6410.88	6414.16	6417.44	6420.72	6424.00	6427.28
		30.56 64									
		68.87 64									
	63.37	96.18 64									
		28.99 65									
	96.18	61.80 65									
	96.18 28.99	0.	1.	9.	3.	4.	5.	6.	7.	8.	9.

2000 to 2899.

Metres.					Metres.	(Units)				
bfartæ.	0.	l.	2.	8,	4.	5.	6.	7.	8.	9.
	Eng.Feet.	Eng.Feet.					Eng.Feet.		-	
2000	6561.80	6565.08		l .	6574.92	i	6581.48	l .	6588.05	6591.83
2010	6594.61	6597.89	1	6604.45		6611.01	6614.29		6620.85	6624.14
2020	6627.42	0680.70		6637.26		6648.82	6647.10	l	6653.66	6656.94
20 30 2040	6660.23 6693.03	6663.51 6696.82	1	6670.07 6702.88		6676.68	6679.91	6688.19	6686.47	6699.78
2040	0033.03	0090-82	9055.00	0102.00	0100.10	6709.44	6712.72	6716.00	6719.28	6722.56
2050	6725.84	67 29 .12	6782.41	6735.69	6738.97	6742.25	6745.58	6748.81	6752.09	6755.37
2060	6758.65	6761.98		6768.49		6775.06	6778.34	6781.62	6784.90	6788.18
2070	6791.46	6794.74	6798.02	6801.80	6804.58	6807.87	6811.15		6817.71	6820.99
2080	6824.27	6827.55	6830.83		6837.89	6840.67	6843.96	6847.24	6850.52	6853.80
2090	6857.08	6860.86	6868.64	6866.92	6870.20	6878.48	6876.76	6880.05	6888.33	6886.61
2100	6889.89	6898.17	6896.45	6899.78	6908.01	6906.29	6909.57	6912.85	6916.14	6919.4
2110	6922.70	6925.9 8				6939.10	6912.88		6948.94	6952.2
2120	6935.51	6958.79	i	6965.88		6971.91	6975.19	1	6981.75	6985.0
2130	6988.32	6991.60	6994.88	6998.16	7001.44	7004.72	7008.00	1	7014.56	7017.8
2140	7021.12	7024.41	7027.69	7030.97	7084.25	7087.58	7040.81	7044.09	7047.87	7050.6
2150	7058.98	7057.21	7060.49	7063.78	7067.06	7070.84	7078.62	7076.90	7080.18	7088.4
2160	7086.74	7090.02	7093.30	7096.58	7099.87	7108.15	7106.48	7109.71	7112.99	7116.2
2170	7119.55	7122.83	7125.11	7129.89	7182.67	7135.96	7139.24	7142.52	7145.80	7149.0
2180	7152.86	7155.64	7158. 9 2	7162.20	7165.48	7168.76	7172.05	7175.88	7178.61	7181.89
2190	7185.17	7188.45	7191.78	7195.01	7193. 29	7201.57	7204.85	7208.14	7211.42	7214.70
2200	7217.98	7221.26	7224.54	7227.82	7281.10	7284.38	7287.66	7240.94	7244.23	7247.5
2210	7250.79	7254.07		7260.68		7267.19	7270.47	7273.75	7277.03	7280.3
2220	7288.60	7286 .88	1	ı	7296.72	7800.00		l .	7809.84	7313.1
2230	7816.41	7819.69		7826.25		7332.81	7336.09	•	7842.65	7845.9
2240	7849.21	7352.49	7855.78	7859.06	7362.34	7865.62	7368.9 0	7872.18	7875.46	7878.7
2250	7882.02	7885.30	1	7891.87	l	7898.43	7401.71	7404.99	7408.27	7411.5
2260	7414.88	7418.11		7424.67		7431.24	1		7441.08	7444.8
2270	7447.64	7450.92	i .	7457.48		7464.05			7473.89	7477.1
2280	7480.45	7488.78	1	7490.29		7496.85	7500.14		7506.70	7509.9
2290	7513.26	7516.54	7519.82	75 28 .10	7526.38	75 29.66	7582.94	7586.28	7539.51	7542.7
2300	7546.07	7549.35	7552.64	7555.91	7559.19	7562.47	7565.75	7569.08	7572.82	7575.6
2310	7578.88	7582.16	1	7588.72	ľ	7595.28	7598.56	ł	7605.12	7608.4
2320	7611.69	7614.97	7618.25	7621.58	7624.81	7628.09	7681.87	7684.65	7637.98	7641.2
2330	7644.50	7647.78		7654.84		7660.90	7664.18	7667.46	7670.74	7674.0
2840	7677.80	7680.58	7688.87	7687.15	7690.48	7698.71	7696.99	7700.27	7708.55	7706.8
2350	7710.11	7718.89	7716.67	7719.96	7728.24	7726.52	7729.80	7788.08	7736.36	7739.6
2360	7742.92	7746.20	7749.48	7752.76	7756.05	7759.88	7762.61	7765.89	7769.17	7772.4
2370	7775.78	7779.01	7782.29	7785.57	7788.85	7792.14	7795.42	7798.70	7801.98	7805.20
2380	7808.54	7811.82	7815.10	7818. 3 8	7821.66	7824.94	7828.28	7881.51	7834.79	7888.0
2390	7841.85	7844.68	7847.91	7851.19	7854.47	7857.75	7861.08	7864.32	7867.60	7870.8
	0.	1.	2,	8.	4.	5.	6.	7.	8.	9.

9400 to 2799.

Metres.					Metrus.	(Units)				
Meries.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	-	Eng.Feet.				Eng.Feet.		Eng.Font		
2400 ·	7874.16	7877.44			7887.28		7898.84	1	1	7903.6 9
2410	7906.97	7910.25			7920.09		7926.65	7929.93		7936.50
2420	7939.78	7948.06		7949.62	7952.90	7956.18	7959.46	1	7966.02	7969.30
2430	7972.59	7975.87		7982.48	7985.71	7988.99	7992.27		7998.83	8002.11
2440	8005.39	8008.67	8011.96	8015.24	8018.52	8021.80	8025.08	8028.86	8031.64	8034.92
2450	8038.20	8041.48	8044.76	8048.05	8051.88	8054.61	8057.89	8061.17	8064.45	8067.73
2460	8071.01	8074.29	8077.57	8080.85	8084.14	8087.42	8090.70	8098.98	8097.26	8100.5
2470	8103.82	8107.10	8110.88	8113.66	8116.94	8120.22	8123.51	8126.79	8130.07	8133.3
2480	8136.63	8139.91	8143.19	8146.47	8149.75	8158.03	8156.32	8159.60	8162.88	8166.16
2490	8169.44	8172.72	8176.00	8179.28	8182.56	8185.84	B189.12	8192.41	8195.69	8198.97
2500	8202.25	8205.53	8208.81	8212.09	8 215.87	8218.65	8221.98	8225.21	8228.50	8231.78
2510	8235.06	8238.84	8241.62	8244.90	8248.18	8251.46	8254.74	8258.02	8261.30	8264.59
2520	8267.87	8271.15	8274.43	8277.71	8280.99	8284.27	8287.55	8290.83	8294.11	6 297.3 9
2530	8300.67	8308.96	8807.24	8310.52	8313.80	8817.08	8320.36		8826.92	8330.20
2540	8833.48	8886.76	8840.05	8348.88	8346.61	8849.89	8858.17	8 356 .45	8359.73	8363.01
2550	8366.29	8869.87	8372.85	8876.14	8879.42	8882.70	8385.98	8889.26	8392.54	8395.82
2560	8399.10	8402.38	8405.66	8408.94	8412.23	8415.51	8418.79	8422.07	8425.85	8428.6
2570	8431.91	8435.19	8438.47	8441.75	8445.08	8448.32	8451.60	8454.88	8458.16	8461.4
2580	8464.72	8468.00	8471.28	8474.56	8477.84	8481.12	8484.41	8487.69	8490.97	8494.2
2590	8497.53	8500.81	8504.09	8507.37	8510.65	8513.98	8517.21	8520.50	8523.78	8527.00
2600	8580.84	8533.62	8536.90	8540.18	8548.46	8546.74	8550.02	8558.30	8556.58	8559.8
2610	8568.15	8566.43	8569.71	8572.99	8576.27	8579.55	8582.83		8589.39	8592.6
2 620	8595.96		i		8609.08		8615.64	1	8622.20	8625.4
263 0	8628.76	8632.05	8685.83		8641.89	8645.17	8648.45		8655.01	8658.2
2640	8661.57	8664.85	8668.14	8671.42	8674.70	8677.98	8681.26	8684.54	8687.82	8691.1
2650	8694.39	8697.66	8700.94	8704.28	8707.51	8710.79	8714.07	1	8720.63	8723.9
2660	8727.19	8730.47		8737.08		8748.60	8746.88	1	8753.44	8756.7
2670	8760.00	8768.28		8769.84	8773.12	8776.41	8779.69		8786.25	8789.5
2680	8792.81	8796.09		8802.65	i .	8809.21	8812.50		8819.06	8822.3
2690	8825.62	8828.90	8882.18	8835.46	8838.74	8842.02	8845.30	8848.59	8851.87	8855.1
2700	8858.43	8861.71	8864.99	8868.27	8871.55	8874.83	8878.11	8881.89	8884.67	8987.9
2710	8891.24	8894.52		8901.08	1	8907.64	8910.92	1	8917.48	
2720	8926.05	8927.33	8930.61	8933.89	8987.17	8940.45	8948.78	8947.01	8950. 29	8953.5
2730	8956.85	8960.14	8963.42	8966.70	8969.98	8973.26	8976.54	8979.82	8983.10	8986.3
2740	8989.66	8992.94	8996.23	8999.51	9002.79	9006.07	9009.85	9012.63	9015.91	9019.1
2750	9022.47	9025.75	9029.03	9032.82	9035.60	9038.88	9042.16	9045.44	9048.72	9052.00
2760	9055.28	9058.56	9061.84	9065.12	9068.41	9071.69	9074.97	9078.25	9081.53	9084.8
2770	9088.09		1	1	9101.21	8	9107.78		9114.34	9117.65
2780	9120.90	9124.18	9127.46	9180.74	9134.02	9187.80	9140.59	9143.87	9147.15	9150.43
2790	9153.71	9156.99	9160.27	9163.55	9166.88	9170.11	9173.39	9176.68	9179.96	9183.2
	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.

2800 to 3000.

					, w et					
					Metree.	(Units.)				
Metres.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	For Fort	For Feet	For Post	Eng Past	Fra Ford	Eng.Feet.	Por Post	Eng Post	Fra Veet	For Pari
2800						9202.92				
2810	9219.33	9222.61	9225.89	9229.17	9232.45	9285.78	9289.01	9242.29	9245.57	9248.8
2820	9252.14	9255.42	9258.70	9261.98	9265.26	9268.54	9271.82	9275.10	9278.38	9281.66
2830	9284.94	9288.23	9291.51	9294.79	9298.07	9301.35	9804.64	9307.91	9311.19	9314.47
2840	9317.75	9321.03	9824.82	9827.60	9330.88	9334.16	9337.44	9340.72	9844.00	9347.28
				Ì		1		i		
2850	9350.56	9353.84	9357.12	9360.41	9363.69	9866.97	9870.25	9373.53	9876.81	9380.09
2860	9383.87	9386.65	9389.93	9393.21	9396.50	9399.78	9403.06	9406.84	9409.62	9412.90
2870	9416.18	9419.46	9422.74	9426.02	9429.30	9432.59	9435.87	9489.15	9442.43	9445.71
2880	9448.99	9452.27	9455.55	9458.83	9462.11	9465.39	9468.68	9471.96	9475.24	9478.52
2890	9481.80	9485.08	9488.86	9491.64	9494.92	9498.20	9501.48	9504.76	9508.05	9511.88
						ľ	Į.			
2900						9531.01				
2910	11					9563.82				
2920	9580.23	9583.51	9586.79	9590.07	9593.35	9596.63	9599.91	9603.19	9606.47	9609.75
2930	11					9629.44				
2940	9645.84	9649.12	9652.41	9655.69	9658.97	9662.25	9665.53	9668.81	9672.09	9675.87
		1								
2950					1	9695.06	ı	1 1		
2960	H	1				9727.87		1		
2970	11					9760.68			i - 1	
2980	н .					9793.48				
2990	11				1	9826.29	1			
3000	9842.70	9845.98	9849.26	9852.54	9855.82	9859.10	9862.38	9865.66	9868.94	9872.23

Proportional Parts.

Metres.					Decin	netres.				
Meries.	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.
	Eng.Feet.	Eng.Feet.	Eng.Feet.	Eng. Feet.	Eng.Feet.	Eng.Feet.	Eng.Feet	Eng.Feet.	Eng.Font.	Eng.Feet.
0	0.0000	0.8281	0.6562	0.9848	1.3124	1.6404	1.9685	2.2966	2.6247	2.9528
1	8.2809	8.6090	8.9371	4.2652	4.5988	4.9213	5.2494	5.5775	5.9056	6.2387
2	6.5618	6.8899	7.2180	7.5461	7.8742	8.2022	8.5803	8.8584	9.1865	9.5146
8	9.8487	10.1708	10.4989	10.8270	11.1551	11.4881	11.8112	12.1898	12.4674	12.7955
4	13.1286	13.4517	18.7 7 98	14.1079	14.4360	14.7640	15.0921	15.4202	15.7483	16.0764
5	16.4045	16.7826	17.0607	17.8888	17.7169	18.0449	18.8780	18.7011	19.0292	19.8573
6	19.6854	20.0135	20.8416	20.6697	20.9978	21.3258	21.6539	21.9820	22.8101	22.6382
7	22.9663	28.2944	23.6225	23.9506	24.2787	24.6067	24.9848	25.2629	25.5910	25.9191
8	26.2472	26.5758	26.9034	27.2315	27.5596	27.8876	28.2157	28.5488	28.8719	29.2000
9	29.5281	29.8562	30.1843	30.5124	80.8405	31.1 6 85	31.4966	31.8247	31.1528	32.4809
	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.

VIIL CONVERSION OF METRES INTO AMERICAN FERT AND DECIMALS.

1 Metre = 8.28070878 American Feet.

Motres.		·		2 XII	Hund	trods.				
Thousands.	0.	100.	200.	800.	400.	500.	600.	700.	500.	900.
	Am Feet.	Am Feet.	Am. Feet.	Am. Feet	Am. Feet	Am.Feet	Am. Feet	Am. Feet.	Am.Feet	Am. Foot
0	0.0	829.1	656.1	984.2	1812.3	1640.4	1968.4	2296.5	2624.6	2952.6
1000	3280.7	3608.8	3936.9	4261.9	4598.0	4921.1	5249.1	5577.2	5905.3	6233.3
2000	6561.4	6889.5	7217.6	7545.6	7878.7	8201.8	8629.8	8857.9	9186.0	9514.1
8000	9842.1	10170.2	10498.3	10826.8	11154.4	11482.5	11810.6	12138.6	12466.7	12794.8
4000	13122.8	13450.9	13779.0	14107.0	14485.1	14768.2	15091.8	15419.8	16747.4	1 0075 .5
5000	16408.5	16731.6	17059.7	17887.8	17715.8	18048.9	18872.0	18700.0	19028.1	19356.2
6000	1			1	20996.5				22308.8	
7000		1			24277.2				25569.5	
8000	26245.7	26578.7	26901.8	27229.9	27558.0	27886.0		ı		
9000						21166.7	,	1	,	
Tens.	0.	1.	9.	2.	Un.	ite. 5.	6.	7.	8.	9.
0	Am Feet 0.000	Am Feet. 8.281	Am. Feet 6.561	Am. Feet. 9.842	Am.Feet 18.123	Am Feet. 16.404	Am. Feet 19.684		Am. Feet. 26,246	Am. Feet 29.526
10	32.807	86.088			45.980					
20	65.614	68.895			78.737	82.018			91.860	95.141
80	98.421			108.268					124.667	
40		134.509			144.851				157.474	
				22.040		-11.002	.30.010			
50	164.085	167.816	170.597	178.878	177.158	180.439	183.720	187.000	190.281	193.562
60	196.848	200.123	208.404	206.685	209.965	213.246	216.527	219.807	223.088	226.369
70	229.650	232.930	286.211	289.492	242.772	246.053	249.334	252.615	255.895	259.176
80	262.457	265.737	269.018	272.299	275.580	278.860	282.141	285.422	288.702	291.983
90	295.264	298.544	301.825	805.106	808.387	311.667	814.948	318.229	321.509	324.790

IX. CONVERSION OF METRES INTO RHINE OR PRUSSIAN FEET AND DECIMALS.

1 Metre = 8.1861995 Rhine Feet.

Motres.					Hun	dreds.				
Thousands	0.	100.	200.	800.	400.	500.	600.	700.	800.	900.
	Rhine Ft.	Rhine Ft.	Rhine Pt.	Rhine Ft.	Rhine Ft.	Rhine Pt	Rhine Ft.	Rhine Ft.	Rhine Ft.	Rhine Ft.
0	0.0	818.6	687.2	955.9	1274.5	1593.1	1911.7	2230.3	2549.0	2667.6
1000	8186.2	3504.8	8823.4	4142.1	4460.7	4779.3	5097.9	5416.5	5735.2	6053.8
2000	6372.4	6691.0	7009.6	7328.3	7646.9	7965.5	8284.1	8602.7	8921.4	9240.0
3000	9558.6	9877.2	10195.8	10514.5	10633.1	11151.7	11470.8	11788.9	12107.6	12426.2
4000	12744.8	18063.4	18882.0	18700.7	14019.8	14387.9	14656.5	14975.1	1 5293. 8	15612.4
5000	15931.0	16249.6	16568.2	16886.9	17205.5	17524.1	17842.7	18161.3	18480.0	16798.6
6000	19117.2	19485.8	19754.4	20073.1	20391.7	20710.8	21028.9	21347.5	21666.2	21984.8
7000	22808.4	22622.0	22940.6	23259.3	23577.9	23896.5	24215.1	24583.7	24852.4	25171.0
8000	25489.6	25808.2	26126.8	26445.5	26764.1	27082.7	27401.8	27719.9	28038.6	28357.2
9000	28675.8	28994.4	29313.0	29631.7	29950.3	30268.9	30587.5	30906.1	31224.8	31543.4

PARIS OR FRENCH FEET

INTO DIFFERENT MEASURES OF LENGTH.

X. CONVERSION OF PARIS OR FRENCH FRET INTO TOISES.

1 French Foot = 0.1606666 Tolse.

					Hun	ireds.				
Franch Foot. Thousands.	0.	100.	200.	800.	400.	500.	600.	700.	800.	900.
	Toises.	Toless.	Toises.	Toises.	Toises.	Tolog	Tolans.	Tolees.	Toises.	Toises-
0	0.00	16.67	38.38	50.00	66.67		100.00			150.00
1000	166.67			216.67						1
2000	833.83				400.00		433.88	450.00	466.67	483.88
3000	500.00						l	616.67	683.33	650.00
4000	666.67				788.88		766.67	788.83	800.00	816.67
8000	883.33	850.00	866.67	883.83	900.00	916.67	938.38	950.00	966.67	983.88
6000	1000.00	1016.67	1088.83	1050.00	1066.67	1088.33	1100.00	1116.67	1133.83	1150.00
7000	1166.67	1183.83	1200.00	1216.67	1238.38	1230.00	1266.67	1283.83	1800.00	1316.67
8000	1333.33	1350.00	1866.67	1883.33	1400.00	1416.67	1483.88	1450.00	1466.67	1488.88
9000	1500.00	1516.67	1588.88	1550.00	1566.67	1583.83	1 600.0 0	1616.67	1688.33	1650.00
10000	1666.67	1688.33	1700.00	1716.67	1788.88	1750.00	1768.67	1783.88	1800.00	1816.67
11000	1833.38	1850.00	1866.67	1883.83	1900.00	1916.67	1933.33	1950.00	1966.67	1983.38
12000	2000.00	2016.67	2033.38	2050.00	2066.67	2088.38	2100.00	2116.67	2183.83	2150.00
13000	2166.67	2183.83	2200.00	2216.67	2233.88	2250.00	2266.67	2288.83	2300.00	2316.67
14000	2333.83	2850.00	2866.67	2388.83	2400.00	2416.67	2488.8 3	2450.00	2466.67	2488.33
15000	2500.00	25 16.67	2538.33	2550.00	2566.67	2583.33	2600.00	2616.67	2633.83	2650.00
16000	2666.67	2683.33	2700.00	2716.67	2783.38	2750.00	2766.67	2783.33	2800.00	2816. 67
17000	2883.88	2850.00	2866.67	2883.83	2900.00	2916.67	2933.83	2950.00	2966.67	2983.33
18000	8000.00	3016.67	3033.38	8050.00	3066.67	8063.33	8100.00	3116.67	8138.33	3150.00
19000	8166.67	3183.83	3200.00	3216.67	3233.33	8250.00	3266.67	3283.33	8800.00	35 16.67
20000	3333.83	3350.00	3366.67	8383.83	8400.00	3416.67	8433.83	3450.00	3466.67	3483.88
21000	8500.00	3516.67	3583.83	8550.00	3566.67	3583.83	3600.00	3616.67	8633.33	3650.00
22000	3666.67	3688.83	8700.00	3716.67	8788.83	8750.00	3766.67	3783.83	3800.00	3816.67
23000					3900.00					
24000					4066.67					
25000	4166.67	4183.33	4200.00	4216.67	4283.33	425 0.00	4266.67	4 283.8 3	4300.00	4816.67
26000	4333.33	4350.00	4366.67	4393.83	4400.00	4416.67	4433.38	4450.00	4466.67	4488.38

XI. CONVERSION OF PARIS OR FRENCH FEET INTO METRES.

1 Paris Foot - 0.32483948 Metres.

French Foot.					Hund	lreds.				-
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Motres.	Metres.	Metres.	Motres.	Motres.	Motres.	Metres.	Motres.	Metres.	Motres
0	000.00		64.97				l			
1000	824.84									
2000	649.68		714.65	l	1					
8000	11				1104.45		1		1	l
4000	1299.86	1881.84	1864.33	1896.81	1429.29	1461.78	1494.26	1026.75	1559.23	1591.7
5000	1624.20	1656.68	1689.16	1721.65	1754.18	1786.62	1819.10	1851.58	1884.07	1916.5
6000	11				2078.97			1	1	1
7000	II .	l			2408.81		ł	1	ł	l
8000	2598.72	2631.20	2663.68	2696.17	2728.65	2761.14	2793.62	2826.10	2858.59	2891.0
9000	2923.55	2956.04	29 88.52	8021.01	3053.49	3065.97	8118.46	8150.94	3183.43	32 15.9
10000	8248.89	3280.88	8818.36	8345.85	3878.33	8410.81	844 8.3 0	8475.78	3508.27	3540.7
11000	и	1	,		3703.17			ı	•	1
12000	3898.07	3980.56	3963.04	8995.52	4028.01	4060.49	4092.98	4125.46	1157.94	4190.4
13000	4222.91	4255.40	4287.88	4820.36	4352.85	4885.83	4417.82	4450.80	4482.78	4515.2
14000	4547.75	4580.24	4612.72	4645.10	4677.59	4710.07	4742.56	4775.04	4807.52	4840.0
15000	4872.59	4905.08	4937.56	4970.04	5002.58	5085.01	5067.49	5099.9 8	5132.46	5164.9
16000					5827.87				5457.30	
17000	H			1	5652.21		5717.17	5749.66	5782.14	5814.6
18000	5847.11	5879.59	5912.08	5944.56	5977.05	6009.58	6042.01	6074.50	6106.98	6139.
19000	6171.95	6204.48	6 286. 92	6 269.4 0	6301. 88	6884.87	6866. 85	6399.34	6431.82	616173
20000	6496.79	6529.27	6561.76	6594.24	6626.72	6659.21	6691.69	6724.18	6756.66	6789.1
21000	6821.63	6854.11	6886.60	6919.08	6951.56	6984.05	7016.53	7049.02	7081.50	7118.9
22000	7146.47	7178.95	7211.44	7248.92	7276.40	7308.89	7841-87	7373. 86	7406.34	7438.
23000	7471.81	7508.79	7536.27	7369.76	7601.24	7683.73	7666.21	7698.69	773 1.18	7763.6
24000	7796.15	78 2 8.63	7861.11	7893.60	7926.08	7958.57	7991.05	8028.53	8056.02	8088.
25000					8250.92					
26000	8445.83	8478.31	8310.79	8543.28	8575.76	8608.24	8640.73	8673.21	8705.70	8738.1
27000	8770.66	8808.15	8835.63	8868.12	8900.60	8988.08	8965.57	8998.03	9030.54	9063.0
					Un	ite.				
Tens.	0.	1.	3.	3.	4.	5.	6.	7.	8.	9.
	Metres.	Motros.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres
0	0.0000	0.8248			1.2994	1.6242	1.9490		2.5987	
10	3.2484	3.5732	3.8981	4.2229	4.5478	4.8726	5.1974	5.5228	5.8471	6.171
20	6.4968	6.8216	7.1465	7.4718	7.7961	8.1210	8.4458	8.7707	9.0955	9.420
30	9.7452	10.0700	10.8949	10.7197	11.0445	11.3694	11.6942	12.0191	12.3439	12.668
40	12.9986	18.8184	13.6438	13.9681	14.2929	14.6178	14.9426	15.2675	15.5923	15.917
50	16.2420	16.5668	16.8916	17.2165	17.5418	17.8662	18.1910	18.5158	18.8407	19.165
60	19.4904	19.8152	20.1400	20.4649	20.7897	21.1146	21.4894	21.7642	22.0891	22.413
70	22.7888	28.0686	23.3884	23.7188	24.0381	24.3630	24.6878	25.01 26	25.3875	25.662
80					27.2863					
90	29.2355	OO KRO I	20 8859	90 9101	20 K9 IA	On exer	91 19 18	01 EAG 4	91 2949	99 150

XII. CONVERSION OF PARIS OR FRENCH FEET INTO ENGLISH FEET AND DECIMALS.

1 French Foot = 1.06576527 English Feet.

Franch Feet.					Hund	ireds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
			. •		Eng. feet.		Eng. feet.			
1000	0.0	106.6		819.7	426.8	532.9				
1000	1065.8				l		1	1	1	
2000	2131.5								l	8090.7
2000 4000	3197.8 4263.1								1	
			122002							
5000	5828.8						l		6181.4	
6000	6894.6		I		l		l	1		
7000	7460.4			i e	1					
8000	8526.1									
9000	9591.9	9698.5	9805.0	9911.6	10018.2	10124.8	10281.3	10887.9	10444.5	10551.1
10000	10657.7	10764.2	10870.8	10977.4	11084.0	11190.5	11297.1	11408.7	11510.3	11616.8
11000	11728.4	11830.0	11936.6	12043.1	12149.7	12256.8	12862.9	12469.5	12576.0	12682.6
12000	12789.2	12895.8	13002.3	13108.9	18215.5	13322.1	18428.6	13535.2	13641.8	18748.4
13000	13855.0	13961.5	14068.1	14174.7	14291.3	14887.8	14494.4	14601.0	14707.6	14814.1
14000	14920.7	15027.8	15183.9	15240.4	15847.0	15453.6	15560.2	1 5666. 8	15773.8	15879.9
****	15000 5	* 6000		10000	16410 0	10510 4	10007.0	10000 6	10000 1	100.0
15000						16519.4				
16000	1	•				17585.1				
17000					18544.3		18757.5			
18000 19000					19610.1 20675.8		19828.2 20889.0			
19000	20219.0	20300.1	20462.7	20569.8	20070.0	20/52.4	20009.0	20990.0	21102.2	21200.7
20000	21315.3	21421.9	21528.5	21685.0	21741.6	21848.2	22054.8	22161.3	22167.9	2 32 74.5
21000	22381.1	22487.7	22594.2	22700.8	22807.4	22914.0	23020.5	23127.1	28288.7	28840.3
22000	28446.8	28558.4	23660.0	23766.6	23873.1	28979.7				
23000	24512.6	24619.2	24725.8	24882.3	24988.9	25045.5	25152.1	25258.6	25865.2	25471.8
24000	25578.4	25684.9	25791.5	25898.1	26004.7	26111.3	26217. 8	26824.4	26481.0	26587 .6
25000	266411	26750 7	26257.2	98082 0	97070 4	27177.0	97988 A	27890.2	971 98 .7	27602.2
26000	1					28242.8		1		
27000						29808.5				
					Un	its.				
Tens.	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.
0	Eng. feet. 0.000	Rng. feet. 1.066	Eng. feet. 2.132	Eng. feet. 8.197	Eng. feet. 4.263	Eng. feet. 5.829	Rng. feet. 6.395	Ing. feet. 7.460	Eng. feet. 8.526	Eng. feet 9.592
10	10.658		12.789	13.855	14.921	15.986	17.052			20.250
20	21.815	22.381	23.447		25.578		1			
80	31.978					37.802				
40	42.631	33.039 43.696	84.104 44.762	35.170 45.828	86.286 46.894	47.959			51.157	52.223
50	53.288	54.854	55.420	56.486	57.551	58.617			61.814	
60	63.946	65.012		67.148	68.209	69.275			72.472	
70	74.604	75.669		77.801	78.867				83.130	
80	85.261	86.827	87.393	88.459	89.524	90.590			93.787	
90	95 919	96.985	98.050	99 118	100.182	101.248	102.313	103.379	104.445	105.511

XIII. CONVERSION OF PARIS OR FRENCH FRET INTO AMERICAN FEET.

1 French Foot = 1.0657084 American Foot.

French Feet,					Hun	dreds.				
Thousands.	•.	100.	200.	800.	400.	500.	600.	700.	800.	900.
	Am. Foot.	Am. Foot	Am. Foot.	Am. Foot.	Am Foot	Am. Foot.	Am. Foot	Am. Foot.	Am. Foot	Am. Feet
0	0.0	106.6	218.1	819.7	426.8	532.9	639.4	746.0	852.6	959.1
1000	1065.7	1172.3	1278.8	1885.4	1492.0	1598.6	1705.1	1811.7	1918-3	2024.8
2000	2131.4		1		2557.7	2664.3	1			
8000	3197.1	3808.7			3623.4	8730.0	1			4156.2
4000	4262.8	4 36 9.4	4476.0	4582.5	4689.1	4795.7	4902.2	5606.8	5115.4	5221.9
5000	5828.5	5485.1	5541.7	5648.2	5754.8	5861.4	5967.9	6074.5	6181.1	6287.7
6000	6394.2	6500.8	6607.4	6713.9	6820.5	6927.1	7088.6	7140-2	7246-8	7853.4
7000	7459.9	7566.5	7673.1	7779.6	7886.2	7992.8	8099.8	8205.9	8312.5	8419.1
8000	8525.6	8682.2	8788.8	8845.8	8951.9	9058.5	9165.1	9271.6	9378-2	9484.8
9000	9591.8	9697.9	9804.5	99 11.0	10017.6	10124.2	10230.8	10337.8	10443.9	10550.5
10000	10657.0	10763.6	10870.2	10976.7	11083.3	11189.9	11296.5	11403.0	11509-6	11616.2
11000	11722.7	11829.3	11935.9	12042.5	12149.0	12255.6	12362.2	12468.7	12575.3	12681.9
12000	12788.4	12895.0	13001.6	18108.2	18214.7	13321.3	18427.9	13534.4	13641-0	18747.6
18000	13854.1	18960.7	14067.3	14178.9	14280.4	14887.0	14498.6	14600.1	14706.7	14813.3
14000	14919.9	15026.4	15188.0	15239.6	15346.1	15452.7	15559.8	15665.8	15772.4	15679.0
15000	15985.6	16092.1	16198.7	16305.3	16411.8	16518.4	16625.0	16731.5	16838.1	16944.7
16000	1		t .	1	l .	17584.1			1	1
17000	1		1			186 19.8			1	1
18000	1		ľ		1	19715.5			1	i
19000			1	L		20781.2			ı	1
20000	21814.1	21420.6	21527.2	21633.8	21740.4	21846.9	21958-5	22060.1	22166.6	22273.2
21000						22912.6			1	1
22000					4	23978.8			ł	1
28000						25044.0				
24000				1	1	26109.7			,	
25000	26642.6	26749.2	26855.7	26962.3	27068.9	27175.4	27282.0	27388.6	27495.2	27601.7
26000				1	1	28241.1				
27000						29806.8				
29000)		30372.6				
					Un	its.				3
Tens.	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.
	Am. Feet.	Am, Feet.	Am Rest	Am Foot	Am Feet	Am Post	Am Foot	Am Feet.	Am Feet	Am. Feet.
	0.00	1.07	2.13	3.20	4.26	5.33	6.89	7.46	8.53	9.59
10	10.66	11.72	12.79	13.85	14.92	15.99	17.05	18.12	19.18	20.25
20	21.31	22.38	23.45	24.51	25.58	26.64	27.71	28.77	29.84	30.91
80	31.97	83.04	84.10	35.17	36.23	37.30	88.87	39.43	40.50	41.56
40	42.63	48.69	44.76	45.83	46.89	47.96	49.02	50.09	61.15	52.22
50	53.29	54.35	55.42	56.48	57.55	58.61	59.68	60.75	61-81	62.88
60	68.94	65.01	66.07	67.14	68.21	69.27	70.84	71.40	72.47	78.53
70	74.60	75.66	76.78	77.80	78.86	79.93	80.99	82.06	83.12	84.19
80	85.26	86.82	87.39	88.45	89.52	90.58	91.65	92.72	93.78	94.85

ENGLISH YARDS AND FEET

INTO DIFFERENT MEASURES OF LENGTH.

XIV. CONVERSION OF ENGLISH YARDS INTO FRENCH TOISES.

1 English Yard = 0.4691465 Tolse.

English Yards					Hun	trods.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
 -	Toises.	Tolses.	Toises.	Toises.	Tolees.	Toises.	Toises	Toises.	Toises.	Toises.
0	0.00	46.91	93.88	140.74	187.66	284.57	281.49	828.40	375.82	422.23
1000	469.15	516.06	562.98	609.89	656.80	708.72	750.63	797.55	844.46	891.88
2000	938.29	985.21	1032-12	1079.04	1125.95	1172.87	1219.78	1266.70	1313.61	1360.52
3000	1407.44	1454.35	1501.27	1548.18	1595.10	1642.01	1688.93	1735.84	1782.76	1829.67
4000	1876.59	1923.50	1970.41	2017.83	2064.24	2111.16	2158.07	2204.99	2251.90	2298.82
5000	2345.73	2392.65	2439.56	2486.48	2533.39	2580.31	2627.22	2674.13	2721.05	2767.96
6000	2814.88	2861.79	2908.71	2955.62	8002.54	8049.45	3096.37	3143.28	3190.20	3237.11
7000	3284.02)					1	
8000	8758.17									
9000	4222.32	4269.23	4316.15	4363.06	4409.98	4456.89	4503.81	4550.72	4597.63	4644.55

XV. CONVERSION OF ENGLISH YARDS INTO METRES.

1 English Yard = 0.91488848 Metre.

English Yards.					Hund	ireds.				
Thousands.	0.	100.	200.	200.	400.	500.	600.	700.	800.	200.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Motres.
0	0.00	91.44	182.88	274.82	365.75	457.19	548.68	640.07	781.51	822.95
1000	914.38	1005.82	1097.26	1188.70	1280.14	1371.58	1463.01	1554.45	1645.99	1737.38
2000	1828.77	1920.21	2011.64	2103.08	2194.52	2285.96	2377.40	2468.84	2560.27	2651.71
3000	2743.15	2834.59	2926.03	3017.47	3108.90	8200.84	3291.78	3383.22	3474.66	3566.10
4000	3657.53	3748.97	3840.41	8981.85	4023.29	4114.78	4206.16	4297.60	4889.04	4480.48
5000	4571.92	4663.86	4754.79	4846.23	4987.67	5029.11	5120.55	5211.99	5808.42	5894.86
6000	5486.30	5577.74	5669.18	5760.62	5852.05	5943.49	6034.93	6126.37	6217.81	6309.25
7000	6400.68	6492.12	6588.56	6675.00	6766.44	6857.88	6949.81	7040.75	7132.19	7223.63
8000	7315.07	7406.51	7497.94	7589.88	7680.82	7772.26	7863.70	7955.14	8046.57	8138.01
9000	8229.45	8320.89	8412.83	8508.77	8595.20	8686.64	8778.08	8869.52	8960.96	9052.40

XVI. CONVERSION OF ENGLISH FEET INTO METRAS.

1 English Foot = 0.30479449 Metre.

Hoglish Foot.					Hone	treds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	200.
	Metres.	Metres.	Motres.	Metres.	. Motres.	Motres.	Metres.	Motres.	Motres.	Motres.
0	11	30.4794		91.4883					243.886	
1000		385.274	365.768	396.233	426.712	457.192	487.671		548.630	1
2000 2000		640.068 944.868	670.548 975.842	701.027 1005.82	781.507 1086.80	761.986 1066.78			858.425 1158.22	
4000		1249.66	1280.14	1810.62		1871.58			1463.01	
5000	1523.97	1554.45	1584.98	1615.41	1645.89	1676.87	1706.85	1737.83	1767.81	1796.2
6000	1828.77	1859.25	1889.73	1920.21	1950.68	1981.16	ı	ı	2072.60	i
7000	2133.56	2164.04	2194.52	2225.00	2255.48	2285.96	2816.44	2846.92	2377.40	2407.8
8000	2438.36	2468.84	2499.81	2529.79	2560.27	2590.75	2621.28	2651.71	2682.19	2712.6
9000	2743.15	2778.63	2804.11	2834.59	2865.07	2895.55	2926.03	2956.51	2986.99	2017.4
10000	3047.94	3078.42	3108.90	3139.38	8169.86	3200.84	į.	ı	3291.7 8	1
11000	3852.74	3883.22	3413.70	3444.18	3474.66	3505.14	8585.62	3566.10	3596.57	3627.0
12000	3657.58	3688.01	3718.49	8748.97	8779.45	8809.93	3840.41	3870.89	3901.37	3931.8
13000	3962.38	8992.81	4033.29	4058.77	4084.25	4114.78	4145.21	4175.68	4206.16	4236.6
14000	4267.12	4297.60	4228.08	4858.56	4889.04	4419.52	4450.00	4480.48	4510.96	4541.4
15000	4571.92	4602.40	4632.88	4663.36	4693.84	4724.31	4754.79	4785.27	4815.75	4846.2
16000	4876.71	4907.19	4987.67	4968.15	4998.63	50 29. 11	5059.59	5090.07	5120.55	5151.0
17000	5181.51	5211.99	5242.47	5272.94	5808.42	5333.90	5364.38	5894-86	5425.34	5455.8
18000	5486.80	5516.78	5547.26	5577.74	5608.22	5638.70	5669.18	5699.66	5780.14	5760.6
19000	5791.10	5821.57	5852.05	5882.58	5913.01	5948.49	5973.97	6004.45	6034.93	6065.4
20000	6095.89	6126.37	6156.85	6187.83	6217.81	6248.29	6278.77	6309.25	6339.73	6370.2
21000	6400.68	6481.16	6461.64	6492.12	6522.60	6553.08	6588.56	6614.04	6644.52	6675.0
22000	6705.48	6785.96	6766.44	6796.92	6827.40	6857.88	6888.36	6918.83	6949.81	6979.7
23000	7010.27	7040.75	7071.28	7101.71	7182.19	7162.67	7193.15	7228.63	7254.11	7284.5
24000	7315.07	7845.55	7376.08	7406.51	7436.99	7467.47	7497.94	7528.42	7558.90	7589.3
25000	7619.86	7650.34	7680.82	7711.30	7741.78	7772.26	7802.74	7833.22	7863.70	7894.1
26000	7924.66	7955.14	7985.62	8016.10	8046.57		l		8168.49	1
27000	8229.45	8259.93	8290.41	8320.89	8351.37	8381.85	8412.83	8442.81	8478.29	8503.7
28000	8584.25	8564.73	8595.20	8625.68	8656.16	8686.64	8717.12	8747.60	8778.08	8806.5
					Un	ite.				
Tens.	0.	1.	9.	3.	4.	5.	6.	7.	8.	9.
	Motres.	Motres.	Motres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metree.
0	0.00000		0.60959	0.91438		1.52397			2.43836	
10	8.04794			3.96233	4.26712				5.48630	
20	1					7.61986			1	1
80						10.6678				
40	12.1918	12.4966	12.8014	13.1062	13.4110	18.7158	14.0205	14.3258	14.6301	14.934
50						16.7637				
60	18.2877	18.5925	18.8978	19.2021	19.5068	19.8116	20.1164	20.4212	20.7260	21.030
70	21.3356	21.6404	21.9452	22.2500	22.5548	22.8596	23.1644	23.4692	23.7740	24.078
80	24.3836	24.6884	24.9931	25.2979	25.6027	25.9075	26.2123	26.5171	26.8219	27.126
90		07 7000	00 0111		00 0000	28.9555	00 0000	00 5053		

1 English Foot = 0.9883929 Paris Foot.

English Foot.					Hund	ireds.				
Thousands.	0.	100.	200.	800.	400.	500.	600.	700.	800.	900.
		l.		Par. Feet.	Par. Feet.				Par. Feet.	Par. Feet.
0	0.000	!	187.7	1	875.3	469.1	563.0			844.5
1000	938.3		1	4	1313.6	ľ	1		ŀ	1782.8
2000	1876.6		2064.2	1	2251.9		i e	1		2721.0
8000	2814.9					l .				l
4000	8758.2	3847.0	3940.8	4084,7	4128.5	4222.8	4816.1	4410.0	4503.8	4597.6
5000	4691.5	4785.8	4879.1	4978.0	5066.8	5160.6	5254.4	5848.3	5442.1	5535.9
6000	5629.8	5723.6	5817.4	5911.2	6005.1	6098.9	6192.7	6286.6	6380.4	6474.2
7000	6568.0	6661.9	6755.7	6849.5	6943.4	7037.2	7181.0	7224.9	7318.7	7412.5
8000	7506.3	7600.2	7694.0	7787.8	7881.7	7975.5	8069.3	8163.1	8257.0	8350.8
9000	8444.6	8538.5	8632.8	8726.1	8820.0	8918.8	9007.6	9101.4	9195.3	9289.1
10000	9382.9	9476.8	9570.6	9664.4	9758.2	9852.1	9945.9	10039.7	10133.6	10227.4
11000				10602.7						ì
12000	ll	1	1	11541.0	1		l .	ı	1	l
13000				12479.8						
14000				13417.6						
15000	14074 4	14160 0	1 1969 0	14355.9	14440 7	14840 8	14697 4	14701 9	14998 0	14010 0
16000	i i	ł	ì	15294.2	1		ı	ł	1	
17000	li .	ŧ	1	16232.5	ľ		1	1	ı	
18000			1	17170.8			1		1	
19000	II .		1	18109.0	1	Ì	l	1	I .	
20000				19047.8	1		1	1	1	
21000		1		19985.6	1		I .			
22000				20928.9			(l.	1	
23000		ľ		21862.2				ŀ		
24000	22019.0	22012.9	22706.7	22800.5	22094.5	22900.2	28062.0	28170.8	25209.1	2000.0
25000	23457.8	28551.1	28645.0	23738.9	23832.6	23926.5	24020.3	24114.1	24208.0	24301.8
26000	24395.6	24489.4	24588.3	24677.1	24770.9	24864.8	24958.6	25052.4	25146.2	25240.1
27000				25615.4			1)	1	
28000	26272.2	26366. 0	26459.9	26558.7	26647.5	26741.3	26835.2	26929. 0	27022.8	27116.7
	1				Un	ite.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
			Par Fast	Par. Feet.	Par Fast	Par Foot	Par. Fact	Par. Foot	Par. Vest	Par. Feet
0	0.00	0.94	1.88	2.81	8.75	4.69	5.68	6.57	7.51	8.44
10	9.38	10.32	11.26	12.20	18.14	14.07	15.01	15.95	16.89	17.88
20	18.77	19.70	20.64	21.58	22.52	23.46	24.40	25.33	26.27	27.21
80	28.15	29.09	30.03	30.96	31.90	82.84	83.78	84.72	85.66	36.59
40	87.53	88.47	89.41	40.85	41.28	42.22	48.16	44.10	45.04	45.98
50	48.02	47 OE	48.79	49.73	50.67	51.61	52.54	53.48	54.42	55.36
	46.91	47.85			60.05	60.99	61.93	62.87	63.80	64.74
60	56.80	57.24	58.17	59.11	1	1	71.31	72.25	73.19	74.18
70	65.68	66.62	67.56	68.50	69.48 78.82	70.87	80.69	81.63	73.19 82.57	83.51
80	73.06	76.00	76.94	77.88		79.75	ı	1		
90	84.45	85.38	86.32	87.26	88.20	89.14	90.08	91.01	91.95	92.89

XVIII. CONVERSION OF ENGLISH FEET INTO AMERICAN FRET AND DECIMALS.

1 English Foot = 0.90004197 American Foot.

					Hund	treds.				
ling. Feet. Thousands.	•.	100.	200.	800.	400.	500.	600.	700.	800.	900.
					Am.Feet.			Am. Foot.		
0	0.00	99.99	199.99	299.98	399.98	499.97	599.97	699.96	799.95	899.95
1000	999.94	1099.94	1199.93	1299.92	1399.92	1499.91	1599.91	1699.90	1799.90	1899.89
2000	1999.88	2099.88	2199.87	2299.87	2399.86	2499.85	2599.85	2699.84	2799-84	2899.83
8000	2999.83	8099.82	3199.81	8299.81	8899. 80	8499.80	8599.79	3699.79	3799.7 8	3899.77
4000	8999.77	4099.76	4199.76	4299.75	4399.74	4499.74	4599.78	4699.78	4799.72	4899.7 2
5000	4999.71	5099.70	5199.70	5299.69	5 29 9.69	5499.68	5599.6 8	5699.67	5799.66	589 9.66
6000	5999.65	6099-65	6199.64	6299.68	6399.63	6499.62	6599.62	6699. 61	6799.61	6899.60
7000	6999. 59	7099.59	7199.58	7299.58	7399.57	7499.56	7599.56	7699.55	7799.55	7899.54
8000	7999.54	8099.53	8199.52	8299.52	8399.51	8499.51	8599.50	8699.50	8799.49	8899.48
9000	8999.48	9099.47	9199.47	9299.46	9899.45	9499.45	9599.44	9699.44	9799.43	9699.43
10000	9999.42	10099.4	10199.4	10299.4	10399.4	10499.4	10599.4	10699.4	10799.4	10899.4
11000	10999.4	11099.4	11199.4	11299.3	11899.8	11499.8	11699.8	11699.3	11799.3	11899.3
12000	11999.3	12099.3	12199.8	12299.8	12399.8	12499.3	12599.3	12699.8	12799.3	12699.2
18000	12999.2	13099.2	18199.2	18299.2	18899.2	18499.2	13599.2	18699.2	18799.2	13899.2
14000	13999.2	14099.2	14199.2	14299.2	14399.2	14499.2	14599.2	14699.1	14799.1	14899.1
15000	14999.1	15099.1	15199.1	15299.1	15899.1	15499.1	15599.1	15699.1	15799.1	15699.1

The following Table of Differences between English and American Feet, for every hundred feet, will make it easy to convert English into American Feet, or American into English Feet, by adding to, or subtracting from, the number of feet to be converted, which is contained in the first column, the numbers found in the other columns.

XIX. DIFFERENCES BETWEEN ENGLISH AND AMERICAN FEET.

To obtain English Feet add. To obtain American Feet subtract.

10000 American Feet = 10000.5808 English Feet.

Number of Feet.			Hundred	١,		Number of Feet.			Hundrede	.	
Thou-	0.	200.	400.	600.	800.	Thou-	0.	200.	400.	600.	800.
	Diff feet	Diff.feet	Diff feet	Diff.foot.	Diff feet		Diff.foot.		DML feet		
0	±0.000	±0.012	±0.023	±0.085	±0.046	15000	±0.870	±0-882	±0.894	±0.905	±0.9 17
1000	0.058	0.070	0.082	0.098	0.105	16000	0.928	0.940	0.952	0.963	0.975
2000	0.116	0.128	0.139	0.151	0.162	17000	0.987	0.998	1.010	1.021	1.033
2000	0.174	0.186	0.197	0.209	0.221	18000	1.045	1.036	1.068	1.079	1.091
4000	0.232	0.244	0.255	0.267	0.279	19000	1.103	1.114	1.126	1.137	1.149
5000	0.290	0.802	0.313	0.825	0.337	20000	1.161	1.172	1.184	1.195	1.207
6000	0.848	0.860	0.371	0.883	0.395	21000	1.219	1.230	1.242	1.253	1.265
7000	0.406	0.418	0.429	0.441	0.453	22000	1.277	1.288	1.300	1.311	1.323
8000	0.464	0.476	0.487	0.499	0.511	28000	1.335	1.346	1.858	1.370	1.331
9000	0.522	0.584	0.546	0.557	0.569	24000	1.898	1.404	1.416	1.428	1.439
10000	0.580	0.592	0.604	0.615	0.627	25000	1.451	1.462	1.474	1.486	1.497
11000	0.688	0.650	0.662	0.673	0.685	26000	1.509	1.520	1.582	1.544	1.553
12000	0.696	0.708	0.720	0.731	0.748	27000	1.567	1.578	1.590	1.602	1.613
13000	0.754	0.766	0.778	0.789	0.801	28000	1.625	1.636	1.648	1.660	1.671
14000	0.812	0.824	0.836	0.847	0.859	29000	1.683	1.694	1.606	1.718	1.729

AMERICAN YARDS AND FEET

INTO DIFFERENT MEASURES OF LENGTH

XT. CONVERSION OF AMERICAN YARDS INTO FRENCH TOISES.

1 American Yard = 0.4691737 Toise.

American Yardı					Hun	ireds.				
Thousands	0.	100.	200.	800.	400.	500.	600.	700.	800.	900.
	Tones.	Loises.	Toises.	Toless.	Tokes	Toises.	Toises	Toises.	Toises.	Colses.
0	0.30	46.92	93.83	140.75	187.67	284.59	281.50	328.42	375.84	423.26
1000	469.17	516.09	563.01	609.98	656.84	708.76	750.68	797.60	844.51	891.48
2000	938.35	985.26	1032-18	1079.10	1126.02	1172.93	1219.85	1266.77	1813.69	1360.60
8000	1407.52	1454.44	1501-36	1548.27	1595.19	1642.11	1689.02	1785.94	1782.86	1829.78
4000	1876.69	1923.61	1970.53	2017.45	2064.86	2111.28	2158.20	2205. 12	2252.03	2298.95
5000	2345.87	2392.79	2439.70	2486.62	2583.54	2580.45	2627.87	2 674.29	2721.21	2768.12
6000	2815.04	2861.96	2908.88	2955.79	8002.71	8049.68	8096.55	3143.46	3190.38	8287.80
7000			1	3424.97						
8000	3753.39	8800.81	3847.22	3894.14	8941.06	3987.98	4034.89	4081.81	4128.78	4175.65
9000	4222.56									

XXI. CONVERSION OF AMERICAN YARDS INTO METRES.

1 American Yard = 0.91448655 Metre.

American Yards,				•	Hun	dreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres	Metres.	Metres.	Metres.	Metrus.	Metres.	Metres.	Metres.
0	0.00	91.44	182.89	274.38	365.77	457.22	548.66	640.11	781.55	822.99
1000	914.44	1005.88	1097.32	1188.77	1280.21	1371.65	1468.10	1554.54	1645.99	1737.48
2000	1828.87	1920.32	2011.76	2103.20	2194.65	2286.09	2377.54	2468.98	2560.42	2651.87
3000	2743.81	2834.75	2926.20	8017.64	3109.08	3200.53	3291.97	8883.42	3474.86	3566.80
4000	3657.75	3749.19	3840.63	3932.08	4023.52	4114.96	4206.41	4297.85	4389.30	4480.74
5000	4572.18	4663.63	4755.07	4846.51	4937.96	5029.40	5120.84	5212.29	5803.78	5895.18
6000	5486.62	5578.06	5669.51	5760.95	5852.89	5943.84	6035.28	6126.72	6213.17	6309.61
7000	6401.06	6492.50	6583.94	6675.89	6766.83	6858.27	6949.72	7041.16	7132.61	7224.05
8000	7315.49	7406.94	7498.88	7589.82	7681.27	7772.71	7864.15	7955.60	8047.04	8138.49
9000	8229 93	8321.87	8412.82	8504.26	8595.70	8687.15	8778.59	8870.03	8961.48	9052.92

XXII. CONVERSION OF AMERICAN PEET INTO METRES.

1 American Foot = 0.30481218 Metre.

Amer. Foot.					Hund	reds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Motres.	Metres.	Metres.	Metres.	Metres.	Metres.	Motres.	Motres.	Metres.	Motres.
0	0.00	30.48	60.96	91.44	121.92	152.41	182.89	218.37	l	
1000	804.81	885.29	865.77	896.26				i .	i	579.14
2000	609.62	640.11		701.07		762.08	792.51			
8000	914.44	944.92	975.40	1	1026.86				1158.29	
4000	1219.25	1249.78	1 2 80.21	1310.69	1841.17	1871.65	1402.14	1432.62	1463.10	1493.5
5000					1645.99				1767.91	
6000	1828.87	1859.85	1889.84	1910.82	1940.80	1971.28	2001.76	2032.24	2062.72	2093.2
7000	2123.69	2154.17	2184.63	2225.13	2255.61	2286.09	2816.57	2847.05	2377.54	2408.0
8000	2438.50	2468.98	2499.46	2529.94	2560.42	2590.90	2621.38	2651.87	2682.35	2712.8
9000	2743.81	2773.79	2804.27	2884.75	2865.23	2 895.72	2 926. 2 0	2956.68	2987.16	3017.6
10000	8048.12	3078.60	3109.06	2189.57	8170.05	8200.58	328 1.01	3261.49	329 1.97	3822.4
11000	11		1	l .	8474.86		8585.82	8566.80	8596.78	3627.2
12000	11	ì	1	1	3779.67		8840.68	3871.11	8901.60	3932.0
13000	11			4054.00			4145.45	4175.93	4206.41	4236.89
14000	H	1	1	1	4389.30	4419.78	4450.26	4480.74	4511.22	4541.70
15000	4572.18	4602.66	4633.15	4662.68	4694.11	4724.59	4755.07	4785.55	4816.08	4846.5
16000	H	l .	I	i	1998.92			1	5120.84	ı
17000					5308.78			ı	5425.66	
18000	11	1	1	ŀ	5608.54			ı	5780.47	
19000				5882. 88				1	6035.2 8	
20000	6096.24	6126.72	6157.21	6187.69	6218.17	6248.65	6279.13	6809.61	6340.09	6370.5
21000	8401.06	6481.54	6462.02	6492.50	6522.98	6553.46	6583.94	6614.42	6644.91	6675.3
22000					6827.79				6949.72	
28000	11	1	!	1	7182.61		1	ŀ	7254.53	
24000				i e	7487.42		1	1	7559.84	
25000	7620.80	7850.79	7681.27	7711.75	7742.28	7772.71	7808.19	7833.67	7864.15	7894.6
26000					8047.04					
27000	11	1	I		8351.85				8473.78	
28000					8656.67					
					Un	ite.				
Tens.	G.	1.	9.	2.	4.	5.	6.	7.	8.	9.
					Motres.		Motres.	Metres.	Metres.	Metres.
0	Metres. 0.0000	Metres. 0.3048	Metres. 0.6096	Motres. 0.9144	1.2192	Motres. 1.5241	1.8289			
10	3.0481	3.8529	8.6577	3.9626	4.2674	4.5722	4.8770		1	5.7914
					7.8155					1
20 80	0.0802	0.4011	0.7008	10.0589	10.8686	10.688	10.9789	11,2781	11,5820	
40	12.1925	12.4978	12.8021	18.1069	13.4117	18.7165	14.0214	14.8262	14.6810	14.9358
**	li i		1		16.4599		l	į		l
50	10.2400	10 500	10.0002	10 1000	19.4080	10.7047	90 0170	20.2994	20.6979	20.9320
	110.2007	10.0999	19.0804	15.1052	12.4000	10.1120	50.0110	20.0254	20.3212	
60	01 0000	01 544-	01 0 40-	80 0010	00 550*	00 0000	OO TOES	99 /905	99 7754	ومعميوا
70 80	21.2869	21.5417	21.8465	22.2513	22.5561 25.6042	22.8609	28.1657	28.4705	28.7754	24.0802

XXIII. CONVERSION OF AMERICAN FEET INTO PARIS OR FRENCH FEET.

1 American Foot = 0.98834787 Paris Foot.

Amer. Feet.					Hun	dreds.				
Thousands.	0.	100.	900.	300.	400.	500.	600.	700.	800.	900.
	Par.Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par.Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.
0	0.0	98.8	187.7	281.5	875.3	469.2	563.0	656.8	750.7	844.5
1000	938.3	1032.2	1126.0	1219.9	1313.7	1407.5	1501.4	1595.2	1689.0	1782.9
2000	1876.7	1970.5	l	1	2252.0	2345.9	2439.7	2533.5	2627.4	2721.2
3000	2815.0				8190.4	3284.2	8378.1		8365.7	
4000	3758.4	8847.2	8941.1	4034.9	4128.7	4222.6	4816.4	4410.2	4504.1	4597.9
5000 .	4691.7	4785.6					5254.7	5348.6		1
6000	5630.1	5723.9	5817.8			6099.3	6198.1	6286.9		1
7000	6568.4			1			7131.4			
8000	7506.8	7600.6	7694.4	7788.8	7882.1	7976.0	8069.8	8163.6	8257.5	8351.8
9000	8445.1	8539.0	8632.8	8726.6	8820.5	8914.8	9008.1	9102.0	9195.8	9289.6
10000	9383.5	9477.8	9571.1	9665.0	9758.8	9852.6	9946.5	10040.8	10184.2	10228.0
11000	10321.8	10415.7	10509.5	10603.3	10697.2	10791.0	10884.8	10978.7	11072.5	11166.3
12000	11260.2	11854.0	11447.8	11541.7	11635.5	11729.3	11823.2	11917.0	12010.8	12104.7
13000	12198.5	12292.3	12386.2	12480.0	12573.9	12667.7	12761.5	12855.4	12949.2	13048.0
14000	13136.9	18280.7	18824.5	18418.4	13512.2	18606.0	18699.9	18793.7	18887.5	13981.4
15000	14075.2	14169.0	14262.9	14856.7	14450.5	14544.4	14688.2	14782.1	14825.9	14919.7
16000	15013.6	15107.4	15201.2	15295.1	15388.9	15482.7	15576.6	15670.4	15764.2	15858.1
17000	15951.9	16045.7	16139.6	16283.4	16327.2	16421.1	16514.9	16608.7	16702.6	16796.4
18000	16890.8	16984.1	17077.9	17171.8	17265.6	17359.4	17453.3	17547.1	17640.9	17784.8
19000	17828.6	17922.4	18016.3	18110.1	18203.9	18297.8	18391.6	18485.4	18579.8	18673.1
20000	18766.9	18860.8	18954.6	19048.4	19142.8	19286.1	19380.0	19423.8	19517.6	19611.5
21000	19705.8	19799.1	19893.0	19986.8	20080.6	20174.5	20268.8	20362.1	20456.0	20549.8
22000	20643.6	20787.5	20831.8	20925.1	21019.0	21112.8	21206.6	21300.5	21394.3	21488.2
23000	21582.0	21675.8	21769.7	21863.5	21957.8	22051.2	22145.0	22238.8	22832.7	22426.5
24000	22520.3	22 614.2	22708.0	22801.8	22895.7	2 2 989.5	28083.8	23177.2	23271.0	23364.8
25000	23458.7	23552.5	23646.4	28740.2	28884.0	23927.9	24021.7	24115.5	24209.4	24308.2
26000	24397.0	24490.9	24584.7	24678.5	24772.4	24866.2	24960.0	2505 3.9	25147.7	25241.5
27000						25804.5				
28000	26278.7	26367.6	26461.4	26555.2	26649.1	26742.9	26836.7	26930.6	27024.4	27118.2
					Un	its.				
Tons.	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.
	Par.Feet	Par Foot	Par Foot	Par Foot	Par Fast	Par. Foot.	Par Fant	Par Feet	Par Feet	Par.Foot
o	0.00	0.94	1.88	2.82	8.75	4.69	5.68	6.57	7.51	8.45
10	9.38	10.32	11.26	12.20	13.14	14.08	15.01	15.95	16.89	17.83
20	18.77	19.71	20.64	21.58	22.52	28.46	24.40	25.84	26.27	27.21
30	28.15	29.09	30.03	30.97	81.90	82.84	88.78	34.72	35.66	86.60
40	37.58	88.47	89.41	40.85	41.29	42.23	43.16	44.10	45.04	45.98
50	46.92	47.86	48.79	49.78	50.67	51.61	52.55	58.49	54.42	55.36
60	56.30	57.24	58.18	59.12	60.05	60.99	61.98	62.87	68.81	64.75
70	65.68	66.62	67.56	68.50	69.44	70.88	71.81	72.25	78.19	74.18
80	75.07	76.01	76.94	77.88	78.82	79.76	80.70	81.64	82.57	83.51
90	84.45	85.89	86.33	87.27	88.20	89.14	90.08	91.02	91.96	92.90

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KLAFTER AND FEET OF VIENNA

INTO DIFFERENT MEASURES OF LENGTH.

1 KLAFTER OF VIENNA = 6 FEET OF VIENNA = 0.9780317 Tolse DU PÉROU.

From this value are derived the equations used in computing the following tables.

XXIV. CONVERSION OF KLAFTER OF VIENNA INTO FRENCH TOISES.

1 Klafter = 0.9780817 Toles.

Kiafter of Vienna.					Hund	ireds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	200.
	Toises.	Toises.	Tolses.	Tolses.	Toises.	Tolses.	Tolses.	Toises	Toises.	Toires.
0	0.00	97.80	194.61	291.91	889.21	486.52	583.82	681.12	778.43	875.7
1000	973.03	1070.83	1167.64	1264.94	1362.24	1459.55	1556.85	1654.15	1751.46	1848.7
2000	1946.06	2043.87	2140.67	2287.97	2385.28	2432.58	2529.88	2627.19	2721.49	2621.7
8000	2919.10	3016.40	3113.70	8211.00	8306.31	3403.61	3502.91	8600.22	8697.52	3794.8
4000	8392.13	8999.48	1086.78	4184.04	4281.84	4378.64	1475.95	4578.25	4670.55	4767.8
5000	4865.16	1962.46	5059.76	5157.07	5254.87	5851.67	5448.96	5 546.2 8	5643.58	5749. 8
Klafter.					Un	its.				
Tens.	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.
	Toises.	Tolees.	Toises.	Toises.	Tolses.	Toises.	Toises.	Toises.	Tokes.	Toises
0	0.000	0.978	1.946	2.919	2.892	4.865	5.838	6.811	7.784	8.757
10	9.730	10.703	11.676	12.649	13.622	14.595	15.569	16.542	17.515	18.488
20	19.461	20.434	21.407	22.880	23.358	24.826	25.299	26.272	27.245	28-218
80	29.191	80.164	81.137	82.110	88.088	84.036	35.029	86.002	\$6.975	37.948
40	38.921	39.894	40.867	41.840	42.818	43.786	44.759	45.782	46.706	47.679
50	48.652	49.625	50.598	51.571	52.544	58.517	54.490	55.468	56.436	57.409
60	58.382	59.855	60.828	61.801	62.274	63.247	64.220	65.198	66.166	67.139
70	68.112	69.085	70.058	71.031	72.004	72.977	73.950	74.928	75.896	76.870
80		mo 010	79.789	80.762	81.735	82,708	88.681	84.654	85.627	86.600
	77.843	78.816	13.103	OV. (OZ	01.190	02.100	00.001	04.004	03.04/	00.000

EXV. CONVERSION OF KLAFTER OF VIENNA INTO METRES.

1 Kinfter = 1.8964741 Metres.

Klafter of	li				Hunc	ireds.				
Vienna. Thousands.	0.	100.	200.	800.	400.	500.	600.	700.	800.	900.
	Metres.	Motres.	Motres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres
0	0.00	189.65	879.29	568.94	758.59	948.24	1137.88	1327.58	1517.18	1706.8
1000	1896.47	2086.12	2275.77	2465.42	2655.06	2844.71	3034.36	8224.01	3418.65	3603.8
2000	8792.95	3982.60	4172.24	4361.89	4551.54	4741.19	4930.88	5120.48	5310.13	5499.7
3000	5689.42	3879.07	6068.72	6258.36	6448.01	6637.66	6827.81	7016.95	7206.60	7396.2
4000	7585.90	7775.54	7965.19	8154.84	8344.49	8584.13	8 723.7 8	8913.43	9103.08	9292.7
Klafter.					Un	its.				
Tens.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metre
0	0.000	1.896	3.793	5.689	7.586	9.482	11.879	18.275	1	17.06
10	18.965	20.861	22.758	24.654	26.551	28.447	80.344	82.240		36.03
20	87.929	39.826	41.722	43.619	45.515	47.412		51.205		54.99 78.96
80	56.894	58.791	60.687	62.584	64.480	66.877		70.170		
40	75.859	77.755	79.632	81.548	83.445	85.841	87.288	89.184	91.081	92.92
50	94.824	96.720	98.617	100.518	102.409	104.806	106.203	108.099	109.995	111.89
60	113.788	115.685	117.581	119.478	121.874	123.271	125.167	127.064	128.960	130.85
70	182.753	134.650	136.546	138.443	140.889	142.286	144.182	146.029	147.925	149.82
80	151.718	158.614	155.511	157.407	159.804	161.200	163.097	164.993	166.890	168.78
90	170.683	172.579	174.476	176.372	178.269	180.165	182.062	183.938	185.854	187.75
	•		1 Klafter	= 5.82811						
Kiafter of						ireds.	001.			
Klafter of Vienna. Thousands.	0.	100.	200.	300.			600.	700.	800.	900
Vienna.	<u> </u>		200.	300.	Hune 400.	500.				
Vienna.	Par. Feet.	Par.Feet.		300. Par. Feet.	Hund 400.	500.	600.	Par.Feet.	Par. Feet.	Par.Fee
Vienna. Thousands.	Par. Feet.	Par.Feet. 583-82	Par.Feet.	300. Par. Foot. 1751.46	400. Pur.Feet. 2335.28	500. Par.Feet. 2919.10	600.	Par. Feet. 4086.73	Par. Feet. 4670.55	Par.Fee 5254.3
Vienna. Thousands.	Par.Feet. 0.00 5889.19	Par.Feet. 583.82 6422.01	Par.Feet. 1167.64	300. Par. Feet. 1731.46 7589.65	Hune 400. Par.Feet. 2335.28 8173.47	500. Par.Feet. 2919.10 8757.29	600. Par.Feet. 8502.91	Par.Feet. 4086.73 9924.92	Par.Feet. 4670.55 10508.7	Par.Fee 5254.3 11092.
Vienna. Thousands. 0 1000 2000 8000	Par.Feet 0.00 5889.19 11676.4 17514.6	Par.Feet. 583.82 6422.01 12260.2 18098.4	Par.Feet. 1167.64 7003.88 12844.0 18682.2	300. Par. Feet. 1731.46 7589.65 18427.8 19266.0	Hund 400. Par.Feet. 2335.28 8173.47 14011.7 19649.8	500. Par.Feet. 2919.10 8757.29 14595.5 20488.7	600. Par.Foot. 8502.91 9341.10 15179.3 21017.5	Par.Feet. 4086.73 9924.92 15768.1 21601.8	Par. Feet. 4670.55 10508.7 16346.9 22185.1	Par.Fee 5254.3 11092. 16930. 22768.
Vienna. Thousands. 0 1000 2000	Par.Feet 0.00 5889.19 11676.4 17514.6	Par.Feet. 583.82 6422.01 12260.2 18098.4	Par.Feet. 1167.64 7003.88 12844.0 18682.2	300. Par. Feet. 1731.46 7589.65 18427.8 19266.0	Hund 400. Par.Feet. 2335.28 8173.47 14011.7 19649.8	500. Par.Feet. 2919.10 8757.29 14595.5	600. Par.Foot. 8502.91 9341.10 15179.3 21017.5	Par.Feet. 4086.73 9924.92 15768.1 21601.8	Par. Feet. 4670.55 10508.7 16346.9 22185.1	Par.Fee 5254.3 11092. 16930. 22768.
Vienna. Thousands. 0 1000 2000 3000 4000	Par.Feet 0.00 5889.19 11676.4 17514.6	Par.Feet. 583.82 6422.01 12260.2 18098.4	Par.Feet. 1167.64 7003.88 12844.0 18682.2	300. Par. Feet. 1731.46 7589.65 18427.8 19266.0	Hund 400. Par.Feet. 2335.28 8173.47 14011.7 19649.8	Far.Feet. 2919.10 8757.29 14595.5 20488.7 26271.9	600. Par.Foot. 8502.91 9341.10 15179.3 21017.5	Par.Feet. 4086.73 9924.92 15768.1 21601.8	Par. Feet. 4670.55 10508.7 16346.9 22185.1	Par.Fee 5254.3 11092. 16930. 22768.
Vienna. Thousands. 0 1000 2000 8000	Par.Feet 0.00 5889.19 11676.4 17514.6	Par.Feet. 583.82 6422.01 12260.2 18098.4	Par.Feet. 1167.64 7003.88 12844.0 18682.2	300. Par. Feet. 1731.46 7589.65 18427.8 19266.0	Hund 400. Par.Feet. 2335.28 8173.47 14011.7 19849.8 23688.0	Far.Feet. 2919.10 8757.29 14595.5 20488.7 26271.9	600. Par.Foot. 8502.91 9341.10 15179.3 21017.5	Par.Feet. 4086.73 9924.92 15768.1 21601.8	Par. Feet. 4670.55 10508.7 16346.9 22185.1	Par.Fee 5254.3 11092. 16930. 22768.
Vienna. Thousands. 0 1000 2000 3000 4000 Klafter.	Par.Feet.	Par.Feet. 583-82 6422.01 12260.2 18098.4 23936.6	Par.Feet. 1167.64 7005.88 12844.0 18682.2 24520.4	300. Par. Feet. 1751.46 7589.65 18427.8 19266.0 25104.2	Hune 400. Par.Feet. 2335.28 8173.47 14011.7 19849.8 23658.0	500. Par. Feet. 2919-10 8757-29 14595-5 20488-7 26271-9	600. Par.Feet. 8502.91 9341.10 15179.3 21017.5 26855.7	Par.Feet. 4086.73 9924.92 15768.1 21601.3 27489.5	Par.Feet. 4670.55 10508.7 16346.9 22185.1 28023.8	Par.Fee 5254.3 11092. 16930. 22768. 28607.
Vienna. Thousands. 0 1000 2000 3000 4000 Klafter.	Par.Feet. 0.00 5889.19 11676.4 17514.6 23352.8	Par.Feet. 583-82 6422.01 12260.2 18098.4 23936.6	Par.Feet. 1167.64 7005.88 12844.0 18682.2 24520.4	300. Par. Feet. 1751.46 7589.65 18427.8 19266.0 25104.2	Hune 400. Par.Feet. 2335.28 8173.47 14011.7 19849.8 23688.0 Un	500. Par.Feet. 2919:10 8757.29 14595.5 20488.7 26271.9	600. Par.Feet. 8502.91 9341.10 15179.3 21017.5 26855.7	Par.Feet. 4086.73 9924.92 15768.1 21601.3 27489.5	Par.Feet. 4670.55 10508.7 16346.9 22185.1 28023.8	Par.Fee 5254.3 11092. 16930. 22768. 28607.
Vienna. Thousands. 0 1000 2000 8000 4000 Klafter. Tens.	Par.Feet.	Par.Foet. 583-82 6422-01 12260-2 18098-4 23936-6	Par.Feet. 1167.64 7005.88 12844.0 18682.2 24520.4	300. Par. Feet. 1751.46 7589.65 18427.8 19266.0 25104.2	Hune 400. Par.Feet. 2335.28 8173.47 14011.7 19849.8 25658.0 Un 4.	Far.Feet. 500. Par.Feet. 2919:10 8757:29 14595.5 20488:7 26271.9	600. Par.Feet. 8502.91 9341.10 15179.3 21017.5 26855.7	Par.Feet. 4086.73 9924.92 15768.1 21601.3 27439.5	Par.Feet. 4670.55 10508.7 16846.9 22185.1 28023.8 Par.Feet.	Par.Fee 52.54.3 11092. 16930. 22768. 28607. Par.Fee 52.5
Vienna. Thousands. 0 1000 2000 8000 4000 Klafter. Tens.	Par. Feet. 0.00 5889.19 11676.4 17514.6 23352.8 Par. Feet. 0.00 58.38	Par.Feet. 583-82 6422-01 12260-2 18098-4 28936-6 1. Par.Feet. 5.84 64-22	Par.Feet. 1167-64 7003-83 12844-0 18682-2 24520-4 2. Par.Feet. 11.68 70.06	300. Par. Feet. 1751.46 7589.65 18427.8 19266.0 25104.2 8. Par. Feet. 17.51	Hund 400. Par. Feet. 2335, 28 8173.47 14011.7 19649.8 25658.0 Un 4. Par. Feet. 23.85 81.73	Far.Feet. 2919.10 8757.29 14595.5 20488.7 26271.9 its. 5. Par.Feet. 29.19 87.57	GOO. Par.Feet. 8502.91 9341.10 15179.3 21017.5 26855.7	Par.Feet. 4086.73 9924.92 15768.1 21601.3 27439.5 7. Par.Feet. 40.87 99.25	Par.Feet. 4670.55 10508.7 16346.9 22185.1 28023.8 S. Par.Feet. 46.71 105.09	Par.Fee 5254.3 11092.16930. 22768. 28607. Par.Fee 52.5 110.9
Vienna. Thousands. 0 1000 2000 8000 4000 Klafter. Tens.	Par. Feet. 0.00 5889.19 11676.4 17514.6 23352.8 Par. Feet. 0.00 58.38	Par. Feet. 583-82 6422-01 12260-2 18098-4 28936-6 1. Par. Feet. 5.84 64.22 122-60	Par.Feet. 1167.64 7003.88 12844.0 18682.2 24520.4 2. Par.Feet. 11.68 70.06 128.44	300. Par. Foet. 1751.46 7589.65 18427.8 19266.0 25104.2 3. Par. Feet. 17.51 75.90	Hund 400. Par. Feet. 2335, 28 8173.47 14011.7 19649.8 25658.0 Un 4. Par. Feet. 23.85 81.73	Far.Feet. 2919.10 8757.29 14595.5 20488.7 26271.9 its. 5. Par.Feet. 29.19 87.57	600. Par.Feet. 8502.91 9341.10 15179.3 21017.5 26855.7 6. Par.Feet. 25.03 98.41 151.79	Par.Feet. 4086.73 9924.92 15768.1 21601.3 27439.5 7. Par.Feet. 40.87 99.25	Par. Feet. 4670.55 10508.7 16346.9 22185.1 28023.8 S. Par. Feet. 46.71 105.09 163.47	Par.Fee 5254.3 11092.16930. 22768. 28607. Par.Fee 52.5. 110.9. 169.3
Vienna. Thousands. 0 1000 2000 8000 4000 Klafter. Tens.	Par. Feet. 0.00 5889.19 11676.4 17514.6 23852.8 0. Par. Feet. 0.00 58.38 116.76	Par. Feet. 583-82 6422-01 12260-2 18098-4 28936-6 1. Par. Feet. 5.84 64.22 122-60	Par.Feet. 1167.64 7003.83 12844.0 18682.2 24520.4 2. Par.Feet. 11.68 70.06 128.44	300. Par. Foet. 1751.46 7589.65 18427.8 19266.0 25104.2 3. Par. Feet. 17.51 75.90 184.28	Hund 400. Par. Feet. 2335, 28 8173.47 14011.7 19649.8 25658.0 Un 4. Par. Feet. 23.85 81.73 140.12	500. Par.Feet. 2919.10 8757.29 14595.5 20488.7 26271.9 its. 5. Par.Feet. 29.19 87.57	600. Par.Feet. 8502.91 9341.10 15179.3 21017.5 26855.7 6. Par.Feet. 25.03 98.41 151.79	Par. Feet. 1086.73 9924.92 15768.1 21601.3 27439.5 7. Par. Feet. 40.87 99.25 157.63	Par. Feet. 4670.55 10508.7 16346.9 22185.1 28023.8 S. Par. Feet. 46.71 105.09 163.47	Par.Fee 5254.3 11092. 16930. 22768. 28607. Par.Fee 52.5 110.9 169.3 227.6
Vienna. Thousands. 0 1000 2000 3000 4000 Klafter. Tens. 0 10 20 30 40	Par. Feet. 0.00 5889.19 11676.4 17514.6 23852.8 0. Par. Feet. 0.00 58.38 116.76 175.15 238.53	Par. Feet. 583-82 6422-01 12260-2 18098-4 28936-6 1. Par. Feet. 5.84 64.22 122.60 180.98 239.37	Par.Feet. 1167.64 7003.83 12844.0 18682.2 24520.4 2. Par.Feet. 11.68 70.06 128.44 186.82 245.20	300. Par. Feet. 1751.46 7589.65 18427.8 19266.0 25104.2 Par. Feet. 17.51 75.90 184.28 192.66 251.04	Hune 400. Par.Feet. 2335.28 8173.47 14011.7 19849.8 23688.0 Un 4. Par.Feet. 23.85 81.73 140.12 198.50 256.88	500. Par.Feet. 2919.10 8757.29 14595.5 20483.7 26271.9 its. 5. Par.Feet. 29.19 87.57 145.95 204.84 262.72	600. Par.Feet. 8502.91 9341.10 15179.3 21017.5 26855.7 6. Par.Feet. 85.03 98.41 151.79 210.17 268.56	Par. Feet. 4086.73 9924.92 15768.1 21601.3 27439.5 Par. Feet. 40.87 99.25 157.63 216.01 274.39	Par. Feet. 4670.55 10508.7 16346.9 22185.1 28023.8 S. Par. Feet. 46.71 105.09 163.47 221.85 280.23	Par. Fee 5254.3 11092. 16930. 22768. 228607. Par. Fee 52.5 110.9 169.3 227.6 286.0
Vienna. Thousands. 0 1000 2000 3000 4000 Klafter. Tens. 0 10 20 30 40 50	Par. Feet. 0.00 5889.19 11676.4 17514.6 23852.8 0. Par. Feet. 0.00 58.38 116.76 175.15 238.53	Par. Feet. 583-82 6422-01 12260-2 18098-4 28936-6 1. Par. Feet. 5.84 64.22 122-60 180-98 239-37	Par.Feet. 1167.64 7003.83 12844.0 18682.2 24520.4 2. Par.Feet. 11.68 70.06 128.44 186.82 245.20 803.59	300. Par. Feet. 1751.46 7589.65 18427.8 19266.0 25104.2 Par. Feet. 17.51 75.90 184.28 192.66 251.04 809.42	Hune 400. Par.Feet. 2335.28 8173.47 14011.7 19849.8 23688.0 Un 4. Par.Feet. 23.85 81.73 140.12 198.50 256.88 815.26	500. Par.Feet. 2919.10 8757.29 14595.5 20483.7 26271.9 itia. 5. Par.Feet. 29.19 87.57 145.95 204.84 262.72	600. Par.Feet. 8502.91 9341.10 15179.3 21017.5 26855.7 6. Par.Feet. 85.03 93.41 151.79 210.17 268.56	Par. Feet. 4086.73 9924.92 15768.1 21601.3 27439.5 Par. Feet. 40.87 99.25 157.63 216.01 274.39	Par. Feet. 4670.55 10508.7 16346.9 22185.1 28023.8 S. Par. Feet. 46.71 105.09 163.47 221.85 280.23 338.62	Par. Fee 5254.3 11092. 16930. 22768. 228607. Par. Fee 52.5 110.9 169.3 227.6 286.0
Vienna. Thousands. 0 1000 2000 3000 4000 Klafter. Tens. 0 10 20 30 40 50 60	Par. Feet. 0.00 5889.19 11676.4 17514.6 23352.8 Par. Feet. 0.00 58.38 116.76 175.15 233.53	Par. Feet. 583-82 6422-01 12260-2 18098-4 28936-6 1. Par. Feet. 5.84 64.22 122-60 180-98 239-37 297.75 856-13	Par.Feet. 1167.64 7003.83 12844.0 18682.2 24520.4 2. Par.Feet. 11.68 70.06 128.44 186.82 245.20 803.59 361.97	300. Par. Feet. 1751.46 7589.65 18427.8 19266.0 25104.2 Par. Feet. 17.51 75.90 184.28 192.66 251.04 809.42 867.81	Hune 400. Par.Feet. 2335.28 8173.47 14011.7 19849.8 23658.0 Un 4. Par.Feet. 23.85 81.73 140.12 198.50 256.88 815.26 278.64	500. Par.Feet. 2919.10 8757.29 14595.5 20483.7 26271.9 its. 5. Par.Feet. 29.19 87.57 145.95 204.84 262.72 821.10 379.48	600. Par.Feet. 8502.91 9341.10 15179.3 21017.5 26855.7 6. Par.Feet. 85.03 93.41 151.79 210.17 268.56 826.94 385.32	Par. Feet. 4086.73 9924.92 15768.1 21601.3 27439.5 7. Par. Feet. 40.87 99.25 157.63 216.01 274.39 882.78	Par. Feet. 4670.55 10508.7 16346.9 22185.1 28023.8 S. Par. Feet. 46.71 105.09 163.47 221.85 280.23 338.62 397.00	Par. Fee 52.5. 110.9. 169.3 227.68. 28607. Par. Fee 52.5. 110.9. 169.3 227.6. 286.0 344.4 402.8
Vienna. Thousands. 0 1000 2000 3000 4000 Klafter. Tens. 0 10 20 30 40 50	Par. Feet. 0.00 5889.19 11676.4 17514.6 23852.8 0. Par. Feet. 0.00 58.38 116.76 175.15 238.53	Par. Feet. 583-82 6422-01 12260-2 18098-4 28936-6 1. Par. Feet. 5.84 64.22 122-60 180-98 239-37 297.75 856-13	Par.Feet. 1167.64 7003.83 12844.0 18682.2 24520.4 2. Par.Feet. 11.68 70.06 128.44 186.82 245.20 803.59 420.35	300. Par. Feet. 1751.46 7589.65 18427.8 19266.0 25104.2 Par. Feet. 17.51 75.90 184.28 192.66 251.04 809.42	Hune 400. Par.Feet. 2335.28 8173.47 14011.7 19649.8 23658.0 Un 4. Par.Feet. 23.85 81.73 140.12 198.50 256.88 815.26 278.64 432.03	500. Par.Feet. 2919.10 8757.29 14595.5 20483.7 26271.9 itia. 5. Par.Feet. 29.19 87.57 145.95 204.84 262.72	600. Par.Feet. 8502.91 9341.10 15179.3 21017.5 26855.7 6. Par.Feet. 85.03 93.41 151.79 210.17 268.56	Par. Feet. 4086.73 9924.92 15768.1 21601.3 27439.5 Par. Feet. 40.87 99.25 157.63 216.01 274.39	Par.Feet. 4670.55 10508.7 16346.9 22185.1 28023.3 S. Par.Feet. 46.71 105.09 163.47 221.85 280.23 338.62 397.00 455.88	5254.3 11092. 16930. 22768. 28607. Par.Fee 52.5. 110.9: 169.3 227.6: 286.0 344.4 402.8

XXVII. CONVERSION OF KLAFTER OF VIENNA INTO ENGLISH FEET.

1 Klafter = 6.2221408 English Feet.

Klafter of					Hund	ireds.				
Vienna. Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	1		, •	_	Eng. feet.	-		. •	_	, -
0	li			t	2488.86					
1000	6222.14	6844.85	7466.57	8088.78	8711.00	9333.21	9955.42	10577.6	11199.9	11822.1
2000	12444.3	13066.5	13688.7	14310.9	14933.1	15555.4	16177.6	16 79 9-8	17422.0	18044.2
3000	18666.4	19288.6	19910.8	20583.1	21155.8	21777.5	22399.7	23021.9	23644.1	2 1266.3
4000	24888.6	25510.8	26133.0	26755.2	27877.4	27999.6	28621.8	29244.1	29 866.3	30488.3
Klafter.					Un	its.				
Tens.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet,	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.
0	0.00	6.22	12.44	18.67	24.89	81.11	37.33	43.55	49.78	56.00
10	62.22	68.44	74.67	80.89	87.11	93.33	99.55	105.78	112.00	118.22
20	124.44	130.66	136.89	148.11	149.33	155.55	161.78	168.00	174.22	180.44
80	186.66	192.89	199.11	205.83	211.55	217.77	224.00	230.22	236.44	242.66
40	248.59	235.11	261.33	267.55	273.77	280.00	286.22	292.44	298.66	304-88
50	311.11	317.33	323.55	329.77	336.00	842.22	348.44	854.66	360.88	367.11
60	373.33	379.55	385.77	391.99	398.22	404.44	410.66	416.88	423.11	429.33
	11		447.99	454.22	460.44	466.66	472.88	479.10	485.33	491.55
70	435.55	441.77	447.99	101.22						
70 80	435.55 497.77	441.77 503.99	510.22	516.44	522.66	528.88	535.10	541.33	547.55	553.77

XXVIII. CONVERSION OF FEET OF VIENNA INTO METRES.

1 Foot of Vienna = 0.8160790 Metre.

Feet of					Hune	ireds.				
Vienus. Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Motres.	Metres.
0	0.00	81.61	63.22	94.82	126.43	158.04	189.65	221.26	252.86	284.4
1000	816.08	847.69	879.29	410.90	442.51	474-12	505.78	537.33	568.94	600-5
2000	632.16	663.77	695.37	726.9 8	758.59	790.20	821.81	853.41	885.02	916.6
3000	948.24	979.84	1011.45	1043.06	1074.67	1106.28	1137.88	1169.49	1201.10	1232.7
4000	1264.32	1295.92	1827.53	1359.14	1890.75	142 2.3 6	1458.96	1485.57	1517.18	1548.7
5000	1580.40	1 612.0 0	1643.61	1675.22	1706.83	1788.43	1770.04	1801.65	18 33.2 6	1864.8
6000	1896.47	1928.08	1959.69	1991.30	2022.91	2054.51	2086.12	2117.73	2149.34	2160.9
7000	2212.55	2244.16	2275.77	2807.88	2338.98	2370.59	2402.20	2483.81	2465.42	2497.0
8000	2529.63	2560.24	2591.85	2623.46	2653.06	2686.67	2718.28	2749.89	2781.50	2813.1
9000	2844.71	2876. 8 2	290 7.9 3	2989.53	2971.14	3002.75	3084.86	3065.97	8097.57	3129.1
10000	3160.79	8192.40	8224.01	3255.61	3287.02	8818.83	8850.44	3882.05	3418.65	3445.2
11000	8 176.87	3508.48	3540.08	3571.69	3608.30	8684.91	3666.52	3698.12	3729.73	8761-3
12000	3792.95	8824.56	8856.16	8887.77	3919.38	8950.99	8982.60	4014.20	4045.81	4077.4
18000	4109.03	4140.64	4172.24	4203.85	4285.46	4267.07	4298.67	4830.28	4361.89	4393.5
14000	4425.11	4456.71	4488.32	4519.93	4551.54	4583.15	4614.75	4646.34	4677.97	4709.5
15000	4741.19	4772.79	4804.40	4886.01	4867.62	4899.22	4920.88	4962.44	4994.05	5025.6

XIX. CONVERSION OF FEET OF VIENNA INTO PARIS OR FRENCH FEET AND DECIMALS.

1 Foot of Vienna = 0.9730317 Paris Foot.

Foot of					Hund	reds.				
Vienna. Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Par. feet.	Par. feet.	Par. feet.	Par. feet.	Par. feet.	Par. feet.	Par. feet.	Par. feet.	Par. feet.	Par. feet.
0	0.0	97.80	19,46	29.19	88.92	48.65	58.38	68.11	77.84	87.57
1000	973.0	1070.8	1167.6	1264.9	1862.2	1459.5	1556.9	1654.2	1251.5	1848.8
2000	1946.1	2043.4	2140.7	3288.0	2885.8	2482.6	2530.0	2627.2	2724 5	2821.8
3000	2919.1	3016.4	8113.7	3211.0	8308.3	8405.6	8502.9	8600.2	8697.5	3794.8
4000	8892.1	3989.4	4086.7	4184.0	4281.3	4378.6	4475.9	4578.2	4670.6	4767.9
5000	4865.2	4962.5	5059.8	5157.1	5254.4	5851.7	5449.0	5546.8	5643.6	5740.9
6000	5838.2	5935.5	6032.8	6130.1	6227-4	6324.7	6422.0	6519.3	6616.6	6713.9
7000	6811.2	6908.5	7005.8	7103.1	7200.4	7297.7	7395.0	7492.3	7589.6	7687.0
8000	7784.3	7881.6	7978.9	8076.2	8178.5	8270.8	8368.1	8465.4	8562.7	8660.0
9000	8757.8	8854.6	8951.9	9049.2	9146.5	9243.8	9841.1	9438.4	9535.7	9633.0
10000	9730.8	9827.6	9924.9	10022.2	10119.5	10216.8	10314.1	10411.4	10508.7	10606.0
11000	10703.8	10800.7	10898.0	10995.3	11092.6	11189.9	11287.2	11384.5	11481.8	11579.1
12000	11676.4	11773.7	11871.0	11968.3	12065.6	12162.9	12260.2	12357.5	12454.8	12552.1
13000	12649.4	12746.7	12844.0	12941.3	18088 6	13135.9	13233.2	13380.5	18427.8	18525.1
14000	18622.4	18719.7	18817.1	18914.3	14011.7	14109.0	14206.3	14803.6	14460.9	14498.2
15000	14595.5	14692.8	14790.1	14887.4	14984.7	15082-0	15179.8	15276.6	15373.9	15471.2
16000	15568.5	15663.8	15763.1	15860.4	15957.7	16055.0	16152.3	16249.6	16346.9	16444.2

XXX. CONVERSION OF FEET OF VIENNA INTO ENGLISH FEET AND DECIMALS.

1 Foot of Vienna = 1.0370284 English Foot.

Feet of Vienna.					Hund	reds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. fee
0	0.0	103.7	207.4	811.1	414.8	518.5	622.2	725.9	829.6	938.
1000	1037.0	1140.7	1244.4	1848.1	1451.8	1555.5	1659.2	1762.9	1866.6	1970.
2000	2074.0	2177.7	2281.5	2385.2	2488.9	2592.6	2696.3	2800.0	2903.7	3007.
3000	8111.1	3214.8	3318.5	3422.2	8525.9	3629.6	8738.3	8887.0	8940.7	4044.
4000	4148.1	4251.8	4355.5	4459.2	4562.9	4666.6	4770.8	4874.0	4977.7	5081.
5000	5185.1	5288.8	5292.5	5496.2	5599. 9	5703.6	5807.8	5911.0	6014.7	6118.
6000	6222.1	6325.8	6429.5	6538.2	6636.9	6740.7	6844.4	6948.1	7051.8	7155.
7000	7259.2	7862.9	7466.6	7570.3	7674.0	7777.7	7881.4	7985.1	8088.8	8192.
8000	8296.2	8399.9	8503.6	8607.8	8711.0	8814.7	8918.4	9022.1	9125.8	9229
9000	9338.2	9436.9	9540.6	9644.3	9748.0	9851.7	9955.4	10059.1	10162.8	10266
10000	10370.2	10478.9	10577.6	10681.8	10785.0	10888.7	10992.4	11096.2	11199.9	11308.
11000	11407.8	11511.0	11614.7	11718.4	11822.1	11925.8	12029.5	12138.2	12236.9	1 23 40.
12000	ls .	ì	t .	1	12859.1		l .	18170.2	1	1
13000	13481.3	13585.0	13688.7	13792.4	13896.1	13999.8	14103.5	14207.2	14310.9	14414
14000	It.	1	ı	1	14933.1		1			1
15000	15555.4	1	1	1	1		1	1	1	1

RHINE OR PRUSSIAN FEET

INTO DIFFERENT MEASURES OF LENGTH.

The Rhine Foot is used in Physical Geography, though not so extensively as the French or Paris Foot, in the northwestern part of Germany, Denmark, and Holland. Its legal value in the Prussian system of weights and measures is 139.13 French or Paris Lines, from which are derived the equations used in computing the following tables.

XXI. CONVERSION OF RHINE OR PRUSSIAN FRET INTO FRENCH TOISES.

1 Rhine Foot = 0.1610301 Toise.

	Hundreds.												
0.	100.	200.	800.	400.	500.	600.	700.	800.	900.				
Toises.	Toises.	Toises.	Toises.	Tolses.	Tolses.	Toises.	Toises.	Toises.	Tolens.				
0.00	16.10	82.21	48.31	64.41	80.52	96.62	112.72	128.82	144.93				
161.03	177.13	193.24	209.84	225.44	241.55	257.65	273.75	289.85	205.9€				
822.06	338.16	854.27	870.87	886.47	402.58	418.68	484.78	450.88	466.99				
488.09	499.19	515.30	581.40	547.50	568.61	579.71	595.81	611.91	628.01				
684.12	650.22	666.88	692.48	608.58	724.64	740.74	756.84	772.94	789.06				
805.15	821.25	887.86	853.46	869.56	885.67	901.77	917.87	983.97	950.06				
966.18	982.28	998.39	1014.49	1030.59	1046.70	1062.80	1078.90	1095.00	1111.11				
1127.21	1143.31			1 1				1	1				
			i .					ľ	ı				
	1								t .				
	Tolses. 0.00 161.03 322.06 483.09 684.12 805.15 966.18 1127.21 1288.24	Toises. Toises. 0.00 16.10 161.03 177.13 322.06 338.16 483.09 499.19 684.12 650.22 805.15 821.25 966.18 982.28 1127.21 1143.31 1288.24 1804.84	Totses. Totses. Totses. 0.00 16.10 32.21 161.03 177.13 193.24 322.06 338.16 354.27 483.09 499.19 515.30 634.12 650.22 666.33 805.15 921.25 837.36 966.18 982.28 998.39 1127.21 1143.31 1159.42 1288.24 1804.34 1820.45	Toises. Toises. Toises. Toises. 0.00 16.10 32.21 48.31 161.03 177.13 193.24 209.34 322.06 338.16 854.27 870.37 483.09 499.19 515.30 581.40 684.12 650.22 666.38 692.43 805.15 821.25 837.36 853.46 966.18 982.28 998.39 1014.49 1127.21 1143.31 1159.42 1175.52 1288.24 1804.34 1820.45 1886.55	Toises. 44.41 25.44 49.41 49.41 49.41 49.41 49.41 49.41 49.41 49.41 49.41 49.41 49.41 <th< td=""><td>Toises. <t< td=""><td>Toises. <t< td=""><td>Toises. <t< td=""><td>Column Tolumn</td></t<></td></t<></td></t<></td></th<>	Toises. Toises. <t< td=""><td>Toises. <t< td=""><td>Toises. <t< td=""><td>Column Tolumn</td></t<></td></t<></td></t<>	Toises. Toises. <t< td=""><td>Toises. <t< td=""><td>Column Tolumn</td></t<></td></t<>	Toises. Toises. <t< td=""><td>Column Tolumn</td></t<>	Column Tolumn				

XXXII. CONVERSION OF RHINE OR PRUSSIAN FEET INTO METRES.

1 Rhine Foot = 0.31385350 Metre.

Rhine Feet.	Rhine Feet Hundreds.											
Thousands.	0.	100.	200.	800.	400.	500.	600.	700.	800.	900.		
	Metres.	Motres.	Motres.	Metres.	Motres.	Metres.	Motres.	Metres.	Motres.	Metres.		
0	0.00	81.39	62.77	94.16	125.54	156.98	188.81	219.70	251.08	282.47		
1000	818.85	845.24	376.62	408.01	489.89	470.78	502.17	533.55	564.94	596.82		
2000	627.71	659.09	690.48	721.86	758.25	784.63	816.02	847.40	878.79	910.18		
3000	941.56	972.95	1004.33	1035.72	1067.10	1098.49	1129.87	1161.26	1192.64	1224.03		
4000	1255.41	1286.80	1818.18	1849.57	1880.96	1412.84	1448.78	1475.11	1506.50	1537.88		
5000	1569.27	1600.65	1632.04	1663.42	1694.81	1726.19	1757.58	1788.97	1820.85	1851.74		
6000	1888.12	1914.51	1945.89	1977.28	2008.66	2040.05	2071.48	2102.82	2184.20	2165.59		
7000	2196.97	2228.36	2259.75	2291.18	2822.52	2353.90	2885.29	2416.67	2448.06	2479.44		
8000	2510.83	2542.21	2578.60	2604.98	2686.37	2667.76	2699.14	2780.58	2761.91	2793.80		
9000	2824.68	2856.07	2897.45	2918.84	2950.22	2981.61	8012.99	8044.88	8075.76	8107.15		

XXXIII. OF RHINE OR PRUSSIAN FRET INTO FRENCH FEET AND DECIMALS. 1 Rhine Foot = 0 96618056 French Foot.

Rhine Feet.	Rhine Feet. Hundreds.												
Thousands.	0.	100.	200.	800.	400.	500.	600.	700.	800.	900.			
	Fr. Feet	Fr Feet.	Fr. Feet	Fr. Feet.	Fr Feet	Fr Feet.	Fr. Feet.	Fr.Feet.	Fr Feet.	Fr. Feet.			
0	0.00	96.62	193.24	289.85	886.47	488.09	579.71	676.33	772.94	869.56			
1000	966.18	1062.80	1159.42	1256.03	1352.65	1449.27	1545.89	1642.51	1789.13	1835.74			
2000	1932.86	2028.98	2125.60	2222.22	2818.88	2415.45	2512.07	2608.69	2705.31	2801.92			
2000	2898.54	2995.16	8091.78	3188.40	3285.01	33 81.68	8478.25	3574-87	3671.49	3768.10			
4000	8864.72	8961.34	4057.96	4154.58	4251.19	4347.81	4444.48	4541.05	4637.67	4784.28			
5000	4880.90	4927.52	5024.14	5120.76	5217.88	5818.99	5410.61	5507.23	5603.85	5700.47			
6000	5797.08	5898.70	5990.32	6086.94	6183.56	6280.17	6376.79	6473.41	6570.08	6666.65			
7000	6763.26	6859.88	6956.50	7058.12	7149.74	7246.35	7342.97	7489.59	7536.21	7632.88			
8000	7729.44	7826.06	7922.68	8019.30	8115.92	8212.53	8309.15	8405.77	8502.89	8599.01			
9000	8695.68	8792.24	8888.86	8985.48	9082.10	9178.72	9275.88	9871.95	9468.57	9565.19			

XXXIV. OF BHINE OR PRUSSIAN FEET INTO ENGLISH FEET AND DECIMALS. 1 Rhine Foot = 1 0297217 English Foot.

Rhine Feet.	Rhine Feet. Hundreds.											
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.		
'	ling feet.	Eng. feet.	Eng. feet.	Eng feet.	ling. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.		
0	0.00	102.97	205.94	808.92	411.89	514.86	617.83	720.81	823.7 8	926.75		
1000	1029.72	1182.69	1235.67	1888.64	1441.61	1544.58	1647.55	1750.53	1853.50	1956.47		
2000	2059.44	2162.42	2265.89	2868.86	2471.88	2574.80	2677.2 8	2780.25	2883.22	2986.19		
3000	8089.17	3192.14	3295.11	3398.0 8	8501.05	3604.03	3707.00	8809.97	8912.94	4015.92		
4000	4118.89	4221.86	4324.83	4427.80	4580.78	4633.75	4736.72	4839.69	4942.66	5045.64		
5000	5148.61	5251.58	5354.55	5457.53	5560.50	5668.47	5766.44	5869.41	5972.89	6075.86		
6000	6178.33	6281.30	6884.28	6487.25	6590.22	6693.19	6796.16	6899.14	7002.11	7105.08		
7000	7208.05	7311.02	7414.00	7516.97	7619.94	7722.91	7825.89	7928.86	8031.83	8134.80		
8000	8237.77	8340.75	8443.72	8546.69	8649.66	8752.64	8855.61	8958.58	9061.55	9164.52		
9000	9267.50	9870.47	9478.44	9576.41	9679.88	9782.36	9885.83	9988.30	10091.3	10194.2		

SPANISH OR MEXICAN VARAS AND FEET

INTO DIFFERENT MEASURES OF LENGTH.

XXXV. CONVERSION OF SPANISH OR MEXICAN VARAS INTO METRES.

1 Vara = 0.847965 Metre.

Vares.	Hundreds.											
Thousands.	0.	100.	900.	300.	400.	500.	600.	700.	800.	900.		
	Metres.	Metres.	Metres	Metres.	Motres.	Metres.	Metres.	Metres.	Metres.	Metrus		
0	0.00	84.80	169.59	254.89	839.19	423.98	508.78	593.58	678.87	763.17		
1000	847.96	932.76	1017.56	1102.35	1187.15	1271.95	1356.74	1441.54	1526.34	1611.13		
2000	1695.93	1780.73	1865.52	1950.82	2085.12	2119.91	2204.71	2289.51	2374.30	2459.10		
8000	2543.89	2628.69	2713.49	2798.28	2883.08	2967.88	3052.67	8187.47	3222.27	8307.06		
4000	3891.86	8476.66	3561.45	8646.25	8781.05	3 815.84	3900.64	8985.44	4070.23	4155.03		
5000	4289.82	4824.62	4409.42	4494.21	4579.01	4663.81	4748.60	4883.40	4918.20	5002.99		
6000	5087.79	5172.59	5257.88	5842.18	5426.98	5511.77	5596.57	5681.87	5766.16	5850.96		
7000	5985.75	6020.55	6105.85	6190.14	6274.94	6359.74	6144.58	6529.33	6614.13	6696.92		
8000	6788.72	6868.52	6953.81	7038.11	7122.91	7207.70	7292.50	7877.30	7462.09	7546.89		
9000	7631.68	7716.48	7801.28	7886.07	7970.87	8055.67	8140.46	8225.26	8810.06	8394.85		

XXXVI. OF SPANISH OR MEXICAN VARAS INTO ENGLISH FEET AND DECIMALS.

1 Vara = 2.78209 English Feet.

Varas.	Hundreds.												
Thousands.	0.	100.	200.	800.	400.	500.	600.	700.	800.	900.			
	Rag. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.			
0	0.0	278.2	556.4	834.6	1112.8	1891.0	1669.3	1947.5	2225.7	2503.9			
1000	2782.1	3060.3	3338.5	3616.7	8894.9	4178.1	4451.8	4729.6	5007.8	5286.0			
2000	5564.2	5842.4	6120.6	6398.8	6677.0	6955.2	7233.4	7511.6	7789.9	8068.1			
2000	8346.3	8624.5	8902.7	9180.9	9459.1	9787.3	10015.5	10293.7	10571.9	10850.2			
4000	11128.4	11406.6	11684.8	11963.0	12241.2	12519.4							
5000	18910.4	14188.7	14466.9	14745.1	15028.3	15301.5	15579.7	15857.9	16136.1	16414.3			
6000	16692.5												
7000						20865:7							
8000	22256.7												
	25038.8	25317.0	25595.2	25873.4	26151.6	26429.9	26708.1	26986.3	27164.5	27442.7			

XXXVII. CONVERSION OF CASTILIAN FEET INTO METRES.

1 Castilian Foot = 0.282655 Metre.

Castillan	Hundreds.												
Feet. Thousands.	0.	100.	200.	800.	400.	500.	600.	700.	800.	900.			
	Metres.	Metres.	Motres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.			
0	0.00	28.27	56.58	84.80	113.06	141.88	169.59	197.86	226.12	254.89			
1000	282.65	810.92	339.19	867.45	395.72	423.98	452.25	480.51	508.78	537.04			
2000	565.31	593.58	621.84	650.11	678.37	706.64	734.90	763.17	791.43	819.70			
3000	847.96	876.28	904.50	932.76	961.03	989.29	1017.56	1045.82	1074.09	1102.85			
4000	1180.62	1158.89	1187.15	1215.42	1 243.6 8	1271.95	1300.21	1328.48	1356.74	1385.01			
5000	1413.27	1441.54	1469.81	1498.07	1526.34	1554.60	1582.87	1611.13	1639.40	1667.66			
6000	1695.93	1724.20	1752.46	1780.73	1808.99	1837.26	1865.52	1898.79	1922.05	1950.32			
7000	1978.58	2006.85	2085.12	2063.88	2091.65	2119.91	2148.18	2176.44	2204.71	2232.97			
8000	2261.24	2289.51	2317.77	2846.04	2874.30	2402.57	2480.83	2459.10	2487.36	2515.63			
9000	2543.89	2572.16	2600.43	2628.69	2656.96	2685.22	2718.49	2741.75	2770.02	2798.28			

EXXVIII. CONVERSION OF CASTILIAN FEET INTO PARIS OR FRENCH FEET. 1 Castilian Foot = 0 870188 Paris Foot.

Castilian Feet.	Hundreds.											
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.		
					Par Feet.							
0	0.00	87.01	174.08	261.04	848.06	485.07	522.08	609.10	696.11	783.12		
1000	870.14	957.15	1044.17	1131.18	1218.19	1305.21	1892.22	1479.28	1566.25	1653.26		
2000	1740.28	1827.29	1914.80	2001.32	2088.83	2175.85	2262.36	2849.37	2436.39	2528.40		
8000	2610.41	2697.48	2784.44	2871.46	2958.47	3045.48	8182.50	3219.51	3806.52	3393.54		
4000	3480.55	3567.57	3654.58	3741.59	3828.61	3915.62	4002.64	4089.65	4176.66	4268 .68		
5000	4850.69	4487.70	4524.72	4611.73	4698.75	4785.76	4872.77	4959.79	5046.80	5133.82		
6000	5220.83	5307.84	5394.86	5481.87	5568.88	5655.90	5742.91	5829.93	5916.94	6003.95		
7000	6090.97	6177.98	6265.00	6352.01	6439.02	6526.04	6613.05	6700.06	6787.08	6874.09		
8000	6961.11	7048.12	7135.13	7222.15	7809.16	7396.17	7483.19	7570.20	7657.22	7744.23		
9000	7831.24	7918.26	8005.27	8092.29	81 79.3 0	8266.31	8353.33	8440.34	8527.85	8614.37		

XXXIX. CONVERSION OF CASTILIAN FEET INTO AMERICAN FEET.

1 Castilian Foot = 0.927809 American Foot.

Castilian Feet.	<u> </u>				Hun	dreds.		<u></u>		
Thousands.	0.	100.	200.	800.	400.	500.	600.	700.	800.	900.
	Am. Feet.	Am. Feet.	Am. Feet.	Am. Feet.	Am. Feet.	Am. Feet.	Am. Feet.	Am. Feet	Am. Feet	Am. Feet
0	0.00	92.73	185.46	278.19	370.92	463.65	556.89	649.12	741.85	834.58
1000	927.31	1020.04	1112.77	1205.50	1298.23	1390.96	1483.69	1576.48	1669.16	1761.89
2000	1854.62	1947.85	2040.08	2132.81	2225.54	2318.27	2411.00	2503.74	2596.47	2689.20
3000	2781.93	2874.66	2967.39	3060.12	3152.85	3245.58	3388.31	3481.04	3528.78	3616.51
4000	3709.24	8801.97	3894.70	8987.43	4080.16	4172.89	4265.62	4858.85	4451.08	4543.82
5000	4636.55	4729.28	4822.01	4914.74	5007.47	5100.20	5192.93	5285.66	5878.39	5471.12
6000	5563.86	5656.59	5749.32	5842.05	5934.78	6027.51	6120.24	6212.97	6305.70	6398.43
7000	6491.17	6583.90	6676.63	6769.36	6862.09	6954.82	7047.55	7140.28	7233.01	7325.74
8000	7418.47	7511.21	7603.94	7696.67	7789.40	7882.13	7974.86	8067.59	8160.32	8253.05
9000	8845.78	8438.51	8531.25	8623.98	8716.71	8809.44	8902.17	8994.90	9087.63	9180.36

THE length of the Spanish Vara, and of the Spanish or Castilian foot, used in the late Spanish Colonies of Mexico and South America, owing, no doubt, to the imperfection of the local standards, shows considerable variations from the value on which the preceding tables are based.

A careful comparison of the standard Vara, brought from Mexico by Major Turnbull, and deposited in the United States Office of Weights and Measures, (see above p. 113,) gave for its length 32.9682 American inches = 2.7473333 American feet = 2.7474928 English feet = 0.8374206 metre.

From a series of altitudes published in Mexico, by Cortina, in Castilian feet, and by Orbegozo in metres and Castilian feet, Jul. Schmidt derives the following value of the Vara and of the Castilian foot, used by these authors (see Petermann's *Mittheil*. 1857, p. 371): One Vara = 2.573296 Paris feet = 0.8358065 metre; and one Castilian foot = 0.857764 Paris foot = 0.91417 English foot.

According to Colonel J. Ondarza, one of the authors of the new official Map of Bolivia, the Bolivian government has declared the legal value of the Spanish Vara to be in the ratio of 100 metres = 118 Varas = 354 Spanish feet, which value has been adopted by him in publishing his measured altitudes.

XXXVIII' MEXICO. — CONVERSION OF CASTILIAN FEET INTO METRES, PARIS AND ENGLISH FEET.

Mexican or	Accordi	g to Turnbull's	Standaro.	According	to Schmidt, fro	m Cortins.
Castilian Feet.	Metres.	Paris Foot.	English Feet.	Metres.	Paris Foot.	English Fee
1000	279.14	839.30	915.88	278.64	857.76	914-17
2000	558.28	1718.60	1831.66	557.27	1715.53	1828.34
8000	837.42	2577.99	2747.49	885.91	2578.29	2742.51
4000	1116.56	3437.19	3663.32	1114.54	8431.06	3656.68
5000	1893.70	4296.49	4579.15	1393.18	4288.82	4570.85
6000	1674.84	5155.79	5494.99	1671.81	5146-58	5485.02
7000	1953.98	6015.08	6410.82	1950.45	6004.85	6399.19
8000	2233.12	6874.38	7326.65	2229-08	6862.11	7313.36
9000	2512.26	7788.68	8242.48	2507.72	7719.88	8227.53

XXXIX'. BOLIVIA. — CONVERSION OF SPANISH VARA AND SPANISH FEET.

1 Spanish foot = 0 2824859 metre = 0.8896171 Paris foot, = 0.9268078 English foot.

Bolivian or Spanish Feet.	Metres.	Paris Foot.	English Feet.	Metres.	Spanish Varas.	Spanish Feet.
1000	282.49	869.62	926.81	1000	1190	8540
2000	564.97	1789.23	1858.61	2000	2360	7080
8000	817.46	2608.85	2780.42	8000	8540	10620
4000	1129.94	8478.47	3707.23	4000	4720	14160
5000	1412.48	4348.09	4684.04	5000	5900	17700
6000	1694.92	5217.70	5560.85	6000	7080	21240
7000	1977.40	6087.82	6487.65	7000	8260	24780
8000	2259.89	6956.94	7414.46	8000	9440	28320
9000	2342.37	7826.55	8341.27	9000	10620	21860

FRACTIONAL PARTS OF A TOISE AND OF A FOOT

INTO EACH OTHER.

XL. CONVERSION OF INCHES INTO DUODECIMAL LINES.

1 Inch = 12 Lines.

Inches.					Inches.	Units.				
Tens.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.
0	0	12	24	86	48	60	72	84	96	108
10	120	132	144	156	168	180	192	204	216	228
20	240	252	264	276	288	800	312	824	886	848
30	369	872	884	896	408	420	482	444	456	468
40	480	492	504	516	528	540	552	564	576	586
50	600	612	624	636	648	660	672	684	696	708
60	720	732	744	756	768	780	792	804	816	828
70	840	852	864	876	888	900	912	924	936	948
80	960	972	984	996	1008	1020	1082	1044	1056	1068
90	1080	1092	1104	1116	1128	1140	1152	1164	1176	1188
100	1200	1212	1224	1286	1248	1260	1272	1284	1296	1306

XLI. CONVERSION OF DECIMALS OF A TOISE INTO FRET AND INCHES.

1 Toise = 6 Feet = 72 Inches = 864 Lines.

isea		Hundredths of a Toise.																												
134.	,	0	•		1	l.			2	•		8	ı.		4	L.	1	5	•		6	,	'	7.		8	5.	<u> </u>	9	•
																lin.														
																														5,76
																														8,16
1.2	1.	2.4	1,80	1.	8.	1,4	4	1.	3 .]	10,08	1.	4.	6,72	1.	5.	3,36	11.	6.6	0,00	1.	6.	8,64	1.7.	5,28	1.	8.	1,92	1.	8.1	10,56
1.8	1.	9.7	7,20	1.	10.	8,8	4	1.1	1.	0,48	1.	11.	9,12	2.	0.	5,76	2.	1.5	2,40	2.	1.	11,04	2.2.	7,68	2.	3.	4,32	2.	4.	0,96
1.4	2.	4.9	,60	2.	5.	6,2	4	2.	6.	2,88	2.	6.	11,52	2.	7.	8,16	2.	8.4	1,80	2.	9.	1,44	2.9.	10,08	2.1	0.	6,72	2.1	11.	8,86
1.5	3.	0.0	0,00	8.	0.	8,6	4	3.	1.	5,28	3.	2.	1,92	8.	2.	10,56	8.	8.	7,20	3.	4.	3,84	8.5.	0,48	3.	5.	9,12	8.	6.	5,76
1.6	3.	7.2	2,40	8-	7.	11,0	4	В.	8.	7,68	8.	9.	4,82	3.	10.	0,96	3.	10.	9,60	8.	11.	6,24	4.0.	2,88	4.	0.	11,52	4.	1.	8,16
1.7	4.	24	1,80	4.	8.	1,4	4	4.	8.1	0,08	4.	4.	6,72	4.	5.	3,86	4.	6.0	0,00	4.	6.	8,64	4.7.	5,28	4.	8.	1,92	4.	8.1	0,56
9.6	4.	9.7	7,20	4.	10.	8,8	4	4.1	1.	0,48	4.	11.	9,12	5.	0.	5,76	5.	1.5	2,40	5.	1.	11,04	5.2.	7,68	5.	8.	4,82	5.	4.	0,96
																														8,86

Foot.				1	Hundredth	of a Foot				
Tons.	0.	1.	2.	8.	4.	5.	6.	7.	8.	9.
	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
0.0	0.00	0.12	0.24	0.86	0.48	0.60	0.72	0.84	0.96	1.08
0.1	1.20	1.82	1.44	1.56	1.68	1.80	1.92	2.04	2.16	2.28
0.2	2.40	2.52	2.64	2.76	2.88	8.00	3.12	3.24	3.36	3.48
0.8	3.60	3.72	8.84	8.96	4.08	4.20	4.32	4.44	4.56	4.68
0.4	4.80	4.92	5.04	5.16	5.28	5.40	5.52	5.64	5.76	5.88
0.5	6.00	6.12	6.24	6.86	6.48	6.60	6.72	6.84	6.96	7.06
0.6	7.20	7.32	7.44	7.56	7.68	7.80	7.92	8.04	8.16	8.28
0.7	8.40	8.52	8.64	8.76	8.88	9.00	9.12	9.24	9.86	9.48
0.8	9.60	9.72	9.84	9.96	10.08	10.20	10.32	10.44	10.56	10.68
0.9	10.80	10.92	11.04	11.16	11.28	11.40	11.52	11.64	11.76	11.88

XLIII. CONVERSION OF DECIMALS OF A FOOT INTO INCHES AND DUODECIMAL LINES.

•	1			1	Iundredth	of a Too	ж.			
Foot. Tens	0 _	1.	9.	8.	4.	5.	6.	7.	8.	9.
	In. Line.	In. Line.	In. Line.	In. Line.	In. Line.	In Line	In. Line	In. Line.	In Line	In Line
0.0	0.0,00	0. 1,44	0. 2,88	0. 4,82	0. 5,76	0.7,20	0. 8,64	0.10,08	0.11,52	1. 0,96
0.1	1.2,40	1. 3,84	1. 5,28	1. 6,72	1. 8,16	1.9,60	1.11,04	2. 0,48	2. 1,92	2. 3.36
0.2	2.4,80	2. 6,24	2. 7,68	2. 9,12	2.10,56	3.0,00	3. 1,44	3. 2,88	8. 4,82	8. 5,76
0.8	8.7,20	3. 8,64	3.10,08	8.11,52	4. 0,96	4.2,40	4. 3,84	4. 5,28	4. 6,72	4. 8,16
0.4	4 9,60	4.11,04	5. 0,48	5. 1,92	5. 8,36	5.4,80	5. 6,24	5. 7,68	5. 9,12	5.10,56
0.5	6.0,00	6. 1,44	6. 2,88	6. 4,32	6. 5,76	6.7,20	6. 8,64	6.10,08	6.11,52	7. 0,96
0.6	7.2,40	7. 8,84	7. 5,28	7. 6,72	7. 8,16	7.9,60	7.11,04	8. 0,48	8. 1,92	8. 3,36
0.7	8.4,80	8. 6,24	8. 7,68	8. 9,12	8.10,56	9.0,00	9. 1,44	9. 2,88	9. 4,32	9. 5,76
0.8	9.7,20	9. 8,64	9.10,08	9.11,52	10. 0,96		1 -			10. 8.16
0.9	10.9,60	10.11,04	11. 0,48	11. 1,92	11. 3,36	11.4,80	11. 6,24	11. 7,68	11. 9,12	11.10,56

XLIV. CONVERSION OF INCHES AND DUODECIMAL LINES INTO DECIMALS OF A FOOT.

1 Inch = 0 08888 of a Foot. 1 Line = 0.008944 of a Foot.

						LA	0.66.				•	
Inches.	0.	1.	9.	8.	4.	5.	6.	7.	8.	9.	10.	11.
	Foot.	Foot.	Foot.	Foot.	Foot.	Foot.	Foot.	Foot.	Foot.	Foot.	Foot.	Post
0	0.0000	0.0069	0.0139	0.0208	0.0278	0.0347	0.0417	0.0486	0.0556	0.0625	0.0694	0.0764
1	0.0833	0.0903	0.0972	0.1042	0.1111	0.1181	0.1250	0.1819	0.1389	0.1458	0.1528	0.1597
2	0.1667	0.1786	0.1806	0.1875	0.1944	0.2014	0.2068	0.2153	0.2222	0.2292	0.2361	0.2431
8	0.2500	0.2569	0.2639	0.2708	0.2778	0.2847	0.2917	0.2986	0.8056	0.8125	0.3194	0.3264
4	0.3383	0.8403	0.8472	0.8542	0.8611	0.8681	0.8750	0.3819	0.8889	0.8958	0.4028	0.4097
5	0.4167	0.4286	0.4806	0.4375	0.4444	0.4514	0.4583	0.4653	0.4722	0.4792	0.4861	0.4931
6	0.5000	0.5069	0.5189	0.5208	0.5278	0.5847	0.5417	0.5486	0.5556	0.5625	0.5694	0.5764
7	0.5833	0.5908	0.5972	0.6042	0.6111	0.6181	0.6250	0.6319	0.6389	0.6458	0.6528	0.6597
8	0.6667	0.6736	0.6806	0.6875	0.6944	0.7014	0.7088	0.7158	0.7222	0.7292	0.7861	0.7431
9	0.7500	0.7569	0.7689	0.7708	0.7778	0.7847	0.7917	0.7986	0.8056	0.8125	0.8194	0.8261
10	0.8833	0.8403	0.8472	0.8542	0.8611	0.8681	0.8750	0.8819	0.8889	0.8958	0.9028	0.9097
11	0.9167	0.9286	0.9306	0.9875	0.9444	0.9514	0.9583	0.9658	0.9722	0.9792	0.9861	0.9931

METEOROLOGICAL TABLES.

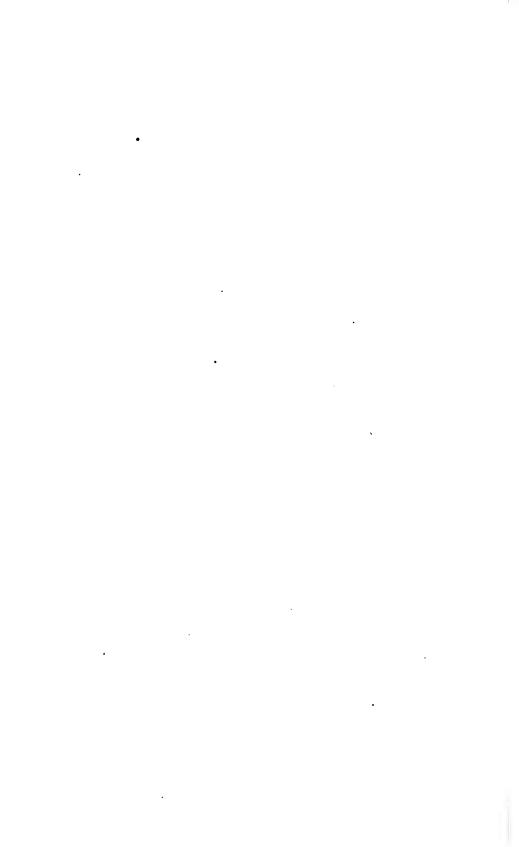
V.

METEOROLOGICAL CORRECTIONS,

OR

TABLES

FOR CORRECTING SERIES OF OBSERVATIONS FOR THE PERIODIC AND NON-PERIODIC VARIATIONS.



[The figures refer to the folio at the bottom of the page.—The letters near them mean, D. = calculated by Dove; Gl. = Ghisher; G. = Guyot; L. = Lefroy. For the letters before the latitudes, see page 12.]

Temperature.

Hourly Corrections for Periodic Variations.

NORTH AMERICA.

		Station.		Latitude.	Scale.	1	Page.
Тав	LE [.	Washington, District Columbia,	B 1.	38 54 N.	Reau.	D.	15
66	II.	Philadelphia, Girard College,	A's.	39 58 N.	Reau.	D.	15
"	III.	Philadelphia, Girard College,	A's.	39 58 N.	Fahr.	G.	16
"	IV.	Frankfort Arsenal, Penn.,	C.	39 57 N.	Reau.	D.	17
"	V.	Frankfort Arsenal, Penn.,	C.	39 57 N.	Fahr.	D.	18:
"	VI.	Toronto, Canada West,	В.	43 40 N.	Fahr.	D.	19
"	VII.	Toronto, Canada West,	B.	43 40 N.	Reau.	D.	2 0
"	VIII.	Toronto, Canada West,	A'6.	43 40 N.	Fahr.	L.	21
"	IX.	Toronto, Canada West,	A'6.	43 40 N.	Reau.	D.	22
"	X .	Montreal, Canada East,	A'1.	45 30 N.	Fahr.	G.	22
u	XI.	Sitka, Russian America,	A'5.	57 3 N.	Reau.	D.	23
"	XII.	Boothia Felix, Arctic America,	A.	69 59 N.	Reau.	D.	24
"	XIII.	Lake Athabasca, Arctic America,	C.	59 N.	Fahr.	L.	25
66	XIV.	Melville Island, Arctic America,	C.	74 47 N.	Reau.	D.	25
"	XV.	Hecla Cove, Spitzbergen,	C.	79 55 N.	Reau.	. D.	25
	•	Appendix.					
"	V'.	Amherst College, Mass.,	A'1.	42 22 N.	Fahr.	D.	28
		SOUTH AMERIC	A.				
66	XVI.	Rio Janeiro, Brazil,	C.	22 54 S.	Fahr.	D.	26
u	XVII.	Rio Janeiro, Brazil,	C.	22 54 S.	Reau.	D.	27

3

E

		ASIA. Station.		Latitude.	Scale.		Paga.
TABI	LE XVIII.	Trevandrum, India,	A.	8 31 N.	Fahr.	D.	31
- 46	XIX.	Trevandrum, India,	Λ.	8 31 N.	Reau.	D.	32
6	XX.	Madras, India,	A.	13 4 N.	Fabr.	D.	33
66	XXI.	Madras, India,	Λ.	13 4 N.	Reau.	D.	34
	XXII.	Bombay, India,	Α.	18 56 N.	Fahr.	D.	35
46	XXIII.	Bombay, India,	A.	18 56 N.	Reau.	D.	36
"	XXIV.	Madras, India,	A'5.	13 4 N.	Reau.	D.	37
44	XXV.	Bombay, India,	A'4.	18 56 N.	Reau.	D.	37
"	XXVI.	Calcutta, India,	A'2.	22 33 N.	Reau.	D.	38
"	XXVII.	Tiflis, Georgia,	A'4.	41 41 N.	Reau.	D.	39
66	XXVIII.	Peking, China,	A'4.	39 54 N.	Reau.	D.	39
44	XXIX.	Nertchinsk, Siberia,	A'6.	51 18 N.	Reau.	D.	40
"	XXX.	Nertchinsk, Siberia,	Λ.	51 18 N.	Reau.	D.	41
"	XXXI.	Barnaul, Siberia,	A.	53 20 N.	Fahr.	D.	42
46	XXXII.	Barnaul, Siberia,	A.	53 20 N.	Reau.	D.	43
44	XXXIII.	Barnaul, Siberia,	A'6.	53 20 N.	Reau.	D.	44
		EUROPE.					
46	XXXIV.	Rome, Italy,	C.	41 54 N.	Reau.	D.	47
"	XXXV.	Padua, Italy,	C.	45 24 N.	Reau.	D.	48
66	XXXVI.	Geneva, Switzerland,	C 10.	46 12 N.	Reau.	D.	49
п	XXXVIL	Geneva, Switzerland,	C'4.	46 12 N.	Reau.	D.	49
**	XXXVIII.	St. Bernard, Switzerland,	C 10.	45 52 N.	Reau.	D.	50
"	XXXIX.	St. Bernard, Switzerland,	C'4.	45 52 N.	Reau.	D.	50
и	XL.	Kremsmünster, Austria,	C. ·	48 3 N.	Reau.	D.	51
"	XLI.	Salzburg, Austria,	A'6.	47 48 N.	Reau.	D.	52
66	XLII.	Munich, Bavaria,	A'6.	48 9 N.	Reau.	D.	52
66	XLIII.	Prague, Bohemia,	A'10.	50 5 N.	Reau.	D.	53
EG.	XLIV.	Prague, Bohemia,	A.	50 5 N.	Reau.	D.	54
"	XLV.	Plymouth, England,	C.	50 22 N.	Fahr.	D.	55
"	XLVI.	Plymouth, England,	C.	50 22 N.	Reau.	D.	56
**	XLVII.	Brussels, Belgium,	В.	50 51 N.	Reau.	D.	57
66	XLVIII.	Brussels, Belgium,	B ′.	50 51 N.	Reau.	D.	58
EE.	XLIX.	Schwerin, Germany,	B's.	53 36 N.	Reau.	D.	58
***	L.	Mühlhausen, Prussia,	C.	51 13 N.	Reau.	D.	59
и	LI.	Utrecht, Holland,	A′2.	52 5 N.	Reau.	D.	60
"	LII.	Greenwich, England,	B′7.	51 29 N.	Reau.	D.	60
ш	LIII.	Greenwich, England,	В.	51 29 N.	Reau.	D.	61
ш	LIV.	Greenwich, England,		51 29 N.	Fahr.	Gl.	62
**	LV.	Halle, Prussia,	C.	51 30 N.	Reau.	D.	63
E	LVI.	Göttingen, Hanover,	C.	51 32 N.	Reau.	D.	64

		Station.		Latituda.	Scale.		Page.
TABL	E LVII.	Berlin, Prussia,	A.	52 30 N.	Reau.	D.	65
44	LVIII.	Salzufien, Germany,	A.	52 5 N.	Reau.	D.	66
"	LIX.	Stettin, Germany,	A'.	53 25 N.	Reau.	D.	67
**	LX.	Apenrade, Sleswick,	C.	55 3 N.	Reau.	D.	68
44	LXI.	Leith, Scotland,	A.	55 59 N.	Fahr.	D.	69
"	LXII.	Leith, Scotland,	A.	55 59 N.	Reau.	D.	70
"	LXIII.	Makerstoun, Scotland,	A′s.	55 36 N.	Reau.	D.	71
66	LXIV.	Dublin, Ireland,	B'4.	53 23 N.	Reau.	D.	71
66	LXV.	Catharinenburg, Russia,	A.	56 50 N.	Reau.	D.	72
	LXVI.	Catharinenburg, Russia,	A'6.	56 50 N.	Reau.	D.	73
46	LXVII.	St. Petersburg, Russia,	A'10.	59 56 N.	Reau.	D.	73
46	LXVIII.	Helsingfors, Finland,	A′8.	60 10 N.	Reau.	Ď.	74
66	LXIX.	St. Petersburg, Russia,	A.	59 56 N.	Reau.	D.	75
24	LXX.	Helsingfors, Finland,	C.	60 10 N.	Reau.	D.	76
66	LXXI.	Christiania, Norway,	C.	59 55 N.	Reau.	D.	77
"	LXXII.	Drontheim, Norway,	C.	63 26 N.	Reau.	D.	78
**	LXXIII.	Strait of Kara, Russia,	A	70 37 N.	Reau.	D.	79
	LXXIV.	Matoschkin Schar, Novaia Zemlia,		73 N.	Reau.	D.	80
14	LXXV.	Bossekop, Norway,	C.	69 58 N.	Reau.	D.	81
"	LXXV'.	Bossekop, Norway,	C.	69 58 N.	Centig	G.	81
	•	AFRICA AND AUSTRA	LIA.				
66	LXXVI.	St. Helena, Africa,	A'5.	15 55 S.	Reau.	D.	85
66	LXXVII.	Cape of Good Hope, Africa,	A'5.	33 56 S.	Reau.	D.	85
"	LXXVIII.	Hobarton, Tasmania,	A′8.	42 53 S.	Reau.	D.	86
		Monthly Corrections for Non-perio	odic V	ariations.			
		Station.		Latitude.	Scale.		Page.
TABL	E LXXIX.	Madras, India,		13 4 N.	Reau.	D.	90
66	LXXX.	Palermo, Sicily,	:	38 7 N.	Reau.	D.	91
"	LXXXI.	Milan, Italy,		45 28 N.	Reau.	D.	92
44	LXXXII.	Geneva, Switzerland,		46 12 N.	Reau.	D.	94
66	LXXXIII.	Vienna, South Germany,		48 13 N.	Reau.	D.	96
"	LXXXIV.	Ratisbon, South Germany,		49 1 N.	Reau.	D.	97
"	LXXXV.	Stuttgard, South Germany,		48 46 N.	Reau.	D.	99
66	LXXXVI.	Carlsruhe, South Germany		49 1 N.	Reau.	D.	100
44	LXXXVII.	Berlin, North Germany,		52 30 N.	Reau.	D.	102
"]	LXXXVIII.	Copenhagen, Denmark,		55 41 N.	Reau.	D.	105
66	LXXXIX.	Paris, France,		48 50 N.	Reau.	D.	107
44	XC.	Zwanenburg, Holland,		52 23 N.	Reau.	D.	108
44	XCI.	London, England,		51 30 N.	Reau.	D.	110
E		5					

Тав	LE XCII.	Kinfauns Castle, Scotland,	56 24 N.	Reau.	D.	112
66	XCIII.	Tornea, Finland,	65 50 N.			
66	XCIV.	Albany, N. Y., North America,	42 39 N.	Reau.	D.	113
"		Salem, Mass., North America,	42 31 N.	Reau.	D.	114
66		Reikiavik, Iceland,	64 8 N.			
		Godthaab, Greenland,	64 10 N.			
		Force of Vapor and Relative 1	Humidity.			
		Hourly Corrections for Periodic Vo	zriations.			
"	XCVIII.	Greenwich, England, Force of Vapor,	by Glaisher,			119
66	YCIY	Greenwich England Relative Humidi	ter her Claigh			190

METEOROLOGICAL CORRECTIONS.

One of the prominent objects of a prolonged series of meteorological observations is to determine the mean condition of the atmosphere, during a given interval of time, such as a day, a month, or a year, as to its temperature, moisture, and barometric pressure. In order to furnish the true means of these elements, free from the periodic changes which depend upon the daily course of the sun and upon the seasons, the observations ought to be made at equal intervals of time, and be so often repeated as actually to represent the sum of the variations which took place during the stated time. It is generally admitted that observations taken at every one of the twenty-four hours of the day give means which do not sensibly differ from the means which would be obtained from a still larger number of observations during the same time; so that means derived from hourly observations may be considered as the true daily, monthly, and annual means of the year in which the observations were taken.

However, as the means of a given month, or year, will generally be found somewhat to differ from those of another year, at the same place, from causes which are not of a periodic nature, it is obvious that the absolute means can only be derived from the means of a series of years, in which the differences arising from these non-periodic variations may be considered as sufficiently balancing each other.

Hourly observations can be expected only from a very few stations, favored with peculiar arrangements for the purpose. By far the larger number of observers must necessarily confine themselves to three or four observations a day. The means, therefore, deduced from such a set of observations, generally differ from the true means which would be given by hourly observations, by a quantity which varies with the hours selected for the observations. If that quantity, however, is known by having been previously determined for every hour, or set of hours, by a long series

METEOROLOGICAL CORRECTIONS.

of hourly observations taken at some station in a similar climatic situation, it is evident that, whatever be the hours at which observations are taken, the means derived from them can always be reduced to the true means by correcting them for that difference.

The following tables furnish such corrections, both for periodic and non-periodic variations of temperature, and for stations situated in various latitudes. They give the quantities which must be added to, or subtracted from, the hourly means, in order to obtain the true means of the day, of the month, and of the year.

Two tables of the same description, for moisture, which may be considered as specimens of the kind, close the set.

Two other tables, for correcting the mean barometric pressures, are found at the end of the Hypsometrical Tables, pp. 92, 93.

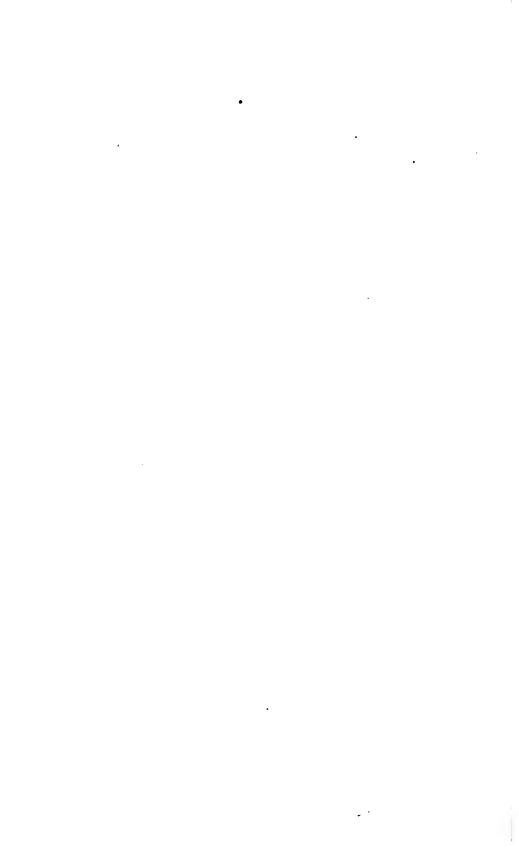
CORRECTIONS FOR TEMPERATURE.

HOURLY CORRECTIONS FOR PERIODIC VARIATIONS,

OB

TABLES

FOR REDUCING THE MEANS OF THE OBSERVATIONS TAKEN AT ANY HOUR OF THE DAY TO THE TRUE MEAN TEMPERATURE OF THE DAY, OF THE MONTH, AND OF THE YEAR.



HOURLY CORRECTIONS FOR PERIODIC VARIATIONS.

OR

CORRECTIONS TO BE APPLIED TO THE MEANS OF THE HOURS OF OBSERVATION, OR SETS OF HOURS, IN ORDER TO OBTAIN THE TRUE MEAN TEMPERATURES OF THE RESPECTIVE DAYS, MONTHS, AND OF THE YEAR.

The following set contains all the tables for correcting the means of observations on atmospheric temperature for the effect of diurnal variation which have been published by Dove, together with a few others of the same description. Dove's tables are found in two papers, published in the Memoirs of the Royal Academy of Berlin for 1846 and for 1856, and in the first Report on the Observations of the Meteorological Institute of Prussia, Berlin, 1851.

In the first paper are twenty-nine tables, in Reaumur's scale, nine of which have been republished, in Fahrenheit's scale, in the *Proceedings of the British Association* for 1847, and will also be found below. In that series the corrections have been formed by finding first the differences between the hourly and the true means, and then computing the observations by Bessel's formula, in order to eliminate the accidental irregularities due to the shortness of the period during which the observations were taken. Calling x the horary angle reckoned from noon, Bessel's formula is

$$tx = u + u' \sin(x + U') + u'' \sin(2x + U'') + u''' \sin(3x + U''').$$

The stations at which hourly observations were made are Trevandrum, Madras, Bombay, Salzufien, Prague, St. Petersburg, Catharinenburg, Barnaul, Nertchinsk, Matoschkin-Schar, Strait of Kara, and Boothia Felix. Bi-hourly observations were taken at Brussels, Greenwich, and Toronto; in all others the night observations are wanting, and were obtained by interpolation. Moreover, in several stations the number of observations was small, at Madras even only thirty-six days. The tables of that series may be readily distinguished from those belonging to the same stations in the second, by their containing the corrections for several sets of hours, which are not found in the tables of the other.

In Dove's second series, and in all other tables, the corrections given are simply the differences, with reverse signs, between the hourly and the true means, excepting, however, the stations of Toronto, in which the corrections were computed, by Bessel's formula, by Colonel Sabine; of Prague, by Jelineck; of Salzburg, and those of Geneva and St. Bernard, by Plantamour.

The observations from which these tables are derived were made hourly at Hobarton during 8 years; at the Cape of Good Hope, for 5½ years; St. Helena, 5 years; Madras, 5 years; Bombay, 4 years; Calcutta, 1½ years; Toronto, 6 years; Philadelphia, 3 years; Makerstoun, 3 years; Utrecht, 1½ years; Prague, 10½ years; Munich, 7 years; Salzburg, 6 years; St. Petersburg, 10 years; Catherinenburg, 6 years; Barnaul, 5 years; Tiflis, 4 years; Nertchinsk, 6 years; Peking, 4 years; Sitka, 5 years. In the following stations the observations were bi-hourly:—Washington, for 1½ years; Greenwich, 7 years; Dublin, 4 years; Brussels, 9 years; Geneva and St. Bernard, 4 years; Schwerin, 3 years.

The observations made in England, and in her colonies, are found in the various government publications. Those of the Russian stations are taken from the Annuaire Météorologique et Magnétique des Ingénieurs des Mines, and in the Annales de

HOURLY CORRECTIONS FOR PERIODIC VARIATIONS.

Poserratoire Physique Central de Russie. The observations made at Prague, Munich, Geneva, with those at St. Bernard, Makerstoun, Greenwich, Brussels, and Washington, were published by their respective Observatories; those of Utrecht, by Buys-Ballot; of Dublin, by Lloyd, in his Notes on the Meteorology of Ireland; those of Schwerin were communicated in manuscript by Dippe; the observations at Melville Island are published in No. 42 of the Parliamentary papers for 1854; and those at Bossekop, by Martins and Bravais, in the Voyage de la Commission Scientifique du Nord.

The tables of this second series being mostly deduced from longer series of observations than those in the first, when the same station is found in both, the table in the

second is generally to be preferred.

Glaisher's table for Greenwich has been taken from the *Greenwich Observations*. Captain Lefroy kindly furnished the tables for Toronto and Lake Athabasca. To him the author is also indebted for the observations made at Montreal by Mr. McCord, from which Table X. was computed. Table III., for Philadelphia, was deduced by the writer from the observations made at Girard College under the direction of Prof. A. D. Bache.

In order to facilitate the selection of the tables, they are marked in the table of

contents with capitals, which have the following signification: -

A and B mean that the tables have been derived from hourly and bi-hourly observations, and have been computed by Bessel's formula; C, that the tables contain values obtained by interpolation.

A', B', and C' indicate the tables based respectively on hourly and bi-hourly or partly interpolated observations, which give simply the differences between the hourly

and the true means.

The figures added to the letters indicate the number of years during which the observations used in forming the table were carried on. The stations are arranged, in each continent, in the order of their latitude.

USE OF THE TABLES.

In order to reduce meteorological means obtained from any set of hours to the true means, the table best suited to the purpose must first be selected. The diurnal variation changing with the seasons, the latitude, the altitude, and the distance from the sea-shore, the station which comes nearest, in all these respects, to the station the observations of which are to be corrected, must be adopted.

Suppose the thermometer has been observed at Baltimore, during the month of January, at 7 A. M., 1 P. M., and 7 P. M., and the monthly means of these hours to be respectively 27°, 35°, and 31° Fahrenheit. We take Table III., Philadelphia, it being the nearest in latitude and climatic situation. We find the correction for the

hours 7, 1, and 7, and we have

Obser	rved Means.	Corrections.		True Means.
For 7 A. M.	27°	$+3^{\circ}.63$	=	30°.63
For 1 P. M.	35°	- 3°.87	=	31°.13
For 7 P. M.	31°	— 1°.13	=	29°.87
Sums,	93°	— <u>1°.37</u>	=	91°.63
Means,	31°	0°.46	=	30°.54 True Mean for January.

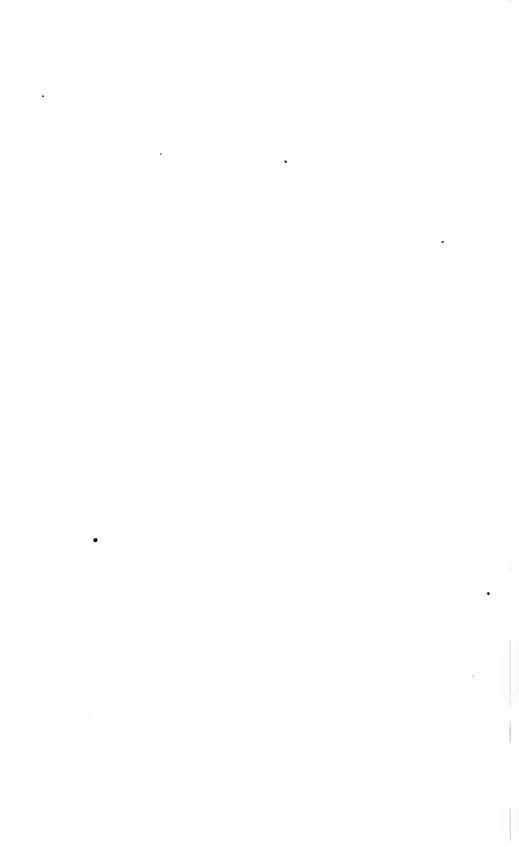
It is obvious that the corrections can be applied, either separately to each hour, as is done above, or collectively, in taking the mean of the three hourly corrections and applying it to the mean of the three observations, as in the last line, which is the more convenient method. Therefore, in order to find the correction for any set of hours, it suffices to take the mean of the corrections given in the table for the hours composing the set. The true daily means can be found in the same way, and the true yearly means can be derived from the corrected monthly means, or by applying the corrections given in the last column.

HOURLY CORRECTIONS

FOR

PERIODIC VARIATIONS.

NORTH AMERICA. - SOUTH AMERICA.



NORTH AMERICA. - WASHINGTON. Lat. 38° 54' N. Long. 77° 3' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Resumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct	Nov.	Dec.	Year.
A.M. 0 12'	1.15	1.26	1.60	1.95	2.83	2.87	2.94	2.81	2.89	1.78	0.85	0.96	1.86
2 12'	1.28	1.86	2.14	2.40	8.15	8.21	8.25	8.07	2.75	2.27	1.84	1.12	2.32
4 12'	1.45	2.18	2.67	2.75	8.56	8.64	3.83	8.49	8.15	2.89	1.92	1.54	2.76
6 12'	1.88	2.82	2.76	2.59	2.20	2.28	2.12	2.81	8.02	8.19	2.18	1.81	2.43
8 12	1.48	1.76	1.68	1.05	0.82	-0.16	0.09	0.28	1.04	1.69	1.88	1.68	1.07
10 12'	-0.18	-0.58	-0.88	-0.76	-1.24	-1.82	-1.82	-1.81	-1.81	-1.25	-0.17	-0.15	-0.96
P.M. 0 12'	-1.47	-2.05	-2.36	-2.89	-2.64	-2.69	-2.55	-2.97	-2.92	-2.89	-1.90	-1.57	-2.87
2 12'	-2.6 0	-8 .15	-8.85	-3.41	-3.57	-3.84	-8.49	-3.88	-8.74	-8.64	-2.44	-2.50	-8.30
4 12'	-2.32	-8.05	-8.20	-3.51	-3.66	-4.29	-4.16	-3.59	-3.65	-3.29	-2.08	-2.19	-8.23
6 12'	-0.76	-1.25	-1.78	-2.18	-2.44	-1.60	-2.24	-1.74	-1.88	-1.84	-1.59	-1.01	-1.69
8 12'	-0.23	0.02	-0.05	0.06	0.27	0.44	-0.21	-0.26	-0.23	0.18	-0.22	-0.26	-0.04
10 12'	0.88	0.69	0.76	1.42	1.67	2.04	1.26	1.79	1.41	0.98	0.28	. 0.48	1.08
Means.	1.82	1.52	6.26	9.02	12.64	18.34	19.29	17.78	16.04	7.47	5.20	1.68	

II.

N. America. — Philadelphia. Lat. 39° 58' N. Long. 75° 11' W. Gr. — Dove. Dogress of Resumur.

Hour.	Jen.	Yeb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct	Nov.	Dec.	Year.
Midn.	0.64	1.27	1.88	1,81	2.06	2.34	2.10	1.94	2.12	1.70	1.81	0.62	1.60
1	0.94	1.48	1.61	2.20	2.82	2.68	2.45	2.19	2.04	1.87	1.22	0.81	1.81
2	1.00	1.67	1.85	2.58	2.64	2.86	2.69	2.41	2.22	2.18	1.43	0.98	2.04
8	1.13	1.95	2.00	2.76	2.96	3.20	2.88	2.44	2.48	2.36	1.50	1.12	2.23
4	1.24	2.05	2.08	2.97	8.27	8.40	8.04	2.74	2.56	2.58	1.74	1.28	2.41
5	1.36	2.13	2.50	8.06	3.82	3.28	3.11	2.89	2.68	2.78	1.88	1.38	2.53
6	1.50	2.24	2.44	2.84	2.68	2.54	2.56	2.64	2.65	2.95	1.89	1.44	2.36
7	1.60	2.28	2.24	2.15	1.68	1.45	1.53	1.84	1.92	2.40	1.88	1.86	1.86
8	1.40	1.46	1.26	1.17	0.65	0.40	0.54	0.67	0.78	1.08	1.21	1.14	•
9	0.78	0.57	0.85	0.28		-0.52	-0.36	-0.20	-0.18	1	0.26	0.52	0.08
10	0.02	-0.89	-0.46		-1.06			-1.05	-1.08 ,	1	-0.56	-0.22	
11	-0.6 8	-1.20	-1.88	-1.54	-1.74	-1.98	-1.74	-1.84	-1.90	-1.96	-1.27	-0.92	-1.50
Noon.	-1.21	-1.77	-1.97	-2.16	-2.24	-2.51	-2.26	-2.84	-2.45	-2.61	-1.77	-1.28	-2.00
1	-1.73	-2.36	-2.4 5	-2.86	-2.71	-3.06	-2.66	-2.67	-2.8 8	-8.14	-2.26	-1.63	-2.53
2	-2.04	-2.66	-2.74	-8.29	-3.11	-3.82	-2.97	-3. 01	-3.22	-8.45	-2.52	-1.84	-2.85
8	-2.10	-2.82	-8.07	-3.42	-8.86	-3.40	-3.15	-3.11	-3.26	-8.45	-2.4 8	-1.85	1
4	-1.98	-2.69	-2.99	-3.44	-3.46	-3.44	-8.06	-2.9 8	-8.17	-3.33	-2.24	-1.63	-2.87
5	-1.80	-2.18	-2.52	-3.14	-3.26	-3.05	-2.94	-2.70	-2.77	-2.46	-1.46	-1.10	-2.41
6	-0.91	-1.87	-1.60	-2.49	-2.46	-2.47	-2.80	-2.08	-1.77	-1.83	-0.82	-0.64	1.68
7	-0.51	-0.80	-0.88	-1.28	-1.28	-1.88	-1.44	-1.02	-0.76	-0.52	-0.83	-0.81	-0.87
8	-0.20	-0.21	-0.20	-0.29	-0.06	0.06	0.08	0.01	0.28	0.18	-0.14	-0.04	
9	0.07	0.11	0.90	0.35	0.65	0.82	0.57	0.60	0.81	0.65	0.29	0.09	0.49
10	0.88	0.48	0.77	0.93	1.24	1.37	1.08	1.09	1.88	1.24	0.45	0.27	0.88
11	0.56	0.75	0.96	1.44	1.74	1.91	1.55	1.44	1.64	1.63	0.79	0.40	1.28
Mean.	0.80	1.12	5.18	8.75	12.18	16.22	18.19	17.52	14.66	8.72	3.67	0.58	

NORTH AMERICA. — PHILADELPHIA. Lat. 39° 58' N. Long. 75° 11' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — GUYOT.

Degrees of Fahrenheit.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midnight.	1.47	2.90	2.90	4.18	4.68	5.28	4.70	4.87	4.47	8.80	2.70	1.40	8.57
1	2.13	8.87	3.63	4.88	5.25	5.98	5.57	4.98	4.60	4.17	2.78	1.83	4.08
2	2.20	3.57	4.17	5.88	5.95	6.45	6.10	5.48	5.00	4.87	8.20	2.20	4.59
8	2.57	4.48	4.50	6.28	6.68	7.28	6.58	5.50	5-47	5.27	8.87	2.63	5 03
4	2.80	4.67	4.70	6.75	7.88	7.68	6.90	6.17	5.77	5.77	8.90		5.45
5	8.07	4.83	1 1	8.95	7.48	7.40	7.03	6.50	6.03	6.23	4.10	8.10	5.70
6	3.40	5.10		6.45	5.98	5.78	5.80	5.93	5.97	6.60	4.23	8.23	5.32
7	3.63	5.17	5.03	4.90	8.80	8.28	8.50	4.13	4.83	5.37	4.20	8.07	4.20
8	8.17	3.83	2.80	2.50	1.48	0.90						2.57	2.16
9	1.77	1.33	0.80	0.58			-0.77				0.57	1.17	0.19
10	0.07			-1.58			-2.2 0					-0.50	
11	-1.40	-2.63	-3. 10	-3.40	-8.90	-4.83	-3. 87	-4.18	-1.27	-4.48	-2. 87	-2.07	-3.87
Noon.												-2.87	
1												-3.67	
2												-4.13	
8	-4.70	-6.80	-6.90	-7.68	-7.55	-7.68	-7.08	-7.60	-7.88	-7.80	-5.60	-4.17	-6.64
4	-1.43	-6.00	-6.73	-7.65	-7.78	-7.78	-6.88	-6 .70	-7.18	-7.53	-5.07	-8.67	-6.44
5	-2.90	-4.87	-5.67	-7.00	-7.38	-6.85	-6 .57	-6.07	-6.23	-5.57	-3.80	-2.47	-5.40
6	-2.03	-3.03	-8.60	-6.55	-5.58	-5.55	-5.18	-4.57	-8.97	-3.06	-1.87	-1.43	-3.77
7	-1.13	-1.77	-1.97	-2.70	-2.88	-8.10	-3.20	-2.30	-1.70	-1.20	-0.77	-0.70	-1-95
8	-0.48	-0.48	-0.48	-0.60	-0.18	0.15	0.08	0.08	0.63	0.87	0.15	-0.10	-0.11
9	0.17	0.80	0.73	0.85	1.48	1.85	1.38	1.87	1.83	1.48	0.63	0.20	1.01
10	0.77	1.18	1.73	2.15	2.80	8.10	2.47	2.47	3.00	2.77	1.00	0.60	2.00
11	1.27	1.78	2.17	8.30	8.98	4.80	3.58	8.23	8.70	8.68	1.77	0.90	2.78
6, 6	0.69	1.04	0.95	0.45	0.20	0.09	0.34	0.68	1.00	1.79	1.18	0.90	0.78
7, 7	1.25	1.70		1.10	0.46	0.09	0.15	0.92	1.32		1.72		1.13
8, 8	1.37	1.45		0.85	0.68	0.58	0.87	0.77	1.01	1.38	1.35	1.21	1.04
9, 9	0.97	0.82	0.76	0.72	0.82	0.85	0.28	0.47	0.72	0.53	0.60	0.69	0.66
10, 10	0.42	0.15	0.85	0.81	0.21	0.18	0.14	0.05	0.29	0.05	-0 .18	0.05	0.17
7, 2, 9	-0.22						-0.61					-0.29	1
6, 2, 8	-0.53		-0.87	- 1		-0.52		-0.29				-0.67	
6, 2, 10	-0.18	0.09		0.74								-0.10	
6, 2, 6	-1.07	-0.72	-1.42	-2.07	-2.19	-2.42	-1.48	-1.82	-1.78	-1.41	-1.10	-0.78	-1.44
7, 2	, ,											-0.53	
8, 2										1		-0.78	1
- 1				,								-0.55	1
7, 1	-0.12	-0.05	-0.24	-0.74	-1.14	-1.80	-1.22	-0.94	-1.07	-0.87	-0.45	-0.80	-0.7B
, 12, 3, 9													

N. AMERICA. — FRANKFORT ARSENAL. Lat. 39° 57′ N. Long. 75° 8′ W. Greenw. Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	1.84	1.46	1.75	1.87	2.60	8.41	8.07	2.69	2.63	2.40	1.18	1.84	2.15
2	1.51	1.73	2.13	2.33	8.05	8.73	8.51	8.04	8.05	2.67	1.27	1.50	2.46
8	1.82	1	2.56	I	1	8.92	8.88	8.32	8.49	2.94	1.41	1.66	2.77
4	2.18	1	2.90		ı	8.84	8.84	8.86	3.73	3.13	1.51	1.80	2.94
5	2.81	2.46	2.95	8.31	8.82	3.36	3.40	2.99	3.54	8.12	1.73	1.87	2.86
6	2.25	2.85	2.62	2.88	2.65	2.46	2.52	2.21	2.84	2.82	1.38	1.80	2.39
7	1.88	2.01	1.91	1.94	1.66	1.26	1.84	1.15	1.71	2.19	1.06	1.52	1.64
8	1.22	1.83	0.94	0.85	0.57	-0.03	0.08	0.01	0 86	1.26	0.58	0.97	0.68
9	0.84	0.80	_0.07	-0.20	-0.45	-1.20	-1.06	-1.00	-0.96	0.12	-0.02	0.18	-0.84
10								-1.78					
11	-1.54							-2.34					
Noon		4						-2.78					
110011.	2.00		""				5.10		""	0.00			2.00
] 1]	-2.85	-8.01	-2.74	-2.72	-8.07	-8.51	-3.58	-8.16	-8.86	-4.05	-2.88	-2.87	-8.15
2	-8.02	-8.18	-3.01	-3.19	-3.52	-8.77	-8.87	-8.48	-4.07	-4.86	-2.54	-2.89	-8.41
8	-2.92	-2.98	-8.10	-8.58	-8.78	-8.89	-8.94	-3.61	-4.02	-4.22	-2.40	-2.54	-3.41
4	-2.58	-2.44	-2.95	-8.55	-8.70	-8.75	-3.67	-3.42	-3.68	-3.66	-1.96	-1.94	-8.10
1	}	ł	l	ł	į ·	1		1					
5	11	ı						-2. 81				1	
6					1			-1.88				-0.55	
7	-0.87	-0.46	-0.92		1			-0.67			0.14		-0.68
8	0.29	0.12	-0.06	0.02	-0.10	0.07	0.28	0.48	0.66	0.48	0.69	0.42	0.27
9	0.76	0.66	0.61	0.85	0.80	1.17	1.17	1.29	1.49	1.17	1.02	0.71	0.98
10	1.02				1	2.02	1.79	1.84	1.96	1.66	1.15	0.90	1.42
11	1.18		1.31		ı	2.61	2.24	2.15	2.18	1.96	0.91	1.06	1.67
Midn	1.19		1.48			8.04	2.68	2.40		2.18	1.15	1.20	1.88
Miuit	1.15	1.50	1.40	1.02	2.01	0.04	2.00	2.40	2.00	2010	1.10	1.20	1.00
			1										
6. 6	0.56				ŀ			0.19		0.58			
7. 7	0.76	0.78	0.50					0.24	0.62		0.60		0.51
8. 8	0.76		0.44	0.48	0.24		0.18	0.22		0.85	0.63		0.48
9. 9	0.55		0.27	0.33		-0.02	0.06	0.14	0.26	0.64	0.50		0.32
10.10	0.20	0.11	0.03	0.18	0.07	-0.05	-0.08	0.08	-0.05	0.26	0.28	0.07	0.08
7. 2. 9	-0.18	-0.17	-0.18	-0.18	-0.85	-0.45	-0.45	-0.85	-0.29	-0.88	-0.15	-0.22	-0.27
6. 2. 8	-0.16	!		-0.11				-0.28					
6. 2.10	0.08	1	0.22		l .				l I		1	-0.06	0.14
6. 2. 6	-0.64							-1.08				ł	
U. 4. U		J.65	0.,2	5.00					2.03				
7. 2	-0.57	-0.59	-0.55	-0.63	-0.98	-1.26	-1.27	-1.17	-1.18	-1.09	-0.74	-0.69	-0.89
8. 2								-1.74					
8. 1								-1.58					
7. 1	-0.49	-0.50	-0.42	-0.89	-0.71	-1.18	-1.12	-1.10	-1.08	-0.93	-0.66	-0.68	-0.76
	1			i :	i			ł	Į	l		1	ł
	-1.03	1	1										
7. 2.2(9)	0.10	0.04	-0.03	0.11	−0.07	-0.04	-0.05	0.06	0.16	0.04	0.14	0.01	0.04
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N. AMERICA. — FRANKFORT ARSENAL. Lat. 39° 57' N. Long. 75° 8' W. Greenw. Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Monn.
Morn. 1	3.02	8.29	8.94	4.21	5.85	7.67	6.91	6.05	5.92	5.40	2.66	3.02	4.84
2	8.40	8.89	4.79	5.24	6.86	8.89	7.90	6.84	6.86	6.01	2.86	3.38	5.54
8	4.10	1	5.76	6.48	7.72	8.82	8.62	7.47	7.85	6.62	8.17	3.74	6.23
4	4.79	5.02	6.58	7.40	8.03	8.64	8.64	7.56	8.39	7.04		4.05	6.62
]													
5	5.20	5.54	6.64	7.45	7.74	7.56	7.65	6.78	7.97	7.02	3.89	4.21	6.44
6	5.06	5.29	5.90	6.87	5.96	5.54	5.67	4.97	6.39	6.35	8.11	4.05	5.38
.7	4.23	4.52	4.30	4.87	8.74	2.84	8.02	2.59	3.85	4.93	2.39	3.42	3.69
8	2.75	2.99	2.12	1.91	1.28	-0.07	0.18	0.02	0.81	2.84	1.81	2.18	1.53
9	0.77	0.68	-0.16	-0.45	-1.01	-2.70	-2.39	-2.25	-2.16	0.27	-0.05	0.41	-0.77
10	-1.40	-1.62	1	-2.86					-4.64	-2.54		-1.71	-2.86
11			-3.96					-5.27				-8.83	-4.59
Noon	-5.18	-5.85	-5.22	-5.00	-5.29	-7.13	-7.11	-6.26	-7.8 1	-7.54	-4.41	-5.51	-6.03
1	-6.41	_0 77	_0 14	<i>a</i> 19	_# 01	_7 00	^_	_7 11	_0 60	-0 11	_K 96	-6.46	-7.09
2												-6.58	
	-6.57							-8.12				-5.72	
								-7.70				-1.37	I I
7	0.00	0.10	0.03	1.00	0.00		0.20	••••		0.2.			
5	-4.28	-4.21	-5.63		-7.2 0			-6.82	-6.39	-6 .19	-8.42	-2.77	-5.63
6	-2.57	-2.50	-4.01	-5.02	-5.20	-5.24	-4.50	-4.12	-3.87		-1.26		-3.60
7	-0.83	-1.04	-2.07	-2.45				-1.51	-1.08	-1.22	0.32		-1.42
8	0.65	0.27	-0.14	0.05	-0.23	0.16	0.63	0.97	1.49	0.97	1 55	0.95	0.61
9	1.71	1.48	1.87	1.91	1.80	2.63	2.63	2.90	3.35	2.63	2.80	1.60	2.21
10	2.30	2.09	2.36	1.97	3.22	4.55	4.03	4.14	4.41	8.74	2.59	2.03	8.20
11	2.54	2.66	2.95	3.38	4.16	5.87	5.04	4.84	4.91	4.41	2.05	2.39	3.76
Midn	2.68	8.06	8.83	3.65	4.52	6.84	5.92	5.40	5.29	4.91	2.59	2.10	4.23
6. 6	1.26	1.40	0.95	0.68	0.88	0.16	0.59	0.43	1.26	1.31	0.92	1.40	0.90
7. 7	1.71	1.76	1.13	0.95	0.54	0.11	0.59	0.54	1.40	1.87	1.85	1.71	1.15
3.8	1.71	1.62	0.99	0.97	0.54	0.05	0.41	0.50	1.15	1.91	1.42	1.58	1.06
9. 9	1.24	1.08	0.61	0.74	1	-0.05	0.14	0.82	0.59	1.44	1.13	0.99	0.72
10.10	0.45	0.25	0.07	0.29		-0.11			-0.11	0.59	0.52	0.16	0.18
7. 2. 9	-0.29			1				-0.79				-0.50	! !!
6. 2. 8	-0.86			1	-0.72							-0.50	;
6. 2.10	0.18	0.07		0.72	0.43	0.54	0.84		0.54	0.09	0.00		0.32
6. 2. 6	-1.44	-1.46	-1.62	-1.94	-2.89	-2.72	-2. 52	-2.32	-2.21	-2.39	-1.25	-1.24	-1.96
7. 2	-1.28	-1.88	1									-1.55	• 11
8. 2	-2.08	-2.09	-2.84									-2.16	
8. 1	-1.85		-2.03									-2.14	
7. 2	-1.10	-1.18	-0.95	-0.88	-1.60	-2.54	-2.52	-2.27	-2.43	-2.09	-1.49	-1.53	-1.71
9.12.3.9	-2.82	-2.57	-2.75	-2.88	-8.26	-3.98	-3.91	-3.44	-3.92	-3.53	-1.80	-2.32	-3.06
7. 2.2(9)	0.23		1		1	-0.09	ı			0.09	•		
Dail.ext.	-0.81	-0.81	-0.18	-0.27	-0.25	0.04	-0.11	-0.29	-0.38	-1.89	-0.92	-1.15	-0.51
200000	"												انتنيا

VI.

N. ANERICA. - Toronto. Lat. 43° 39' 35" N. Long. 79° 21' 30" W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenhelt.

Hours.	Jan.	Feb.	March.	April	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	1.87	0.92	8.04	4,48	5.90	5.94	6.30	5.06	5.74	4.16	1.91	1.04	8.87
2	2.16	1.33	8.56	5.11	6.64	6.62	7.18	5.68	6.68	4.68	2.14	1.18	4.41
8	2.89	1.91	4.19	5.76	7.36	7.29	8.01	6.82	7.68	5.04	2.89	1.40	5.02
4	2.68	2.66	4.75	6.17	7.65	7.56	8.44	7.61	8.19	5.20	2.61	1.78	5.45
1 1													
5	8.02	8.40	4.95	5.94	7.07	6.98	7.88	7.49	7.94	5.02	2.68	2.16	5.38
6	3.29	8.92	4.61	4.97	5.49	5.38	6.14	6.14	6.71	4.48	2.52	2.89	4.68
7	8.26	8.98	8.65	3.38	8.17	8.04	3.49	3.67	4.52	8.44	2.05	2.27	8.33
8	2.72	8.40	2.12	1.42	0.68	0.48	0.52	0.68	1.78	1.91	1.15	1.71	1.55
1 1					i								
9	1.58	2.83	0.29	-0.50	1			-2.09	-1.06		-0.07	0.79	-0.36
10	0.00	0.61	-1.60	-2.07	1	_		-4.14	-3.62	-2.25	-1.46	1	-2.12
11	-1.71	-1.15	-3.26	-3.26				-5.88		-4.39	-2.79	-1.44	-3.58
Noon.	-3 .11	-2.66	-4.55	-4.19	-5.00	-5.18	-5.90	-5.96	-7.25	-6.12	-3.78	-2.30	-4.66
1	-3.89	-8.67	-5.86	-5.00	-5.99	-5.94	-6.59	-6.50	-8.33	-7.11	-1.28	-2.77	-5 45
2	-8.98	-4.07	-5.72	-5.76			-7.47		-8.89		-4.14	-2.86	-5 94
И	-3.53	-8.92	-5.60		-8.15		-8.28	1	-8.87		-8.51	-2.66	-6.08
4		-8.88	-5.02				1		-8.12				
- 1		0.00	0100	0.10			0.00	*****	****	3120			0.12
5	-2.14	-2.63	-4.08	-5.94	-7.76	-7.43	-7.83	-6.95	-6.59	-8.53	-1.44	-1.71	-4.84
6 ∦	-1.62	-1.89	-2.75	-4.66		-5.65		-5.00	-1.48	-1.91	-0.45	-1.18	-3.44
7	-1.24	-1.24	-1.31	-2.81	-8.08	-3.04	-8.17	-2.25	-1.94	-0.50	0.82	-0.54	-1.78
8	-0.88	-0.68	0.05	-0.77	-0.16	-0.18	-0.18	0.65	0.48	0.65	0.86	0.02	-0.02
11													
9	-0.48	-0.25	1.15	1.06	2.80	2.30	2.39	2.97	2.80	1.58	1.17	0.47	1.42
10	0.16	0.11	1.89	2.41	3.94	3.98	4.14	4.82	3.58	2.25	1.87	0.81	2.41
11	0.88	0.38	2.84	3.26	4.82	4.98	5.11	4.77	4.87	2.90	1.53	0.97	8.02
Midn	1.42	0.68	2.66	3.85	5.88	5.45	5.64	4.84	5.00	8.56	1.71	1.01	3.42
ļ	- 1												
امما	0.88			0.10	0.10			0.56		V 80	• •	0.00	0.01
6. 6 7. 7	1.01	1.01 1.27	0.95	0.10	-0.18 -0.05	0.14	0.11	0.72	1.18	1.28 1.49	1.04 1.19	0.63	0.61 0.81
8. 8	0.92	1.37	1.17 1.08	0.29	0.27	0.00	0.16	0.72	1.10	1.49	1.19	0.86	0.77
9. 9	0.59	0.99	0.72	0.29	0.41	0.12	0.16 0.14	0.45	0.68	0.74	0.56	0.68	0.54
10.10	0.07	0.36	0.72	0.16	0.43	0.27	0.07	0.09	-0.02	0.00	-0.05	0.23	0.14
10.10	0.07	0.30	0.14	0.10	0.40	V-21	0.07	0.00	-0.02	0.00	-0.00	0.20	0.14
7. 2. 9	-0.88	-0.11	-0.82	-0.45	-0.56	-0.52	-0.54	-0.16	-0.70	-0.77	-0.32	-0.05	-0.41
- 11	-0.52	-0.27	-0.36	-0.52		-0.56	-0.50		-0.59		-0.25	-0.16	
LI LI	-0.18	-0.02	0.27	0.54	0.77	0.83	0.95	1.18	0.47	-0.18	-0.09	0.11	0.38
6. 2. 6			-1.28	-1.82			-2.48			-1.55	-0.70		
		2.00											
7. 2	-0.86	-0.05	-1.04	-1.19	-2.00	-1.94	-2.00	-1.78	-2.18	-1.91	-1.06	-0.29	-1.81
	-0.68	,	-1.80		-8.24			-8.22		-2.68		-0.59	
31	-0.59	-0.14	-1.62	-1.80	-2.66	-2.77	-3.04		-8.29	-2.61	-1.58	-0.54	-1.96
	-0.82		-0.86						-1.91		-1.18	-0.25	-1.06
li li	1												
	-1.87	-1.15	-2.18	-2.5 0		-3.13	-3.49	-3.20	-8.71	-2.79	-1.55		-2.43
7. 2.2(9)	-0.41	-0.16	0.07	-0.07	0.16	0.18	0.20	0.63	0.07	-0.18	0.07	0.09	0.05

N. America. — Toronto. Lat. 43° 89' 35" N. Long. 79° 21' 30" W. Greens.

Corrections to be applied to the Means of the Hours of Observation to obtain the true
Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Houm.	Jan.	Pob.	March.	April.	May.	June.	July.	Aug.	Sopt.	Ocs.	Nov.	Dec.	Mess
Morn. 1	0.88	0.41	1.85	1.97	2.62	2.64	2.80	2.25	2.55	1.85	0.85	0.46	1.72
2	0.96	0.59	1.58	2-27	2.95	2.94	8.17	2.57	2.97	2.08	0.95	0.50	1.96
8	1.06	0.85	1.86	2.56	8.27	8.24	8.56	3.08	8.29	2.24	1.06	0.62	2.23
4	1.19	1.18	2.11	2.74	8.40	3.86	8.75	3 38	8.64	2.81	1.16	1	2.42
5	1.84	1.51	2.20	2.64	8.14	8.10	8.50	3.23	8.58	2.23	1.19	0.96	2.39
6	1.46	1.74	2.06	2.21	2.44	2.89	2.78	2.78	2.96	1.99	1.12	1.06	2.08
7	1.45	1.77	1.62	1.50	1.41	1.85	1.55	1.63	2.01	1.53	0.91	1.01	1.48
8	1.21	1.51	0.94	0.68	0.80	0.19	0.23	0.80	0.79	0.85	0.51	0.76	0.69
9	0.70	0.99	0.18	-0.22	-0.67	-0.82	-0.94	-0.93	-0.47	-0.02	-0.03	0.85	-0.16
10	-0.00	0.27										-0.15	
1 11	-0.76	-0.51						-2.87		•	,		
Noon	-1.88	-1.18						-2.65					
1			-2.88							-8.16			
2	-1.77	-1.81	-2.54	-2.56	-8.18	-8.06	-8.32	-8.16	-8.95	-3.22	-1.84	-1.27	-2.64
8	-1.57	-1.74	-2.49	-2.82	-8.62	-8.44	-3.68	-3.42	-8.9 4	-2.90	-1.56	-1.18	-2.7 0
4	-1.26	-1.50	-2.28	-2.88	-8.78	-3. 59	-8.80	-8.47	-8.6 1	-2.30	-1.12	-0.99	-2.54
5	-0.95	-1.17	-1.79	-2.64	-8.45	-8.80	-8.48	-3.09	-2.93	-1.57	-0.64	-0.76	-2.15
6	-0.72		-1.22	-2.07			-2.64				-0.20	1	-1.53
7		-0.55	-0.58	-1.25	-1.87	-1.35	-1.41	-1.00	-0.86	-0.22			-0.77
8	-0. 39	0.80	0.02	-0.84	-0.07	-0.08	-0.08	0.29				0.01	
9	-0.19	-0.11	0.51	0.47	1.02	1.02	1.06	1.82	1.02	0.68	0.52	0.21	0.63
10	0.07	0.05	0.84	1.07	1.75	1.77	1.84	1.92	1.59	1.00	0.61	0.36	1.07
11	0.37	0.17	1.04	1.45	2.14	2.19	2.27	2.12	1.94	1.29	0.68	0.48	1.34
Midn	0.68	0.28	1.18	1.71	2.87	2.42	2.53	2.15	2.22	1.58	0.76	0.45	1.52
6. 6	0.87	0.45	0.42	0.07	-0.08	0.06	0.05	0.25	0.50	0.57	0.46	0.28	0.27
7. 7	0.45	0.61	0.52	0.18	0.02	0.00	0.07	0.82	0.57	0.66	0.58	9.38	0.36
8. 8	0.41	0.61	0.48	0.15	0.12	0.06	0.07	0.80	0.49	0.57	0.45	0.38	0.34
9. 9	0.26	0.44	0.82	0.13	0.18	0.10	0.06	0.20	0.28	0.38	0.25	0.28	0.24
10.10	0.08	0.16	0.06	0.07	0.19	0.12	0.03		-0.01	i	-0.02	0.10	0.06
7. 2. 9	-0.17	-0.05	-0.14	-0.20	-0.25	-0.28	-0.24	-0.07	-0.31	-0.34	-0.14	-0.02	-0.18
6. 2. 8	-0.23	-0.12	-0.16	-0.28	-0.27	-0.25	-0.22	-0.05	-0.26	-0.31	-0.11	-0.07	-0.19
6. 2.10	-0.08	-0.01	0.12	0.24	0.84	0.87	0.42	0.50	0.21	-0.08	-0.04	0.05	0.17
6. 2. 6	-0.84	-0.80	-0.57	-0.81	-1.11	-1.06	-1.08	-0.88	-0.98	-0.69	-0.31	-0.24	-0.70
7. 2	-0.16	-0.02	-0.46	-0.53	-0.89	-0.86	-0.89	-0.77	-0.97	-0.85	-0.47	-0.13	-0.58
8. 2	-0.2 8	-0.15	-0.8 0	-0.97	-1.44	-1.44	-1.55	-1.48	-1.58	-1.19	-0.67	-0.26	-0.96
8. 1	-0.26	-0.06	-0.72	-0.80	-1.18	-1.28	-1.85	-1.30	-1.46	-1.16	-0.70	-0.24	-0.87
7. 1	-0.14	0.07	-0.88	-0.36	-0.63	-0.65	-0.69	-0.68	-0.85	-0.82	-0.50	-0.11	-0.47
9.12.8.9	-0.61	-0.51	-0.97	-1.11	-1.37	-1.89	-1.55	-1.42	-1.65	-1.24	-0.69	-0.41	-1.08
7. 2.2(9)	1	-0.07		-0.03	1					-0.08	l		
Dail. ext.	-0.16	-0.02	-0.17	-0.07	-0.19	-0.12	-0.03	-0.05	-0.16	-0.46	-0.36	-0.11	-0.14

VIIL

NORTH AMERICA. — TORONTO. Lat. 43° 40' N. Long. 79° 21' W. Greenw. Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — LEFROY.

Degrees of Fahrenhelt.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec	Year.
Midnight.	1.47	1.78	2.63	8.22	5.02	5.15	6.87	5.88	5.96	8,22	1.80	0.90	3.57
1	1.95	2.09	8.11	8.79	5.98	6.00	7.13	6.06	4.57	8.80	2.10	1.50	4.00
2	2.05	2.46	3.47	4.48	6.77	6.70	7.68	6.69	5.17	4.13	2.86	1.85	4.48
3	2.20	2.82	8.76	5.08	7.45	7.50	8.41	7.29	5.59	4.81	2.66	1.96	4.92
4	2.28	8.20	4.07	5.38	7.93	8.06	9.08	7.68	6.18	4.61	2.85	2.04	5.27
5	2.46	8.62	4.85	5.75	7.88	7.88	9.02	7.89	6.77	4.77	2.76	2.07	5.43
6	1.83	4.23	4.75	5.48	5.40	5.21	5.92	6.57	6.17	4.71	2.52	2.89	4.60
7	1.94	4.84	8.98	3.22	2.48	2.41	2.88	8.28	3.6 8	8.94	2.52	2.55	8.05
8	1.66	8.29	1.89	1.09	0.06		-0.81	0.21	1.02	1.66	1.53	2.12	1.25
9	0.63	1.02		-1.01		-1.82			-1.52	-1.01	0.01	0.92	-0.82
10	-0.59	-0.9 5	-1.91	-2.45		-3.49		-4.18	-8.47	-2.98	-1.41	-0.53 -1.72	-2.47 -8.77
11	-1.70	-2.44	-3.14	-8. 85	-4.92	-4.77	-0.49	-5.57	-4.80	-4.33	-2.44	-1.72	-8.77
Noon.	-2.48	-3.5 6	1	-4.86		-5.88		-6.89				-2.52	1
1 (-2.92		•		-6.83		1 1	-7.11			-8.74	-3.06	
2	-3.20	-4.88					-8.26		1	1		-3.31	1 1
8	-3.16	-4.90	-5.15	-6.16	-7.ZU	-7.87	-8.84	-7.98	-7.01	-0.85	-3.61	-8. 18	-5.82
4	-2.68	-4.47	-4.65	-5.81	-7.17	-7.60	-8.25	-7.79	-6.7 5	-5.17	-2.88	-2.47	-5.47
5	-1.68			-5.12		-7.18	-7.93	-7.2 0	-5.78	-3.40		-1.49	-4.61
6	-0.90	-1.87	1		-5.05	-5.78	-6.57	-5.89	-8 .16	-1.87		-0.82	-8.12
7	-0.40	-0.98	0.91	-0.91	-2.19	-2.99	-3.2 8	-1.64	-0.48	-0.25	-0.15	-0.47	-1.22
8	-0.12	-0.18	0.03	0.66	0.48	0.88	0.68	1.23	0.81	0.48	0.19	-0.12	0.88
9	0.07	0.52	1.00	1.78	2.81	2.44	2.09	2.70	1.90	1.25	0.44	0.18	1.46
10	0.44	1.06	1.68	2.59	3.29 4.20	8.80	4.24 5.21	8.78	2.94 8.61	1.97 2.68	0.78 1.13	0.47	2.24
11	0.77	1.60	2.01	8.07	4.20	4.76	5.21	4.54	8-01	2-00	1.15	0.08	2.00
6, 6	0.46	1.18	1.20	1.08	0.17	-0.26	-0.82	0.59	1.50	1.67	1.88	0.78	0.74
7, 7	0.77	1.67		1.14	0.12		-0.45	0.82	1.62	1.84	1.18	1.04	0.91
8,8	0.77	1.58	0.96	0.87	0.24		0.18	0.72	0.91	1.45	0.98	1.15	0.82
9, 9	0.85	0.77	0.87	0.38	0.10	0.81	0.80	0.22	0.19	0.10	0.22	0.55	0.82
10, 10	-0.07	0.05	-0.14	0 .07	-0.26	0.25	0.18	-0.22	-0.26	-0.48	-0.81		-0.11
6, 2, 10	-0.81	0.14	0.86	0.64	0.52	0.66	0.63	0.89	0.72	0.21		-0.15	0.81
7, 2, 9	-0.40	-0.01	-0.09		-0.80	-0.78	-0.96	-0.55	-0.46	-0.28	-0.29	-0.19	-0.43
9, 12, 8, 9	-1.23	-1.78	-2.01	-2.56	-8.22	-8.16	-3.61	-8.48	-8.14	-2.74	-1.68	-1.14	-2.48
Moan.	25.82	23.70	29.79	41.99	52.92	60.67	66.89	65.86	57.55	44.14	86.18	27.40	44.37

NORTH AMERICA. - TORONTO. Lat. 43° 40' N. Long. 79° 21' W. Gr.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Resumur.

Hour.	Jan.	Peb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	6.6 8	0.81	1.10	1.45	3.24	2.86	2.91	2.43	1.76	1.44	0.81	0.40	1.53
1	0.88	0.98	1.81	0.78	2.62	2.67	8.29	2.72	2.08	1.71	0.94	0.66	1.80
2	0.92	1.13	1.48	2.08	2.99	2.98	8.54	8.02	2.29	1.85	1.06	0.83	2.01
8	0.99	1.32	1.61	2.17	8.81	8.82	3.86	3.32	2.49	1.92	1.20	0.88	2.20
4	1.08	1.45	1.78	2.86	8.52	8.58	4.14	8.48	2.76	2.06	1.28	0.90	2.36
5	1.11	1.61	2.01	2.52	8.49	3.49	4.16	8.57	8.04	2.18	1.23	0.91	2.44
6	0.79	1.86	2.13	2.47	2.40	2.82	2.74	2.92	2.74	2.04	1.11	1.09	2.05
7	0.83	1.92	1.75	1.45	1.08	1.07	1.11	1.60	1.60	1.70	1.11	1.16	1.26
8	0.73	1.47	0.87	0.45	0.09	0.08	-0.05	0.15	0.38	0.70	0.64	0.97	0.56
9	0.80	0.44	-0.10	-0.48	-0.94	-0.81	-1.08	-0.96	-0.69	-0.49	-0.04	0.45	-0.36
10	-0.25	-0.45	-0.87	-1.11	-1.69	-1.55	-1.78	-1.84	-1.57	-1.85	-0.68	-0.2 0	-1.11
11	-0.77	-1.16	-141	-1.72	-2.20	-2.12	-2.47	-2.48	-2.20	-1.96	-1.13	-0.75	-1.70
Noon.	-1.12	-1.69	-1.87	-2.18	-2.62	-2.61	-8.05	-8.04	-2.64	-2.86	-1.48	-1.11	-2.15
1	-1.84	-2.07	-2.16	-2.60	-8.08	-2.98	-8.46	-8.25	-2.90	-2.55	-1.66	-1.42	-2.4 5
2	-1.46	-2.25	-2.41	-2.76	-8. 18	-8.12	-3.84	-8.51	-8.08	-2.70	-1.69	-1.49	-2.62
8		-2.24		-2.80	-8.21	-8.29	-8.92	-8.66	-8.09	-2.60		-1.38	-2.63
4	-1.21	-2.00		-2.62			-8.93	-3.60	-3.00	-2.28	1		
5	-0.77	-1.47	-1.78	-2.80	-8.02	-8.13	-3.72	-8.35	-2.57	-1.50	-0.68	-0.67	-2.08
6	-0.40	-0.82	-1.08	-1.50	-2.24	-2.55	-3.06	-2.51	-1.38	-0.59	-0.82	-0.86	-1.40
7	-0.17	-0.88	-0.88	-0.37	-0.96	-1.88	-1.54	-0.74	-0.18	-0.10	-0.06	-0.21	-0.53
8	-0.03	0.00	0.05	0.83	0.24	0.18	0.83	0.56	0.89	0.23	0.08	-0.04	0.19
9	0.06	0.28	0.50	0.81	1.02	1.09	1.88	1.26	0.85	0.57	0.20	0.07	0.67
10	0.28	0.53	0.79	1.16	1.45	1.69	1.98	1.72	1.82	0.90	0.36	0.20	1.02
11	0.37	0.76	1.08	1.88	1.86	2.12	2.45	2.07	1.60	1.20	0.52	0.25	1.31
Mean.	-2.97	-3.88	-0.99	4.72	9.29	12.75	15.11	15.00	11.37	5.42	1.88	-2.03	

X.

NORTH AMERICA. — MONTREAL. Lat. 45° 30' N. Long. 73° 22' E. Gr.

						8							
Hour.	Aug.	Sept.	Oct.	Nov.	Dec.	Jan.	Feb.	March.	April.	May.	June.	July.	Year.
Midn.	4.00	8.89	2.88	1.36	1.68	1.10	1.28	1.81	2.52	4.55	5.25	4.39	2.85
2	5.89	4.84	4.01	1.59	1.00	2.36	2.69	2.88	4.87	6.95	7.42	7.17	4.20
4	6.84	5.60	4.84	1.81	1.88	2.88	8.36	5.56	7.09	6.95	7.18	7.57	4.96
6	5.99	4.59	4.98	1.36	1.82	8.54	3.90	5.22	5.56	6.61	5.55	5.46	4.50
8	2.79	2.19	2.52	0.78	0.92	8.10	3.22	8.30	8.44	3.06	0.88	0.60	2.24
10	-1.74	-1.48	-0.99	-0.41	0.21	-0.21	-0.81	-0.08	-0.79	-0.97	-1.75	-2.85	-0.93
Noon.	-5.63	-5.43	-1.22	-1.87	-1.22	-2.82	-8.50	-4.28	-5.01	-7.10	-5.17	-5.46	-4.30
2	-7.98	-6.60	-6.96	-2.87	-2.54	-4.07	-5.48	-6.49	-5.99	-8.76	-7.72	-7.36	-6.02
4	-7.72	-6.70	-5.62	-2.52	-8.22	-3.88	~8.60	-5.96	-5.79	-6.35	-7.00	-7.51	-5.65
6	-5.68	-2.80	-2.79	-1.04	-1.30	-1.77	-1.50	-8.48	-8.88	-3.87	-5.02	-5.40	-3.20
8	-0.70	0.10	-0.25	0.08	0.02	-0.90	-0.59	-1.28	-0.81	-1.61	-1.10	-0.67	-0.65
10	1.99	2.89	1.42	1.18	0.89	0.17	0.22	-0.80	0.64	-1.87	2.47	2.64	1.30
Mean.	66.40	57.70	48.31	30.39	23.42	8.10	20.84	27.81	42.27	56.61	64.88	70.39	43.01

X.

NORTH AMERICA. - MONTREAL, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year.

Degrees of Fahrenheit.

Hour.	Aug.	Sept.	Oct.	Nov.	Dec.	Jan.	Feb.	March.	April.	May.	June.	July.	Year.
A.M.1	5.03	4.92	2.58	1.16	0.88	1.48	1.61	4.38	8.12	4.85	4.55	5.07	3.80
8	5.99	5.20	8.61	1.58	1.79	1.30	2.72	5.18	5.14	6.51	5.10	6.80	4.25
5	6.44	5.43	4.45	2.08	2.21	1.87	8.95	6.84	6.54	6.56	6.30	7.76	5.05
7	2.10	8.47	3.61	2.01	2.08	1.96	5.22	7.07	3.84	3.56	4.72	8.04	3.56
9	-0.58	0.78	0.77	0.63	1.14	1.16	3.99	2.96	0.71	0.50	-0.02	0.22	1.02
11	-3.61	-2.20	-2.78	-1.85	-0.49	-1.08	-0.17	-2.51	-2.48	-2.79	-3.42	-3.21	-2.17
P.M.1	-6.61	-5.12	-5.41	-3.47	-2.85	-1.49	-4.80	-7.41	-4.93	-5.78	-5.97	-6.08	-4.95
3	-7.34	-6.63	-5.80	-3.22	-2.78	-2.36	-6.06	-9.03	-6.33	-6.46	-6.93	-8.01	-5.91
5	-5.47	-5.88	-3.15	-1.19	-1.44	-0.63	-4.12	-6.48	-5.63	-6.62	-6.18	-6.53	-4.43
7	-1.45	-0.62	-1.00	-0.44	-0.70	-0.60	-1.23	-2.40	-2.98	-8.50	-8.17	-2.88	-1.74
9	1.58	1.82	0.82	0.18	-0.71	-0.66	-0.96	-0.75	0.44	0.61	1.58	1.17	0.34
11	8.10	8.02	2.47	1.48	0.22	0.61	0.24	1.78	2.06	2.52	8.55	8.39	2.02
Mean.	69.69	57.53	44.70	32.76	15.91	18.96	14.52	22.50	84.47	51.88	65.08	67.42	41.24

XI.

NORTH AMERICA.—SITKA. Lat. 57° 3' N. Long. 135° 18' W. Gr.—Dove.

Degrees of Resumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec	Year.
Midn.	0.33	0.58	0.97	1.51	1.80	1.81	1.68	1.84	1.07	1.19	0.41	0.28	1.08
1	0.84	0.66	1.09	1.68	2.04	2.06	1.88	1.53	1.18	1.11	0.46	0.83	1.20
2	0.85	0.72	1.17	1.81	2.20	2.25	2.04	1.66	1.88	1.18	0.49	0.83	1.29
8	0.51	0.78	1.86	1.89	2.43	2.49	2.16	1.77	1.24	0.64	0.48	0.18	1.83
4	0.45	0.86	1.47	2.02	2.55	2.57	2.20	1.82	1.29	0.68	0.49	0.18	1.38
5	0.45	0.83	1.57	2.07	2.89	2.47	2.95	1.89	1.88	0.70	0.49	0.14	1.52
6	0.45	0.84	1.56	1.89	1.76	1.77	1.67	1.63	1.88	0.78	0.46	0.18	1.26
7	0.52	0.82	1.37	1.18	0.96	1.08	0.96	1.09	1.05	0.58	0.40	0.17	0.85
8	0.48	0.76	0.75	0.81	0.00	0.26	0.26	0.40	0.47	0.58	0.33	0.12	0.39
9	0.89	0.49		-0.63	-0.82	-0.52	-0.58	-0.26	-0.17	0.12	0.23	, ,	-0.15
10	0.16	-0.03		-1.12	-1.85	-1.28	-1.27	-0.95	-0.78	-0.28	0.00	-0.11	-0.64
11	-0.19	-0.60	-1.29	-1.68	-1.75	-1.70	-1.97	-1.57	-1.28	-0.75	-0.3 5	-0.11	-1.11
Noon.	-0.57	-1.05	-1.71	-2.18	-2.17	-2.11	-2.11	-2.04	-1.65	-1.14	-0.72	-0.82	-1.48
1	-0.83	-1.36	-1.74	-2.88	-2.85	-2.8 5	-2.25	-2.83	-1.56	-1.88	-0.84	-0.46	-1.65
2	-0.95	-1.44	-1.99	-2.28	-2 .40	-2.42	-2.81	-2.16	-1.86	-1.42	-1.00	-0.50	-1.78
3	-0.95	-1.47	-1.94	-2 .10	-2.28	-2.81	-2.18	-2.00	-1.72	-1.87	-0.94	-0.44	-1.64
4	-0.78	-1.20	-1.67	-1.91	-2.04	-2.09	-1.94	-1.76	-1.56	-1.18	-0.75	-0.32	-1.43
5	-0.50	-0.85	-1.17	-1.68	-1.78	-1.76	-1.65	-1.43	-1.24	-0.88	-0.45	-0.20	-1.12
6	-0.25	-0.45	-0.82	-1.13	-1.87	-1.48	-1.26	-1.02	-0.64	-0.50	-0.21	-0.10	-0.77
7	-0.15	-0.10	-0.29	-0.48	-0.76	-1.00	-0.81	-0.49	-0.28	-0.16	-0.04	-0.03	-0.88
8	-0.01	0.11	0.13	0.15	-0.23	-0.41	-0.22	0.12	0.19	0.06	0.07	0.01	0.00
9	0.15	0.80	0.44	0.70	0.48	0.27	0.88	0.66	0.52	0.21	0.22	0.12	0.37
10	0.23	0.87	0.64	1.07	1.02	0.97	0.99	0.96	0.76	0.30	0.29	0.19	0.65
11	0.31	0.48	0.84	1.28	1.57	1.46	1.38	1.19	0.90	0.95	0.48	0.22	0.93
Mean.	-1.39	-1.07	0.55	8.51	6.21	9.10	10.24	10.28	7.96	5.26	2.52	1.73	

XIL.

ARCTIC AMERICA. — BOOTHIA FELIX. Lat. 69° 59' N. Long. 92° 1' W. Greens.

Corrections to be applied to the Means of the Hours of Observation to obtain the true
Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

				·									
Hours.	Jen.	Peb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Men.
					•				0.00	0.00	0.00	0.10	
Morn. 1	0.08	0.42	1.61	2.17	2.64	2.88	1.78		0.56			0.12	
j 2	0.10	0.28	1.85	2.25		2.55	1.78	1.80	0.62	0.32	0.18	0.13	1.15
8	0.11	0.25	2.10	2.80	2.61	2.45	1.65	1.17	0.66	0.33	0.29	0.10	1.12
4	0.11	0.21	2.80	2.26	2.28	2.05	1.35	1.02	0.66	0.84	0.31	0.06	1.02
5	0.10	0.22	2.38	2.02	1.76	1.39	0.99	0.86	0.56	0.32	0.24	0.02	0.87
6	0.10	0.26	2.28	1.53		0.65	0.61	0.70	0.46	0.27	0.13	-0.04	0.64
7	0.09	0.29	1.77	0.81	0.35	-0.04	0.26	0.50	0.27	0.17	0.02	-0.07	0.37
8	0.08	0.22	0.98	-0.06	-0.82	-0.68	-0.03	0.24	0.05	0.01	0.01	−0.10	0.04
9	0.06	0.05					l .	-0.10			-0.04	-0.10	
10	0.02	-0.26			-1.54		1	-0.49		-0.41	1	-0.10	1 1
11	-0.02		1			ľ	1	•				-0.11	1 10
Noon	-0.05	-0.87	-3.05	-2.86	-z.46	-2.02	-1.48	-1.16	-0.82	-v.69	-0.82	-0.12	-1.32
1	-0.11	-1.02	-8.22	-8.02	-2.66	-2.22	-1.70	-1.84	-0.98	-0.68	-0.80	-0.14	-1.47
2	1		4		ì	1		-1.38				-0.13	
8	1	-0.78	•					-1.82		•		-0.10	
4	1		1					-1.18		1		-0.05	
-	"""	0.10											1
5	-0.11	-0.14	-1.29	-1.50	-1.45	-1.86	-1.18	-1.01	-0.44	0.01	0.24	0.01	-0.69
6	-0.09	0.13	-0.57	-0.74	-0.88	-0.66	-0.78	-0.78	-0.17	0.14	0.31	0.07	-0.34
7	-0.06	0.82	0.01	0.06	-0.84	-0.01	-0.84	-0.50	0.08	0.22	0.36	0.10	-0.01
8	-0.05	0.43	0.44	0.78	0.20	0.51	0.07	-0.16	0.26	0.25	0.38	0.11	0.27
		0.70	0.00			0.00	0.00	0.04	W 00		Λ ==	0.10	0.53
9	-0.08	0.50	0.76	1.35		0.92	0.50	0.24	0.88	0.26	0.38	0.10	
10	-0.02	0.51	0.99	1.74	1.28	1.26	0.90	0.66	0.44	0.26	0.35	0.10	
11	0.02	0.52	1.19 1. 3 8	1.95 2.08		1.68 2.04	1.20	1.01	0.48	0.26 0.29	0.15	0.12	0 57 1.02
Midn	0.05	0.48	1.00	2.00	2.80	2.04	1.00	1.25	0.51	0.25	0.15	0.12	1.02
<u> </u>													
6. 6	0.01	0.20	0.83	0.40	0.07	-0.01	-0.09	-0.04	0.15	0.21	0.09	0.02	0.15
7. 7	0.02	0.31	0.89	0.44	0.01	-0.08	-0.04	-0.00	0.18	0.20	0.17	0.02	0.18
8.8	0.02	0.88	0.71	0.86	-0.06	-0.04	0.02	0.04	0.16	0.13	0.20	0.01	0.16
9. 9	0.02	0.28	0.85	0.19	-0.11	-0.04	0.07	0.07	0.18	0.03	0.17	-0.00	0.10
10.10	-0.00	0.13	-0.12	-0.04	-0.18	-0.04	0.10	0.09	0.01	-0.08	0.11	-0.00	0.00
1	1												
7. 2. 9	-0.03	-0.06			-0.52					-0.05		-0.08	-0.2 0
6. 2. 8	1							-0.28				-0.02	-0.19
6. 2.10	-0.02		1 1					-0.01			0.01		-0.04
6. 2. 6	-U.U4	-0.20	-U.53	- v.72	~ 0.54	~0.88	-V.68	-0.49	-U.ZZ	-U.U5	-0.00	-0.03	-0.3 9
7. 2	-0.03	-0.85	-0.75	-1.08	-1.15	-1.26	-0.80	-0.44	-0.84	-0.20	-0.11	-0.10	-0.55
8. 2	-0.08											-0.12	
8. 1	1							-0.55				-0.12	
7. 1	-0.01	1								l .		-0.11	
9.12.8.9	-0.04	-0.28	-1.28	-1.29	-1.27	-1.12	-0.77	-0.59	-0.37	-0.25	-0.01	-0.06	-0.61
7. 2.2(9)	-0.08	0.08	0.01	0.14	-0.21	-0.17	-0.15	-0.10	0.02	0.03	0.14	-0.00	-0.03
Dail.ext.	-0.02	0.9E	-0 50	_0	0.05	0.04	_0 04		_0.14	_0 10	0.00		_0.36
Dan. ext.	1 -0.02	V.20	7.00	V.5/	0.00	U.U4	-U.U4	-U.UZ	-U.14	_0.19	0.03	_A.01	-0.16

XIII.

N. AMERICA. — LAKE ATHABASCA. Lat. 59° N. Long. 111° W. Greenw. For continuous to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — LEFROY.

The corrections for April and May are derived from observations made at Fort Simpson, Lat. 62° N.

Degrees of Fahrenheit.

Hour.	April.	May.	October.	November.	December.	January.	February.
daily ext.	1.58	1.71	0.88	0.25	-0.17	0.77	1.19
6, 6	1.15	0.51	1.07	0.59	0.27	0.84	1.19
7, 7	1.50	0.16	0.76	0.54	0.90	0.58	1.81
8, 8	1.72	0.18	0.69	0.55	0.62	0.95	1.27
9, 9	0.54	0.80	0.37	0.82	0.84	0.80	0.78
10, 10	-0.48	-0.08	-0.82	-0.06	0.84	0.12	0.81
11, 11	-1.68	-1.20	-0.57	-0.87	0.10	-0.62	-0.23
6, 2, 10	0.47	0.46	-0.81	-0.21	-0.22	-0.17	-0.05
7, 8, 11	0.46	0.59	-0.40	0.16	0 17	0.06	-0.26
Mean.	\$2.48	44.56	21.44	9.76	0.40	-23.00	4.79

XIV.

Arctic America. — Melville Island. Lat. 74° 47' N. Long. 110° 48' W. Gr. — Dove.

Degrees of Resumur.

Hour.	Jeansy.	February.	March.	October.	Hour.	November.	December.
A.M. 1	0.12	0.10	1.04	0.04	A.M. 2	-0.12	-0.09
8	0.18	0.05	1.22	0.12	4	-0.02	-0.06
5	0.07	0.25	0.90	0.24	6	0.00	0.11
7	0.11	0.29	0.57	0.20	8	-0.22	0.07
9	-0.18	-0.24	0.29	-0.15	10	-0.88	0.11
11	-0.85	-0.43	-1.83	-0.46	12	-0.41	0.24
P.M. 1	-6.22	-0.65	-1.72	-0.48	P.M. 2	-0.27	0.14
8	-0.25	-0.52	-1.00	0.22	4	0.16	0.00
5	0.04	0.04	-0.48	-0.24	6	0.27	-0.12
7	0.04	0.24	0.06	-0.10	8	0.38	-0.26
9	0.11	0.85	0.88	0.11	10	0.86	-0.12
11	0.40	0.49	0.66	0.43	12	0.25	0.00
Mean.	-29.75	-27.58	-22.73	-14.82	Mean.	-18.65	-25.75

XV.

SPITZBERGEN. — HECLA COVE. Lat. 79° 55' N. Long. 16° 49' E. Gr. — Dove.

Hour.	June.	July.	August.	Hour,	June.	July.	August.
A.M. 1	0.68	0.62	0.42	P.M. 1	-0.67	-0.67	-0.63
8	0.48	0.84	0.54	8	-0.58	-0.42	-0.58
5	0.26	0.51	0.58	5	-0.27	-0.44	-0.32
7	-0.12	-0.02	0.25	7	0.26	-0.17	0.06
9	-0.29	-0.09	-0.09		0.21	0.06	0.14
11	-0.47	-0.49	-0.45	11	0.61	0.26	0.24
		<u> </u>		Mean.	1.71	8.68	2.84

XVI.

S. America. — Rio Janeiro. Lat. 22° 54' S. Long. 48° 16' W. Greens.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

					<u> </u>	M OT JA				-	_		
Hours.	Jen.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct	Nov.	Dec.	Mess.
	0.54			0.00		A #0	1 05	1.81	1.04	0.97	1.76	1.81	1.24
Morn. 1	0.74	1.51	1.80			0.56	1.85						
2	1.64	2.41	2.48	1.64	2.12	1.58	2.75	2.00	1.69	1.64	2.32	2.05	2.03
8	2.50	3.11	8.02	2.32	2.98	2.43	3.47	2.66	2.27	2.21	2.75	2.66	2.70
4	8.06	8.90	8.24	2.79	3.88	8.04	8.87	3.04	2.59	2.50	2.98	2.99	3.06
5	8.22	3.29	8.15	2.90	8.40	3.29	3.83	3.0 6	2.66	2.52	2 79	2.99	8.06
6	2.98	2.84	2.75	2.75	3.06	8.20	3.47	2.79	2.41	2.27	2.82	2.68	2.79
7	2.30	2.21	2.14	2.30	2.48	2.84	2.70	2.25	2.00	1.82	1.67	2.12	2.23
8	1.49	1.49	1.40	1.71	1.85	2.89	1.96	1.60	1.46	1.28	0.90	1.40	1.58
9	0.68	0.72	0.59	1.04	1.15	1.82	1.15	0.90	0.86	0.68	0.14	0.59	0.86
10	-0.07	-0.05	-0.23	0.82	0.50	1.18	0.82	0.23	0.18	0.05	-0.56	-0.23	-0.14
11	-0.77	-0.86	-1.01	-0.45	-0.28	0.82	-0.50	-0.50	-0.54	-0.59	-1.22	-1.04	-0.61
Noon	-1.40	-1.64	-1.71	-1.22	-0.99	-0.65		-1.19				-1.82	-1.35
1	-2.00	-2.80	-2.80	_1 94	_1 71	-1.67	-2.16	_1.91	-1.89	-1.78	-2.82	-2.48	-2.08
2			-2.66										
	-2.59		-2.84			-2.00	-8.40	-2.84	-2.50	-2.27	-2.79	-2.86	-2.77
4			-2.77										
•	1 1										l i		
5			-2.50										
6	-1.51	-1.82	-2.12	-1.76	-2.2 1	-2.23	-8.04	-2.28	-1.55	-1.87	-1.67		
7			-1.67									-0. 99	
8	-0.72	-1.18	-1.22	-0.95	-1.67	-1-43	-1.85	-1.18	-0.83	-0.77	-0.59	-0.61	-1.06
9	-0.59	-0.92	-0.77	-0.72	-1.44	-1.26	-1.22	-0.70	-0.61	-0.61	-0.14	-0.8 8	-0.79
0	-0.56	-0.68	-0.25	-0.52	-1.18	-1.18	-0.59	-0.82	-0.41	-0.45	0.23	-0.16	-0.50
11	-0.41			-0.25			0.09		-0.09		0.65	0.14	0.00
Midn	0.00	0.59	1.06	0.23	0.14	-0.29	0.92	0.61	0.88	0.82	1-15	0.65	0.47
6. 6	0.72	0.52	0.32	0.50	0.48	0.50	0.80	0.29	0.48	0.45	0.84	0.61	0.45
7. 7	0.63	0.41	0.25	0.52	0.29	0.54	0.16	0.29	0.45	0.41	0.29	0.56	0.41
8.8	0.88	0.18	0.09	0.88	0.09	0.50	0.07	0.25	0.82	0.27	0.16	0.41	0.25
9. 9	0.05	-0.11	-0.09	-0.16	-0.16	0.29	-0.05	0.11	0.14	0.05	0.00	0.11	0.05
10.10	-0.82	-0.84	-0.25	-0.11	-0.22	0.00	-0.14	-0.05	-0.11	-0.20	-0.18	-0.20	-0.18
7. 2. 9			-0.48			-0.29	-0.47	-0.82	-0.32	-0.32	-0.88	-0.36	-0.36
6. 2. 8			-0.38					-0.27				-0.25	
6. 2.10			-0.05			-0.14	0.00				-0.05	-0.09	-0.07
6. 2. 6	-0.84	_0 80	-0.68	_0 47	-0.47	-0.50	-0.83	-0.63	_0.KA	-0.48	-0.69	-0.54	-0.56
7. 2		-0.27			0.09			-0.11					. ,
8. 2	1		-0.63					-0.45					
8. 1	1 1		-0.45					-0.16					
ا ا													
7. 1		1	-0.09	1			-0.27				-0.84		
9.12.8.9	1	-1.19		-0.90				-0.97					
7. 2.2(9)	-0.32	-0.61	-0.52	-0.88	-0.68	- 0.54	-0.65	-0.41	-0.38	-0.38	~0. 3 2	~V.\$6	-0.47
Dail. ext.	0.32	0.27	0.20	0.14	0.84	0.14	0.14	0.09	0.09	0.14	0.07	0.07	0.16

XVII.

S. AMERICA. - RIO JANRIBO. Lat. 22° 54' S. Long. 43° 16' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

						of Re							
Hours.	Jen.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
X 1	0.38	0.67	0.80	0.40	0.50	0.25	0.82	0.58	0.46	0.48	0.78	0.58	0.55
Morn. 1				0.73			1.22		0.75		ı	0.91	
2	0.78	1.07	1.10		0.94	0.68		0.89					
8	1.11	1.88	1.84	1.08	1.30	1.08	1.54	1.18		0.98		1.18	
4	1.87	1.51	1.44	1.24	1.50	1.35	1.72	1.35	1.15	1.11	1.30	1.23	1.86
5	1.48	1.46	1.40	1.29	1.51	1.46	1.70	1.87	1.18	1.12	1.24	1.33	1.87
6	1.30	1.26	1.22	1.22	1.86	1.42	1.54	1.24	1.07	1.01	1.08	1.19	1.24
7	1.02	0.98	0.95	1.02	1.10	1.26	1.20	1.00	0.89	0.81	0.74	0.94	0.99
8	0.66	0.66	0.62	0.76	0.82	1.06	0.87	0.71	0.65	0.57	0.40	0.62	0.70
9	0.80	0.32	0.26	0.46	0.51	0.81	0.51	0.40	0.88	0.80	0.06	0.26	0.88
10			-0.10								-0.25		
11			-0.45					-0.22			•		1 1
Noon	1 1		-0.76			-					-0.80		-0.60
	1										1		
1			-1.02										
2			-1.18										
8			-1.26										
4	-1.09	-1.20	-1.28	-1.14	-1.22	-1.85	-1.60	-1.80	-1.05	-0.94	-1.18	-1.15	-1.20
5	-0.91	-1.02	-1.11	-0.98	-1.13	-1.22	-1.54	-1.19	-0.89	-0.79	-1.00	-0.98	-1.06
6			-0.94										, ,
7			-0.74										
8			-0.54										
<u> </u>											i I		1 1
9	-0.26	-0.41	-0.34	-0.82	-0.64	-0.56	-0.54	-0.31	-0.27	-0.27			
10	-0.25	-0.28	-0.11	-0.28	-0.50	-0.50	-0.26	-0.14	-0.18	-0.20	0.10	-0.07	-0.22
11	-0.18	-0.06	0.16	-0.11	-0.28	-0.88	0.04	-0.04	-0.04	-0.07	0.29	0.06	-0.04
Midn	0.00	0.26	0.47	0.10	0.06	-0.13	0.41	0.27	0.17	0.14	0.51	0.29	0.21
6. 6	0.82	Λ 99	0.14	0.22	0.19	A 49	0.10	0.18	0.19	0.20	0.15	0 27	0.20
7. 7	0.32										•		
8. 8	0.17	1			1				0.14		1		
9. 9			-0.04		-0.07		-0.02		0.06		-0.00		0.02
10.10			-0.11										
10.10	0.17	-0.15	_0.11	-0.00	-0.14	-0.00	-0.00	-0.02	-0.00	0.00	0.00	0.00	0.00
7. 2. 9	-0.10	-0.22	-0.19	-0.12	-0.19	-0.13	-0.21	-0.14	-0.14	-0.14	-0.17	-0.16	-0.16
6. 2. 8			-0.17										
6. 2.10	-0.01	-0.08	-0.02	-0.08	-0.05	-0.06	-0.00	-0.00	-0.05	-0.05	-0.02	-0.04	-0.08
6- 2- 6			-0.80										
7. 2	-0.03	-0.12	-0.12	-0.03	0.04	0.08	-0.04	-0.05	-0.08	-0.08	-0.22	-0.16	-0.07
8. 2	-0.21	-0.28	-0.28	-0.16	-0.10	-0.02	-0.21	-0.20	-0.20	-0.20	-0.89	-0.32	-0.21
8. 1	-0.12	-0.18	-0.20					-0.07					
7. 1			-0.04		•			0.08			-0.15		
0.10.00	0.40			0.40			0	0 10	_0 00	.0.00		-0 EV	المدا
	-0.48												
7. 2.2(9)	-0.14	-U.Z7	-0.23	-U.17	-0.50	-0.24	-0.20	_0.19	-0.17	-0.17	-0.14	-0.10	-V.Z1
Dail.ext.	0.14	0.12	0.09	0.06	0.15	0.06	0.06	0.04	0.04	0.06	0.08	0.08	0.07

N. America. - Amherst College. - Lat. 42° 22' N. Long. 72° 30' W. Greene.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — DEWEY.

Degrees of Fahrenheit.

						M OC FM		•					
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Test
Moen. 1	3.90	2.78	4.78	6.28	5.51	6.64	6.89	5.14	5.36	4.87	2.84	1.63	4.6
2	4.24	3.03	4.81	6.69	6.48	7.28	6.88	5.66	6.12	5.65	2.99	2.20	5.1
8	4.18	8.20	5.36	7.42	7.41	7.92	7.28	6.08	6.92	6.46	3.49	2.55	5.6
4	4.50	8.94	5.69	7.85	7.88	8.04	7.43	6.29	6.56	7.09	8.72	2.70	6.0
5	4.72	4.20	6.04	8.12	8.18	7.80	7.54	6.66	7.88	7.72	4.03	3.32	6.3
6	4.68	4.78	6.12	7.77	6.77	5.96	6.02	5.81	7.44	7.65	4.34	8.78	5.9
7	4.75	4.78	4.62	5.97	4.22	4.20	8.80	4.48	5.32	6.87	4.28	3.97	4.7
8	8.63	3.78	2.06	8.04	1.62	1.40	1.09	1.96	2.52	4.81	2.68	4.18	2.7
9	1.46	1.45	-0.46	0.08	-0.60	-0.88	-0.87	-0.98	-0.56	0.88	0.34	2.40	0.1
10	-1. 2 6	-0.85	-2.57	- 2.69	-1.12	-8.12	-8.80	-8.04	-8.82	-2.24	-1.48	-0.55	-2.5
11	-4.10	-2.72	-4.77	- 5.65	-5.12	-5.68	-6.43	-5.45	-6.01	-5.02	-8.01	-2.76	-4.7
Noon.	-6.82	-4.26	-6.8 8	- 7.92	-6.75	-6.06	-8.50	-6.86	-6.16	-7.06	-5.01	~4.3 0	-6.6
1	-7.46	-5.85	-7.65	- 9.46	-8.15	-9.36	-6.88	-6.23	-0 .12	-8.24	-6.12	-6.14	-7.8
2	-7.80	-6.06	-8.84	-10.42	-8.75	-9.00	-9.5 0	-7.86	-9.80	-9.2 8	-5.97	-6.3 0	-8.2
8	-7.82	-5.80	-8.11	- 9. 81	-8.27	-8.60	-7.50	-7.67	-9.20	-9 .24	-5.28	-5.60	-7.7
4	-5.84	-4.89	-7.28	- 8.61	-7.86	-7.84	-7.17	-6.23	-8.40	-6.24	-8.85	-8.76	-6.6
5	-8.82	-8.10	-5.65	- 7.04	-5.97	-6.00	-5.83	-5.26	-6.44	-5.65	-2.28	-2.03	-4.8
6	-2.06	-1.18	-3.46	- 4.50	-4.08	-4.20	-4.17	-2.82	-3.52	-8.50	-0.85	-0.68	
7	0.24	-1.05	0.17	- 1.69	-2.38	-1.92	-1.54	-1.44	-1.47		-0.64	ı	-1.1
8	0.64	-0.48	0.93	0.27	-0.19	0.04	0.98	0.88	0.11	0.18	0.08	0.20	0.3
9	1.50	0.29	1.89	1.77	1.66	1.96	8.05	1.59	1.99	1.16	0.80	0.69	1.4
10	2.01	0.57	8.29	8.31	2.78	8.20	8.79	8.02	3.53	1.90	1.16	1.20	2
11	2.42	1.19	4.29	4.28	8.99	4.20	4.24	8.79	4.61	8.24	1.96	1.58	8.4
lidnight.	2.50	1.70	4.85	4.92	4.75	5.48	5.81	4.52	5.84	4.09	2.40	1.98	8.9
3, 9, 3, 9	-0.05	-0.22	-0.06	- 0.18	0.05	0.10	0.49	0.26	-0.21	-0.20	-0.16	-0.01	-0.0
9, 9	1.48	0.87	0.72	0.98	0.58	0.54	1.09	0.83	0.72	1.00	0.57	1.55	9.0
10, 10	0.88	-0.14	0.86	0.81	0.81	0.04	0.00	-0.51	0.11	-0.17	-0.13	0.33	0.1
7, 2, 9	-0.48	-0.88	-0.61	- 6.89	-0.96	-0.95	-0.88	-0.60	-0.88	-0.42	-0.29	-0.5 5	-0.6
8, 2, 10	-0.87	-0.24	0.36	- 0.24	0.25	0.05	0.10	0.32	0.39	0.09		-0.44	0.0
7, 2, 10	-0.35	-0.04	-0.14	- 0.88	-0.60	-0.58	-0.64	-0.12	-0.32	-0.17		-0.8 8	-0.8
7, 2, 11	-0.21	-0.08	0.19	- 0.07	-0.18	-0.20	-0.49	0.14	0.04	0.28	0.09	-0.25	-0.0
6, 8, 9, 4, 3 10, 19		0.02	0.18	0.00	-0.12	-0.18	-0.06	0.20	0.11	0.07	0.13	0.17	0.0
,2,2,(9)	-0.01	<u>-0.18</u>	0.01	- 0.28	-0.80	-0.22 	0.10	-0.05 	-0.12 	-0.02	-0.02	-0.24	-0.1
Mean.	22.94	28.57	34.81	48.54	56.92	61.60	71.61	67.44	59.80	50.46	84.80	29.28	47.2

The numbers without sign must be added; those with the sign — must be subtracted.

The above Table has been derived from one year of hourly observations made at Amherst College, Massachusetts, in 1839, under the direction of Professor Snell, and communicated by Professor Chester Dewey. It gives the simple differences of the monthly means of each hour from the monthly means of the twenty-four hours which are found in the last line.

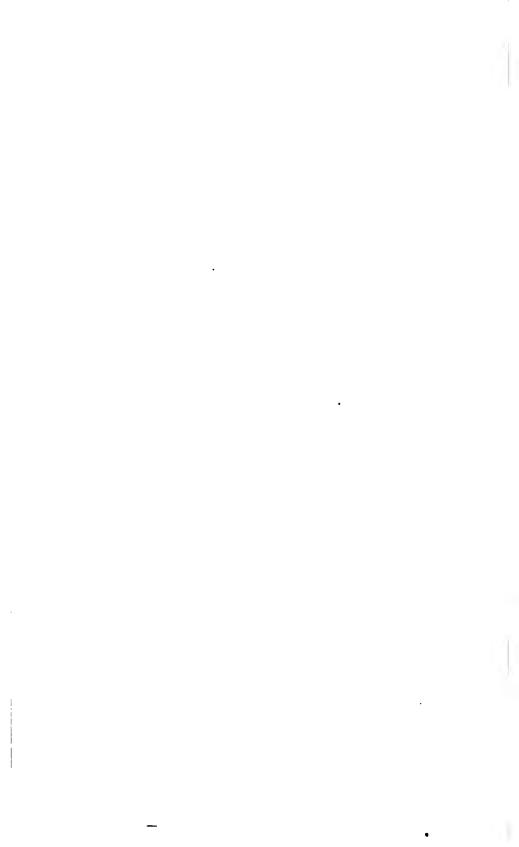
HOURLY CORRECTIONS

FOR

PERIODIC VARIATIONS.

ASIA.

E 20



XVIII.

India. — Trevandrum. Lat. 8° 31' N. Long. 74° 50' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dovs.

Degrees of Fahrenbelt.

Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	4.41	4.08	3.80	3.85	3.26	2.66	2.41	2.88	2.99	8.06	8.38	4.25	8.42
2	5.13	4.95	4.64	4.46	8.80	3.02	2.75	3.24	8.44	3.44	8.83	4.86	3.96
3	6.03	6.12	5.67	5.15	4.39	3.47	3.17	ı	8.98	8.92	4.46	5.67	4.66
4	6.95	7.81	6.64	5.74	4.82	8.80	3.58	4.21	4.48	4.34	5.04	6.50	5.29
5	7.56	8.15	7.18	5.81	4.82	3.83	3.76	4.41	4.61	4.46	5.22	6.98	5.56
6	7.34	8.01	6.78	5.11	4.14	8.35	8.49	4.07	4.14	4.01	4.78	6.57	5.15
7	6.01	6.59	5.20	3.53	2.81	2.84	2.68	8.06	8.02	2.88	3.40	5.11	3.89
8	3.56	8.92	2.66	1.22	0.95	0.90	1.35	1.49	1.26	1.18	1.40	2.70	1.87
9	0.41	0.50	-0.47	-1.42	-1.18	-0.74	-0.27	-0.45	-0.81	-0.99	-0.92	-0.29	-0.54
10			-3.58	-3.89				-2.41				-8 24	-2.93
11	-5.51	-5.85	-5.94	-5.76	-4.48	-3.53	-8.33		-4.50	-4.78		!	-4.84
Noon	-7.25	-7.58			-5.33	1	-4.82			-5.72			-6.01
1	-7.92	-8.17	-7.72	-7.04	-5.60	_4.R9	-4.70	– გ. 6 9	-5.87	-5.94	-5.90	-7.49	-6.41
2	1 1	-7.83	-7.22					-5.60					
8	-7.09		-6.26	-5.65	-4.79		-4.30			-4.66		-6.57	
4		-5.99								-3 .53			
5	_5.15	-4.88	_2 R2	_9.11	_9 88	_2 52	-9 59	-2.90	-2.59	-2.32	-8.15	-4.61	-8.88
6	-3.92		-2.57	-1.71		-1.42			-1.31		-2.03		-2.16
7			-1.81	-0.84	-0.50			-0.27				-1.89	
8	1 1	-1.04	1	0.92	0.68	0.70			0.92	0.97			0.82
9	0.68	0.28	1.06	1.91	1.58	1.46	1.40	1.76	1.69	1.71	1.42	1.19	1.35
10	2.03	1.64	1.96	2.61	2.16	1.96	1.85	2.80	2.18	2.25	2.21	2.48	2.14
11	3.08	2.57	2.68	8.06	2.57	2.23	2.09	2.54	2.48	2.57	2.68	3.26	2.66
Midn	3.88	8.81	8.17	3.42	2.88	2.41	2.23	2.68	2.70	2.81	2.99	8.80	8.02
1													
6. 6	1.71	2.14	2.09	1.71	1.24	0.97	1.04	1.24	1.42	1.46	1.35	1.60	1.51
7. 7	1.76	2.07	1.96	1.60	1.17	1.01	1.19	1.40	1.44	1.44	1.28	1.62	1.49
8.8	1.38	1.44	1.81	1.06	0.79	0.79	1.01	1.19	1.08	1.06	0.88	1.19	1.10
9. 9	0.54	0.48	0.29	0.25	0.20	0.36	0.56	0.65	0.48	0.26	0.25	0.45	0.41
10.10	-0.41	-0.65	-0.79	-0.63	-0.45	-0.18	-0.02	-0.07	-0.84	-0.41	-0.45	-0.40	-0.41
7. 2. 9	-0.36	-0.29	-0.82	-0.38	-0.84	-0.27	-0.23	-0.27	-0.29	-0.82	-0.27	-0.32	-0.32
6. 2. 8	-0.45	-0.29	-0.18	-0.18	-0.20	-0.18			-0.18	-0.18	-0.16	-0.84	-0.28
6. 2.10	0.54	0.61	0.50	0.88	0.32	0.23	0.18	0.25	0.25	0.25	0.45	0.59	0.38
6. 2. 6	-1.44		-1.01	-1.06	-0.97			-1.04	-0.92	-0.88	-0.97	-1.35	-1.06
7. 2	-0.88	-0.68	-1.01	-1.58	-1.28	-1.15	-1.06	-1.28	-1.81	-1.88	-1.10	-1.08	-1.18
8. 2	-2.12	-1.96	-2.80	-2.70		-1.87		•		-2.21	-2.12	ı	-2.14
8. 1	-2.18		-2.54	-2.93			-1.78	•	1	-2.41		1	-2.27
7. 1	-0.97		-1.26		-1.40			-1.38	1	i		-1.19	-1.26
9.12.3.9	-8.31	-3.42	-8.26	-2.99	-2.48	-1.96	-1.87	-2.23	-2.3 9	-2.41	-2.54	-8.17	-2.66
7. 2.2(9)	1	-0.11	0.02	0.20		0.16	0.18		0.20		0.16		

XIX.

India. - Trevandrum. Lat. 8° 31' N. Long. 74° 50' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

			_										
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	1.96	1.79	1.69	1.71	1.45	1.18	1.07	1.28	1.33	1.86	1.48	1.89	1.52
2	2.28	2.20	2.06	1.98			1.22	1.44	1.58	ı	1.70	2.16	1.76
	2.68	2.72	2.52	2.29	1.95	1.54	1.41	1.66	1.77	1.74	1.98	2.52	2.07
8	3.09					1.69	1.59	1.87	1.90	1.93	2.24	2.89	2.35
4	3.03	8.25	2.95	2.55	2.14	1.00	¥.00	1.01	1.50	1.50	2.24	2.00	
5	3.36	8.62	8.17	2.58	2.14	1.70	1.67	1.96	2.05	1.98	2.82	8.08	2.47
6	8.26	8.56	2.99	2.27	1.85	1.49	1.55	1.81	1.84	1.78	2.10	2.92	2.29
7	2.67	2.98	2.81	1.57	1.25	1.04	1.19	1.86	1.84	1.28	1.51	2.27	1.73
8	1.58	1.74	1.18	0.54	0.42	0.40	0.60	0.66	0.56	0.50	0.62	1.20	0.83
	0.10		0.01	0.00	A 50	_A 99	-Λ 19	-0.20	_^ •6	_0.44	_0 41	_0 19	
9	0.18	0.22	-0.21	-0.05	-0.00	7.00	-0.12	7.20	_1.97	_1.96	_1 98	_1 44	_1 20
10	-1.26	-1.82	-1.57	-1.78	-1.85	-1.UZ	-0.85	-1.07	-1.27	-1.30	_0.11	-0.49	_9 15
11	-2.45							-1.80					
Noon	-8.22	–8.37	-8.27	-5.08	-2.87	-1.98	-1.92	-2.80	-Z.46	-Z.54	-z.5Z	-2.11	2.07
1	_8 52	-8.68	-8.48	-8.18	-2.49	-2.08	-2.18	-2.53	-2.61	-2.64	-2.62	-3.33	-2.85
2	-8.45	-8.48	-8.21	-2.93	-2.89	-2.05	-2.12	-2.49	-2.49	-2.46	-2.49	-3.22	-2.73
8	-8.15	-8.10	-2.78	-2.51	-2.13	-1.86	-1.91	-2.24	-2.16	-2.07	-2.20	-2.92	-2.42
4	-2.74	-2.66	-2.25	-1.98	-1.75	-1.54	-1 56	-1.82	-1.69	-1.57	-1.83	-2.52	-1.99
•	-2.14	2.00	2.20	2.50	****		2.00	1.05	2.00				
5	-2.28	-2.17	-1.70	-1.88	-1.28	-1.12	-1.12	-1.29	-1.15	-1.03	-1.40	-2.05	-1.50
6	-1.74	-1.66	-1.14	-0.76	-0.75	-0.68	-0.62	-0.70	-0.58	-0.49	-0.9 0	-1.49	-0.96
7								-0.12				-0.84	
8		l	-0.08	0.41			0.80		0.41		0.17	-0.14	0.14
						0.00	0.00		0.00	0.76	0.63	0.53	0.60
9	0.80		0.47	0.85			1	1 1	0.75				1 7 1
10	0.91	0.78	0.87	1.16			1		0.97			1.08	1 11
11	1.87	1.14	1.17				0.93		1.10		1.19	1.45	
Midn	1.70	1.47	1.41	1.52	1.28	1.07	0.99	1.19	1.20	1.25	1.33	1.69	1.34
6. 6	0.76	0.95	0.98	0.76	0.55	0.43	0.46	0.55	0.68	0.65	0.60	0.71	0.67
7. 7	0.78	0.92	0.87	0.71					0 64			0.72	0.66
8. 8	0.59	i	0.58	0.47					0.48		0.89	0.53	0.49
9. 9	0.24	0.19	0.18	0.11	0.09	0.16		0.29	0.19	0.16	0.11	0.20	0.18
10.10	-0.18		-0.85			-0.08		1 1			-0.20		1
10.10	0.10		"		ŀ						ŀ		1
7. 2. 9	-0.16	-0.13	-0.14	-0.17	-0.15	-0.12	-0.10	-0.12	-0.18	∸0.14	-0.12	-0.14	-0.14
6. 2. 8	-0.20	1	-0.06	-0.08	-0.09	-0.08	-0.09	-0.09	-0.08	-0.08	-0.07	-0.15	-0.10
6. 2.10	0.24	0.27	0.22	0.17	0.14	0.10	0.08	0.11	0.11	0.11	0.20	0.26	0.17
6. 2. 6	-0.64	-0.58	-0.45	-0.47	-0.43	-0.40	-0.40	-0.46	-0.41	-0.39	-0.43	-0.60	-0.47
					1						l	i	i !
7. 2	-0.39	-0.28	-0.45	-0.68	-0.57	-0.51	-0.47	-0.57	-0.58	-0.59	-0.49	-U-48	0.50
8. 2	1	,	-1.02	-1.20	-0.99	-0.88	-0.76	-0.92	-0.97	-U.98	-0.94	-1.01	-0.90
8. 1		-0.95	-1.13	-1.80	-1.04	-0.84	-0.77	-0.94	-1.08	-1.07	-1.00	-1.07	-1.01
7. 1	-0.43	-0.35	-0.56	-0.78	-0.62	-0.52	-0.47	-0.59	-0.64	-0.68	-0.56	-0.53	-0.56
0 10 0 0	_1 4~	_1 =0	_3 48	_1 00	_1 00	0 0~	_A e=	-0.99	1.08	-1.07	_1.12	-1.41	-1.18
9.12.8.9		-0.05	0.01						0.09				
7. 2.2(9)	-0.05	J-0.08	0.01	0.08	0.00	V.01	0.00	0.11	0.00	0.00	5.51		
Dail.ext.	-0.08	-0.01	-0.18	-0.28	-0.18	-0.19	-0.23	-0.29	-0.28	-0.33	-0.15	-0.13	-0.19
	<u> </u>											<u> </u>	لحصنا

XX.

INDIA. - MADRAS. Lat. 13° 4' N. Long. 80° 19' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

	4	1	1	1		1		ī	ī	ī	1		lı
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midnight.	2.05	2.54	2.25	3.65	2.74	3.03	2.90	2.86	2.34	1.84	2.05	1.89	2.50
1	2.54	3.26	2.90	3.08	3.31	8.50	3.10	3.01	2.70	2.27	2.54	2.25	2.87
2	2.96	3.95	8.60	8.57	8.72	8.86	3.55	8.39	3.10	2.79	3.03	2.63	3 85
8	8.33	4.52	4.25	4.07	4.07	4.27	8.93	8.69	8.55	8.12	8.50	2.96	8.77
4	8.62	5.06	4.79	4.40	1	4.68	4.81	3.98	8.95	8.46	8.91	8.19	4.15
5	3.81	5.49	5.24	4.45	1	4.95	4.66	4.84	4.28	8.71	4.23	3.60	4.45
6	4.05	5.64	5.11	3.78	1	4.21	4.31	4.07	3.82	3.28	4.05	8.78	4.16
7	2.43	3. 33	2.54	1.78	2.07	2.51	2.92	2.79	2.43	1.80	2.00	2.38	2.41
8	-0.04			1	-0.11		l .	1		1	-0.56		0.23
9	-2.02		-1.89			-1.73		-0.90		-1.26		-1.73	
10	1 1		-3.67					1 1			-3.53		
11	-4.02	-4.81	-4.81	-4.83	-5.75	-5.02	-4.25	~4.16	-4.54	-8.17	-4.09	-3.62	-4.42
Noon.	1 1	1						-5.28		ı	1		
1	-4.40						l			-3.73		-3.86	
2	-4.14				-4.99			-5.40					
8	-3.4 6	-4.85	-4.27	-4.07	-4.00	-4.61	-4.92	-4.59	-3.73	-3.03	-3.05	-2.88	-3.95
4	-2.41	-3.64	-3.10	-2.65				-8.44				1	1
5	-1.19	-2.27		-1.03	-1.01		-2. 18			-1.26	-0.88		-1.47
6	-0.38		-0.52	0.20		-0.5 8	-0.81	1 1	-0.52		1 1	-0.88	l
7	0.09	-0.86	0.17	0.88	0.76	0.86	0.16	0.13	0.07	-0.18	0.09	0.00	0.18
8	0.54	0.27	0.58	0.99	1.19	0.97	0.88	0.74	0.47	0.16	0.47	0.84	0.68
9	0.94	0.81	0.97	1.57	1.57	1.42	1.35	1.17	0.99	0.49	0.74	0.67	1.06
10	1.39	1.33	1.89	1.89	1.96	2.11	1.87	1.64	1.39	0.90	1.08	1.03	1.50
11	1.84	1.87	1.84	2.25	2.84	2.41	2.29	2.14	1.89	1.28	1.46	1.44	1.92
6, 6	1.83	2.27	2.29	1.99	1.98	1.81	1.75	1.65	1.65	1.32	1.90	1.67	1.84
7, 7	1.26	1.48	1.85	1.30	1.41	1.43	1.54	1.46	1.25	0.81	1.04	1.19	1.29
8, 8	0.23	0.28	0.87	0.40	0.54	0.67	0.94	0.81	0.59		-0.04	0.17	0.48
9, 9	-0.54	-0.56	-0.46	-0.42	-0.48	-0.15	0.29	0.13	-0.06	-0.88	-0.87	-0.53	-0.33
	-0.93		1		. 1			1	,		1	-1.01	-0.93
7, 1	-0.98		-1.44	-1.87	-1.78			1	-1.30		-1.12	-0.74	-1.83
7, 2, 9	-0.26	-0.39	-0.49	-0.53	-0.45	-0.59	-0.58		-0.41	-0.42	-0.33	-0.18	-0.43
6, 2, 10	0.43	0.56	0.50	0.24	0.28	0.21	0.05	0.10	0.18	0.21	0.47		0.30
Mean.	76.77	78 .2 5	82.24	85.73	87.10	87.01	86.22	84.51	88.50	81.18	78.53	76.75	

XXI.

INDIA. - MADRAS. Lat. 13° 4' N. Long. 80° 19' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dovs.

Morn. 1 1.41 1.22 1.52 1.06 1.26 1.15 0.93 0.83 1.26 1.18 1.04 1.28 1.59 1.42 1.09 1.40 1.52 1.46 1.32 1.50 1.70 1.60 1.76 1.94 1.70 1.26 1.66 1.67 1.70 1.70 1.88 1.90 1.93 1.42 1.66 1.67 1.70 1.70 1.88 1.90 1.93 1.64 1.81 2.42 2.43 1.61 2.20 2.18 1.95 1.42 1.90 1.42 1.66 1.67 1.70 1.88 1.90 1.93 1.66 2.22 2.06 1.46 1.91 1.86 1.77 1.33 1.10 1.39 1.64 1.81 2.27 2.17 2.71 8 1.05 0.36 0.54 0.30 0.27 0.70 0.78 0.46 0.47 0.40 0.50 1.32 0.41 1.11 1.14 1.14 1.15 1.10 1.14 1.15 1.10 1.14 1.14 1.15 1.16 1.17 1.18 1.10 1.18 1.04 1.28 1.70 1.28 1.10 1.28 1.10 1.28 1.10 1.28 1.10 1.28 1.10 1.29 1.14 1.27 1.30 1.12 0.75 1.02 1.14 1.27 1.30 1.12 0.75 1.02 1.14 1.27 1.30 1.12 0.75 0.46 0.47 0.40 0.50 1.32 0.41 1.11 1.14 1.14 1.14 1.15 1.16 0.83 0.16 0.23 0.46 0.47 0.40 0.50 1.32 0.41 1.11 1.14 1.14 1.14 1.14 1.14 1.14				,		Dogree	e of Re	AUMANT.		,				
1.79	Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Moss
2 1.79 1.64 1.42 1.36 1.59 1.42 1.09 1.40 1.52 1.46 1.22 1.50 1.44 1.52 1.53 1.70 1.26 1.66 1.67 1.70 1.68 1.70 1.68 1.70 1.68 1.70 1.88 1.90 1.93 1.55 1.42 1.65 1.67 1.70 1.88 1.90 1.93 1.55 1.42 1.65 1.67 1.88 1.90 1.93 1.55 1.42 1.45 1.65 1.62 1.88 2.02 2.17 1.45 1.65 1.64 1.51 2.25 1.57 1.70 1.81 1.50 1.14 1.24 1.19 1.80 1.17 1.33 1.10 1.39 1.64 1.51 2.25 1.57 1.02 1.14 1.27 2.00 1.5 1.05 0.36 0.54 0.30 0.27 0.70 0.78 0.46 0.47 0.40 0.50 1.32 0.40 0.52 1.38 1.04 1.56 1.67 0.82 0.21 0.18 1.02 1.14 1.27 2.00 1.5 0.59 0.23 0.71 0.75 0.06 0.35 0.16 0.23 0.46 0.35 0.27 0.50 0.22 1.38 1.04 1.56 1.67 0.82 0.21 0.18 1.02 1.18 1.02 1.12 1.14 1.14 1.14 1.14 1.14 1.14 0.14 0.15 0.18 1.02 1.18 1.02 1.18 1.10 0.18 1.02 1.18 1.10 1.18 1.15 1.14 1.14 1.14 1.14 0.14 0.18 0.15 0.18 1.12 1.12 1.12 1.12 1.13 1.15	Morn. 1	1.41	1.22	1.82	1.06	1.26	1.15	0.93	0.83	1.26	1.18	1.04	1.38	1.1
4 2.88 2.42 1.69 2.10 2.17 1.90 1.42 1.66 1.70 1.88 1.90 1.93 1.4 6 2.22 2.05 1.48 1.61 2.20 2.18 1.95 1.42 1.45 1.62 1.88 2.02 2.17 1.4 6 2.22 2.05 1.48 1.91 1.86 1.77 1.83 1.10 1.89 1.64 1.81 2.25 1.7 1.76 1.80 1.14 1.24 1.19 1.80 1.77 1.83 1.10 1.89 1.64 1.81 2.25 1.7 1.05 0.86 0.54 0.80 0.27 0.70 0.78 0.46 0.47 0.40 0.50 1.32 0.4 0.90 0.35 0.59 0.23 0.71 0.75 0.06 0.85 0.16 0.23 0.46 0.47 0.40 0.50 1.32 0.4 0.90 0.35 0.35 0.40 0.47 0.40 0.50 1.32 0.4 0.90 0.35 0.35 0.40 0.47 0.40 0.50 1.32 0.4 0.90 0.35 0.35 0.40 0.47 0.40 0.50 1.32 0.4 0.90 0.35 0.35 0.40 0.47 0.40 0.50 1.32 0.4 0.90 0.35 0.35 0.40 0.47 0.40 0.50 1.32 0.4 0.90 0.35 0.35 0.40 0.47 0.40 0.50 1.32 0.4 0.4 0.45 0.47 0.40 0.50 1.22 0.4 0.4 0.45 0.47 0.40 0.50 0.50 1.32 0.4 0.4 0.4 0.45 0.4 0.45 0.48 0.48 0.48 0.48 0.47 0.40 0.50 0.44 0.45 0.27 0.38 0.48 0.48 0.48 0.48 0.48 0.48 0.48 0.4		1.79	1.64	1.42	1.36	1.59	1.42	1.09	1.40	1.52	1.46	1.32	1.50	1.4
5	3	2.14	2.10	1.50	1.76	1.94	1.70	1.26	1.66	1.67	1.70	1.70	1.68	1.7
6 2.22 2.06 1.48 1.91 1.86 1.77 1.83 1.10 1.89 1.64 1.81 2.25 1.7 1.76 1.80 1.14 1.24 1.19 1.80 1.12 0.75 1.02 1.14 1.27 2.00 1.2 8 1.05 0.86 0.54 0.80 0.27 0.70 0.78 0.46 0.47 0.40 0.50 1.22 0.4 1.10 0.50 0.86 0.54 0.80 0.27 0.70 0.78 0.46 0.47 0.40 0.50 1.32 0.4 1.8 1.0 0.50 0.8 0.54 0.80 0.27 0.70 0.78 0.46 0.47 0.40 0.50 1.32 0.4 1.0 0.50 1.2 0.4 1.0 0.50 0.8 0.15 0.59 0.23 0.71 0.75 0.06 0.83 0.16 0.23 0.46 0.25 0.46 0.25 0.27 0.2 1.0 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0	4	2.88	2.42	1.59	2.10	2.17	1.90	1.42	1.66	1.70	1.88	1.90	1.93	1.9
7 1.76 1.80 1.14 1.24 1.19 1.80 1.12 0.75 1.02 1.14 1.27 2.00 1.2 0.3 0.	5	1	2.43	1.61	2.20							1		i i
8 1.05 0.36 0.54 0.50 0.27 0.70 0.78 0.46 0.47 0.40 0.50 1.32 0.4 9 0.15 -0.69 -0.23 -0.71 -0.75 -0.06 0.35 0.16 -0.23 -0.46 -0.25 0.27 -0.5 10 -0.82 -1.38 -1.04 -1.56 -1.67 -0.82 -0.21 -0.18 -1.02 -1.26 -1.10 -0.94 -1.6 11 1-1.74 -1.94 -1.70 -2.12 -2.31 -1.46 -0.86 -0.62 -1.77 -1.83 -1.75 -2.20 -1.4 Noon2.48 -2.23 -2.06 -2.86 -2.86 -2.84 -1.94 -1.52 -1.12 -2.29 -2.18 -2.12 -2.76 -2.1 1 -2.90 -2.34 -2.10 -2.34 -2.48 -2.20 -2.13 -1.57 -2.47 -2.17 -2.25 -2.98 -2.12 2 -2.97 -2.30 -1.88 -2.14 -1.62 -2.07 -2.43 -1.77 -1.77 -1.50 -1.98 -2.25 -1.9 4 -2.14 -1.81 -1.14 -1.46 -1.11 -1.74 -2.12 -1.43 -1.12 -1.08 -1.61 -1.65 -1.6 5 -1.47 -1.34 -0.83 -1.00 -0.65 -1.28 -1.44 -0.94 -0.50 -0.70 -1.10 -1.13 -1.4 6 -0.81 -0.78 -0.58 -0.48 -0.27 -0.78 -0.65 -0.46 -0.06 -0.38 -0.58 -0.58 -0.72 -0.3 8 0.13 0.30 -0.08 0.49 0.26 0.12 0.62 -0.04 0.27 0.06 0.36 -0.06 0.3 9 0.38 0.62 0.42 0.71 0.45 0.42 0.86 -0.06 0.33 0.26 0.64 0.30 -0.06 0.3 9 0.38 0.62 0.42 0.71 0.45 0.42 0.86 -0.06 0.33 0.26 0.64 0.30 -0.06 0.3 9 0.38 0.62 0.42 0.71 0.45 0.42 0.86 -0.06 0.33 0.26 0.64 0.30 -0.06 0.3 0.70 0.84 0.91 0.91 0.78 0.79 0.87 0.11 0.66 0.67 0.83 0.99 0.7 Midn 1.06 0.96 1.16 0.92 0.99 0.94 0.84 0.47 0.95 0.91 0.89 1.22 0.3 0.27 0.02 0.10 -0.00 -0.15 0.18 0.61 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.0	-	ll .	2.05	1.48										1
9		ll .		1										
10	8	1.05	0.36	0.54	0.80	0.27	0.70	0.78	0.46	0.47	0.40	0.50	1.32	0.6
11	9													
Noon	10													
1	11													
2	Noon	-2.4 8	-2.28	-2.06	-2.86	-2.5 8	-1.94	-1.52	-1.12	-2.29	-2.18	-2.12	-2.76	-2.1
1	1	-2.90	-2.34	-2.10	-2.84	-2.48	-2.2 0	-2.13	-1.57	-2.47	-2.17	-2 .25	-2.98	-2.3
4	2													
5	8													
6 -0.81 -0.78 -0.58 -0.48 -0.27 -0.78 -0.65 -0.46 -0.06 -0.88 -0.58 -0.72 -0.58 -0.14 -0	4	-2.14	-1.81	-1.14	-1.46	-1.11	-1.74	-2.12	-1.43	-1.12	-1.08	-1.61	-1.65	-1.5
7		11												i
8			1	•										
9 0.38 0.62 0.42 0.71 0.45 0.42 0.86 -0.06 0.33 0.26 0.64 0.30 0.40 11 0.79 0.84 0.91 0.91 0.78 0.79 0.87 0.11 0.66 0.67 0.83 0.99 0.71 0.66 0.67 0.83 0.99 0.71 0.66 0.67 0.83 0.99 0.71 0.66 0.67 0.83 0.99 0.71 0.66 0.67 0.83 0.99 0.71 0.66 0.67 0.83 0.99 0.71 0.66 0.67 0.83 0.99 0.71 0.66 0.67 0.83 0.99 0.71 0.66 0.67 0.83 0.99 0.71 0.66 0.67 0.83 0.99 0.71 0.66 0.67 0.83 0.99 0.71 0.66 0.67 0.83 0.99 0.71 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75	-	11		1										
10	8	0.13	0.30	-0.08	0.49	0.26	0.12	0.62	-0.04	0.27	0.06			
11	9	11	ı											
Midn 1.06 0.96 1.16 0.92 0.98 0.94 0.84 0.47 0.95 0.91 0.89 1.22 0.5 6. 6 0.71 0.64 0.45 0.72 0.80 0.50 0.84 0.82 0.67 0.63 0.62 0.77 0.6 7. 7 0.75 0.56 0.40 0.64 0.61 0.50 0.60 0.31 0.60 0.50 0.57 0.81 0.5 8. 8 0.59 0.33 0.28 0.40 0.27 0.41 0.70 0.21 0.37 0.23 0.43 0.63 0.6 9. 9 0.27 0.02 0.10 -0.00 -0.15 0.18 0.61 0.05 0.05 -0.10 0.15 0.29 0.1 10.10 -0.12 -0.31 -0.22 -0.33 -0.53 -0.10 -0.35 -0.12 -0.29 -0.40 -0.15 -0.14 -0.5 7. 2. 9 -0.29 -0.18 -0.11 -0.06 -0.16 -0.17 -0.16 -0.88 -0.31 -0.17 -0.09 -0.15 -0.14 6. 2. 8 -0.21 0.02 -0.16 0.09 -0.00 -0.12 -0.17 -0.25 -0.20 -0.07 -0.01 -0.19 -0.5 6. 2. 6 -0.52 -0.34 -0.83 -0.24 -0.18 -0.42 -0.60 -0.39 -0.31 -0.22 -0.32 -0.41 -0.3 7. 2 -0.61 -0.50 -0.87 -0.45 -0.47 -0.47 -0.68 -0.54 -0.63 -0.32 -0.46 -0.38 -0.54 8. 2 -0.96 -0.97 -0.67 -0.92 -0.93 -0.77 -0.85 -0.68 -0.90 -0.76 -0.84 -0.72 -0.3 8. 1 -0.93 -0.99 -0.76 -1.02 -1.11 -0.75 -0.68 -0.56 -1.00 -0.89 -0.88 -0.85 -0.85 -0.65 7. 1 -0.57 -0.52 -0.48 -0.55 -0.65 -0.45 -0.51 -0.41 -0.73 -0.52 -0.49 -0.49 -0.49 7. 2. 2(9) -0.11 0.06 0.03 0.13 -0.01 -0.03 0.09 -0.30 -0.15 -0.06 0.09 -0.04 -0.40 -0.60 8. 1 -0.93 -0.99 -0.76 -1.05 -0.65 -0.45 -0.51 -0.41 -0.73 -0.52 -0.49		И	1											•
6. 6				1										
7. 7	Midn	1.06	0.96	1.16	0.92	0.98	0.94	0.84	0.47	0.95	0.91	0.89	1.22	0.8
8. 8 0.59 0.33 0.28 0.40 0.27 0.41 0.70 0.21 0.37 0.28 0.43 0.63 0.63 0.70 0.10 0.10 0.10 0.10 0.05 0.05 0.05 0.05 0.05 0.05 0.10 0.15 0.29 0.10 0.10 0.15 0.29 0.10 0.05 0.	6. 6	0.71	0.64	0.45	0.72	0.80	0.50	0.34	0.82	0.67	0.63	0.62	0.77	0.6
9. 9	7. 7	0.75	0.56	0.40	0.64	0.61	0.50	0.60	0.31	0.60	0.50	0.57	0.81	0.5
10.10	8. 8	0.59	0.83	0.28	0.40	0.27								0 (
7. 2. 9		il	1	l .	ľ	1					,			0.1
6. 2. 8 -0.21 0.02 -0.16 0.09 -0.00 -0.12 -0.17 -0.25 -0.20 -0.07 -0.01 -0.19 -0.18 6. 2. 10 -0.06 0.17 0.07 0.22 0.11 0.05 -0.08 -0.26 -0.15 0.06 0.15 0.05 0.06 6. 2. 6 -0.52 -0.34 -0.83 -0.24 -0.18 -0.42 -0.60 -0.39 -0.31 -0.22 -0.32 -0.41 -0.32 7. 2 -0.61 -0.50 -0.37 -0.45 -0.47 -0.48 -0.54 -0.63 -0.32 -0.46 -0.38 -0.1 8. 2 -0.96 -0.97 -0.67 -0.92 -0.93 -0.77 -0.85 -0.68 -0.90 -0.76 -0.84 -0.72 -0.1 8. 1 -0.93 -0.99 -0.78 -1.02 -1.11 -0.75 -0.68 -0.56 -1.00 -0.89 -0.89 -0.89 -0.83 -0.83 -0.6 7. 1 -0.57 -0.52 -0.48 -0.55 -0.65 -	10.10	-0.12	-0.31	-0.22	-0.33	-0.53	-0.10	-0.35	-0.12	-0.29	-0.40	-0.15	−0.14	-0.5
6. 2.10	7. 2. 9	-0.29	-0.18	-0.11										
6. 2. 6	6. 2. 8	-0.21	0.02	1				1						
7. 2 $\begin{vmatrix} -0.61 & -0.50 & -0.37 & -0.45 & -0.47 & -0.47 & -0.68 & -0.54 & -0.63 & -0.32 & -0.46 & -0.38 & -0.51 & -0.68 & -0.90 & -0.76 & -0.92 & -0.93 & -0.77 & -0.85 & -0.68 & -0.90 & -0.76 & -0.84 & -0.72 & -0.51 & -0.63 & -0.82 & -0.84 & -0.72 & -0.51 & -0.63 & -0.82 & -0.83$														0.0
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	6. 2. 6	-0.52	-0.34	i		i							ļ	
8. 1	7. 2	-0.61		-0.37	-0.45	-0.47	-0.47	-0.6 8	-0.54	-0.63	-0.82	-0.46	-0.38	-0.8
7. 1		-0.96	-0.97	-0.67	-0.92	-0.98	-0.77	-0.85	-0.68	-0.90	-0.76	-0.84	-0.72	-0.5
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8. 1	1)	1											
7. 2.2(9) -0.11 0.06 0.03 0.13 -0.01 -0.03 0.09 -0.30 -0.15 -0.06 0.09 -0.04 -0.0	7. 1	-0.57	-0.52	-0.48	-0.55	-0.65	-0.45	-0.51	-0.41	−0.73	- 0.52	-0.49	-0.49	-0 8
7. 2.2(9) -0.11 0.06 0.03 0.13 -0.01 -0.03 0.09 -0.30 -0.15 -0.06 0.09 -0.04 -0.0	9.12.8.9	-1.16	-1.08	-0.85	-1.05	-1.13	-0.01	-0.70	-0.70	-0.99	-0.97			
	7. 2.2(9)	-0.11	0.06	0.08								0.09	-0.04	-0.0
	'													١

· XXII.

India. - Bombay. Lat. 18° 56' N. Long. 72° 54' E. Greenic.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of	Fahrenheit.
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Hours.	· Jan.	Feb.	March.	April	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	1.49	1.40	0.99	1.18	1.42	1.15	0.79	0.97	0.86	1.49	2.08	1.55	1.26
2	1.80	1.69	1.38	1.51	1.78	1.40	0.88	1.13	0.97	1.87	2.18	1.87	1.53
8	2.27	2.21	1.91	2.05	2.14	1.69	0.90	1.24	1.24	2.32	2.45	2.41	1.91
4	2.86	2.84	2.59	2.48	2.32	1.91	0.90	1.81	1.53	2.75	2.81	3.11	2.27
5	3.47	8.40	8.04	2.61	2.28	1.96	0.86	1.81	1.71	2.95	8.11	8.78	2.54
4	3.83	8.62	8.06	2.84	1.80	1.80	0.79	1.24	1.67	2.79	3.15	4.16	2.52
7	8.69	8.33	2.54	1.67	1.15	1.42	0.65	1.04	1.22	2.21	2.79	4.01	2.14
8	2.97	2.48	1.58	0.77	0.86	0.88	0.88	0.74	0.79	1.28	1.91	8.24	1.44
9	1.69	1.22	0.38			0.00	0.00		0.00	0.10	0.63	1.87	0.50
10	0.07	-0.23	-0.77	-0.14 -0.90	-0.41 -1.06	0.23 0.43	0.00 -0.52	0.32 -0.20	0.09 -0.65	0.16 -0.95		0.16	-0.52
11	-1.55	-1.55	1	-1.49				-0.79	-1.28	-1.91		-1.60	-1.49
Noon.	-2.86	-2.61		l	-1.94			-1.85		-2.59		-8.08	-2.25
													5,50
1	-8.69	-8.29	-2.66	-2.25	-2.21	-2.12	-1.82	-1.78	-2.12	-2.99	-8.92	-4.10	-2.75
2	-3.98	-8.60	-2.84	-2.50	-2.34	-2.41	-1.78	-2.00	-2.25	-3.13	-4.07	-4.59	-2.95
8	-3.85	-3.6 5	-2.86	-2.61	-2.82	-2.45	-1.44	-1.98	-2. 16	-2.99	-3.85	-4.55	-2.90
4	-3.42	-8.42	-2.72	-2.50	-2.09	-2.25	-0.92	-1.69	-1.87	-2.66	-3.33	-4.12	-2.59
_		0.05									0.01		
5 6	-2.84	-2.95		i .	-1.64	1	i e		-1.87				-2.07
7	-2.18 -1.49	-2.27 -1.44	-1.71 -0.88	-1.87 -0.54	-1.04 -0.88	-1.15 -0.47	0.09 0.88	-0.72 -0.23	-0.74 0.05	-1.46 -0.72	-1.78 -0.88	-2.45 -1.46	-1.40 -0.68
8	-0.79	-0.56	-0.07	0.28	0.18	0.14	0.50	0.16	0.47		0.00		i i
	0	-0.50	0.01	0.20	0.10	0.14	0.00	0.10	0.47	-0.02	0.00	-0.02	-0.02
9	-0.11	0.23	0.56	0.72	0 59	0.54	0.54	1.48	0.86	0.52	0.77	0.29	0.50
10	0.47	0.81	0 90	0.92	0.83	0.79	0.54	0.59	0.99	0.88	1.35	0.86	0.83
11	0.92	1.10	0.97	0.92	0.99	0.96	0.61	0.72	0.97	1.08	1.71	1.19	1.01
Midn	1.24	1.26	0 92	0.95	1.15	0.99	0.70	0.83	0.88	1.26	1.91	1.37	1.13
	:												İ
6. 6	0.81	0.00											
7. 7	1.10	0.68	0.68	0.50	0.88 0.38	0.84	0.48	0.25	0.45	0.68 0.74	0.70 0.95	0.86 1.28	0.56
8. 8	1.08	0.97	0.83	0.50	0.38	0.47 0.50	0.52 0.45	0.41	0.63 0.68	0.74	0.95	1.25	0.72
9. 9	0.79	0.72	0.47	0.29	0.09	0.88	0.27	0.36	0.47	0.84	0.70	1.08	0.50
10.10	0.27	0.29	0.07	0.00	-0.11	0.18	0.02	0.20		-0.05	0.25	0.52	0.16
}				0.00	0.11	0.20	0.02	0.20	0.10	0.00		0.02	5125
7. 2. 9	-0.14	-0.02	0.09	-0.05	-0.20	-0.16	-0.20	-0.18	-0.07	-0.14	-0.18	-0.09	-0.11
6. 2. 8	-0.32	-0.18	0.05	0.02	-0.11	-0.16	-0.16	-0.20	-0.05	-0.11	-0.32	-0.32	-0.16
6. 2.10	0.11	0.27	0 38	0.25	0.09	0.07	-0.16	-0.07	0.14	0.18	0.14	0.14	0.14
6. 2. 6	-0.79	-0.74	-0.50	-0.52	-0.52	-0.59	-0.29	-0.50	-0.45	-0.61	-0.90	-0.97	-0.61
7. 2	-0.10		ا مر ما		0.05								
8. 2	-0.16 -0.52	-0.14		-0.43			l				-0.65		-0.41
8. 1	-0.36	-0.41	-0.63 -0.54	1	-0.99		-0.70		-0.74			-0.68	
7. 1	0.00	0 02		-0.79 -0 29	-0.92 -0.51		-0.72	-0.52	-0.68	-0.86		-0.43 -0.05	
	3.50	0.02	0.07	-0 25	-0 04	-0.30	-0.09	~0.30	-0.40	-0.41	-0.00	-0.05	-v.5Z
9.12.3.9	-1.28	-1.22	-1.06	-0.99	-1.01	-0.83	-0.61	-0.65	-0.77	-1.24	-1.44	-1.87	-1.04
7. 2.2(9)	-0.14	0.05	0.20	0.16	0.00		-0.02		0.18	,	1	0.00	0.05

XXIII. '

India. - Bombay. Lat. 18° 56' N. Long. 72° 54' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Morn. 1 1.0. Feb. March. April. May. June. July. Aug. Sept. Oct. Nov. Dec. Mem.	,													
2	Hours.	Jan.	Feb.	March.	A pril.	May.	June.	July.	Aug.	Sopt.	Oct.	Nov.	Dec.	Mon
2	Morn 1	0.66	0.62	0.44	0.50	0.68	0.51	0.85	0.43	0 88	0.66	0.90	0.69	0.56
1.01 0.98 0.85 0.91 0.95 0.75 0.40 0.55 0.55 1.03 1.09 1.07 0.85 1.27 1.26 1.15 1.10 1.08 0.85 0.40 0.58 0.68 1.22 1.25 1.25 1.01 5					l	1 1		1	l			1	i	0.68
1.27 1.26 1.15 1.10 1.08 0.86 0.40 0.58 0.68 1.22 1.25 1.38 1.01			ı			1			1					i .
5	1 1		Į.	1	l .						-	1		l i
8	}		220									1		į į
7	5	1.54	1.51	1.35	1.16	0.99	0.87	0.38	0.58	0.76	1.81	1.88	1.68	1.13
8	6	1.70	1.61	1.86	1.04	0.80	0.80	0.85	0.55	0.74	1.24	1.40	1.85	1.12
9	7	1.64	1.48	1.13	0.74	0.51	0.68	0.29	0.46	0.54	0.98	1.24	1.78	0.95
10	8	1.82	1.10	0.70	0.34	0.16	0.89	0.17	0.88	0.35	0.57	0.85	1.44	0.64
11	9	0.75	0.54	0.17	-0.06	-0.18	0.10	- 0.	0.14	0.04	0.07	0 28	0.83	0.22
Noon -1.27 -1.16 -1.02 -0.85 -0.86 -0.73 -0.69 -0.80 -1.15 -1.46 -1.37 -1.00 1	10	0.03	-0.10	-0.84	-0.40	-0.47	-0.19	-0.28	-0.09	-0.29	-0.42	-0.37	0.07	-0.23
Noon -1.27 -1.16 -1.02 -0.85 -0.86 -0.73 -0.69 -0.80 -1.15 -1.46 -1.37 -1.00 1	11	-0.69	-0.69	-0.74	-0.66	-0.69	-0.48	-0.48	-0.85	-0.57	-0.85	-0.98	-0.71	-0 66
2	Noon	-1.27											-1.37	-1.00
2		_1 64	_1 40	_1 10	_1 00	-0.00	-0.04	^ 61	_0 70	_0 04	_1 99	_1 74	_1 69	_1 99
3 -1.71 -1.62 -1.27 -1.16 -1.03 -1.09 -0.64 -0.88 -0.96 -1.33 -1.71 -2.02 -1.29 4 -1.52 -1.52 -1.21 -1.11 -0.93 -1.00 -0.41 -0.75 -0.83 -1.18 -1.48 -1.83 -1.15 5 -1.26 -1.31 -1.04 -0.92 -0.73 -0.79 -0.17 -0.55 -0.61 -0.96 -0.06 -0.61 -0.46 -0.51 0.04 -0.32 -0.33 -0.65 -0.79 -1.09 -0.62 7 -0.66 -0.64 -0.89 -0.24 -0.17 -0.21 0.17 -0.10 0.02 -0.32 -0.85 -0.65 -0.79 -1.09 -0.62 7 -0.66 -0.64 -0.89 -0.24 -0.17 -0.10 0.02 -0.82 -0.85 -0.62 9 -0.05 0.10 0.25 0.32 0.26 0.24 0.24 0.19 0.38 0.23 0.34 0.13 0.22 0.21 0.24 0.24														
4	- 1		,											
5	1 1													
6												İ		Į Į
7	1 1													
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9	1 .	1 .												
10	8	-0.85	-0.25	0.08	0.10	0.08	0.06	0.22	0.07	0.21	-0.01	0.	~0.23	-0 01
10	9	-0.05	0.10	0.25	0.82	0.26	0.24	0.24	0.19	0.38	0.23	0.84	0.13	0.22
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	- 1	1										0 60	0.38	0.57
6. 6	1 1		0.49	1		1		0.27	0.82	0.43	0.48	0.76	0.58	0.45
6. 6	Midn	0.55	0 56	0.41	0.42	0.51	0.44	0.31	0.87	0.89	0.56	0.85	0.61	0.50
7. 7 0.49 0.42 0.37 0.25 0.17 0.21 0.23 0.18 0.28 0.33 0.42 0.57 0.33 8. 8 0.48 0.43 0.34 0.22 0.12 0.22 0.20 0.28 0.28 0.42 0.60 0.32 9 9 0.85 0.82 0.21 0.13 0.04 0.17 0.12 0.16 0.21 0.15 0.31 0.49 0.22 i0.10 0.12 0.13 0.03 0.00 -0.05 0.08 0.01 0.09 0.08 -0.02 0.11 0.22 i0.10 0.12 0.13 0.04 -0.02 -0.09 -0.07 -0.09 -0.08 -0.02 0.11 0.22 0.02 0.01 0.09 0.08 -0.02 0.11 0.05 0.07 -0.09 -0.08 -0.02 -0.05 -0.07 -0.09 -0.02 -0.06 -0.05 -0.04 -0.05 -0.07 -0.09 -0.07 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>														
8. 8	6. 6	0.36	0.80	0.80	0.22	0.17	0.15	0.19	0.11	0.20	0.20	0.31	0 38	0.25
8. 8 0.48 0.43 0.34 0.22 0.12 0.22 0.20 0.20 0.28 0.28 0.42 0.60 0.32 0.10 0.12 0.13 0.03 0.00 -0.05 0.08 0.01 0.09 0.08 -0.02 0.11 0.23 0.07 0.23 0.07 0.08 0.01 0.09 0.08 -0.02 0.11 0.23 0.07 0.08 0.14 -0.08 0.02 0.01 0.09 -0.09 -0.08 -0.03 -0.06 -0.08 -0.04 -0.05 -0.07 -0.09 -0.07 -0.09 -0.02 -0.05 -0.14 -0.14 -0.05 0.22 -0.23 -0.25 -0.23 -0.23 -0.25 -0.23 -0.25 -0.23 -0.25 -0.23 -0.25 -0.24 -0.34 -0.34 -0.31 -0.28 -0.33 -0.41 -0.48 -0.32 -0.28 -0.32 -0.28 -0.32 -0.28 -0.32 -0.28 -0.32 -0.28 -0.32 -0.24 -0.34 -0.34 -0.34 -0.34 -0.35 -0.35 -0.35 -0.35 -0.35 -0.35 -0.35 -0.35 -0.35 -0.35 -0.35 -0.35 -0.25	1		ı			1		0.23	0.18	0.28	0.33	0.42	0 57	0.33
i 0.10 0.12 0.13 0.08 0.00 -0.05 0.08 0.01 0.09 0.08 -0.02 0.11 0.23 0.07 7. 2. 9 -0.06 -0.01 0.04 -0.02 -0.09 -0.07 -0.09 -0.08 -0.08 -0.04 -0.05 6. 2. 8 0.14 -0.08 0.02 0.01 -0.05 -0.07 -0.09 -0.02 -0.05 -0.04 -0.05 6. 2. 10 0.05 0.12 0.17 0.11 0.04 0.08 -0.07 -0.03 0.06 0.08 0.06 0.08 0.06	1	0.48	0.43	0.34	0.22	0.12	0.22	0.20	0.20	0 28	0.28	0 42	0.60	0.32
7. 2. 9	9 9	0.85	0 32	0.21	0.13	0.04	0.17	0.12	0.16	0.21	0.15	0.31	0.49	0.22
6. 2. 8	i 0.10	0.12	0.13	0.08	0.00	-0. 05	0.08	0.01	0.09	0.08	-0.02	0.11	0.23	0.07
6. 2. 8	7 9 0		_201	0.04	_0 02	-0.09	-0.07	-0.09	-0.08	-0.08	-0.08	-0.08	-0.04	-0.05
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6. 2 6	1 3		i .	ı										
8. 2	1 '	il .	i	1	1	1								
8. 2	7 9	-0.07		_0 07	0 10	-0.27	-0.22	-0.25	-0.22	-0.22	-0.21	-0.29	-0.18	-0.18
8. 1	1 1													
7. 1														
9.12.2.9 7. 2.2(9)	1 1	i i												
7. 2.2(9) -0.06 0.02 0.09 0.07 0.00 0.01 -0.01 -0.01 0.08 0.01 0.03 0.00 0.02	1		}										. 1	
Dail.ext. -0.04 -0.01 0.05 0.01 0.00 -0.11 -0.21 -0.16 -0.12 -0.04 -0.21 -0.10 -0.09	7. 2.2(9)	-0.06	0.02	0.09	0.07	0.00	0.01	-0.01	-0.01	0.08	0.01	0.03	0.00	0.02
	Dail.ext.	-0.04	-0.01	0.05	0.01	0.00	-0.11	-0.21	-0.16	-0.12	-0.04	-0.21	-0.10	-0.09

XXIV.

India. - Madras. Lat. 13° 4' N. Long. 80° 19' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Resumur.

Hour.	Jan.	Feb.	March.	April	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.91	1.13	1.00	1.62	1.22	1.35	1.19	1.27	1.04	0.82	0.91	0.84	1.11
1	1.13	1.45	1.29	1.37	1.47	1.56	1.38	1.84	1.20	1.01	1.13	1.00	1.28
2	1.32	1.76	1.60	1.59	1.65	1.72	1.58	1.51	1.88	1.24	1.35	1.17	1.49
3	1.48	2.01	1.88	1.81	1.81	1.90	1.75	1.64	1.58	1.39	1.56	1.32	1.69
4	1.61	2.25	2.13	1.96	1.98	2.08	1.92	1.77	1.76	1.54	1.74	1.42	1.85
5	1.74	2.44	2.33	1.98	2.08	2.20	2.07	1.93	1.88	1.65	1.88	1.60	1.98
6	1.80	2.51	2.27	1.68	1.72	1.87	1.92	1.81	1.70	1.46	1.80	1.66	1.85
7	1.08	1.48	1.13	0.79	0.92	1.12	1.30	1.24	1.08	0.80	1.89	1.06	1.07
8	-0.02	0.13	0.07	-0.08	-0.05	0.17	0.47	0.44	0.32	0.06	-0.25	0.00	0.10
9	-0.90	-0.86	-0.84	-1.07	-1.08	-0.77	-0.34	-0.40	-0.50	-0.56	-1.11	-0.77	-0.77
10	-1.45	-1.60	-1.63	-1.84	-2.08	-1.63	-1.19	-1.22	-1.32	-1.04	-1.57	-1.36	-1.49
11	-1.79	-2.14	-2.14	-2.15	-2.56	-2.23	-1.89	-1.85	-2.02	-1.41	-1.82	-1.61	-1.47
Noon.	-1.97	2.25	-2.38	-2.52	-2.61	-2.60	-2.45	-2.35	-2.24	-1.67	-1.92	-1.75	-2.23
1	-1.96	-2.38	-2.41	-2.46	-2.51	-2.69	-2.70	-2.56	-2.24	-1.66	-1.89	-1.72	-2.26
2	-1.84	-2.36	-2.22	-2.20	-2.22	-2.53	-2.67	-2.40	-2.07	-1.58	-1.66	-1.60	-2.11
3	-1.54	-2.16	-1.90	-1.81	-1.78	-2.05	-2.19	-2.04	-1.66	-1.35	-1.36	-1.28	-1.76
4	-1.07	-1.62	-1.38	-1.18	-1.09	-1.59	-1.66	-1.53	-1.14	-1.06	-0.88	-0.91	-1.26
5	-0.53	-1.01	-0.74	-0.46	-0.45	-0.85	-0.97	-0.82	-0.64	-0.56	-0.39	-0.45	-0.66
6	-0.17	-0.49	-0.23	0.09	0.05	-0.26	-0.36	-0.31	-0.23	-0.28	-0.11	-0.17	-0.21
7	0.04	-0.16	0.07	0.37	0.34	0.16	0.07	0.06	0.03	-0.08	0.04	0.00	0.09
8	0.24	0.12	0.26	0.44	0.53	0.48	0.37	0.33	0.21	0.07	0.21	0.15	0.28
9	0.42	0.36	0.48	0.70	0.70	0.63	0.60	0.52	0.44	0.22	0.33	0.30	0.47
10	0.62	0.59	0.62	0.84	0.87	0.94	0.83	0.73	0.62	0.40	0.48	0.46	0.67
11	0.82	0.83	0.82	1.00	1.04	1.07	1.02	0.95	0.84	0.57	0.65	0.64	0.85
Mean.	19.90	20.56	22.33	23.88	24.49	24.45	24.10	26.34	22.89	21.86	20.68	19.89	

XXV.

India. — Bombay. Lat. 18° 56' N. Long. 72° 54' E. Greenw. — Dove. Degrees of Resumur.

Hour.	Jan.	Feb.	March.	April	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	1.76	1.68	1.43	1.40	1.30	0.80	0.57	0.59	0.92	1.36	1.74	1.93	1.29
1	1.91	1.88	1.65	1.54	1.40	0.89	0.65	0.64	0.98	1.52	1.80	2.00	1.40
2	2.04	2.04	1.80	1.75	1.54	0.88	0.68	1.16	1.09	1.62	1.97	2.18	1.56
8	2.18	2.22	1.90	1.92	1.69	0.94	0.65	0.81	1.18	1.74	2.11	2.28	1.68
4	2.89	2.44	2.26	2.02	1.81	1.04	0.76	0.82	1.25	1.89	2.23	2.41	1.78
5	2.65	2.68	2.42	2.26	1.92	1.09	0.83	0.90	1.25	1.96	2.40	2.62	1.92
6	2.88	2.88	2.60	2.20	1.65	1.03	0.84	0.84	1.21	2.00	2.55	2.66	1.94
7	2.58	2.37	1.61	0.76	0.44	0.60	0.55	0.51	0.61	1.02	1.47	2.08	1.21
8	0.72	0.48	-1.04	-0.62	-0.51	-0.01	0.02	0.08	-0.20	-0.31	-0.12	0.20	-0.11
9	-1.04	-1.05	-1.49	-1.53	-1.30	-0.46	-0.46	-0.45	-0.84	-1.53	-1.40	-1.00	-1.03
10	-2.40	-2.29	-2.2 8	-2.00	-1.73	-0.79	-0.74	-0.76	-1.32	-2.17	-2.38	-2.14	-1.75
11	-3.08	-2.98	-2.54	-2.20	-2.08	-1.18	-1.07	-1.12	-1.51	-2.38	-3.18	-2.94	-2.19

XXV.

India. - Bombay, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Resumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Noon.	-8.40	-3.29	-2.52	-2.44	-2.32	-1.40	-1.09	-1.84	-1.72	-2.89	-3.26	-3.32	-2.37
1	-3.02	-3.12	-2.67	-2.53	-2.28	-1.50	-1.12	-1.85	-1.77	-2.22	-2.96	-3.35	-2.32
2	-2.78	-2.89	-2.56	-2.82	-2.14	-1.52	-0.97	-1.35	-1.55	-2.09	-2.55	-2.97	-2.14
3	-2.38	-2.54	-2.25	-2.05	-1.85	-1.81	-0.85	-1.09	-1.37	-1.79	-2.22	-2.59	-1.86
4	-1.96	-2.07	-1.72	-1.49	-1.36	-0.89	-0.68	-0.76	-0.93	-1.38	-1.55	-2.03	-1.40
5	-1.30	-1.41	-1.08	-0.96	-0.88	-0.49	-0.86	-0.34	-0.36	-0.61	-0.67	-1.09	-0.79
6	-0.61	-0.44	-0.16	0.00	0.09	-0.02	0.08	0.18	0.14	0.01	-0.14	-0.52	-0.13
7	-0.28	-0.07	0.19	0.43	0.63	0.22	0.21	0.26	0.28	0.80	0.09	-0.23	0.17
8	0.00	0.23	0.48	0.66	0.87	0.89	0.28	0.84	0.44	0.53	0.86	0.10	0.39
9	0.58	0.63	0.80	0.83	0.92	0.44	0.86	0.41	0.58	0.76	0.85	0.75	0.66
10	1.16	1.15	1.04	1.09	0.95	0.52	0.41	0.52	0.78	0.96	1.82	1.85	0.94
11	1.47	1.48	1.20	1.24	1.17	0.71	0.48	0.56	0.89	1.18	1.58	1.65	1.13
Mean	18.38	19.30	21.00	22.50	28.48	22.85	21.67	21.45	21.42	22.08	21.28	19.54	

XXVI.

India. — Calcutta. Lat. 22° 33′ 5″ N. Long. 88° 19′ 2″ E. Greenw. — Dove.

						Stees O							
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	1.86	1.69	2.06	1.60	1.90	1.12	0.69	0.69	0.71	1.00	1.24	1.51	1.34
1	2.24	2.00	2.37	1.96	2.06	. 1.12	0.80	0.78	0.76	1.17	1.47	1.77	1.54
2	2.53	2.22	2.62	2.18	2.21	1.16	0.91	0.85	0.84	1.26	1.69	2.00	1.71
8	2.80	2.44	2.84	2.27	2.82	1.29	1.02	0.92	0.93	1.26	1.82	2.31	1.85
4	3.06	2.71	3.08	2.40	2.41	1.29	1.11	0.96	1.04	1.46	2.00	2.40	1.99
5	8.83	2.89	3.28	2.47	2.50	1.34	1.24	1.07	1.16	1.58	2.22	2.66	2.14
6	3.53	8.11	8.42	2.58	2.41	1.84	1.24	1.12	1.16	1.62	2.36	2.80	2.23
7	8.71	8.24	8.42	2.22	1.90	1.03	0.96	0.89	0.93	0.86	2.81	2.93	2.03
8	2.73	2.20	1.97	1.18	0.81	0.45	0.42	0.82	0.27	0.31	0.93	1.68	1.11
9	0.91	0.71	0.46	0.11	-0.84	-0.18	-0.16	-0.22	-0.24	-0.47	-0.13	0.35	0.07
10	-0.78	-0.62	-0.98	-0.44	-1.39	-0.66	-0.69	-0.33	-0.73	-0.58	-1.02	-0.76	-0.73
11	-2.09	-1.64	-2.14	-1.82	-2.14	-1.15	-1.18	-1.08	-1.16	-1.60	-1.91	-1.87	-1.64
Noon.	-3.31	-2.62	-3.16	-2.67	-2.76	-1.60	-1.51	-1.51	-1.40	-1.94	-2.44	-2.80	-2.31
1	-4.14	-3.28	-8.87	-8.09	-3 .12	-1.68	-1.58	-1.55	-1.44	-2.05	-2.80	-3.29	-2.66
2	-4.52	-3.64	-4.25	-8.47	-8.82	-1.73	-1.29	-1.80	-1.68	-2.12	-3.07	-3.69	-2.89
3	-4.65	-3.87	-4.40	-3.62	-3.43	-1.92	-1.24	-1.20	-1.27	-1.83	-2.98	-3.69	-2.8
4	-8.7 8	-3.69	-4.23	-8.40	-3. 10	-1.58	-0.96	l .	1	-1.49		-2.76	,
5	-3.07	-3.13	-3.3 6	-2.73	-2.43	-1.20	-0.64	-0.68	-0.56	-0.92	-1.60	-2.18	-1.89
6	-1.87	-1.91	-1.96	-1.42	-1.23	-0.57	-0.31	-0.31	-0.16	-0.25	-0.76	-1.34	-1.01
7	-0.96	-0.93	-0.78	-0.31	-0.14	-0.11	-0.07	-0.09	0.04	0.13	-0.22	-0.63	-0.31
8	-0.20	-0.22	0.00	0.40	0.68	0.20	0.09	0.25	0.22	0.42	0.27	-0.05	0.17
9	0.42	0.38	0.78	0.89	1.08	0.49	0.22	0.45	0.33	0.60	0.62	0.44	0.53
10	40.95	.0.80	1.22	1.20	1.46	0.63	0.86	0.56	0.47	0.75	1.07	0.93	0.57
11	1.37	1.20	1.66	1.54	1.64	0.74	0.49	0.65	0.60	0.88	1.16	1.20	1.09
Mean.	15.49	17.57	21.19	22.51	24.01	23.29	22.68	22.86	22.42	21.78	18.88	16.36	

XXVII.

Asia. — Tiflis. Lat. 41° 41' N. Long. 45° 17' E. Greenw.

orrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept	Oct.	Nov.	Dec.	Year.
Midn.	0.87	1.01	1.54	1.81	1.95	2.88	2.48	2.22	1.60	1.38	0.99	0.80	1.58
1	1.02	1.15	1.80	2.10	2.28	2.67	2.79	2.52	1.81	1.64	1.16	0.94	1.82
2	1.17	1.83	2.02	2.40	2.58	2.94	3.13	2.82	2.08	1.88	1.37	1.04	2.06
8	1.32	1.47	2.23	2.64	2.84	3.22	8.49	8.18	2.29	2.11	1.59	1.14	2.28
4	1.46	1.57	2.89	2.94	3.14	8.48	8.73	3.44	2.59	2.39	1.78	1.25	2.51
5	1.60	1.69	2.58	8.12	8.09	8.09	8.55	3.59	2.74	2.62	1.85	1.85	2.57
6	1.76	1.75	2.63	2.89	2.39	2.35	2.77	3.06	2.68	2.77	1.99	1.40	2.87
7	1.87	1.75	2.14	2.19	1.58	1.28	1.50	2.16	1.99	2.38	1.85	1.42	1.84
8	1.49	1.28	1.23	0.99	0.53	0.35	0.70	1.05	1.07	1.52	1.44	1.19	1.06
9	0.05	0.50	0.16	-0.22	-0.51	-0.65	-0.82	-0.21	-0.03	0.80	0.54	0.49	0.01
10	-0.41	-0.46	-0.91	-1.20	-1.41	-1.66	-1.85	-1.32	-1.15	-0.47	-0.46	-0.19	-0.92
11	-1.17	-1.83	-1.85	-2.06	-2.19	-2.40	-2.27	-2.20	-2.01	-1.77	-1.31	-1.11	-1.81
Noon.	-1.91	-1.94	-2.64	-2.77	-2.89	-2.42	-2.99	-2 .89	-2.67	-2.53	-2.07	-1.76	-2.46
1	-2.37	-2.45	-8.12	-8.2 9	-3.21	-3.42	-3.53	-3.60	-3.17	-3.07	-2.50	-2.21	-3.00
2	-2.59		-3.25	-3.37	-3.34	-3.50	-3.6 8	-3.85	-8.41	-3.56	-2.81	-2.38	-3.20
3	-2.33	-2.58	-8.21	-8.41	-3.25	-3.51	-8.82	-3.9 8	-3.37	-3.41	-2.55	-2.08	-3.12
4	-1.78	-2.07	-2.78	-3.20	-2.97	-8.39	-3.82	-3.72	-2.95	-2.81	-1.87	-1.48	-2.73
5	-0.99	-1.24	-2.08	-2.46	-2.65	-2.86	-3.47	-3.20	-1.53	-1.85	-1.27	-0.90	-2.04
6	-0.57	-0.60	-1.11	-1.56	-1.47	-1.81	-2.36	-2.01	-1.18	-1.17	-0.73	-0.49	-1.26
7	-0.17	-0.19	-0.48	-0.69	-0.45	-0.63	-0.86	-0.85	-0.46	-0.50	-0.35	-0.13	-0.48
8	0.15	0.19	0.12	-0.02	0.26	0.28	0.13	-0.02	0.18	0.11	-0.02	0.19	0.12
9	0.88	0.44	0.51	Q.64	0.83	0.92	0.87	0.72	0.61	0.50	0.24	0.86	0.58
10	0.55	0.65	0.91	1.05	1.28	1.51	1.44	1.83	1.00	0.81	0.48	0.58	0.96
11	0.69	0.89	1.25	1.45	1.68	1.95	1.96	1.80	1.32	1.10	0.76	0.68	1.29
Mean.	-0.20	3.00	5.64	9.99	18.54	16.10	19.01	19.48	15.03	11.40	5.07	2.45	

XXVIII.

CHINA. — PEKING. Lat. 39° 54' N. Long. 116° 26' E. Greenw. — Dove.

Dogress of Resumur.

						-8							i
Hour.	Jan.	Feb.	March.	April.	May.	June	July.	Aug	Sept.	Oct.	Nov.	Dec	Year
Midn.	1.16	1.70	1.83	1.75	2.19	2.24	1.61	1.49	1.69	1.64	1.19	1.25	1.64
1	1.47	2.07	2.19	2.26	2.76	2.73	1.89	1.80	2.04	2.05	1.47	1.39	2.01
2	1.66	2.35	2.78	2.67	3.20	8.12	2.23	2.04	2.32	2.37	1.68	1.65	2.84
3	1.93	2.55	2.93	8.18	3.72	8.47	2.50	2.31	2.55	2.62	1.88	1.83	2.62
4	2.13	2.81	8.27	8.57	4.13	3.82	2.74	2.54	2.97	2.92	2.01	2.46	2.95
5	2.41	2.94	3.57	3.89	4.30	3.88	2.78	2.71	8.10	8.19	2.20	2.10	8.09
6	2.58	8.15	3.65	3.81	8.37	2.86	2.10	2.46	2.96	3.43	2.32	2.18	2.91
7	2.63	3.21	8.19	2.91	2.80	1.95	1.84	1.65	2.10	2.98	2.30	2.29	2.40
8	2.23	2.87	1.84	1.65	1.19	1.07	0.52	0.76	0.87	1.68	1.89	1.78	1.44
9	0.77	0.70	0.49	0.34	0.00	0.03	-0.12	-0.20	-0.24	0.15	0.19	0.81	0.20
10	-0.57	-0.65	-0.81	-0.79	-1.20	-1.06	-0.97	-1.09	-1.36	-1.05	-0.84	-0.97	-0.95
11	-1.35	-1.90	-1.93	-2.03	-1.24	-2.17	-1.71	-1.67	-2.17	-2.18	-1.74	-1.96	-1.84

XXVIII.

CHINA. - PEKING, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Resumur

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year
Noon.	-2.83	-2.80	-2.95	-2.92	-3.05	-2.92	-2.24	-2.02	-2.77	-3.03	-2.39	-2.64	-2.71
1	-8.01	-3.54	-3.54	-3.59	-8.74	E 8.55	-2.65	-2.64	-8.10	-3.65	-2.87	-3. 18	-8.2
2 .	-8.87	-3.84	-4.03	-3.98	-4.08	-8.97	-2.88	-2.90	-3.38	-3.96	-8.07	-3.41	-8.57
3	-3.40	-8.94	-4.12	-4.06	-4.24	-4.00	-2.85	-2.94	-3.44	-8.97	-2.88	-2.74	-3.53
4	-2.88	-3.65	-3.92	-3.86	-4.03	-8.74	-2.74	-2.79	-8.06	-2.43	-2.23	-2.50	-3.15
5	-1.79	-2.83	-3.21	-3.24	-3.65	-3.81	-2.36	-2.20	-2.34	-2.84	-1.18	-1.34	-2.48
6	-0.97	-1.79	-2.20	-2.34	-8.04	-2.44	-1.76	-1.45	-1.18	-1.12	-0.59	-0.64	-1.63
7	-0.48	-0.15	-1.03	-1.13	-1.18	-1.21	-0.72	-0.45	-0.50	-0.54	-0.48	-0.26	-0.68
· 8	-0.02	-0.27	-0.30	-0.83	-0.19	-0.11	0.12	0.08	0.09	-0.02	0.01	0.18	-0.06
9	0.30	0.26	0.26	0.24	0.59	0.59	0.63	0.51	0.57	0.42	0.80	0.54	0.43
10	0.57	0.73	0.88	0.84	1.15	1.14	1.04	0.83	0.97	0.86	0.59	0.77	0.86
11	0.90	1.20	1.30	1.28	1.67	1.65	1.85	1.18	1.32	1.00	0.81	1.01	1.22
Mean	-8.57	-2.01	2.12	9.88	15 89	19.61	21 27	19 80	15.68	9.61	1.79	-2.44	:

XXIX.

Siberia. — Nertchinsk. Lat. 51° 18' N. Long. 117° 20' E. Gr. — Dove.

Dogress of Resumur.

							Netum						
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year
Midn.	0.78	1.38	1.92	2.53	3.10	3.13	2.68	2.51	2.12	1.66	0.96	0.75	1.90
1	1.06	1.61	2.25	2.95	3.71	8.55	8.00	2.87	2.58	1.98	1.22	0.94	2.3
2	1.24	1.84	2.65	8.36	4.20	8.98	8.34	3.25	2.93	2.27	1.42	1.16	2.6
3	1.45	2.15	3.02	8.75	4.78	4.82	3.64	8.57	8.28	2.57	1.70	1.33	2.9
4	1.70	2.40	8.39	4.09	5.04	4.29	3.86	3.79	3.62	2.80	1.91	1.45	3.1
5	1.93	2.72	3.70	4.15	8.97	3.27	3.17	3.68	3.97	3.00	2.06	1.63	8.10
6	2.08	2.94	8.89	2.96	2.31	2.03	1.99	2.61	3.68	8.16	2.15	1.76	2.6
7	2.26	3.00	2.88	1.43	0.82	0.74	1.01	1.31	2.07	2.46	2.35	1.95	1.8
8	2.20	1.82	1.36	0.19	-0.53	-0.45	-1.28	0.11	0.66	0.84	1.61	1.98	0.7
9	0.56	-0.2 0	-0.12	-1.32	-1.77	-1.59	-1.25	-1.06	-0.72	-0.69	-0.03	0.62	-0.6
10	-0.96	-1.27	-1.71	-2.35	-2.73	-2.52	-2.13	-2.10	-1.99	-1.82	-1.17	-0.89	-1.8
11	-1.90	-2.34	-2.61	-3.08	-3.34	-8.17	-2.79	-2.91	-2.94	-2.78	-2.12	-1.85	-2.6
Noon.	-2.70	-3.16	-3.48	-8.70	-3.82	-3.62	-3.28	-3.49	-8.71	-8.41	-2.84	-2.58	-3.3
1	-8.06	-3.75	-3.96	-4.01	-4.06	-3.80	-3.58	-8.76	-4.09	-3.75	-3.09	-2.85	-3.6
2	-3.00	-3.80	-4.23	-4.08	-4.10	-3.78	-8.66	-8.92	-4.20	-3.66	-2.97	-2.52	-3.6
8	-2.50	-3.47	-4.03	-3.84	-3.99	-3.59	-3.48	-3.79	-3.86	-3.26	-2.27	-1.87	-3.3
4	~1.54	-2.73	-3.53	-3.48	-3.55	-3.24	-8.02	-8.21	-8.84	-2.43	-1.34	-0.96	-2.7
5	-0.71	-1.61	-2.75	-2.85	-3.02	-3.78	-2.88	-2.56	-2.48	-1.42	-0.87	-0.43	-1.9
6	-0.23	-0.63	-1.71	-1.97	-2.27	-2.06	-1.73	-1.68	-1.22	-0.50	-0.10	-0.17	-1.2
7	0.02	0.01	-0.34	-0.84	-0.93	-0.93	-0.82	-0.66	-0.49	-0.24	-0.17	-0.70	-0.1
8	0.13	0.89	0.24	0.61	0.27	0.97	0.37	0.41	0.84	0.30	0.06	0.08	0.2
9	0.27	0.63	0.66	1.19	1.34	1.32	1.24	1.30	0.89	0.64	0.34	0.22	il .
10	0.43	0.86	1.06	1.72	1.92	2.02	1.78	1.70	1.30	1.01	0.54	0.43	i)
п	0.57	1.16	1.47	2.17	2.63	2.63	2.29	2.14	1.71	1.81	0.75	0.56	1.6
Mean.	-21.94	-17.54	-8.85	0.04	7.51	1.78	13.91	11.91	6.55	-1.80	-13.44	-21.36	1

XXX.

SIBERIA. — NERTCHINSK. Lat. 51° 18' N. Long. 119° 21' E. Greenw. orrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

	-												
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
										١			
Morn. 1	0.91	1.42	2.07		4.07	4.29	8.07	8.00	2.16		1	1	1
2	1.00	1.69	2.57	8.29	4.69	4.71	3.46	8.48	2.96	2.79	ı	l	2.69
8	1.15	2.08	8.16	8.78	5.08	4.90	8.75	3.89	3.27	8.26	1.26	0.84	3.04
4	1.42	2.52	3.63	8.97	4.98	4.70	8.76	4.04	8.81	3.61	1.66	1.07	8.26
5	1.78	2.84	3.73	3.69	4.24	8.96	3.37	3.72	8.94	3.66	2.06	1.41	8.20
6	2.07	2.80	8.28	2.88	2.86	2.67	2.54	2.89	8.15		1	4	2.71
7	2.06	2.28	2.31	1.68	1.07	0.99	1.37	1.62	2.88	2.47	ı .	1.87	1.85
8	1.60	1.28	0.99	0.16	-0.78	-0.79	0.06	0.15	0.87	1.24	1.58	1.59	0.66
"	1.00	1.20	0.55	0.10	-0.70	0.75	0.00	0.13	0.01	1.24	1.50	1.05	0.00
9	0.65	-0.05	-0.41	-1.26	-2.83	-2.34	-1.19	-1.25	-0.70	-0.23	0.55	0.87	-0.64
10	-0.59	-1.43	-1.67	-2.42	-3.40	-8.41	-1.98	-2.38	-1.74	-1.70	-0.69	-0.17	-1.80
11	-1.79	-2.58	-2.64	-3.22	-3.98	-8.97	-2.92	-3.15	-2.99			-1.23	-2.77
Noon	-2.61	-3.29	-8.25			-4.12				-3.84		-2.01	-3.84
					2.20								
1	-2.87	-3.49	-8.61	-3.76	-4.22	-4.05	-3.64	-3.83	-3.69	-4.25	-2.81	-2.30	-3.54
2	-2.56	-3.27	-3.74	-3.65	-4.18	-3.92	-3.72	-3.88	-4.00	-4.20	-2.50	-2.08	-3.48
3	-1.89	-2.76	-3. 65			-3.77		-3.75	-3.54	-3.77	l	-1.54	-3.18
4	-1.14		-8.31	1	-8.69						ľ	-0.92	-2.65
	1 1												l
5	-0.56	-1.45	-2.65	-2.17	-8.04	-3.07	-2.68	-2.76	-2.68	-2.24	-0.61	-0.47	-2.03
6	-0.28	-0.81	-1.78	-1.39	-2.08	-2.30	-1.82	-1.86	-1.54	-1.86	-0.27	-0.25	-1.31
7	-0.11	-0.21	-0.77	-0.56	-0.92	-1.23	-0.81	-0.80	-0.86	-0.54	-0.12	-0.23	-0.60
8	-0.04	0.31	0.18	0.20	0.26	0.00	0.20	0.24	0.17	0.17	-0.25	-0.24	0.12
ļ ļ	1												i
9	0.09	0.74	0.90	0.82	1.29	1.21	1.06	1.11	0.97	0.74	0.05	-0.17	0.73
10	0.31	1.02	1.34	1.29	2.11	2.25	1.51	1.74	1.17	1.18	0.20	0.02	1.18
11	0.57	1.19	1.56	1.71	2.78	8.09	2.28	2.19	1.78	1.54	0.39	0.28	1.61
Midn	0.78	1.29	1.76	2.15	8.41	8.75	2.65	2.57	1.88	1.90	0.58	0.52	1.94
i i													i i
6. 6	0.92	1.00	0.75	0.75	A 90	0.19	0.86	0.52	0 80	0.97	1.01	0.75	0.70
	1 1			1	0.39				- 1				
7. 7	0.98	1.04	0.77	0.58	0.07	-0.12	0.28	0.41	0.76	0.97	1.03	0.82	0.63
8.8	0.78	0.80	0.58	0.18	-0.26	-0.89	0.18	0.20	0.52	0.71	0.77	0.67	0.39
9. 9	0.87	0.84		-0.22	-0.52	-0.56	-0.06	-0.07	0.13	0.26	0.30	0.35	0.05
10.10	-0.14	-0.20	-0.16	-0.57	-0.65	-0.58	-0.24	-0.82	-0.29	-0.26	-0.25	-0.07	-0.31
7. 2. 9	-0.14	-0.08	-0.18	-0.40	-0.61	-0.57	-0.48	-0.88	-0.22	-0.83	-0.09	-0.13	-0.80
6. 2. 8	-0.18	-0.05		-0.19			-0.33	-0.25	-0.23		-0.08	1	-0.22
6. 2.10	-0.06	0.18	0.29	0.17	0.26	0.88	0.11	0.25	0.11	0.09	0.00		0.14
6. 2. 6	-0.24	-0.43			-1.13		-1.00	-0.95			-0.16	1	-0.69
		J. 10	0.75	-0.12	-1.10	1.10	2.00	V.50	0.00	~.,0	2.10	0.13	
7. 3	-0.41	-0.61	-0.65	-0.07	-1.58	-1.53	-1.14	-1.11	-0.66	-0.89	-0.82	-0.22	-0.85
8. 2	-0.94	-1.84	-1.60	-1.85	-2.32	-2.26	-1.78	-1.88	-1.69	-1.78	-0.97	-0.71	-1.59
8. 1	-0.64	-1.11	-1.81	-1.80	-2.50	-2.42	-1.79	-1.84	-1.41	-1.51	-0.62	-0.36	-1.14
7. 1	-0.25							-1.18					-0.81
			_										
9.12.3.9	-0.48				1	- 1		-1.87					- 11
7. 2.2(9)	-0.06	0.12	0.09	-0. 09	-0.18	-0.13	-0.06	-0.01	9.06	-0.04	-0.05	-0.14	-0.04
Dail.ext.	-0.40	-0.29	_0.07	_0 11	0.49	0.39	0.02	0.08	_0.02	-0.80	-0.26	-0.22	-0.14
1/AIL CXL	0.40	0.00	-0.01	-0.11	U. 13	0.09	U.UZ	U.00	U.U3	-0.00	V.20	0.22	٠٠

XXXI.

SIBERIA. — BARNAUL. Lat. 53° 20' N. Long. 83° 27' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

Degrees of Fahrenheit.													
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec	Mona
,,,,,,	0.54	1.01		- 40	0.00	- 00				- 00		1.00	4.05
Morn. 1	2.54	1.85				1			5.45	8.06		1.82	4 95
2	2.81	2.14	5.47	6.80		1	9.77	8.35	6.50	8.78	2.97	2.00	5.76
8	2.70	2.48	6.28	7.07	10.96	9.59	10.69	9.52	7.65	4.52	3.35	2.07	6.41
4	2.89	2.81	7.02	7.45	10.76	9.14	10.67	10.15	8.48	5.15	3.71	2.18	6.66
5	2.07	8.18	7.48	7.09	9.32	7.58	9.50	9.77	8.60	5.47	4.01	2.45	6.37
6	1.96	8.88		5.87	ľ	5.45	7.18	8.12	5.58	5.29	4.16	2.79	5.65
7	2.00	3.20		3.87	8.38	2.50	4.05	5.86	2.70	4.46	3.96	2.99	3.94
8	1.98	2.59	8.71	1.37	-0.11	-0.18	0.70	1.96		2.97	3.15	2.70	1.96
	1.50	2.00	0.77	1.0.	0.11	0.10	00	1.50			0.20	20	1.50
9	1.53	1.37	0.86	-1.28	-8.02	-2.48	-2.32	-1.44	-0 56	0.99	1.64	1.73	-0.25
10	0.45	-0.36	-2.18	-8.74	-5.06	-4.61	-4.68	-4.32	- 3.67	-1.22	-0.41	0.11	-2.48
11	-1.22	-2.80	-4.91	-5.78	-6.85	-5.99	-6.35	-6.48	-6 .21	-8.31	-2.61	-1.76	-1.43
Noon	-3.08	-4 03	-6.89					-7.97				-8.42	
1 1	-4.59	-5.13	-7 97	-8.85	-8.03	-8.39	-8.42	-8.96	-8-96	-6.05	-5.58	-4.39	-7.07
2	-5.27	-5.8 8	-8.21	-8.71	-8.78	-8.78	-9 .16	-9.68	-9.23	-6.39	-5.72	-4.48	-7.47
8	-4.93	-4.77	-7.76	-8.89	-9.41	-8 91	-9.56	-9. 88	-8.82	-6.05	-5 02	-3.78	-7.27
4	-3 78	-3.56	-6.84	-7.84	-9 .50	-8.01	-9.3 6	-9.50	-7.81	-5.22	-3.85	-2.6 8	-6.46
5	-2.25	-2.14	-5.65	-5.58	-8.66	-6.32	-8.85	-8.28	-6.26	~4.05	-2.57	-1.60	5.15
6	-0.90	-0.88			-6.82	1		-6.19				-0.83	
7	0.02	0.09						1	-2 07	,		-0.43	1
8	0.47	0.68	-0.97		-1.31		-1.81			-0.86		-0.23	
9	0.70	0.92	0.68	2.61	1.46	1.80	1.24	1.80	1.76	0.54	0.00	0.00	1.13
10	0.95	1.10	2.00	3.62	8.78	3.49	8.38	8.67	2.99	1.28	0.52	0.38	2.27
11	1.42	1.28	8.18	4.25	5.69	4.75	5.20	4.97	8.85	1.87	1.15	0.92	3.22
Midn	2.03	1.55	3.98	4.82	7.86	6.26	6.82	6.03	4.59	2.45	1.85	1:44	410
6. 6	0.54	1.24	1.46	1 96	-0.07	0.54	0.84	0.97	1.69	1.28	1.31	0 99	8.97
7. 7	1.01	1.64	1.64		-0.41	0.27	0.02	0.92	1.76	1.49	1.55	1 28	1.06
8. 8	1.24	1.62	1.87		-0.72			0.65	1.35	1.31	1.37	1.24	0.86
9. 9	1.10	1.15	0.74		-0.79	-0.34	-0.54	0.03	0.59	0.77	0.83	0.86	0.43
10.10	0.70	0.88				-0.56			-0.34	0.05	0.07	0.25	
10.10	0.70	U.30	-0.09	-0.07	~0.03	-0.00	0.00	-U.J-1		0.00	0.07	0.20	V.11
7. 2. 9	-0.86	-0.43	-0.56	-0.74	-1.31	-1.49	-1.28	-0.88	-0.63	-0.47	-0.59	-0.50	-0.81
6. 2. 8	-0.95				-1.13		-1.10					-0.63	
6. 2.10	1	-0.32		0.27		0.05		0.72	0.47			-0.43	
6. 2. 6			-1.76								-1.04		-1.85
	-,-,	••••						-:-					
7. 2	-1.64	-1.09	-1.16	-2.42	-2.7 0	-8.14	-2.56	-2.14	-1.83	-0 97		-0.75	-1.77
8. 2	-1.65	-1.40	-2 25	-8.67	-4-45	-4.48	-4.28	-3.84	-3.27	-1.71	-1.29	-0.89	-2.76
8. 1	-1.81	-1.27	-2.13	-8.4 9	-4.07	-4.29	-3.86	-8.50	-3. 18	-1.54	-1.22	-0.85	-2.56
7. 1	-1.80	-0.97	-1.04	-2.24	-2.83	-2.93	-2.19	-1.80	-1.69	-0.80	-0.81	-0.70	-1.57
9.12.3.9	_, ,=	1 00	0.00			4 00		4 0-	0.00		1 00	,	0 17
	-1.45							-4.37		1			
7. 2.2(9)	-0.47	-U.U9	-0.27	0.09	-U.63	-0.68	-∪.63	-0.18	U.US	-0.28	~∪.45	v.83	-U.31
Dail. ext.	-1.24	-1.04	0.59	-0.68	0.74	0.84	0.56	0.14	-0 82	-0.47	-0 79	-0.74	-0.41
					<u>'</u>			ليسيبا			<u></u>	ــــــــــــــــــــــــــــــــــــــ	احسيا

XXXII.

SIBERIA. — BARNAUL. Lat. 53° 20' N. Long. 83° 27' E. Greenw. orrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Resumur. Hours. March. April. May. June. July. Sept. Oct. Nov. Dec. Mean. Jan. Feb. Aug. 1.18 0.82 2.09 2.44 8.92 3.48 8.72 8.16 2.42 1.86 1.10 0.81 2.20 Morn. 1 1.25 2.48 2.80 4.58 8.94 4.84 8.71 2.89 1.68 1.82 0.89 2.56 0.95 1.20 2.79 3.14 4.87 4.26 4.78 4.28 8.40 2.01 1.49 0.922.85 3 1.10 2.29 1.65 0.97 2.96 1.06 4.78 4.06 4.74 4 1.253.12 8.81 4.51 8.77 4.222.43 1.78 1.09 2.88 5 0.921.39 3.30 4.14 8.87 4.84 8.82 3.15 0.87 2.61 2.97 2.42 8.19 8.61 8.40 2.35 1.85 1.24 2.51 6 1.48 4.17 1.75 0.89 2.62 1.80 2.38 1.98 1.76 1.83 7 1.42 1.72 1.50 1.11 2.48 8 0.881.15 1.65 0.61-0.05-0.08 0.31 0.87 1.20 1.321.40 1.20 0.87 0.68 0.88 -0.57 -1.84 -1.10 -1.03 -0.64 -0.25 0.44 0.78 0.77 9 0.61 10 0.20 -0.16 -0.97 -1.66 -2.25 -2.05 -2.08 -1.92 -1.63 -0.54 -0.18 0.05 - 1.10-0.54 - 1.02 - 2.18 - 2.57 - 2.82 - 2.66 - 2.82 - 2.88 - 2.76 - 1.47 - 1.16 - 2.82 - 2.88 - 2.76 - 2.88 - 2.88 - 2.76 - 2.88 --0.78 -1.97 11 -1.37 | -1.79 | -3.06 | -3.26 | -3.20 | -3.25 | -3.34 | -3.54 | -3.55 | -2.22 | -1.99 | -1.52 | -2.67Noon. . . **-8.9**8 -2.04 -2.28 -3.54 -3.71 -3.57 -8.73 -8.74 -3.98 | -2.69 | -2.48 | -1.95 | -3.14 2 -2.34 -2.39 -3.65 -3.87 -3.90 -3.90 -4.07 -4.28 -4.10 -2.84 -2.54 -1.99 -3.82 -4.39 -3.92 -2.69 -2.23 -1.68 -3.23 -2.19 -2.12 -3.45 -3.78 -4.18 -3.96 -4.25 2 -1.68 |-1.58 |-3.04 |-3.26 |-4.22 |-3.56 |-4.16 |-4.22 |-3.47 |-2.32 |-1.71 |-1.19 |-2.87 4 -1.00 -2.51 -2.48 -3.85 -2.81 -8.71 -8.68 -2.78 -1.80 -1.14 -0.71 -2.29 5 -0.95-1.22 | -0.69 | -0.37 | -1.666 0.40 -0.37-2.87 -1.49 -3.03-1.95**-2.**88 -2.75-1.89 -0.66 -0.38 -0.19 -0.81 7 0.01 0.04-1.16 -0.46 -1.85 -0.86 -1.78 -1.56-0.92 0.01 -0.16 -0.18 -0.10 -0.11 0.210.28 -0.48 0.46 -0.58 0.05 -0.58 -0.30 8 0.81 0.41 0.28 1.16 0.65 0.80 0.559.80 0.78 0.24 0.00 , 0.00 0.50 0.420.49 1.61 1.68 1.55 1.50 1.63 1.33 0.57 0.28 0.17 1.01 10 0.89 0.63 0.57 1.39 1.89 2.53 2.11 2.31 2.211.71 0.83 0.51 0.41 1.48 0.82 0.90 3.27 2.78 3.08 2.68 2.04 1.09 0.64 1.82Midn. . . 0.691.77 2.14 0.240.55 0.65 0.56 - 0.030.24 0.15 0.430.75 0.57 0.58 0.44 0.436. 6 0.63 -0.18 0.01 0.41 0.78 0.66 0.69 0.57 0.47 7. 7 0.45 0.73 0.73 0.12 8. 8 0.55 0.72 0.61 0.54 - 0.32-0.02 -0.13 0.290.60 0.58 0.61 0.550.88 0.30 -0.85 0.08 0.34 0.87 0.38 0.19 9. 9 0.49 0.510.33-0.15 -0.24 0.260.17 -0.04 -0.03 -0.28 -0.25 -0.29 10.10 0.31-0.15-0.15 0.02 0.08 0.11 -0.05 7. 2. 9 -0.38-0.19 -0.25 --0.33|--0.58|--**0.66|--**0.57| -0.37-0.28 -0.21 -0.26-0.226. 2. 8 -0.42-0.21 0.03 -0.27 -0.50 -0.48 -0.49 -0.82-0.28 -0.22 -0.29 -0.28 -0.81 -0.15 0.320.08 -0.19 6. 2.10 -0.35 -0.14 0.47 0.12 0.250.02 0.21 0.210.07 -0.62 -0.43 -0.78 -0.92 -1.82 -1.14 -1.25 -1.14 -0.86 -0.57 -0.46 -0.37 -0.826. 2. 6 -0.52 -1.80 -1.20 -1.40 -1.14 -0.95 -0.81 -0.43 -0.39 7. 2 -0.49 -0.33 -0.79 -1.45 -0.76 -0.57 -0.40 -1.23 8. 2 -0.73|-0.62|-1.00|-1.63|-1.98|-1.99|-1.88|-1.71| -0.58 -0.57 |-0.95|-1.55|-1.81|-1.91|-1.72|-1.56|-0.69-0.54-0.38 -1.14 8. 1 -1.397. 1 -0.58 | -0.43 | -0.46 | -1.00 | -1.04 | -1.31 | -0.97 | -0.80 | -0.75 | -0.36 -0.36 -0.81 -0.70 -1.46 - 1.60 - 2.02 - 1.88 - 2.02 - 1.94 - 1.74 - 1.06 - 0.879.12.3.9 -0.64 |--0.72 | -0.61 -1.88 -0.21 -0.04 -0.12 0.04 -0.28 -0.80 -0.29 -0.08 -0.02 -0.10 -0.20-0.17 --0.15 7. 2.2(9)

0.25

0.06 | -0.14 | -0.21 | -0.85 | -0.88 | -0.18

0.33

Dail. ext.

-0.55 --0.46

0.26 - 0.28

XXXIII.

SIBERIA. - BARNAUL. Lat. 53° 20' N. Long. 83° 27' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — DOVE.

Degrees of Resumur.

Hour.	Jan.	Feb.	March.	April.	May.	Inne.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year
Midn.	0.99	1.98	2.48	2.65	8.70	3.75	8.48	8.10	2.80	1.99	1.06	0.77	2.3
1	1.15	2.21	2.77	3.03	4.11	4.30	4.07	8.50	3.20	2.24	1.22	0.86	2.7
2	1.26	2.36	8.18	3.24	4.47	4.83	4.49	8.90	8.63	2.50	1.39	0.95	8.0
8	1.41	2.47	8.34	3.49	4.72	4.95	4.77	4.29	8.92	2.69	1.46	1.01	3.2
4	1.56	2.56	3.61	8.59	4.20	4.41	4.40	4.23	4.11	2.89	1.51	1.07	3.1
5	1.55	2.68	8.70	2.78	2.85	8.12	8.84	8.60	8.90	2.91	1.57	1.10	2.7
6	1.61	2.69	2.90	1.58	1.44	1.75	1.88	2.29	8.06	2.68	1.59	1.09	2.0
7	1.53	2.80	1.63	0.46	0.28	0.49	0.50	0.85	1.54	1.84	1.50	1.18	1.1
8	0.94	1.15	0.13	-0.69	-0.80	-0.65	-0.54	-0.51	-0.08	0.87	0.93	0.93	0.1
9	0.27	-0.47	-1.85	-1.80	-1.94	-1.78	-1.81	-1.79	-1.62	-0.73	-0.03	0.11	-1.0
10	-0.79	-1.90	-2.86	-2.6 8	-2.71	-2.75	-2.70	-2.80	-2.84	-1.96	-1.12	-0.83	-2.1
11	-1.69	-2.95	-3.31	-3.27	-8.39	-8.89	-3.44	-3.41	-8.75	-2.81	-1.93	-1.62	-2.9
Noon.	-2.35	-3.89	-3.78	-3.66	-3.73	-3.98	-3.90	-3.81	-4.19	-3.48	-2.42	-2.04	-3.4
1	-2.61	-4.25	-4.11	-3.6 8	-4.04	-4.19	-4.09	-4.11	-4.41	-3.72	-2.57	-2.12	-3.6
2	-2.39	-4.23	-4.07	-3.65	-4.13	-4.34	-4.21	-4.10	-4.34	-3.64	-2.39	-1.70	-3.6
8	-1.88	-3.62	-3.69	-3.89	-4.09	-4.19	-3.89	-8.91	-4.11	-3.17	-1.66	-1.09	-3.2
4			-2.67	-2.62	-3.51	-3.57	-8.65	-3.68	-3.21	-2.53	-1.05	-0.76	-2.5
5	-0.81	-1.80	-1.69	-1.82	-8.09	-8.01	-3.07	-2.78	-2.29	-1.49	-0.71	-0.53	-1.8
6	-0.41	-0.56	-0.84	-0.62	-1.92	-2.19	-2.09	-1.54	-1.05	-0.72	-0.33	-0.28	-1.0
7	-0.20	0.09	0.35	0.27	-0.46	-0.84	-0.69	-0.20	-0.17	-0.08	-0.03	-0.02	-0.1
8	0.12	0.69	0.89	0.99	0.77	0.51	0.52	0.67	0.60	0.31	0.23	0.19	0.5
9	0.32	1.08	0.88	1.50	1.64	1.48	1.42	1.46	1.26	0.82	0.42	0.39	1.0
10	0.73	1.47	1.46	2.02	2.42	2.31	2.22	2.04	1.85	1.29	0.58	0.58	1.5
11	0.78	1.76	1.92	2.35	8.11	8.05	2.88	2.58	2.36	1.68	0.83	0.75	2.0
Mean.	-14.71	-18.47	-5.47	1.77	7.78	18.62	14.98	12.76	7.53	1.58	-8.36	-13.07	4.94

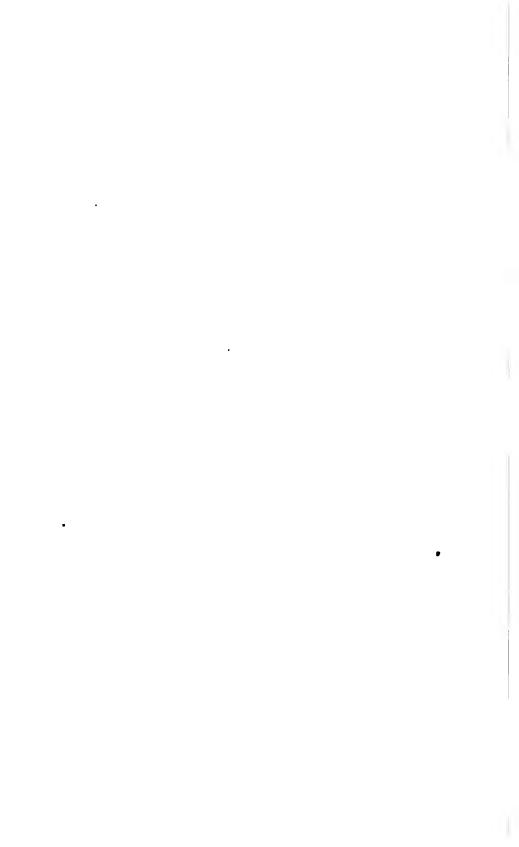
The numbers without sign must be added; those with the sign — must be subtracted.

HOURLY CORRECTIONS

FOR

PERIODIC VARIATIONS.

EUROPE.



XXXIV.

ITALY. - ROME. Lat. 41° 54' N. Long. 12° 25' E. Greenw.

orrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	0.00	- 00			- 00		0.10		W 00	1 80		0.98	1.55
Morn. 1	0.90	1.08	1.22	1.55	1.88	2.44	2.17	2.20	1.63	1.50	1.15		
2	0.99	1.26	1.50	1.84	2.10	2.59	2.41	2.49	1.91	1.75	1.29	1.02	1.76
8	1.14	1.58	1.96	2.31	2.56	3.02	2.99	8.00	2.88	2.12	1.53	1.19	2.15
4	1.36	1.99	2.46	2.80	3.06	8.51	3.6 8	8.54	2.91	2.58	· 1.87	1.48	2.60
l						1		1					
5	1.60	2.36	2.80	8.07	8 30	8.71	4.06	8.79	8.25	2.96	2.22	1.70	2.90
6 [1.77	2.52	2.76	2.92	3.04	3.86	8.81	3.53	8.17	3.10	2.42	1.87	2.86
7	1.74	2.33	2.24	2.25	2.19	2.38	2.82	2.62	2.58	2.82	2.38	1.83	2.84
8	1.40	1.78	1.29	1.15	0.98	0.98	1.27	1.22	1.51	2.05	1.82	1.47	1.40
				l i		1			1				
9	0.72	0.78	0.10	-0.15	-0.47	-0.51	-0.44	-0.35	0.15	0.86	0.93	0.78	0 20
10	-0.24	-0.39	-1.08	-1.39	-1.68	-1.75	-1.89	-1.78	-1.28	-0.58	-0.22	-0.15	-1.08
11	-1.27	-1.54	-2.06		(1		-2.84	-2.41		-1.41	-1.14	-2.09
Noon	-2.15		-2.71		-8.01		-3.88				I	I	i I
NOOE	2.15	2.48	2.11	2.50	3.01	9.00	0.00	-0.45	0.24	0.14	2.03	1.00	01
1 1	-2.69	-3.07	-8.02	_8.27	-3.23	-8.40	-8.61	-8.81	-8.70	-3.82	-8.00	-2.52	-8.26
2	-2.78		1 1		-3.81	í		-8.92		-3.99	ı	1	
1 - 1									1			-2.44	
8	-2.44	-3.03	-2.84			-8.97			-8.59			l .	
4	-1.83	-2.51	-2.45	-2.72	-3.14	-4.05	-2.58	-8.62	-8.11	-8.04	-2.41	-1.90	-2.59
1 - 1											_1 80	_1 05	
5	-1.11	-1.81	-1.89		-2.70					-2.21		-1.85	
6	-0.45			1				-2.18	1	-1.82	•	1	-1.52
7	0.05	-0.84	-0.44	-0.53	-0.84	-1.42	-1.38	-1.01	-0.51	-0.50	ı		-0.64
8	0.89	0.25	0.26	0.80	0.29	0.13	0.08	0.21	0.88	0.19	0.05	0.17	0.28
i !		l				•		1	l I		ı	1	1 1
9	0.59	0.67	0.78	0.94	1.22	1.46	1.33	1.22	1.05	0.71	0.46	0.46	0.91
10	0.71	0.90	1.07	1.31	1.76	2 29	2.10	1.86	1.43	1.05	0.76	0.66	1.33
111	0.78	0.99	1.15	1.44	1.98	2.57	2.33	2.11	1.54	1.24	0.95	0.79	1.49
Midn	0.84	1.02	1.15	1.46	1.88	2.51	2.24	2.14	1.55	1.36	1.06	0.86	1.51
				2.12								1	1 1
i i								1					
6. 6	0.66	0.74	0.78	0.76	0.57	0.28	0.57	0.68	0.85	0.89	0.67	0.56	0.67
7. 7	0.90	1.00	0.90	0.86	0.68	0.48	0.72	0.80	1.08	1.16	0.92	0.80	0.85
8. 8	0.89	0.99	0.77	0.72	0.61	0.55	0.67	0.71	0.95	1.12	0.94	0.82	1 1
1										ı	0.70	0.62	0.55
9. 9	0.65	0.72	0.44	0.40	0.37	0.48	0.45	0.48	0.60	0.78		i	1 1
10.10	0.24	0.26	-0.01	-0.04	0.04	0.27	0.10	0.04	0.10	0.28	0.27	0.26	0.15
1			0.01	0.00	0.00	A A*	A 10	0.00	0.00	-0.15	-0.12	-0.12	-0.05
7. 2. 9	-0.15	l .			0.08	0.05	0.18		-0.06		l .		1 3
6. 2. 8	-0.21	-0.16	-0.01	-0.02	0.01	-0.07	0.04		-0.08		1	4	-0.10
6. 2.10	-0.10	0.06	0.26	0.32	0.50	0.65	0.72	0.49	0.27	0.05		-0.04	
6. 2. 6	-0.49	-0.59	-0.49	-0.58	-0.73	-1.04	-0.87	-0.86	-0.70	-0.74	-0.61	-0.51	-0.68
1	l											١	
7. 2	-0.52												
8. 2	-0.69	-0.76	-0.88	-1.07			-1.25	-1.85	-1.15				-1.00
8. 1	-0.65	-0.67					-1.17				-0.59		
7. 1	-0.48	-0.37	-0.39	-0.51	-0.52	-0.51	-0.40	-0.60	-0.56	-0.50	-0.34	-0.35	-0.46
1									ı	l	ł		
9.12.3.9	-0.82	-1.02	-1.17	-1.82	-1.89	-1.53	-1.60	-1.62	-1.41	-1.82	-0.98	-0.80	-1.25
7. 2.2(9)	0.04	0.11	0.19		0.83	0.40	0.48	0.29	0.22	0.06	0.02	0.02	0.19
(-)									1	l	ĺ		1
Dail.ext.	-0.51	-0.87	-0.12	-0.11	-0.01	-0.17	0.09	-0.07	-0.28	-0.45	-0.87	-0.40	-0.25
L'au. CAb.	U.01	7.01	U.14		0.01	U.L.	7.03						

XXXV.

ITALY. - PADUA. Lat. 45° 24' N. Long. 11° 52' E. Greenso.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

						s of Re							
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Monn
	·												
Morn. 1	0.38	0.57	0.89	1.28	2.48	2.21		2.27	1.59		•		1.45
2	0.58	0.81	1.20	1.49	2.70	2.40	3.20	2.70	1.85	1.08	1.16	0.96	1.67
8	0.76	0.97	1.42	1.66	8.00	2.68	8.53	8.05	2.10	1.20	1.26	0.96	1.88
4	0.79	1.18	1.68	1.97	8.14	2.71	8.78	8.44	2.34	1.89	1.35	1.05	2.06
il l						i							
5	1.06	1.81	1.89	2.26	2.97		3.34	3.44	2.66	1.58	1.42		
6	1.18	1.46	2.06	2.22	1.96	1.22	2.07	2.98	2.54	1 54	1.49	1.16	1.82
7	1.25	1.58	1.86	1.82	0.66		0.56	1.82	1.78	1.37	1.58	1.23	1.30
8	1.07	1.42	0.66	1.08	-0.28	-0.65	-0.25	0.58	0.79	0.81	0.97	1.00	0.60
	0.00	0.00	0.61	A 10			1.00		A ro	A 10	0.02	Λ 00	-0.28
9	0.70	0.82	0.61			-1.24							
10						-1.66							
11						-2.28							
Noon	-v.96	-1.24	-1.52	-1.27	-2.74	-2.52	-6.16	-2.97	-z.14	-1.41	-z.U2	-1.00	-1.54
1	-1.89	-1.45	-1.54	_1.69	-2.89	-2.61	-8.52	_8.84	-2.54	-1.74	-2.49	-1.90	-2,25
2						-2.62							
8						-2.59							
4						-2.20							
	-1.10	-1.0-1		-2.10	-2.01	-2.20	2.02	-0.20		-1.04	1.00		
5	-0.87	-0.98	-1.89	-1.96	-2.06	-1.60	-2.44	-2.49	-1.60	-1.05	-0.73	-0.74	-1.50
6						-1.00						-0.83	
7						-0.12						-0.15	Ħ
8			-0.48						-0.10			1 1	0.06
	0.0.	0.25	"-	0.20	0.22			0.00		5.55	0.00	.5.7.7	i
9	0.05	-0.14	-0.10	-0.11	1.11	1.38	1.54	1.01	0.28	0.26	0.49	0.26	0.50
10	0.18	0.09	0.24	0.27	1.44	1.72	1.67	1.36	0.58	0.52	0.72	0.46	0.77
11	0.29	0.31	0.48	0.60	1.75	1.86	2.14	1.78	0.84	0.68	0.86	0.59	1.02
Midn	0.87	0.49	0.72	0.85	2.02	2.10	2.48	2.23	1.36	0.78	0.94	0.70	1.25
1 1							i l	l i					- 11
1		1									_		
6.6	0.27	0.34											0.46
7. 7	0.47	0.48				-0.02				0.62		0.54	0.47
8.8	0.50	0.50		0.28		-0.14			0.85	0.48			0.33
9.9	0.88	0.84	0.26	0.04	0.02		-0.05	1 1	-0.18	0.22		0.30	0.11
10.10	0.14	0.01	-0.80	-0.06	-0.18	0.08	-0.81	-0.27	-0.28	0.01	-0.05	0.10	-0.09
		0.00	0.01		0.00	0.00	. 0 55	-0.90	Λ 60		_0 10	_0 70	_0 01
7. 2. 9		-0.06				-0.39							
6. 2. 8	,, ,		1 1			-0.84							
6. 2.10	11 1	-0.02					-0.00		0.09			-0.15	
6. 2. 6	-0.82	-0.32	-0.23	-0.40	-0.78	-0.80	-1.08	-0.71	-0.38	-0.54	-V.4U	-0.41	-0.31
7. 2	-0.12	-0.02	0.08	-0.05	-1.14	-1.27	-1.59	-0 96	-0.52	-0.32	-0.49	-0.42	-0.57
8. 2						-1.64							
8. 1						-1.68							
7. 1	-0 07					-1.27							
K ** *	""	VIOI	0.10	V.01	1.11	1.2	2.40	30		4.10			
9.12.3.9	-0.42	-0.55	-0.68	-0.84	-1.41	-1.24	-1.70	-1.86	-1 84	-0.75	-0.98	-0.65	-1.03
7. 2.2(9)			-0.02				-0.08					-0.08	
Dail.ext.	-0.18	-0.04	0.08	0.06	0.10	0.05	0.02					-0.42	
					2.10			يتنت					

XXXVI.

SWITZERLAND. - GENEVA. Lat. 46° 12' N. Long. 6° 9' E. Greenw.

corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Resumur.

Hour.	Jen.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oot.	Nov.	Dec.	Year.
Midn.	0.50	0.68	1.38	1.68	2.16	2.77	2.54	2.88	1.86	1.44	0.80	0.48	1.56
1	0.62	0.83	1.88	2.14	2.72	3.32	3.19	8.08	2.41	1.71	0.97	0.54	1.95
2	0.74	1.01	2.34	2.53	3.16	3.68	3.70	8.68	2.98	1.95	1.14	0.61	2.29
3	0.83	1.22	2.70	2.76	8.40	8.74	3.89	4.08	8.84	2.14	1.30	0.70	2.50
4	0.92	1.46	2.89	2.78	8.34	8.50	3.80	4.00	3.49	2.22	1.43	0.81	2.55
5	0.98	1.66	2.83	2.54	2.93	2.88	8.26	8.52	3.30	2.14	1.51	0.91	2.87
6	1.02	1.75	2.49	2.03	2.22	2.08	2.89	2.65	2.72	1.85	1.48	0.97	1.97
7	0.97	1.66	1.90	1.83	1.28	1.06	1.38	1.54	1.84	1.84	1.26	0.92	1.87
8	0.78	1.33	1.09	0.50	0.27	0.08	0.26	0.87	0.78	0.65	0.84	0.70	0.64
9	0.46	0.74	0.17	-0.34	0.69	-0.82	-0.71	-0.70	-0.30	-0.15	0.23	0.34	-0.16
10	-0.02	-0.01	-0.77	-1.10	-1.51	-1.57	-1.58	-1.58	-1.26	-0.98	-0.47	-0.16	-0.91
11	-0.57	-0.80	-1.61	-1.75	-2.17	-2.18	-2.24	-2.29	-2.06	-1.70	-1.14	-0.67	-1.60
Noon.	-1.06	-1.49	-2.26	-2.2 3	-2.66	-2.70	-2.74	-2.85	-2.66	-2.22	-1.66	-1.10	-2.14
1	-1.40	-1.98	-2.70	-2.55	-2.9 8	-3.10	-3.18	-8.29	-3.08	-2.53	-1.94	-1.87	-2.51
2	-1.50	-2.18	-2.87	-2.67	-3.12	-3.35	-8.48	-8.58	-3.2 9	-2.58	-1.94	-1.41	-2.66
8	-1.41	-2.10	-2.81	-2.61	-3.07	-8.42	-8.51	-3.65	-3.2 8	-2.41	-1.74	-1.26	-2.61
4	-1.14	-1.82	-2.54	-2.87	-2.80	-3.25	-8.37	-8.43	-3.04	-2.06	-1.88	-0.97	-2.35
5	-0.79	-1.37	-2.10	-1.97	-2.32	-2.78	-2.90	-2.92	-2.57	-1.59	-0.99	-0.64	-1.91
6	-0.46	-0.94	-1.59	-1.46	-1.70	-2.11	-2.22	-2.18	-1.91	-1.06	-0.62	-0.82	-1.88
7	-0.20	-0.51	-1.06	-0.90	-1.00	-1.29	-1.40	-1.31	-1.16	-0.53	-0.80	-0.07	-0.81
8	-0.01	-0.14	-0.54	-0.34	-0.29	-0.42	-0.49	-0.46	-0.42	-0.02	-0.03	0.11	-0.26
9	0.12	0.14	0.05	0.20	0.38	0.47	0.84	0.32	0.26	0.42	0.20	0.24	0.26
10	0.25	0.37	0.42	0.70	0.91	1.30	1.10	1.02	0.83	0.82	0.42	0.84	0.71
11	0.87	0.54	0.90	1.20	1.51	2.07	1.87	1.70	1.85	1.15	0.62	0.41	1.14
Mean	-0.58	1.24	8.41	6.77	10.87	13.81	14.80	13.58	11.46	7.48	8.76	0.58	

XXXVII.

SWITZERLAND. — GENEVA. Lat. 46° 12' N. Long. 6° 9' E. Gr. — DOVE.

Degrees of Resumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.45	0.69	1.26	1.44	1.54	1.98	2.12	1.63	1.44	0.94	0.50	0.59	1.21
2	0.70	0.96	2.21	2.62	2.60	8.20	3.18	2.88	2.72	1.46	0.78	0.66	1.99
4	1.01	1.33	2.91	3.36	3.11	8.55	8.82	8.51	8.26	1.90	1.02	0.80	2.46
6	1.19	1.49	2.70	2.87	2.26	2.38	2.47	2.82	2.79	1.74	1.13	0.97	2.07
8	1.22	1.22	1.42	0.74	0.27	0.13	0.22	0.49	0.72	0.94	0.90	0.95	0.77
10	-0.02	-0.25	-0.68	-1.70	-1.30	-1.34	-1.25	-1.01	-1.10	-0.78	-0.26	-0.14	-0.78
Noon.	-0.13	-1.80	-1.97	-2.14	-2.42	-2.54	-2.50	-2.34	-2.38	-1.86	-1.18	-1.22	-1.91
2	-1.69	-1.70	-2.82	-2.94	-2.97	-8.09	-3.11	-3.17	-8.03	-2.35	-1.55	-1.46	-2.49
4	-1.30	-1.61	-2.70	-2.94	-2.46	-2.87	-2.89	-3.04	-2.86	-1.58	-1.19	-1.05	-2.20
6	-0.54	-0.90	-1.79	-2.06	-1.40	-1.89	-2.24	-2.04	-1.74	-0.88	-0.45	-0.43	-1.86
8	-0.09	-0.21	-0.89	-0.70	-0.10	-0.25	-0.58	-0.38	-0.3 8	-0.08	0.03	0.10	-0.29
10	0.20	0.28	0.34	0.40	0.86	0.78	0.78	0.69	0.57	0.47	0.29	0.18	0.49
Mean.	1.20	0.47	2.28	6.81	9.48	12.82	14.48	18.74	10.66	7.73	8.30	0.12	

XXXVIII.

SWITZERLAND. - St. BERNARD. Lat. 45° 52' N. Long. 9° 22' E. Gr.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dovs.

Degrees of Resumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.48	0.81	1.84	1.96	2.10	1.72	1.62	1.30	0.76	1.02	0.59	0.31	3.17
1	0.63	0.91	1.58	2.22	2.45	1.99	1.98	1.58	0.97	1.17	0.66	0.33	1.36
2	0.81	1.09	1.82	2.40	2.78	2.15	2.14	1.82	1.17	1.80	0.78	0.40	1.55
8	0.99	1.26	1.98	2.46	2.81	2.24	2.24	1.94	1.34	1.86	0.89	0.50	1.67
4	1.08	1.38	2.02	2.84	2.67	2.14	2.17	1.91	1.41	1.34	0.98	0.52	1.66
5	1.08	1.84	1.84	2.00	2.28	1.88	1.90	1.70	1.85	1.19	0.98	0.66	1.52
6	0.91	1.14	1.42	1.45	1.72	1.42	1.44	1.84	1.14	0.92	0.86	0.62	1.20
7	0.60	0.74	0.79	0.70	0.81	0.81	0.82	0.76	0.77	0.83	0.61	0.50	0.73
8	0.17	0.18	0.00	-0.16	-0.08	0.09	0.10	0.12	0.29	0.06	0.26	0.26	0.11
9	-0.31	-0.48	-0.85	-1.06	-1.10	-0.66	-0.66	-0.58	-0.26	-0.46	-0.22	-0.06	-0.55
10	-0.78	-1.18	-1.63	-1.86	-1.94	-1.86	-1.84	-1.13	-0.79	-0.94	-0.68	-0.41	-1.16
11	-1.14	-1.66	-2.2 8	-2.50	-2.58	-1.95	-1.90	-1.60	-1.22	-1.83	-1.09	-0.71	-1.66
Noon.	-1.84	-1.98	-2.58	-2.87	-2.96	-2.84	-2.26	-1.90	-1.51	-1.58	-1.36	-0.94	-1.97
1	-1.88	-2.04	-2.62	-2.98	-8.06	-2.51	-2.40	-2.02	-1.62	-1.66	-1.47	-1.03	-2.07
2	-1:24	-1.86	-2.8 8	-2.78	-2.89	-2.44	-2.33	-1.94	-1.56	-1.59	-1.39	-0.99	-1.95
8	-0.98	-1.47	-1.92	-2.36	-2.51	-2.21	-2.08	-1.74	-1.35	-1.38	-1.16	-0.82	-1.66
	-0.63	-0.97	-1.34	-1.79	-1.98	-1.80	-1.70	-1.42	-1.05	-1.07	-0.83	-0.57	-1.26
5	-0.82	-0.43	-0.78	-1.17	-1.40	-1.82	-1.26	-1.06	-0.70	-0.72	-0.46	-0.27	-0.82
6	-0.05	0.04	-0.19	-0.54	0.81	-0.80	-0.80	-0.70	-0.88	-0.86	-0.10	0.00	-0.89
7	0.14	0.39	0.25	0.04	-0.25	-0.28	-0.84	-0.34	-0.11	-0.03	0.19	0.21	-0.01
8	0.23	0.60	0.56	0.54	0.27	0.20	0.09	0.00	0.10	0.24	0.38	0.34	0.30
9	0.30	0.69	0.78	0.96	0.76	0.63	0.50	0.32	0.27	0.47	0.49	0.38	0.55
10	0.84	0.72	0.96	1.88	1.22	1.02	0.89	0.64	0.42	0.67	0.53	0.38	0.76
11	0.38	0.74	1.14	1.66	1.68	1.40	1.26	0.97	0.58	0.85	0.55	0.33	0.96
Mean.	-9.26	-6.62	-5.72	-2.97	0.74	3.55	4.82	4.82	2.40	-0.91	-3.95	-5.86	

XXXIX.

SWITZERLAND. — St. BERNARD. Lat. 45° 52' N. Long. 9° 22' E. Gr. — Dove.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct	Nov.	Dec.	Year.
Midn.	0.34	0.55	0.75	1.19	1.26	1.89	1.02	1.08	0.81	0.66	0.33	0.28	0.80
2	0.52	0.78	1.14	1.64	1.75	1.88	1.62	1.53	1.16	0.94	0.42	0.27	1.14
4	0.82	1.06	1.50	1.84	1.91	1.98	1.82	1.71	1.84	1.17	0.65	0.42	1.35
6	0.63	0.86	1.20	1.50	1.58	1.46	1.46	1.27	0.98	0.88	0.50	0.32	1.05
8	0.48	0.26	0.14	-0.08	-0.25	0.01	0.22	0.16	0.08	0.28	0.27	0.15	0.14
10	-0.35	-0.91	-1.06	-1.26	-1.39	-1.18	-1.11	-0.94	-0.86	-0.68	-0.54	-0.23	-0.88
Noon.	-1.40	-1.66	-1.74	-2.11	-2.15	-1.92	-1.81	-1.77	-1.58	-1.45	-1.26	-0.91	-1.65
2	-1.87	-1.55	-1.89	-2.12	-2.12	-2.23	-2.01	-1.97	-1.54	-1.52	-1.23	-1.22	-1.73
4	-0.42	-0.71	-1.14	-1.55	-1.47	-1.65	-1.49	-1.80	-0.88	-0.86	-0.37	-0.02	-0.98
6	0.09	0.17	0.09	-0.26	-0.35	-0.71	-0.57	-0.46	-0.26	-0.07	0.08	0.22	-0.17
8	0.25	0.44	0.49	0.49	0.50	0.85	0.30	0.26	0.26	0.22	0.70	0.30	0.38
10	0.37	0.55	0.55	0.71	0.76	0.64	0.56	0.48	0.46	0.43	0.40	0.40	0.52
Mean.	-6.09	-8.83	-6.66	-3.01	-0.42	2.71	4.82	4.70	2.07	-0:36	-5.46	-6.18	

XL.

Austria. — Kremshünster. Lat. 48° 3' N. Long. 14° 7' E. Greenw. orrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Hours. Jan. Feb. March April. May. June. July. Aug. Sept. Oct. Nov. Dec. Morn. 1 0.58 0.90 1.05 1.14 2.80 2.77 1.86 1.94 1.52 1.26 0.61 0.4 2 0.66 1.03 1.30 1.36 2.66 3.08 2.16 2.26 1.94 1.58 0.72 0.4 3 0.71 1.07 1.57 1.63 2.84 3.14 2.35 2.50 2.32 1.82 0.78 0.4 4 0.78 1.12 1.80 1.88 2.78 2.90 2.34 2.54 2.58 1.97 0.83 0.4 5 0.84 1.19 1.99 2.44 2.82 2.08 2.30 2.60 1.98 0.83 0.4 6 0.83 1.24 1.82 1.88 1.86 1.54 1.54 1.80 2.34	1 1.60 2 1.76 1 1.83 3 1.75 4 1.52 1 1.15 3 0.66 3 0.10 5 -0.56 3 -1.08
2 0.66 1.03 1.30 1.36 2.66 8.08 2.16 2.26 1.94 1.58 0.72 0.4 3 0.71 1.07 1.57 1.63 2.84 3.14 2.35 2.50 2.32 1.82 0.78 0.4 4 0.78 1.12 1.80 1.88 2.78 2.90 2.34 2.54 2.58 1.97 0.83 0.4 5 0.84 1.19 1.90 1.99 2.44 2.82 2.08 2.30 2.60 1.98 0.88 0.4 6 0.88 1.24 1.82 1.86 1.54 1.54 1.80 2.34 1.91 0.93 0.5 7 0.84 1.26 1.50 1.41 1.11 0.68 0.94 1.11 1.81 1.63 0.92 0.5 8 0.67 1.07 0.96 0.87 0.81 -0.15 0.28 0.35 1.09 1.21 0.80 0.5 9 0.35 0.67 0.30 0.14 -0.45 -0.86 -0.42 -0.37 0.28 0.62 0.51 0.51	1 1.60 2 1.76 1 1.83 3 1.75 4 1.52 1 1.15 3 0.66 3 0.10 5 -0.56 3 -1.08
2 0.66 1.03 1.30 1.36 2.66 8.06 2.16 2.26 1.94 1.58 0.72 0.4 3 0.71 1.07 1.57 1.63 2.84 3.14 2.35 2.50 2.32 1.82 0.78 0.4 4 0.78 1.12 1.80 1.88 2.78 2.90 2.34 2.54 2.58 1.97 0.83 0.4 5 0.84 1.19 1.90 1.99 2.44 2.82 2.08 2.80 2.60 1.98 0.88 0.4 6 0.88 1.24 1.82 1.86 1.54 1.54 1.50 2.34 1.91 0.93 0.5 7 0.84 1.26 1.50 1.41 1.11 0.68 0.94 1.11 1.81 1.63 0.92 0.5 8 0.67 1.07 0.96 0.87 0.81 -0.15 0.28 0.35 1.09 1.21 0.80 0.5 9 0.35 0.67 0.30 0.14 -0.45 -0.86 -0.42 -0.37 0.28 0.62 0.51 0.51	1 1.60 2 1.76 1 1.83 3 1.75 4 1.52 1 1.15 3 0.66 3 0.10 5 -0.56 3 -1.08
8 0.71 1.07 1.57 1.63 2.84 3.14 2.35 2.50 2.32 1.82 0.78 0.4 4 0.78 1.12 1.90 1.88 2.78 2.90 2.34 2.54 2.58 1.97 0.83 0.4 5 0.84 1.19 1.90 1.99 2.44 2.82 2.08 2.30 2.60 1.98 0.88 0.4 6 0.88 1.24 1.82 1.88 1.86 1.54 1.54 1.80 2.34 1.91 0.93 0.5 7 0.84 1.26 1.50 1.41 1.11 0.68 0.94 1.11 1.81 1.63 0.92 0.5 8 0.67 1.07 0.96 0.87 0.81 -0.15 0.28 0.35 1.09 1.21 0.80 0.5 9 0.35 0.67 0.30 0.14 -0.45 -0.86 -0.42 -0.37 0.28 0.62 0.51 0.3	1.76 1.83 1.75 1.52 1.15 0.66 0.10 5 -0.56 3 -1.08
4 0.78 1.12 1.80 1.88 2.78 2.90 2.34 2.54 2.58 1.97 0.83 0.4 5 0.84 1.19 1.90 1.99 2.44 2.82 2.08 2.30 2.60 1.98 0.88 0.4 6 0.88 1.24 1.82 1.88 1.86 1.54 1.54 1.80 2.34 1.91 0.93 0.5 7 0.84 1.26 1.50 1.41 1.11 0.68 0.94 1.11 1.81 1.63 0.92 0.5 8 0.67 1.07 0.96 0.87 0.81 -0.15 0.28 0.35 1.09 1.21 0.80 0.5 9 0.35 0.67 0.30 0.14 -0.45 -0.86 -0.42 -0.37 0.28 0.62 0.51 0.3	1.88 1.75 1.52 1.15 0.66 0.10 5 -0.56 3 -1.08
5 0.84 1.19 1.90 1.99 2.44 2.82 2.08 2.80 2.60 1.98 0.88 0.4 6 0.88 1.24 1.82 1.88 1.86 1.54 1.54 1.80 2.34 1.91 0.93 0.5 7 0.84 1.26 1.50 1.41 1.11 0.68 0.94 1.11 1.81 1.63 0.92 0.5 8 0.67 1.07 0.96 0.87 0.81 -0.15 0.28 0.35 1.09 1.21 0.80 0.5 9 0.35 0.67 0.30 0.14 -0.45 -0.86 -0.42 -0.37 0.28 0.62 0.51 0.3	1.75 1.52 1.15 0.66 0.10 5 -0.56 3 -1.08
6 0.88 1.24 1.82 1.88 1.86 1.54 1.54 1.80 2.34 1.91 0.93 0.5 7 0.84 1.26 1.50 1.41 1.11 0.68 0.94 1.11 1.81 1.63 0.92 0.5 8 0.67 1.07 0.96 0.87 0.81 -0.15 0.28 0.35 1.09 1.21 0.80 0.5 9 0.35 0.67 0.30 0.14 -0.45 -0.86 -0.42 -0.37 0.28 0.62 0.51 0.3	1.52 1.15 0.66 0.10 -0.56 -1.08
6 0.88 1.24 1.82 1.88 1.86 1.54 1.54 1.80 2.34 1.91 0.93 0.5 7 0.84 1.26 1.50 1.41 1.11 0.68 0.94 1.11 1.81 1.63 0.92 0.5 8 0.67 1.07 0.96 0.87 0.81 -0.15 0.28 0.35 1.09 1.21 0.80 0.5 9 0.35 0.67 0.30 0.14 -0.45 -0.86 -0.42 -0.37 0.28 0.62 0.51 0.3	1.52 1.15 0.66 0.10 -0.56 -1.08
7 0.84 1.26 1.50 1.41 1.11 0.68 0.94 1.11 1.81 1.63 0.92 0.5 8 0.67 1.07 0.96 0.87 0.81 -0.15 0.28 0.35 1.09 1.21 0.80 0.5 9 0.35 0.67 0.30 0.14 -0.45 -0.86 -0.42 -0.37 0.28 0.62 0.51 0.8	1.15 0.66 0.10 -0.56 -1.08
8 0.67 1.07 0.96 0.87 0.81 -0.15 0.28 0.35 1.09 1.21 0.80 0.5 9 0.35 0.67 0.30 0.14 -0.45 -0.86 -0.42 -0.37 0.28 0.62 0.51 0.8	0.66 0.10 -0.56 -1.08
9 0.35 0.67 0.30 0.14 -0.45 -0.86 -0.42 -0.37 0.28 0.62 0.51 0.3	0.10 -0.56 -1.08
	-0.56 -1.08
	-0.56 -1.08
"A _0 10 0 01 _0 41 _0 69 _1 10 _1 49 _0 06 _0 09 _0 69 _0 19 0 06 0 0	-1.08
11 -0.58 -0.72 -1.06 -1.20 -1.65 -1.84 -1.39 -1.47 -1.23 -0.92 -0.47 -0.3	
Noon -0.98 -1.87 -1.56 -1.65 -2.09 -2.17 -1.75 -1.86 -1.81 -1.68 -0.97 -0.76	-1.56
1 -1.22 -1.78 -1.89 -1.93 -2.42 -2.42 -2.05 -2.21 -2.28 -2.25 -1.30 -1.0	-1.90
2 -1.26 -1.90 -2.02 -2.06 -2.62 -2.58 -2.26 -2.88 -2.56 -2.53 -1.40 -1.0	
8 -1.12 -1.69 -1.99 -2.04 -2.67 -2.62 -2.33 -2.46 -2.65 -2.49 -1.28 -0.9	
4 -0.86 -1.32 -1.79 -1.89 -2.51 -2.49 -2.22 -2.34 -2.52 -2.17 -1.01 -0.6	
4 -0.00 -1.32 -1.19 -1.09 -2.01 -2.45 -2.22 -2.34 -2.32 -2.17 -1.01 -0.0	1.30
5 -0.59 -0.92 -1.48 -1.60 -2.15 -2.16 -1.88 -2.00 -2.18 -1.69 -0.68 -0.8	-1.47
6 -0.35 -0.57 -1.08 -1.18 -1.62 -1.66 -1.88 -1.49 -1.66 -1.14 -0.41 -0.1	-1.05
7 -0.18 -0.86 -0.65 -0.68 -0.98 -1.08 -0.76 -0.86 -1.05 -0.66 -0.22 0.0	-0.62
8 -0.04 -0.19 -0.28 -0.17 -0.84 -0.85 -0.15 -0.24 -0.46 -0.26 -0.11 0.0	1 1
	1 3.2
9 0.07 -0.02 0.13 0.28 0.28 0.34 0.38 0.30 0.06 -0.06 -0.02 0.1	0.16
10 0.20 0.18 0.42 0.61 0.84 1.02 0.82 0.76 0.46 0.34 0.11 0.11	0.49
11 0.84 0.46 0.63 0.82 1.86 1.68 1.19 1.15 0.80 0.68 0.27 0.2	0.80
Midn 0.47 0.70 0.88 0.97 1.85 2.27 1.52 1.58 1.14 0.94 0.46 0.8	1.08
6. 6 0.27 0.34 0.87 0.85 0.12 0.06 0.06 0.16 0.84 0.89 0.26 0.2	
7. 7 0.88 0.45 0.43 0.87 0.07 -0.18 0.09 0.18 0.88 0.48 0.85 0.2	1 1
8. 8 0.82 0.44 0.37 0.85 -0.02 -0.10 0.04 0.06 0.82 0.48 0.85 0.2	
9. 9 0.21 0.83 0.22 0.21 -0.09 -0.26 -0.02 -0.04 0.17 0.84 0.25 0.2	1 1
10.10 0.05 0.10 0.01 0.02 -0.13 -0.20 -0.07 -0.11 -0.03 0.11 0.09 0.1	0.00
7. 2. 9 -0.12 -0.22 -0.13 -0.12 -0.41 -0.52 -0.31 -0.32 -0.23 -0.28 -0.17 -0.1	-0 9K
6. 2. 8 -0.14 -0.28 -0.14 -0.12 -0.37 -0.46 -0.29 -0.27 -0.23 -0.29 -0.19 -0.1	
6. 2. 6 -0.24 -0.41 -0.48 -0.45 -0.79 -0.90 -0.70 -0.69 -0.63 -0.94 -0.36 -0.1	V.56
7. 2 -0.21 -0.32 -0.26 -0.33 -0.76 -0.95 -0.66 -0.63 -0.38 -0.45 -0.24 -0.2	-0.45
8. 2 -0.30 -0.42 -0.53 -0.60 -1.16 -1.22 -1.02 -1.02 -0.74 -0.66 -0.30 -0.2	7 -0.69
8. 1 -0.28 -0.86 -0.47 -0.53 -1.06 -1.14 -0.91 -0.98 -0.60 -0.52 -0.25 -0.2	-0.61
7. 1 $ -0.19 -0.26 -0.20 -0.26 -0.66 -0.87 -0.56 -0.55 -0.24 -0.81 -0.19 -0.26 $	
9.12.3.9 -0.42 -0.60 -0.78 -0.82 -1.23 -1.83 -1.03 -1.10 -1.08 -0.87 -0.44 -0.3	
7. 2.2(9) -0.07 -0.17 -0.07 -0.02 -0.24 -0.81 -0.15 -0.17 -0.14 -0.19 -0.18 -0.0	7 -0.14
Dail.ext. -0.19 -0.32 -0.06 -0.04 0.09 0.36 0.01 0.04 -0.03 -0.28 -0.24 -0.2	-0.08

XLI.

Austria. - Salzburg. Lat. 47° 48' N. Long. 13° 1' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees	ď	Resumur.
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Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.54	0.70	1.06	1.81	2.08	2.07	1.87	1.57	1.21	1.02	0.48	0.42	1.19
1	0.59	0.79	1.29	1.58	2.87	2.27	2.13	1.81	1.45	1.15	0.65	0.50	1.39
2	0.72	0.97	0.51	1.79	2.64	2.56	2.86	2.05	1.61	1.27	0.81	0.59	1.49
8	0.82	1.08	1.75	2.04	2.90	2.73	2.64	2.24	1.87	1.41	0.88	0.70	1
4	0.96	1.09	1.89	2.21	8.10	2.82	2.62	2.28	2.04	1.52	0.91	0.69	1.8
5	1.03	1.28	2.01	2.87	8.10	2.75	2.59	2.24	2.14	1.72	1.08	0.81	1.9
6	1.06	1.84	2.14	2.28	2.76	2.45	2.81	2.26	2.18	1.77	1.03	0.87	1.87
7	1.09	1.86	2.06	1.86	1.89	1.58	1.61	1.74	1.94	1.74	1.06	0.94	1.57
8	1.12	1.24	1.58	1.06	0.84	0.68	0.67	0.89	1.15	1.26	1.07	1.00	1.04
9	0.91	0.75	0.76	0.14	-0.10	-0.25	0.20	0.04	0.33	0.48	0.64	0.74	0.35
10	0.38	0.04	-0.06	-0.67	-0.92	-1.10	-0.97	-0.76	-0.58	-0.35	0.06	0.21	-0.39
11	-0.26	-0.62	-0.96	-1.39	-1.80	-1.87	-1.63	-1.40	-1.25	-1.17	-0.62	-0.35	-1.1
Noon.	-0.90	-1.19	-1.75	-1.99	-2.36	-2.90	-2.14	-2.18	-2.00	-1.84	-1.25	-0.93	-1.78
1	-1.47	-1.68	-2.26	-2.48	-2.82	-2.84	-2.59	-2.59	-1.48	-2.39	-1.68	-1.47	–2 .1:
2	-1.70	-1.96	-2.55	-2.74	-3.08	-8.03	-2.77	-2.73	-2.7 1	-2.55	-1.85	-1.64	-2.4
8	-1.68	-2.04	-2.61	-2.74	-8.21	-8.04	-2.90	-2.75	-2.67	-2.51	-1.75	-1.55	-2.45
4	-1.40	-1.80	-2.55	-2.60	-8.27	-3.00	-2.90	-2.85	-2.56	-2.21	-1.87	-1.19	-2.31
5	-1.00	-1.46	-2.26	-2.10	-2.97	-2.64	-2.64	-2.46	-2.09	-1.63	-0.85	-0.72	-1.90
6	-0.60	-0.76	-1.51	-1.52	-2.27	-2.10	-2.05	-1.78	-1.81	-0.88	-0.35	-0.42	-1.29
7	-0.31	-0.27	-0.76	-0.75	-1.48	-1.21	-1.24	-0.85	-0.48	-0.29	-0.10	-0.15	-0.6
8	-0.25	-0.02	-0.16	-0.07	-0.48	-0.13	-0.24	0.06	0.15	0.16	0.11	0.04	-0.06
9	-0.04	0.20	0.17	0.51	0.48	0.71	0.67	0.70	0.50	0.48	0.24	0.17	0.40
10	0.12	0.48	0.46	0.81	1.03	1.41	1.22	1.09	0.78	0.76	0.34	0.33	0.73
11	0.28	0.58	0.76	1.08	1.50	1.70	1.56	1.38	0.76	1.03	0.52	0.41	0.96
Mean.	-2.71	1.14	2.49	6.90	10.42	13.22	18.93	18.66	10.80	7.97	1.52	1.68	

XLII.

GERMANY. - MUNICH. Lat. 48° 9' N. Long. 11° 37' E. Greenw. - Dove.

Hour.	Jan.	Feb.	March.	April.	May.	June	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year
Midn.	0.71	0.92	1.54	2.27	2.58	2.49	2.84	2.37	2.17	1.58	0.91	0.46	1.73
1	0.90	1.04	1.88	2.37	8.02	8.06	8.27	2.64	2.88	1.59	0.87	0.58	1.96
2	0.97	1.18	2.04	2.62	8.80	8.39	3.56	2.94	2.61	1.67	0.94	0.67	2.16
8	1.04	1.80	2.16	2.89	3.61	3.66	3.80	3.19	2.81	1.78	1.00	0.77	2.33
4	1.08	1.88	2.25	8.12	8.85	3.82	4.05	8.41	2.98	1.91	1.04	0.85	2.47
5	1.07	1.48	2.87	8.29	3.69	8.25	8.71	8.50	8.16	2.01	1.12	0.92	2.46
6	1.14	1.52	2.56	2.93	2.61	2 11	2.41	2.79	3.08	2.14	1 13	0 99	2.12
7	1.17	1.55	2.17	1.80	1.21	0.77	0.98	1.48	2.22	1.84	1.13	0.97	1.44
8	1.10	1.14	1.14	0.36	-0.07	-0.35	-0.28	0.18	0.59	0.99	0.75	0.88	0.54
9	0.46	0.86	-0.11	-0.79	-1.00	-1.21	-1.25	-1.05	-0.74	-0.24	0.06	0.41	-0.42
10	-0.72	-0.61	-1.18	-1.80	-1.99	-1.96	-2.12	-1.88	-1.70	-1.34	-0.79	-0.42	-1.35
11	-1.06	-1.46	-2.04	-2.39	-2.59	-2.69	-2.66	-2.58	-2.61	-2.19	-1.49	-0.97	-2.06

XLII.

GERMANY. - MUNICH, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Resumur.

Hour.	Jen.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Noon	-1.70	-1.93	-2.67	-2.99	-3.28	-2.98	-3.14	-3.09	-3.18	-2.69	-1.94	-1.02	-2.5
1	'-2.0 8	-2.81	-8.01	-8.27	-3.59	-3.41	-3.48	-3.55	-8.58	-3.0 8	-2.23	-1.83	-2.9
2	-2.15	-2.40	-3.24	-3.60	-3.77	-8.79	-3.75	-3.72	-8.74	-8.15	-2.05	-1.85	-3.1
3	-1.83	-2.15	-3.17	-3.45	-8.77	-8.54	-3.83	-3.58	-3.56	-2.87	-1.75	-1.43	-2.9
4	-1.08	-1.67	-2.64	-3. 18	-3.41	-8.84	-3.49	-3.30	-3.24	-2.27	-1.02	-0.76	-2.4
5	-0.46	-0.95	-1.98	-2.51	-2.87	-2.80	-3.07	-2.76	-2.56	-1.27	-0.43	-0.34	-1.8
6	-0.16	-0.87	-0.94	-1.58	-2.05	-1.94	-2.32	-1.81	-1.29	-0.44	-0.12	-0.13	-1.0
7	0.04	-0.07	-0.20	-0.36	-0.74	-0.84	-2.99	-0.47	-0.80	0.08	0.20	0.06	-0.4
8	0.23	0.22	0.28	0.40	0.41	0.61	0.40	0.55	0.87	0.56	0.44	0.14	0.8
9	0.39	0.45	0.55	0.91	1.18	1.35	1.20	1.15	0.98	0.88	0.57	0.23	0.8
10	0.49	0.59	1.02	1.31	1.65	1.86	1.87	1.60	1.40	1.14	0.74	0.33	1.1
11	0.61	0.77	1.33	1.69	2.18	2.28	2.41	2.06	1.80	1.34	0.85	0.40	1.4
Mean	-2.15	-0.12	0.75	5.57	9.29	12.74	18.65	12.98	9.45	6.28	1.53	-1.28	

XLIII.

Bohemia. — Prague. Lat. 50° 5′ N. Long. 14° 25′ E. Greenw. — Dove.

					D	egrees of	Kesum	ur.					
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug	Sept.	Oct.	Nov.	Dec.	Year.
Midn	0.80	0.52	1.03	1.47	1.70	1.68	1.72	1.17	1.23	0.84	0.36	0.25	1.02
1	0.40	0.60	1.14	1.68	1.97	1.97	2.05	1.78	1.49	1.02	0.45	0.32	1.24
2.	0.50	0.71	1.29	1.95	2.25	2.23	2.84	2.10	1.72	1.19	0.54	0.39	1.43
3	0.55	0.88	1.44	2.17	2.46	2.47	2.60	2.38	1.96	1.81	0.61	0.50	1.61
4	0.65	0.89	1.60	2.39	2.75	2.71	2.91	2.63	2.19	1.49	0.70	0.56	1.79
5	0.71	0.99	1.72	2.64	2.96	2.86	8.07	2.88	2.48	1.65	0.77	0.65	1.94
6	0.77	1.00	1.81	2.75	2.96	2.71	2.92	2.93	2.61	1.78	0.82	0.72	1.98
7	0.68	0.99	1.58	2.32	2.11	1.88	2.13	2.84	2.29	1.65	0.79	0.73	1.62
, 8	0.78	0.88	1.28	1.29	0.98	0.82	1.02	1.80	1.62	1.29	0.66	0.70	1.05
9	0.62	0.57	0.63	0.32	0.06	-0.14	0.17	0.21	0.60	0.70	0.41	0.54	0.89
10	0.26	0.15	-0.11	-0.53	-0.91	-0.98	-0.95	-0.77	-0.51	-0.10	-0.12	0.17	-0.36
11	-0.16	-0.45	-0.77	-1.51	-1.60	-1.58	-1.62	-1.50	-1.46	-0.86	-0.46	-0.22	-1.02
Noon.	-0.60	-0.92	-1.37	-2.09	-2.16	-2.08	-2.16	-2.18	-2.02	-1.53	-0.86	-0.65	-1.55
1	-0.93	-1.27	-1.83	-2.48	-2.56	-2.48	-2.59	-2.61	-2.56	-2.01	-1.18	-0.95	-1.95
2	-1.10	-1.50	-2.20	-2.74	-2.80	-2.78	-2.83	-2.89	-2.84	-2.81	-1.25	-1.07	-2.19
8	-1.11	-1.51	-2.29	-2.88	-2.90	-2.79	-2.93	-3.01	-2.96	-2.82	-1.28	-0.99	-2.25
4	−0.93	-1.35	-2.20	-2.76	-2.82	-2.71	-2.92	-2.85	-2.78	-2.10	-0.87	-0.79	-2.09
5	-0.68	-0.97	-1.83	-2.46	-2.53	-2.56	-2.83	-2.66	-2.35	-1.58	-0.62	-0.55	-1.80
6	-0.44	-0.61	-1.26	-1.91	-2.17	-2.10	-2.86	-2.11	-1.64	-1.01	-0.86	-0.87	-1.36
7	-0.31	-0.82	-0.70	-1.12	-1.49	-1.87	-1.59	-1.23	-0.87	-0.54	-0.19	-0.21	-0.83
8	-0.23	-0.06	-0.24	-0.33	-0.51	-0.39	-0.58	-0.84	-0.24	-0.10	0.01	-0.19	-0.27
9	0.01	0.12	0.09	0.20	0.27	0.80	0.22	0.20	0.27	0.28	0.16	0.06	0.18
10	0.10	0.26	0.40	0.72	0.80	0.91	0.90	0.81	0.74	0.51	0.29	0.16	0.55
11	0.19	0.39	0.66	1.12	1.24	1.28	1.32	1.20	1.08	0.85	0.48	0.25	0.83
Mean.	-1.69	0.64	2.20	7.27	11.27	14.47	15.66	15.01	11.52	7.94	8.02	-0.12	

XLIV.

BOHEMIA. — PRAGUE. Lat. 50° 5' N. Long. 14° 24' E. Greenso.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degre	es of Re	aumur.						
Hours.	Jan.	Feb.	March	April.	May.	June.	July.	Aug.	Sept.	Oct	Nov.	Dec.	Mon
Morn. 1	0.45	0.76	0.86	1.78	1.47	1.90	1.98	1.59	1.46	1.06	0.73	0.45	1.20
2	0.52	0.88	1.05	2.06	1.77		2.24	1.85	1.69			0.52	1
8	0.54	0.98	1.24	2.45	2.08	2.62	2.86	2.04	1.85	1.23	0.82	0.54	1.56
4	0.58	1.06	1.42	2.82	2.81	3.02	2.27	2.10	1.95	1.24	0.78	0.55	1.67
5	0.50			3.02	2.35	3.22	2.01	2.01	1.97	1.22	1	0.60	1.70
6	0.49		1			1	1.62	1.76		ſ	l.	0.70	1.61
7	0.47	1	ı	2.48	1.62	2.40	1.16	1.86	1.69	1.10	l	0.80	1.37
8			1.24	1.59	0.92	1.40	0.66	0.83	1.28	0.90	0.69	0.82	0.97
9	0.29				0.15				0.64		0.42	0.67	
10	0.08	l .		-0.56	l .	-0.85		-0.51					-0.81
11	-0.21	Į.	-0.52	ı	1	-1.68		-1.23		ı	-0.55		•
Noon	-0.52	-1.10	-1.16	-2.25	-1.60	-2.28	-1.84	-1.86	-2.00	-1.47	-1.10	-0.70	-1.49
1	11	l .	I	1	ı					1		-1.08	
2	11	1	I		1	•						-1.23	
8	11	•	ı		ı			1			1 1	-1.13	
4			1		1			1				-0.87	
5	11	ı	1	l .	1	ı	i .					-0.56	
6	11	1	1	1						1		-0.81	
7	11	1	•									-0.17	
8	-0.06	-0.09	-0.40	-0.64	-0.56	-0.85	-0.24	-0.12	-0.08	0.13	0.10	-0.11	-0.24
9	0.02	0.11	0.10		0.03	0.06	0.19	0.80	0.26	0.84	0.20	0.07	0.12
10	0.11	1.85	0.18	0.71	0.52	0.81	0.61	0.65	0.57	0.51	0.32	0.01	0.53
н	0.22	1			0.89	1.32	1.05	0.97	0.87			0.14	0.77
Midn	0.84	0.61	0.65	1.46	1.18	1.64	1.51	1.28	1.17	0.89	0.61	0.31	0.97
6. 6	0.09	0.24	0.25	0.40	0.21	0.29	0.17	0.29	0.42	0.29	0.25	0.19	0.26
7. 7	0.15	0.38	0.39	0.50	0.22	0.23	0.22	0.37	0.59	0.47	0.23	0.32	0.26
8. 8	0.18	1	0.42	0.47	0.18	0.27	0.21	0.36	0.60	0.51	0.89	0.35	0.36
9. 9	0.16	0.83	0.81	0.82	0.90	0.15	0.15	0.25	0.45	0.42	0.31	0.30	0.27
10.10	0.09	0.17	0.17	0.08	-0.08	-0.02	0.04	0.07	0.18	0.22	0.15	0.16	0.11
7. 2. 9	-0.13	-0.17	-0.16	-0.15	-0.16	-0.10	-0.44	-0.80	-0.31	-0.26	-0.20	-0.17	-0.21
6. 2. 8	-0.15	-0.21	-0.23	-0.24	-0.19	-0.19	-0.48	-0.31	-0.36	-0.30	-0.23	-0.21	-0.25
6. 2.10	-0.09			0.21	0.17							-0.17	
6. 2. 6	-0.23	-0.40	-0.46	-0.74	-0.58	-0.78	-0.77	-0.6 6	-0.69	-0.54	-0.36	-0.28	-0.54
7. 2	-0.21											-0.22	
8. 2	1												-0.58
8. 1	-0.17											-0.13	
7. 1	-0.15	-0.21	-0.06	-0.16	-0.15	-0.08	-0.61	-0.49	-0.47	-0.45	-0.35	-0.14	-0.28
9.12.8.9	-0.27	-0.52	-0.60	-1.17	-0.92	-1.21	-1.05	-0.98	-0.97	-0.68	-0.48	-0.81	-0.76
7. 2.2(9)	-0.09	-0.10	-0.15	-0.09	-0.12	-0.06	-0.2 8	-0.15	-0.17	-0.11	-0.10	-0.14	-0.13
Dail ext.	-0.17	-0.18	-0.16	-0.08	0.05	0.12	-0.15	-0.24	-0.46	-0.49	-0.88	~0.21	-0.22
	11		-										

XLV.

England. — Plymouth. Lat. 50° 22' N. Long. 4° 7' W. Greenw.

orrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenhelt.

Hours.	Jan.	Feb.	March.	April	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	0.86			4.01									
Morn. 1	-	1.46	2 32		5.18	4.84	4.75	4.16	3.24	2.66	1.58	0.95	2.95
2	0.90	1.67	2.68	4.48	5.94	4.82	5.88	4.79	8.60	2.79	1.69	0.86	8.29
3	0.99	1.87	8 02		6.62	5.18	5.69	5.45	4.03	8.02	1.80	0.74	8.60
4	1.15	2.12	8.81	5.18	6.75	5.00	5.58	5.76	4.84	8.81	1.96	0.81	8.76
5	1.87	2.86	3.40	4.91	6.03	4.57	4.82	5.42	4.25	8.51	2.09	1.04	3.65
6	1.58	2.48	3.08	8.98	4.87	2.79	8.85	4.21	3.62	8.88	2.14	1.81	8.02
7	1.46	2.80	2.25	2.89	2.00	0.95	1.92	2.25	2.32	2.66	1.89	1.40	
8	1.10	1.67	0.97	0.29	-0.54	-1.01	-0.65	-0.11	0.50	1.26	1.24	1.18	0.50
9	0.86	0.59	-0.63	-1.94	-2.88	-2.70	-2.57	-2.39	-1.53	-0.65	0.16	0.41	-1.15
10	-0.61	-0.83	-2.23	-8.94	-4.57	-3.87	-4.08	-4.21	-3.44	-2.70	1	-0.61	
11	-1.58	-2.25	-3.56	-3.40	-5.63	-4.64	-5.02	-5.36	-4.93	-4.41	-2.43	-1.67	-8.92
	-2.32	-3.33	-4.43	-6.17	-6.12	-4.93	-5.58	-5.87	-5.74	-5.40	-3.29	-2.43	-4.64
Noon. 1	-2.63	-3.85	-4.70	-6.37	-6.37	-5.02	-5. 81	-5.96	-5.92	-5.51	-3.56	-2.7 0	-4.86
2	-2.50	-3.69	-4.43	-5.99		-4.91		-5.72	-5.49		-3.22	-2.45	
8	-1.96	-3.02	-3.74	-5.22	-6.12		-5.40				t		1 1
4	-1.26	-2.07	-2.81	-4.14	-5.47	-4.03	-4.64	-4.52	-8.49	-2.45			-8.13
5	-0.59	-1.10	-1.76	-2.86	-4.82	-8.04	-3.47	-8.44	-2.18	-1.8 8	-0.77	-0.41	-2.12
6	-0.07	-0.88	-0.74	-1.42	-2.68	-1.78		-2.28	l .	-0.45	-0.23		-1.06
7	0.29	0.09	0.14	0.00	-0.81	-0.27		-0.47	0.36	0.28	0.07	0.84	1 1
8	0.50	0.86	0.86	1.26	0.99	0.74	1.10	1.06	1.37	0.79	ı	0.52	1 1
9	0.68	0.56	1.85	2.25	2.86	2.21	2.27	2.28	2.12	1.83	0.47	0.72	1.55
10	0.72	0.77	1.69	2.98	8.29	2.93	8.11	2.97	2.59	1.85	0.77	0.88	2.05
11	0.79	0.99	1.89	3.85	3.89	8.44	8.67	3.40	2.84	2.28	1.08	1.01	
Midn	0.88	1.26	2.07	8.67	4.46	8.87	4.21	3.71	2.99	2.48	1.37	1.04	2.66
6. 6	0.74	1.06	1.17	1.28	0.86	0.54	0.68	0.99	1.37	1.46	0.97	0.68	0.99
7. 7	0.88	1.19	1.19	1.19	0.61	0.34	0.52	0.90	1.85	1.44		0.88	
8.8	0 81	1.01	0.92	0.79	0.23	0.14	0.28	0.47	0.95	1.04	1	0.88	1 1
9. 9	0.50	0.59	0.86	0.16		-0.25		-0.09	0.29	0.84	0.32	0.56	
10.10	0.07	-0.05		-0.52			-0.47		I	i	1	0.14	
7. 2. 9	-0.14	-0.27	-0.27	-0.45	-0.68	-0.59	-0.70	-0.41	-0.36	-0.29	-0.29	-0.11	-0.38
6. 2. 8	-0.16	-0.29	-0.16	-0.25	-0.34	-0.45	-0.43	-0.16					
6. 2.10	-0.09	-0.16	0.11	0.32	0.43	0.27	0.23	0.50	0.25	0.14	-0.11	-0.09	0.16
6. 2. 6	-0.84	-0.54	-0.70	-1.15	-1.55	-1.28	-1.46	-1.24	-0.92	-0.63	-0.48	-0.36	-0.88
7. 2	-0.52	-0.70	-1.10	-1.80	_2.18	-1.98	-2.18	-1.78	-1.60	-1.10	-0.68	-0.54	-1.35
8. 2	-0.70	-1.01	-1.73	-2.86	-8.47	-2.97	-3.22			1	-0.99		1
8. 1	-0.77	-1.10	-1.87	-3.04	-8.47	-8.02	-3.24	-3.04	1	1		-0.79	
7. 1	-0.59	-0.79	-1.24	-2.00	-2.18	-2.05	-2.21	-1.87	-1.80	-1.44	-0.88	1	
9.12.3.9	-0.83	-1.31	-1.87	-2.77	-4.20	-2.52	-2.81	-2.84	-2.4 5	-2 .12	-1.28	-0.79	-2.07
7. 2.2(9)	0.07	-0.07	0.14	0.28	0.09	0.11	0.05	0.25	0.27	0.11	-0.09	0.09	0.11

XLVI.

England. - Plymouth. Lat. 50° 22' N. Long. 4° 7' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

				_									
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.38	0.65	1.03	1.78	2.28	1.93	2.11	1.85	1.44	1.18	0.70	0.42	1.31
2	0.40	0.74	1.17	1.97	2.64	2.14	2.39	2.13	1.60	1.24			1.46
8	0.44	0.83	1.34	2.18	2.94	2.28	2.53	2.42	1.79	1.84	0.80	1	1.60
4	0.51	0.94	1.47	2.28	8.00	2.22	2.48	2.56	1.93			1	
•	0.51	0.54	1.47	2.20	9.00	2.22	2.40	2.50	1.55	1.47	0.07	0.30	1.67
5	0.61	1.05	1.51	2.18	2.68	2.08	2.14	2.41	1.89	1.56	9.93	0.46	1.62
6	0.68	1.10	1.37	1.77	1.94	1.24	1.49	1.87	1.61	1.50	0.95	0.58	1.34
7	0.63	1.02	1.00	1.06	0.89	0.42	0.63	1.00	1.08	1.18	0.84	0.62	0.86
8	0.49	0.74	0.48	0.18	-0.24	-0.45	-0.2 9	-0.05	0.22	0.56	0.55	0.50	0.22
9	0.16	0.26	-0.28	-0.86	-1.28	-1. 2 0	-1.14	-1.06	-0.68	-0.29	0.07	0.18	-0.51
10	-0.27		1 1		-2.03			-1.87				1	1 1
11		-1.00						-2.38			1		
Noon		-1.48						-2.61			1	j.	1
1	•	-1.71	-2.09		-2.83			-2.65					
2	1 1		-1.97					-2.54					
8	1	-1.84						-2.34					
4	-0.56	-0.92	-1.25	-1.84	-2.43	-1.79	-2.06	-2.01	-1.55	-1.09	-0.69	-0.49	-1.39
5	-0.26	-0.49	-0.78	-1.27	-1.92	-1.35	-1.54	-1.58	-0.97	-0.59	-0.84	-0.18	-0.94
6	-0.03	-0.17	-0.33	-0.68		-0.77	-0.89	1 1		-0.20	1		-0.47
7	0.13	0.04	0.06		-0.36	-0.12	-0.17	-0.21	0.16	0.10		1	1
8	0.22	0.16		0.56		0.33	0.49	0.47		0.85	0.11	0.23	ı
9	0.28	0.23	0.60	1.00	1.05	0.98	1.01	0.99	0.94	0.59	0.21	0.82	0.69
10	0.32	0.34	0.75	1.30	1.46	1.30	1.38	1.32	1.15	0.82	0.34	0.39	1 1
11	0.35	0.44	0.84	1.49	1.78	1.53	1.63	1.51	1.26	0.99	0.48	0.45	1.06
Midn	0.37	0.56	0.92	1.68	1.98	1.72	1.87	1.65	1.38	1.10	0.61	0.46	1.18
6. 6	0.88	0.47	0.52	0.57	0.38	0.24	0.80	0.44	0.61	0.65	0.43	0.30	0.44
7. 7	0.89	0.58	0.58	0.58	0.27	0.15	0.28	0.40		0.64	0.44	0.39	0.42
8.8	0.86	0.45	0.41	0.85		-0.06	0.10	0.21	0.42	0.46	0.88	0.87	0.29
9. 9	0.22	0.26	0.16		-0.12		-0.07	-0.04	0.18	0.15	0.14	0.25	0.09
10.10	0.08		1		-0.29				-0.19			0.06	-0.14
7. 2. 9	-0.06	-0.12	_0 19	_0 90	_0 90	_0 96	_0 91	_0.10		A 10	_0.10		-0.17
6. 2. 8		-0.12 -0.13	-0.12 -0.07		-0.30 -0.15			-0.18					
6. 2.10								-0.07			1	1	
6. 2. 6	1	-0.07	0.05	0.14	0.19	0.12	0.10	0.22	0.11		-0.05	1	0.07
0. 2. 0	70.10	-0.24	-0.81	-U.D1	-0.69	-0.57	-0.65	-0.55	-U.41	-v.Z8	-0.19	-0.16	-0.39
7. 2	-0.28	-0.81	-0.42	-0.80	-0.97	-0.88	-0.97	-0.77	-0.71	-0.49	-0.30	-0.24	-0.60
8. 2	-0.81	-0.45	-0.77					-1.80					-0.92
8. 1	-0.84	-0.49	-0.83	-1.35	-1.54	-1.84	-1.44	-1.35	-1.21	-0.95	-0.52	-0.35	-0.98
7. 1	-0.26	-0.35	-0.55	-0.89	-0.97	-0.91	-0.98	-0.88	-0.80	-0.64	-0.87	-0.29	~0.6 5
9.12.3.9	-0.87	-0.58	-0.83	-1.23	_1.49	-1.12	-1.25	-1.26	-1.09	04	_0 57	-0.35	_0 00
7. 2.2(9)		-0.03	0.06			0.05	0.02	1 .	0.12		-0.04	i	
Dail.ext.	-0.25	-0.81	-0.29								į .	1	-0.25
		umbere									<u> </u>		

XLVII.

Belgium. - Brussels. Lat. 50° 51' N. Long. 4° 22' E. Greenw.

corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees	of	Resumur.

Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Meen.
N 1	0.58	0.67	1 10	0.00	0 80	0.00	0.04	0.40	1.71	0.85	0.49	0.73	1.56
Morn. 1		1	1.19	2.23	2.57	2.88	2.84	2.49					
2	0.60	0.73	1.36	2.59	2.89	8.12	2.57	2.84	2.00	0.99	0.49	0.39	1.71
8	0.60	0.79	1.54	2.99	8.17	8.18	2.74	3.20	2.33	1.15	0.54	0.08	1.86
4	0.60	0.86	1.70	8.29	3.28	8.14	2.74	8.42	2.57	1.31	0.65	0.02	1.97
5	0.62	0.92	1.79	8.29	8.06	2.71	2.47	3.82	2.58	1.40	0.77	0.25	1.98
6	0.64	0.97	1.74	2.86	2.45	2.00	1.88	2.82	2.28	1.85	0.85		1.71
7	0.61	0.93	1.50	2.01	1.52	1.10	1.06	1.94	1.67	1.11	0.81	0.97	1.27
8	0.46	0.75	1.03			0.16	0.15	0.82	0.82	0.68	0.58	0.97	0.64
•	0.40	0.75	1.00	0.86	0.44	0.10	0.15	0.82	0.02	V.00	0.00	0.57	0.04
9	0.18	0.89	0.89	-0.35	-0.59	-0.61	-0.69	-0.84	-0.14	0.08	0.19	0.56	-0.08
10	-0.22	-0.13	-0.36			-1.85		-1.37		-0.60	-0.31	-0.18	-0.81
11	-0.65	-0.71	-1.11			1	}	-2.19		-1.23	1	-0.84	-1.44
Noon	-1.01	-1.28	-1.72			ľ	i	-2 .81		-1.71		-1.29	i i
Nooil	1.01	1.20	1	_2.,,	2.02	2.21	2.00	2.01	2120	2.7.1	1	***	1.02
1 1	-1.20	-1.57	-2.13	-8. 11	-2.89	-2.65	-2.29	-8.27	-2.88	-1.96	-1.82	-1.33	-2.22
2	-1.19				-8.21		l .		-3.05			•	-2.33
8	-0.99	-1.49	-2.21				1	-3.69	1	-1.71			-2.28
4	1							-3.53				-0.26	
•	0.70	1.14	1.50	-9.10	-0.00	3.10		-3.03	2.03	1.01	"""	0.20	2.00
5	-0.89	-0.72	-1.51	-2.76	-2.97	-2.88	-2.47	-8.02	-2.05	-0.84	-0.45	-0.16	-1.68
6	-0.15	-0.83	-1.03	-2.05	-2.21	-2.17	-1.91	-2.19	-1.30	-0.39	-0.18	-0.25	-1.18
7	0.02							-1.15		-0.01		-0.87	-0.61
8	0.12	0.17			-0.12			1	0.23	0.28	0.19	-0.88	-0.03
1 1		0.2.	0.20	0.20	J	0.02	0.20	0.00	0.20	0.20			
9	0.21	0.81	0.28	0.69	0.82	0.68	0.64	0.82	0.78	0.48	0.82	0.05	0.50
10	0.31	0.41	0.59	1.81	1.51	1.37	1.31	1.48	1.18	0.60	0.41	0.37	0.90
n	0.42	0.50	0.83	1.70	1.96	1.97	1.77	1.89	1.33	0.68	0.47	0.75	1.19
Midn	0.52	0.59	1.02	1.96	2.28	2.44	2.08	2.19	1.49	0.75	0.49	0.89	1.39
												ì	
6. 6	0.25	0.82	0.35	0.41		-0.09	•	0.31	0.49	0.48		0.20	0.26
7.7	0.81	0.45	0.47	0.44	0.16	-0.09	-0.02	0.89	0.59	0.55	0.42	0.80	0.33
8.8	0.29	0.46	0.47	0.85	0.16	-0.07	-0.03	0.87	0.58	0.48	0.89	0.32	0.81
9.9	0.20	0.85	0.84	0.17	0.12	0.04	-0.02	0.24	0.32	0.28	0.25	0.25	0.21
10.10	0.05	0.14	0.11	0.05	0.04	0.01	-0.01	0.05	0.03	0.00	0.05	0.12	0.05
1 1			1	1	1	١.						ا ۔ ۔ ا	
7. 2. 9	-0.12	ı	-0.17	l .	-0.29	ı	-0.27	1			-0.05		-0.19
6. 2. 8	-0.14	-0.17	-0.22	-0.20		I	-0.28		ł				-0.22
6. 2.10	-0.08	-0.09	0.01	0.29	0.25	0.18	0.28	0.24	0.12	0.00	-0.00	-0.00	0.09
6. 2. 6	-0.23	-0.84	-0.58	-0.88	-0.99	-1.05	-0.85	-0.98	-0.69	-0.83	-0.20	-0.21	-0.60
					0.00			0.00		_0.40	-0 ee		
7. 2	-0.29		-0.40	1	1			-0.82	ľ			-0.08	
8. 2	-0.87							-1.38				-0.08	
8.1	-0.87							-1.23		-0.64		-0.18	
7. 1	-0.80	-0.82	-0.32	-0.55	-0.69	-0.78	-0.62	-0.67	-0.61	-0.43	-0.26	-0.18	-0.48
اعمما		۸	0.00		_1 40	_1 00	_1 90	_1 51	-1.21	-0.72	0.48	-0.34	-0.95
9.12.2.9	1		-0.82		-1.42				1			-0.04	
7. 2.2(9)	-0.04	-U.U3	-0.06	0.08	-0.01	-0.18	-0.04	-0.00	0.05	0.08	0.00	0.04	-0.02
Dail.ext.	-0.28	-0.84	-0.25	-0.02	-0.06	-0.04	0.02	-0.14	-0.24	-0.28	-0.24	-0.18	-0.18
DIME. UKL	0.20	1 0.03	U.20	V.02	, 0.00		, 0.02		,	0.20			

XLVIII.

Belgium. - Brussels. Lat. 50° 51' N. Long. 4° 22' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Resumur.

Hour.	Jan.	Peb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year
Midn.	0.80	0.60	1.09	1.72	2.27	2.46	2.20	1.88	1.52	0.92	0.51	0.30	1.3
2	0.56	0.82	1.39	2.19	8.00	2.82	2.77	2.44	2.03	1.20	0.77	0-47	1.7
4	0.64	0.97	1.66	2.64	8.82	3.53	8.14	2.76	2.38	1.44	0.83	0.62	1.9
6	0.66	1.08	1.83	2.48	2.44	2.27	2.80	2.44	2.47	1.56	0.93	0.63	1.7
8	0.67	0.84	1.02	0.76	0.49	0.41	0.82	0.68	1.03	0.96	0.79	0.63	0.7
9	0.86	0.83	0.21	-0.88	0.61	-0.61	-0.68	-0.39	-0.14	0.07	0.21	0.34	0.0
10	0.07	-0.09	-0.54	-1.18	-1.43	-1.32	-1.86	-1.26	-1.19	-0.78	-0.36	-0.08	-0.7
Noon.	-0.92	-1.27	-1.78	-2.42	-2.61	-2.47	-2.85	-2.47	-2.46	-1.87	-1.27	-0.83	-1.8
2	-1.15	-1.65	-2.80	-2.95	-3.22	-8.21	-2.92	-3.08	-3.04	-2.17	-1.42	-1.04	-2.3
4	-0.72	-1.19	-2.04	-2.63	-3.15	-8.18	-2.90	-2.93	-2.70	-1.61	-0.90	-0.63	-2.0
6	-0.21	-0.49	-0.94	-1.71	-2.44	-2.57	-2.38	-1.87	-1.21	-0.37	-0.28	-0.18	-1.2
8	-0.08	-0.05	-0.00	0.13	0.05	-0.16	-0.15	0.17	0.21	0.23	0.07	-0.03	0.0
9	0.18	0.17	0.81	0.63	0.76	0.80	0.79	0.76	0.64	0.43	0.24	0.07	0.4
10	0.20	0.30	0.58	1.04	1.25	1.45	1.39	1.27	1.01	0.54	0.38	0.14	0.8
Mean.	0.52	2.45	8.56	7.27	10.87	18.10	13.69	13.58	11.22	7.69	4.72	1.89	

XLIX.

GERMANY. - SCHWERIN. Lat. 53° 36' N. Long. 11° 30' E. Gr. - Dove.

1		1		1	t	ı	i	ı	i	l .	1 .	
Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
0.05	0.49	0.92	1.66	1.97	2.10	2.12	1.92	1.70	0.87	0.21	0.16	1.18
0.08	0.69	1.20	2.17	2.44	2.69	2.72	2.41	2.19	1.14	0.24	0.84	1.53
0.27	0.88	1.43	2.58	2.96	2.97	2.96	2.62	2.54	1.51	0.42	0.48	1.79
0.35	0.86	1.62	2.67	2.07	1.80	1.94	2.13	2.70	1.67	0.62	0.48	1.56
0.59	1.19	1.24	0.98	0.56	0.25	0.12	0.32	0.95	1.21	0.70	0.63	0.73
0.17	0.18	-0.11	-0.97	-1.15	-1.20	-1.26	-1.17	-1.12	-0.84	0.01	0.13	-0.57
-0.42	-0.97	-1.82	-2.34	-2.47	-2.86	-2.20	-2.29	-2.42	-1.80	-0.77	-0.43	-1.6 5
-0.61	-0.72	-2.21	-8.50	-8.38	-8.23	-8.26	-3.45	-8.58	-2.54	-0.91	-0.68	-2.42
-0.43	-1.22	-2.13	-2.86	-2.70	-2.62	-2.76	-2.76	-8.08	-1.85	-0.62	-0.62	-1.97
-0.02	-0.42	-0.95	-1.54	-1.62	-1.71	-1.70	-1.37	-1.82	-0.55	-0.23	-0.27	-0.98
-0.07	-0.07	-0.11	0.18	0.11	-0.02	0.08	0.84	0.26	0.16	0.02	-0.14	0.06
0.06	0.21	0.45	1.01	1.15	1.28	1.29	1.80	1.19	0.57	0.24	-0.02	0.73
-1.05	-2.00	1.18	5.26	8.45	12.19	18.50	13.02	10.42	7.48	1.42	-1.38	
	0.05 0.08 0.27 0.35 0.59 0.17 -0.42 -0.61 -0.43 -0.02 -0.07 0.06	0.05 0.49 0.08 0.69 0.27 0.83 0.35 0.86 0.59 1.19 0.17 0.18 -0.42 -0.97 -0.61 -0.72 -0.43 -1.22 -0.07 -0.07 0.06 0.21	0.05 0.49 0.92 0.27 0.83 1.43 0.35 0.86 1.62 0.59 1.19 1.24 0.17 0.18 -0.11 -0.42 -0.97 -1.82 -0.61 -0.72 -2.21 -0.43 -1.22 -0.95 -0.07 -0.01 0.06 0.21 0.45	0.05 0.49 0.92 1.66 0.08 0.69 1.20 2.17 0.27 0.83 1.43 2.58 0.35 0.86 1.62 2.67 0.59 1.19 1.24 0.98 0.17 0.18 -0.11 -0.97 -0.42 -0.97 -1.82 -2.34 -0.61 -0.72 -2.21 -8.50 -0.43 -1.22 -2.13 -2.86 -0.02 -0.42 -0.95 -1.54 -0.07 -0.07 -0.11 0.18 0.06 0.21 0.45 1.01	0.05 0.49 0.92 1.66 1.97 0.08 0.69 1.20 2.17 2.44 0.27 0.83 1.43 2.58 2.96 0.35 0.86 1.62 2.67 2.07 0.59 1.19 1.24 0.98 0.56 0.17 0.18 -0.11 -0.97 -1.15 -0.42 -0.97 -1.22 -2.34 -2.47 -0.61 -0.72 -2.21 -8.50 -8.38 -2.86 -2.70 -0.02 -0.42 -0.95 -1.54 -1.62 -0.07 -0.07 -0.11 0.18 0.11 0.06 0.21 0.45 1.01 1.15	0.05 0.49 0.92 1.66 1.97 2.10 0.08 0.69 1.20 2.17 2.44 2.69 0.27 0.83 1.43 2.58 2.96 2.97 0.35 0.86 1.62 2.67 2.07 1.80 0.59 1.19 1.24 0.98 0.56 0.25 0.17 0.18 -0.11 -0.97 -1.15 -1.20 -0.42 -0.97 -1.82 -2.34 -2.47 -2.86 -0.61 -0.72 -2.21 -8.50 -8.38 -8.28 -0.43 -1.22 -2.13 -2.86 -2.70 -2.62 -0.02 -0.42 -0.95 -1.54 -1.62 -1.71 -0.07 -0.07 -0.11 0.18 0.11 -0.02 0.06 0.21 0.45 1.01 1.15 1.28	0.05 0.49 0.92 1.66 1.97 2.10 2.12 0.08 0.69 1.20 2.17 2.44 2.69 2.72 0.27 0.83 1.43 2.58 2.96 2.97 2.96 0.35 0.86 1.62 2.67 2.07 1.80 1.94 0.59 1.19 1.24 0.98 0.56 0.25 0.12 0.17 0.18 -0.11 -0.97 -1.15 -1.20 -1.26 -0.42 -0.97 -1.82 -2.34 -2.47 -2.36 -2.20 -0.61 -0.72 -2.21 -8.50 -3.38 -8.23 -8.28 -0.43 -1.22 -2.13 -2.86 -2.70 -2.62 -2.76 -0.02 -0.42 -0.95 -1.54 -1.62 -1.71 -1.70 -0.07 -0.07 -0.11 0.18 0.11 -0.02 0.08 -0.06 0.21 0.45 1.01	0.05 0.49 0.92 1.66 1.97 2.10 2.12 1.92 0.08 0.69 1.20 2.17 2.44 2.69 2.72 2.41 0.27 0.83 1.43 2.53 2.96 2.97 2.96 2.62 0.35 0.86 1.62 2.67 2.07 1.80 1.94 2.13 0.59 1.19 1.24 0.98 0.56 0.25 0.12 0.32 0.17 0.18 -0.11 -0.97 -1.15 -1.20 -1.26 -1.17 -0.42 -0.97 -1.82 -2.34 -2.47 -2.36 -2.20 -2.29 -0.61 -0.72 -2.21 -8.50 -8.38 -8.28 -8.26 -8.45 -0.43 -1.22 -2.13 -2.86 -2.70 -2.62 -2.76 -2.76 -0.02 -0.42 -0.95 -1.54 -1.62 -1.71 -1.70 -1.37 -0.07 -0.07	0.05 0.49 0.92 1.66 1.97 2.10 2.12 1.92 1.70 0.08 0.69 1.20 2.17 2.44 2.69 2.72 2.41 2.19 0.27 0.83 1.43 2.58 2.96 2.97 2.96 2.62 2.54 0.35 0.86 1.62 2.67 2.07 1.80 1.94 2.13 2.70 0.59 1.19 1.24 0.98 0.56 0.25 0.12 0.32 0.95 0.17 0.18 -0.11 -0.97 -1.15 -1.20 -1.26 -1.17 -1.12 -0.42 -0.97 -1.32 -2.34 -2.47 -2.36 -2.20 -2.29 -2.42 -0.61 -0.72 -2.21 -3.50 -3.38 -3.23 -3.26 -3.45 -3.58 -0.43 -1.22 -2.13 -2.86 -2.70 -2.62 -2.76 -2.76 -3.03 -0.07 -0.07	0.05 0.49 0.92 1.66 1.97 2.10 2.12 1.92 1.70 0.87 0.08 0.69 1.20 2.17 2.44 2.69 2.72 2.41 2.19 1.14 0.27 0.83 1.43 2.58 2.96 2.97 2.96 2.62 2.54 1.51 0.35 0.86 1.62 2.67 2.07 1.80 1.94 2.13 2.70 1.67 0.59 1.19 1.24 0.98 0.56 0.25 0.12 0.32 0.95 1.21 0.17 0.18 -0.11 -0.97 -1.15 -1.20 -1.26 -1.17 -1.12 -0.34 -0.42 -0.97 -1.82 -2.34 -2.47 -2.36 -2.20 -2.29 -2.42 -1.80 -0.61 -0.72 -2.21 -8.50 -3.88 -8.23 -8.26 -3.45 -8.58 -2.54 -0.43 -1.22 -2.13 -2.86 -2.70 -2.62 -2.76 -2.76 -8.03 -1.85 -0.02<	0.05 0.49 0.92 1.66 1.97 2.10 2.12 1.92 1.70 0.87 0.21 0.08 0.69 1.20 2.17 2.44 2.69 2.72 2.41 2.19 1.14 0.24 0.27 0.83 1.43 2.53 2.96 2.97 2.96 2.62 2.54 1.51 0.42 0.35 0.86 1.62 2.67 2.07 1.80 1.94 2.13 2.70 1.67 0.62 0.59 1.19 1.24 0.98 0.56 0.25 0.12 0.32 0.95 1.21 0.70 0.17 0.18 -0.11 -0.97 -1.15 -1.20 -1.26 -1.17 -1.12 -0.34 0.01 -0.42 -0.97 -1.82 -2.34 -2.47 -2.26 -2.20 -2.29 -2.42 -1.80 -0.77 -0.61 -0.72 -2.21 -8.50 -8.38 -8.28 -8.26 -8.45	0.05 0.49 0.92 1.66 1.97 2.10 2.12 1.92 1.70 0.87 0.21 0.16 0.08 0.69 1.20 2.17 2.44 2.69 2.72 2.41 2.19 1.14 0.24 0.34 0.27 0.83 1.43 2.58 2.96 2.97 2.96 2.62 2.54 1.51 0.42 0.48 0.59 1.19 1.24 0.98 0.56 0.25 0.12 0.32 0.95 1.21 0.70 0.63 0.17 0.18 -0.11 -0.97 -1.15 -1.20 -1.26 -1.17 -1.12 -0.34 0.01 0.13 -0.42 -0.97 -1.82 -2.34 -2.47 -2.36 -2.20 -2.29 -2.42 -1.80 -0.77 -0.43 -0.61 -0.72 -2.21 -3.50 -3.38 -3.23 -3.26 -3.45 -3.58 -2.54 -0.91 -0.68 -0.43 -1.22 -2.13 -2.86 -2.70 -2.62 -2.76 -3.03 -1

L.

PRUSSIA. — MÜHLHAUSEN. Lat. 51° 13'.N. Long. 10° 27' E. Greenw.

prections to be applied to the Means of the Hours of Observation to obtain the

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — DOVE.

					Degree	s of Re	eumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.71	1.28	1.10	1.84	2.40	8.56	2.91	2.49	1.95	1.39	0.47	0.58	1.72
2	0.75	1.80	1.28	2.19	2.80	3.97	3.30	2.80	2.20	1.65	0.53	0.59	1.95
3	0.77	1.33	1.46	2.40	3.06	4.16	3.50	8.06	8.29	1.85	0.60	0.60	
4	0.82	1.40	1.60	2.74	8.06	8.98	3.42	3.14	2.70	1.99	0.66	0.62	2.18
5	0.86	1.47	1.62	2.61	2.67	8.40	8.00	2.98	2.73	2.05	0.68	0.66	2.06
6	0.91	1.50	1.46	2.25	2.06	2.49	2.22	2.51	2.46	1.93	0.63	0.67	1.76
7	0.86	1.36	1.11	1.41	1.15	1.82	1.20	1.73	1.03	1.50	0.46	0.59	1.14
8	0.62	0.98	0.55	0.58	0.16	0.11	0.09	0.86	0.87	0.84	0.16	0.46	0.52
9	0.21	0.88	-0.02	-0.88	-0.75	-1.02	-0.97	-0.86	-0.26	-0.03	-0.22	0.08	-0.29
10	-0.88	-0.50						1		-0.99	-0.62	-0.54	-1.08
11	-0.98	-1.85		-1.97		-2.77		-2.24		-1.88	1	ı	
Noon	-1.38	-2.02	-1.76	-2.42	-2.44	-8.39	-2.94	-2.89	-8.14	-2.53	-1.09	-1.06	-2.26
1	-1.58	-2.3 8	-2.02	-2.80	-2.71	-3.86	-3.26	-8.29	-8.52	-2.82	-1.08	-1.15	-2.54
2	1	-2.3 8		-2.94							-0.89		
8	-1.24		-1.90		-2.89	-4.18		-8.39			-0.66		
4	-0.84	-1.56	-1.58	-2.39	-2.69	-8.7 8	-8.06	-8.07	-2.65	-1.89	-0.89	-0.50	-2.08
5	-0.44	-1.02	-1.11	-1.95	-2.19	-3.06	-2.52	-2.51	-1.89	-1.21	− 0.14	-0.23	-1.52
6	-0.20		-0.62	1			1	-1.76		1	0.02		-0.95
7	-0.04	-0.17	-0.18		-0.83	-1.02		-0.90			0.06	0.12	-0.88
8	0.18	0.18	0.16	0.09	-0.08	0.05	0.03	-0.05	0.50	0.38	0.22	0.26	0.16
9	0.27	0.41	0.45	0.53	0.58	1.01	0.81	0.71	0.99	0.70	0.26	0.82	0.59
10	0.87	0.66	0.64	0.89	1.10	1.76	1.46	1.24	1.35	0.91	0.84	0.40	0.98
11	0.58	0.89	0.78	1.14	1.56	2.42	2.01	1.78	1.58	1.10	0.38	0.47	1.22
Midn	0.64	1.08	0.94	1.58	1.98	8.05	3.29	2.16	1.75	1.26	0.42	0.54	1.56
6. 6	0.86	0.48	0.42		0.24	0.20		0.88	0.70		0.83	0.88	0.41
7. 7	0.41	0.60	0.47		0.16	0.15	0.18	0.42	0.40	1		0.86	0.88
8. 8 9. 9	0.40		0.36	1 1	0.04	0.08	0.06	0.41	0.69	0.61	0.19	0.36	0.34
10.10	0.24 -0.01	0.87 0.08	0.22 -0.03	0.08	-0.09 -0.20	-0.01 -0.11	-0.08 -0.18	0.18 0.07	0.37 0.08	0.34	0.02 -0.14	0.18	0.15
10.10	0.01	0.00	0.00	0.14	0.20	V.11	0.10		-0.03	-0.04	70.14	-0.07	-0.06
7. 2. 9	-0.18	-0.2 0		-0.23				-0.84			-0.06	1	
6. 2. 8	-0.14		-0.15		-0.80					1	-0.01	•	
6. 2.10	-0.08		0.01	0.07	0.10	0.04	0.09	0.10	t .	-0.05	i .	-0.01	0.03
6. 2. 6	-0.27	-0.47	-U.41	-0.68	U.80	-1.25	-0.99	-∪.90	-0.71	-0.5 5	-0.08	-0.15	-0.60
7. 2	-0.88	-0.51	-0.48	-0.77	-0.86	-1.41	-1.11	-0.87	-1.26	-0.75	-0.22	-0.26	-0.74
8. 2	4		-0.76										
8. 1	-0.48		-0.74										
7. 1	-0.36	~ 0.51	-0.46	-0.7 0	–∪.7 8	-1.27	-1.03	-0.78	-1.25	~ 0.66	0.8 1	-0.28	-0.70
9.12.3.9	-0.54	-0.84	-0.81	-1.28	-1.88	-1.88	-1.62	-1.48	-1.41	-1.09	-0.48	-0.88	-1.10
7. 2.2(9)	-0.03	-0.05	-0.02							1	1		-0.07
Dail.ext.	-0.84	-0.44	-0.23	-0.10	0.00	0.01	0.04	-0.16	-0.18	-0.47	-0.91	-0.94	-0.22
MAII. CAL.	7.04	V.77	U.23	0.10	0.08	0.01	0.04	-0.10	A.19	1-0.47	7.21	V-44	-V.22

HOLLAND. — UTRECHT. Lat. 52° 5' N. Long. 5° 8' E. Greene.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Resumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year
Midn.	0.86	0.62	1.13	1.71	2.56	2.74	2.64	1.87	1.91	1.07	0.76	0.11	1.4
1	0.87	0.74	1.18	1.87	2.86	3.29	2.67	1.91	2.10	1.11	0.70	0.19	1.5
2	0.46	0.82	1.24	2.00	8.00	3.21	2.82	2.02	2.21	1.18	0.78	0.32	1 1.6
8	0.51	0.87	1.27	2.10	8.02	8.25	2.97	2.07	2.84	1.25	0.82	0.42	1.7
4	0.57	0.90	1.31	2.16	2.70	2.84	2.76	2.06	2.45	1.31	0.82	0.44	1.6
5	0.61	0.97	1.26	1.92	1.80	1.82	1.86	1.80	2.42	1.42	0.90	0.50	1.4
6	0.66	0.98	1.02	1.80	0.67	0.44	0.33	1.05	1.87	1.22	0.91	0.46	0.9
7	0.64	0.84	0.62	0.37	-0.88	-0.70	-0.77	0.04	0.72	0.39	0.78	0.38	0.2
8	0.50	0.56	-0.01	-0.40	-1.17	-1.50	-1.28	-0.68	-0.39	0.12	0.29	0.31	-0.5
9	0.13	-0.07	-0.53	-1.20	-1.68	-2.02	-1.69	-1.83	-1.12	-0.50	-0.22	0.14	-0.5
10	-0.26	-0.49	-1.05	-1.71	-2.06	-2.42	-2.02	-1.65	-1.79	-1.12	-0.71	-0.14	-1.5
11	-0.62	-0.97	-1.50	-2.16	-2.46	-2.78	-2. 2 7	-1.87	-2.84	-1.68	-1.15	-0.83	-1.6
Noon.	-0.85	-1.34	-1.77	-2.41	-2.78	-2.94	-2.58	-2.16	-2.83	-1.98	-1.49	-0.62	-1.9
1	-0.98	-1.58	-1.88	-2.42	-2.94	-8.00	-2.61	-2.40	-8.07	-2.11	-1.62	-0.75	-2.
2	-1.02	-1.54	-1.82	-2.42	-2.88	-2.94	-2.60	-2.80	-2.99	-1.99	-1.43	-0.66	-2.0
8	-0.81	-1.21	-1.54	-2.24	-2.58	-2.64	-1.58	-2.18	-2.68	-1.64	-1.08	-0.47	-1.
4	-0.60	-0.89	-1.25	-1.82	-2.06	-2.20	-2.00	-1.79	-2.06	-1.10	-0.70	-0.23	-1.5
5	-0.3 5	-0.48	-0.75	-1.23	-1.42	-1.58	-1.62	-1.30	-1.84	-0.52	-0.42	-0.17	-0.9
6	-0.19	-0.21	-0.24	-0.47	-0.76	-0.74	-0.76	-0.61	-0.52	-0.11	-0.18	-0.10	-o.
7	-0.05	-0.03	0.14	0.20	0.07	0.17	0.02	0.14	0.10	0.22	-0.02	-0.03	0.0
8	0.05	0.12	0.48	0.72	0.85	1.01	0.82	0.86	0.62	0.58	0.18	0.02	0.4
9	0.22	0.23	0.74	1.13	1.51	1.77	1.50	1.24	1.17	0.84	0.40	0.06	0.9
10	0.86	0.40	0.94	1.41	1.92	2.25	1.96	1.52	1.51	1.01	0.58	0.04	1.1
11	0.86	0.67	1.02	1.58	2.16	2.58	2.17	1.70	1.76	1.14	1.06	0.02	1.5
lean.	-2.83	4.18	8.20	7.14	10.55	12.95	13.75	12.90	10.87	6.88	4.65	0.76	

LII.

England. — Greenwich. Lat. 51° 28′ 38" N. Long. 0° 0'. — Dove.

					ν	aliam o	Weihmi	ur.					
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
A.M.1	0.44	0.75	1.44	2.82	2.72	8.24	2.78	2.49	2.05	1.84	0.67	0.47	1.72
3	0.62	0.94	1.66	2.66	8.04	8.70	8.11	2.82	2.40	1.42	0.80	0.56	1.99
5	0.75	1.06	1.92	2.84	2.84	3.25	2.91	2.89	2.58	1.54	0.87	0.56	2.00
7	0.86	1.08	1.60	1.31	0.75	0.80	0.88	1.22	1.65	1.26	0.88	0.60	1.07
9	0.41	0.24	-0.22	-0.82	-1.80	-1.52	-1.14	-1.14	-0.76	-0.30	0.11	0.24	-0.50
11	-0.74	-1.03	-1.90	-2.48	-2.60	-2.91	-2.67	-2.64	-2.57	-1.88	-1.06	-0.73	-1.93
P.M. 1	-1.23	-1.73	-2.62	-3.31	-8.38	-8.75	-8.17	-8.40	-3.28	-2.40	-1.64	-1.20	-2.59
8	-1.10	-1.59	-2.48	-3.08	-8.02	-3.60	-8.09	-8.20	-2.94	-2.04	-1.26	-0.85	-2.35
5	-0.36	-0.63	-1.83	-2.04	-2.05	-2.51	-2.24	-2.11	-1.65	-0.78	~0.38	-0.24	-1.37
7	0.03	0.05	0.09	-0.16	-0.29	-0.58	-0.50	-0.11	0.04	0.11	0.09	0.00	-0.10
9	0.10	0.32	0.71	0.99	1.20	1.40	1.18	1.22	0.89	0.68	0.40	0.21	0.77
11	0.23	0.54	1.11	1.77	2.06	2.52	2.08	1.96	1.60	1.07	0.53	0.87	1.33
Mean	2.48	2.53	4.53	6.71	9.62	12.47	18.08	12.98	11.12	7.71	5.47	2.09	!

LIII.'
ENGLAND. — GREENWICH. Lat. 51° 29' N. Long. 0° 0'.

orrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					2708.0	s of Re							
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
36	0.00	A 00	1 00	0.01	0.00	0.10	0.01	0.01	1.00	1 00	0.00	0.40	
Morn. 1	0.88	0.68	1.29	2.21	2.72	8.13	ì	2.61	1.89	1.28	0.60	1	1.65
2	0.68	0.82	1.44	2.31	2.85	8.80	2.71	2.68	2.06	1.45	0.75	0.52	1.79
8	0.83	0.95	1.62	2.44	2.91	8.41	2.74	2.78	2.22	1.56		0.59	1.91
4	0.93	1.02	1.82	2.54	2.85	8.40	2.71	2.86	2.34	1.60	0.95	0.62	1.97
5	0.98	1.08	1.95	2.46	2.60	8.14	2.53	2.81	2.35	1.56	0.95	0.62	1.91
6	0.84	0.97	1.98	2.17	2.08	2.52	2.11	2.48	2.15	1.42	0.89	0.60	1.68
7	0.71	0.84	1.66	1.56	1.25	1.53	1.38	1.77	1.67	1.15	0.75	0.57	1.24
8	0.53	0.61	1.11	0.66	0.20	0.28	0.40	0.72	0.88	0.71	0.52	0.48	0.59
ا و	0.30	0.26	0.30	-0.37	-0.92	-1.02	-0.71	-0.55	-0.18	0.09	0.19	0.28	-0.19
10	-0.01	-0.20						-1.78		1	ı	-0.04	
11	-0.89	-0.75		-2.30					-2.22	1	•	1	-1.73
Noon	-0.79	-1.27	-2.35	-2.87	1					-2.07	-1.25	-0.87	1
1													
1	-1.12							-3.69		-2.45			-2.55
2	1							-3.63				1	1
3	-1.21		-2.57		-2.90	1		-8.34		-2.17			-2.34
4	-0.95	-1.2 9	-2.05	-2.54	-2.54	-3.01	-2.38	-2.89	-2.28	-1.63	-1.10	-0.76	-1.95
5	-0.58	-0.78	-1.40	-1.97	-2.06	-2.67	-2.3 0	-2.30	-1.60	-1.01	-0.59	-0.36	-1.45
6	-0.22	-0.26	-0.75	-1.34	-1.45	-2.10	-1.57	-1.56	-0.91	-0.43	-0.10	-0.01	-0.89
7	0.03	0.14	-0.17	-0.60	-0.71	-1.26	-0.96	-0.69	-0.27	0.02	0.24	0.20	-0.34
8	0.11	0.37	0.30	0.17	0.11	-0.24	-0.19	0.24	0.29	0.32	0.41	0.26	0.18
1													
9	0.08	0.46	0.65	0.84	0.92	0.91	0.64	1.11	0.77	0.52	0.44	0.23	0.62
10	0.08	0.48	0.89	1.42	1.62	1.74	1.41	1.81	1.17	0.69	0.41	0.19	0.99
11	0.04	0.49	1.05	1.81	2.16	2.42	2.01	2.27	1.47	0.87	0.40	0.20	1.27
Midn	0.16	0.56	1.17	2.03	2.51	2.86	2.40	2.51	1.70	1.08	0.46	0.28	1.48
6. 6	0.31	0.86	0.59	0.42	0.31	0.21	0.27	0.46	0.62	0.50	0.39	0.80	0.40
7. 7	0.37	0.49	0.75	0.48	0.27	0.13	0.21	0.54	0.70	0.59	0.50	0.38	0.45
8.8	0.32	0.49	0.71	0.42	0.16	0.02	0.10	0.48	0.59	0.52	0.47	0.37	0.39
9. 9	0.19	0.86	0.48	0.24	0.00	-0.10		0.28	0.32	0.31	0.81	0.25	0.22
10.10	0.01	0.14		-0.00	-0.16		-0.16	0.01		0.02	0.08	0.25	-0.01
10.10	0.01	0.14	0.12	-0.00	-0.10	-0.15	-0.10	0.01	-0.00	0.02	0.00	Ų.U1	-0.01
7. 2. 9	-0.16	-0.17	-0.18	-0.25	-0.33	-0.83	-0.80	-0.25	-0.26	-0.27	-0.17	-0.15	-0.24
6. 2. 8	-0.11	-0.16	-0.21	-0.27		-0.35							-0.24
6. 2.10	1 1	-0.12		0.15	0.18	0.81	-0.20	0.22		-0.12			0.04
6. 2. 6		-0.87					-0.79		-0.66				-0.59
7. 2	1							-0.98					
8. 2	1 1							-1.46					
8. 1	-0.30		-0.84					-1.49				-0.85	-0.98
7. 1	-0.21	-0.41	-0.57	-0.81	-1.01	-0.98	-0.88	-0.96	-0.81	-0.65	-0.42	-0.80	-0.66
9.12.3.9	-0.41	-0.56	_0.00	_1,22	-1.51	-1.68	-1.49	-1.55	-1.29	-0.91	_0 KP	-0.87	-1.05
7. 2.2(9)		-0.01		-		-0.05				-0.07			11
(-)													i i
Dail.ext.	-0.18	-0.39	-0.45	-0.82	-0.18	0.01	-0.15	-0.42	-0.47	-0.44	-0.87	-0.82	-0.80

LIV.

England. - Greenwich. Lat. 51° 29' N. Long. 0° 0'.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year.—GLAISHER.

Degrees of Pahrenheit.

					Degrees								
Hours.	Jan.	Peb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	More.
Midn	1.0	1.6	2.9	4.8	5.4	6.2	5.0	5.1	4.0	2.9	1.7	0.9	2.5
1	0.9	1.8	8.0	5.2	6.0	7.1	5.5	5.5	4.5	3.0	1.8	1.0	3.8
2	1.2	2.0	3.3	5.7	6.4	8.0	6.0	6.0	5.5	8.4	2.0	1.2	4.2
8	1.8	2.1	8.6	6.2	6.7	8.7	6.4	6.8	6.4	8.6	2.0	1.3	4.5
1					-								
4	1.6	2.8	8.9	6.6	6.7	9.8	6.6	6.5	6.6	8.8	2.1	1.4	4.8
5	1.8	2.2	4.0	6.7	6.3	8.8	6.2	6.5	6.2	8.8	2.0	1.4	4.7
6	1.9	2.8	8.9	6.0	4.8	6.4	4.5	5.5	5.3	3.5	1.9	1.4	3.9
7	1.9	2.1	3.6	4.8	2.6	8.0	2.5	8.8	4.0	2.8	1.7	1.5	2.8
]						3		0.0					
8	1.5	1.6	2.5	2.0	0.5	0.0	0.0	0.9	2.1	1.6	1.0	1.8	1.2
9	1.0	0.7	0.2	-0.9	-2.0	-2.5	-2.0	-1.6	-0.4	0.0	0.4	0.9	-0.5
10	0.2	-0.5	-1.9	-8.2	-4.0	-4.5	-4.0	-8.5	-3.0	-2.0	-0.6	0.0	-2.2
11	-1.8	-2.1	-8.5	-5.8	-5.5	-5.8	-5.4	-5.4	-5.0	-3.8	-2.0	-1.3	-8.9
Noon	-2.8	-8.2	-5.0	-6.8	-6.7	-7.3	-6.4	-6.5	-6.4	-5.1	-3.1	-2.1	-5.1
1	-2.9	-8.9	-5.8	-7.9	-7.5	-6.1	-6.7	-7.5	-7.1	-5.5	-3.5	-2.4	-5.7
2	-3.0	-3.9	-5.8	-8.2	-7.7	-8.6	-6.7	-7.7	-7.1	-4.9	-8.6	-2.3	-5.8
3	-2.5	-3.6	-5.5	-7.7	-7.8	-8.4	-6.5	-7.0	-6.6	-3.7	-3.0	-1.9	-5.3
!											1	1	
4	-1.9	-2.8	-4.5	-6.7	-6.1	-7.4	-5,8	-5.5	-5.5	-2.8	-2.1	-1.8	-4.4
8	-1.1	-1.6	-8.3	-5.4	-4.8	-6.1	-4.9	-3.6	-4.2	-1.7	-1.2	-0.8	-3.2
6	-0.6	-0.6	-1.8	-8.5	-3.0	-4.5	-8.5	-2.0	-2.5	-0.8	-0.4	-0.4	-2.0
7	-0.8	0.8	-0.4	-1.1	-1.0	-2.4	-1.5	-0.5	-0.6	0.0	0.1	-0.1	-0.6
			l									ľ	
8	0.1	0.6	0.9	0.7	0.9	0.0	0.8	1.0	1.0	0.7	0.6	0.2	0.6
9	0.4	1.0	1.7	2.0	2.8	1.8	1.9	2.4	1.8	1.8	1.0	0.4	1.5
10	0.6	1.8	2.8	3.2	8.5	3.6	3.8	8.3	2.7	1.9	1.8	0.5	2.8
11	0.7	1.5	2.6	4.1	4.5	5.0	4.2	4.3	8.4	2.4	1.5	0.8	2.9
						1		•					1
					ł	l	ĺ						l
6.6	0.6	0.9	1.0	1.2	0.9	0.9	0.5	1.7	1.4	1.8	0.8	0.5	0.9
7. 7	0.8	1.2	1.6	1.6	0.8	0.8	0.5	1.4	1.7	1.4	0.9	0.7	1.1
8.8	0.8	1.1	1.7	1.8	0.7	0.0	0.1	0.9	1.5	1.1	0.8	0.8	0.9
					١.,					0.0			
9. 9	0.7	0.8	0.9	0.5	0.1	-0.8	-0.0	0.4	0.7	0.6	0.7	0.6	0.5
10.10	0.4	0.4	0.2	0.0	-0.2	-0.4	-0.4	-0.1	-0.1	-0.0	0.4	0.2	0.0
7. 2. 9	-0.2	-0.8	-0.2	-0.6	−0.9	-1.2	-0.8	-0.7	-0.4	-0.2	-0.3	-0.1	-0.5
	-0.3		-0.8	-0.5	-0.7	-0.7	-0.6	-0.4	-0.3	-0.2	-0.4	-0.2	-0.4
6. 2. 8 6. 2.10	-0.3	-0.8 -0.1	0.1	0.3	0.7	0.5	0.4	0.3	0.3	0.2	-0.1	-0.1	0.1
): I	-0.2 -0.6		-1.2	-1.9	-1.9	-2.2	-1.9	-1.4	-1.4	-0.7	-0.7	-0.4	-1.3
6. 2. 6	۵.0	-0.7	-1.2	_1.5	_1.5	-2.2	1.0	_1.4	1	3.7	"."	"."	""
7. 2	-0.5	-0.9	-1.1	-1.9	-2.5	-2.8	-2.1	-2.2	-1.5	-1.0	-0.9	-0.4	-1.5
8. 2	-0.7	-1.1	-1.6	-3.1	-3.6	-4.8	-3.8	-3.4	-2.5	-1.7	-1.3	-0.5	-2.3
8. 1	-0.7	-1.1	-1.6	-2.9	-3.5	-4.0	-8.4	-3.3	-2.5	-1.9	-1.8	1	-2.2
7. 1	-0.5	-0.9	-1.1	-1.8	-2.4	-2.6	-2.1	-2.1	-1.5	-1.4	-0.9	-0.4	-1.5
	3.3	3.5	***	_1.5					1.0	***	"		1
9.12.3.9	-0.8	-1.8	-2.1	-3.3	-3.4	-4.1	-8.2	-3.2	-2.9	-1.9	-1.2	-0.7	-2.4
H1	4						1 5.2	1	, 2.9			,	,

LV.

PRUSSIA. - HALLE. Lat. 51° 30' N. Long. 11° 57' E. Greenw.

orrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					=								
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.58	1.00	1.86	2.52	8.98	3.91	8.72	8.32	2.70	2.01	0.95	0.46	2.21
2	0.56	l .	1.58		1		j.	1	1	1	1	1	2.35
. 8	0.60		1.74		1		1	1	4	1	1	1	
					l .	(8.12	1	1		
4	0.66	1.84	1.82	2.94	8.10	2.95	2.97	8.27	8.02	2.41	1.08	0.54	2.17
5	0.72	1.86	1.72	2.62	2.18	2.09	2.14	2.64	2.62	2.25	1.00	0.55	1.82
6	0.72	1.80	1.42	1.98	1.80	1.18	1.24	1.90	1.97	1.90	0.92	0.58	1.37
7	0.65	1.10	0.94	1.07	0.32	0.25	0.23	0.84	0.98	1.82	0.74	0.55	0.75
8	0.86	0.58	0.20	0.08	-0.56	-0.58	-0.57	-0.20	,	i .	1	1	0.02
9	0.08	-0.08	_0 &e	_0.08	_1.84	_1.84	_1 80	-1.20	_1 14	_0.71	01	-0.09	_0 76
10		•				ı		-2.10	1				, ,
11						1		4		J	1		
		-1.29		l .		l		-2.90		P .	l	1	
Noon	-1.00	-1.77	-2.06	-8.08	-8.14	-8.07	-8.16	-8.85	-8.11	-2.86	-1.66	-1.08	-2.45
1	-1.17	-2.02	-2.22	-3.82	-6.88	-8.85	-8.46	-8.58	-3.30	-8.01	-1.78	-1.09	-2.68
2	-1.06	-1.86	-2.10	-8.26	-3.37	-8.46	-8.54	-8.57		i			
8								-8.30		•	1		
4								-2.84					
•	0.00	2.01		2.00	2.1.2	2.14	2.10	2.00	2.00	1.01	0.75	-0.42	1.00
5	-0.80	-0.59	-0.91	-1.78	-2.24	-2.22	-2.16	-1.97	-1.88	-1.20	-0.40	-0.20	-1.32
6	-0.13	-0.29	-0.52	-0.96	-1.58	-1.50	-1.89	-1.38	-1.12	-0.69	-0.14	-0.08	-0.81
7	-0.00	-0.09	-0.06	-0.34	-0.86	-0.73	-0.55	-0.59	-0.38	-0.21	0.04	0.09	-0.81
8	0.11	0.18	0.26	0.82	-0.10	0.07	0.26	0.15	0.29	0.25	0.21	0.22	-0.18
								1					ı
9	0.21	0.80	0.59	0.88	0.68	0.90	1.09	0.90	0.87	0.68	0.39	0.84	0.65
10	0.81	0.46	0.79	1.83	1.64	1.81	1.87	1.61	1.42	1.12	0.59	0.37	1.11
11	0.41	0.65	0.98	1.78	2.61	2.69	2.64	2.30	1.90	1.47	0.76	0.40	1.55
Midn	0.48	0.83	1.16	2.17	8.48	8.42	8.29	2.86	2.33	1.77	0.89	0.48	1.92
			.										
6. 6	0.21	0.89	0.41	0.42	-0.08	-0.07	-0.01	0.84	0.40	0.58	.0.30	0.18	0.26
7. 7	0.30	0.51	0.45		-0.14			0.26	0.48	0.61	0.89	0.28	0.28
8. 8	0.33	0.51	0.44		-0.27			0.18	0.80	0.56	0.29	0.32	0.22
9. 9	0.24	0.83	0.23			-0.26		-0.03	0.21	0.29	0.26	0.25	0.22
10.10			- 1										
10.10	0.13	0.11	-0.04	-0.00	-0.83	-U.ZZ	-0.11	-0.15	-0.14	-0.02	0.04	0.13	-0.05
7. 2. 9	-0.11	-0.20	-0.18	-0.84	-0.71	-0.70	-0.65	-0.49	-0.35	-0.29	-0.20	-0.10	-0.86
6. 2. 8	-0.15	-0.25	-0.19	-0.85	-0.67	-0.66	-0.62	-0.49	-0.85	-0.82	-0.23	-0.15	-0.87
6. 2.10	-0.08	-0.12	0.03	0.06	-0.16	-0.12	-0.08	-0.00	0.06	-0.03	-0.11	-0.07	-0.05
6. 2. 6	-0.25	-0.42	-0.47	-0.88	-1.18	-1.16	-1.16	-0.95	-0.84	-0.65	-0.88	-0.25	-0.71
7. 2	00	0 00	امد مــ		_1 00	_1 66	_, ,,	-0.82		_0 #o	, _,		
1 1					1								- 1
8. 2				1				-1.85					- 1
8. 1	1 1							-1.26				1	- 1
7. 1	-0.19	-0.24	-0.32	-0.55	-0.92	-0.95	-0.96	-0.78	-0.57	-0.48	-0.87	-0.25	-0.54
9.12.3.9	-0.85	-0.62	-0,84	-1.27	-1.67	-1.66	-1.62	-1.68	-1.40	-1.16	-0.59	-0.84	-1.10
7. 2.2(9)	. ,							-0.33					- 1
(5)	0.00	V-12	٠.٠٠	V.10	2.00	0.01	~	0.00	4.10	7.30	-0.14	-0.02	0.20
Dail.ext.	-0.23	-0.33	-0.20	-0.16	0.37	0.24	0.14	0.00	-0.09	-0.80	-0.3 5	-0.26	-0.14

LVI.

Hanover. — Göttingen. Lat. 51° 32' N. Long. 9° 56' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

						of Re							
Hours.	Jan.	Peb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Moan.
Morn. 1	0.90	1.18	1.58	2.94	8.81	8.48	8.56	8.85	2.81	1.58	0.69	0.60	2.06
il 2	0.92	1.14	1.77	2.49	8.70	3.71	8.82	8.70	2.68	1.75	0.74	0.59	2.25
8	0.94	1.16		2.79		8.78	8.92	8.92	3.28	1.94	1		2.41
4	0.99	1.20		8.04	l	8.57	3.79	8.89	3.63	2.10		1	
1	0.55	1.20	2.22	0.04	0.01	5.01	3	0.00	5.05	2.10	0.52	0.00	2.45
5	1.15	1.26	2.29	8.08	8.55	8.10	8.36	3.52	3.62	2.15	1.00	0.62	2.39
6	1.12	1.20	2.10	2.73	2.62	2.22	2.59	2.79	3.50	1.99	1.08		2.05
7					I						1		
13 1	1.18	1.14	1:77	2.24	1.78	1.21	1.40	1.69	2.62	1.58	0.94	0.65	1.51
8	1.12	0.80	1.02	0.89	0.75	0.49	0.48	0.56	1.86	1.08	0.53	0.54	0.80
ا ما	0.70	0.00		0.10			A 85	A 60	A 60			0.00	
9	0.50							-0.68		-0.21	0.10		-0.19
10	-0.87	-0.88						-1.84				-0.02	
11	-1.26				-2.59			-2.88			1		l 18
Noon	-1.83	-2.17	-2.43	-2.9 8	-8.80	-3.19	-8.4 8	-8.52	-8.87	-2.5 0	-1.46	-1.12	-2.6 1
J)													
1 1	-2.02					1						-1.42	
2	-2.08	-2.28	-3.05						-4.00	-2.98	-1.60	-1.28	-3.0 8
3	-1.74	-1.98	-2.88	-3.48	-3.95	-8.91	-4.00	-4.03	-4.03	-2.84	-1.82	-1.02	-2.93
4	-1.23	-1.35	-2.48	-3.24	-8 .67	-8.6 5	-8.82	-8.71	-8.62	-2.40	-0.90	-0.66	-2.56
5	-0.79	-0.59	-1.79	-2.64	-8.13	-8.09	-8.18	-3.15	-2.94	-1.74	-0.54	-0.36	-2.00
6	-0.83	-0.04								-0.94		-0.14	- 11
7	-0.05		-0.26		-1.44					-0.30			-0.57
8	0.24	0.58	0.84	0.04		-0.15	0.08	0.18	0.05	0.24	0.17	0.20	0.14
1 ° 1	0.24	0.56	0.04	0.04	V.22	-0.15	0.00	U.10	0.05	U.24	0.17	0.20	0.14
9	0.40	0.82	0.78	0.77	0.88	0.79	1.09	1.05	0.78	0.71	0.30	0.30	0.72
10	0.57	0.94	1.05	1.30	1.59	1.78	1.87	1.62	1.28	1.02	0.42	0.40	1.15
14 1							-						
11	0.71	1.01	1.80	1.75		2.69	2.62	2.26	1.71	1.35	0.56	0.44	1.56
Midn	0.88	1.07	1.54	2.11	2.52	8.01	3.18	2.93	2.00	1.44	0.62	0.56	1.22
													1
6. 6	0.40	0.58	0.52	0.44		0.01		0.24	0.77			0.26	0.37
7. 7	0.54	0.78	0.76	0.72	0.17	0.08	0.05	0.80	0.88	0.64	0.48	0.36	0.47
8.9	0.68	0.69	0.68	0.47	0.27	0.17	0.26	0.85	0.71	0.66	0.85	0.37	0.47
9.9	0.45	0.87	0.82	0.81	0.21	0.12	0.22	0.19	0.28	0.25	0.20	0.30	0.27
10.10	0.10	0.03	-0.02	-0.01	0.08	0.07	-0.19	-0.11	-0.09	0.10	-0.00	0.19	0.01
11 1													,
7. 2. 9	-0.17	-0.09	-0.17	-0.18	-0.44			-0.47	-0.20	-0.23	-0.12	-0.11	-0.28
6. 2. 8	-0.22	-0.15	-0.20	-0.26	-0.58	-0.65	-0.49	-0.41	-0.15	-0.25	-0.12	-0.14	-0.30
6. 2.10	-0.11	-0.08	0.08	0.16	0.08	-0.08	0.12	0.09	0.26	0.01	-0.03	-0.07	0.04
6. 2. 6	-0.41	-0.86	-0.67	-0.90	-1.25	-1.84	-1.80	-1.28	-0.82	-0.64	-0.25	-0.25	-0.79
		1					•	1 1					
7. 2	-0.45	-0.55	-0.64	-0.66	-1.10	-1.41	-1.35	-1.23	-0.69	-0.70	-0.83	-0.32	-0.79
8. 2												-0.37	-1.14
8. 1	1	1	-0.90							1			-1.07
7. 1												-0.39	1 11
9.12.8.9	-0.67	-0.85	-1.17	-1.46	-1.71	-1.72	-1.76	-1.80	-1.71	-1.21	-0.60	-0.39	-1.25
7. 2.2(9)	-0.08	1			-0.11	1			0.05	ł .		-0.01	
1			1				}	1			1	•	i li
Dail. ext.	-0.44	-0.58	-0.88	-0.24	-0.03	-0.15	-0.09	-0.12	-0.20	-0.42	-0.26	-0.38	-0.30
L													-

LVII.

PRUSSIA. - BERLIN. Lat. 52° 30' N. Long. 13° 24' E. Greenw.

corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					20810	es or b		<u> </u>					
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midnight.	0.34	0.59	0.90	1.78	2.21	2.15	1.78	1.52	1.50	0.95	0.44	0.84	1.21
1	0.48	0.78	1.18	2.22	8.23	2.80	2.52	2.58	1.99	1.48	0.59	0.87	1.67
2	0.49	0.97	1.38	2.56	8.83	8.88	8.06	8.05	2.41	1.95	0.68	0.48	2.02
8	0.54	1.09	1.64	2.41	4.00	8.46	8.28	8.15	2.76	2.81	0.78	0.46	2.15
4	0.58	1.25	1.85	3.03	8.77	3.18	8.12	8.40	2.94	2.45	0.79	0.52	2.24
5	0.65	1.37	1.97	8.05	8.16	2.59	2.67	8.16	2.89	2.82	0.84	0.56	2.10
6	0.73		1.92	2.69	3.28	l	1.92	2.57	2.56	1.52	0.84	0.71	1.78
7	0.75	1.18	1.62	2.01	1.48	0.94	1.18	1.83	2.03	1.15	0.65	0.63	1.21
8	0.62		1.14		0.42	1	0.44		1.03	1		1	1
9	0.41		1 '	1	I	1	1	-0.36		1		0.88	11
10	0.19			ı	-1.47		l .		l.	-0.81		0.05	1
11	-0.30	-0.66	-1.02	-1.78	-2.20	-1.72	-1.78	-2.07	-1.90	-1.46	-0.55	-0.36	-1.32
Noon.	-0.55	-1.16	-1.44	-2.87	-2.65	-2.17	-2.26	-2.64	-2.49	-1.87	-0.95	-0.69	-1.77
1	-0.93	-1.48	-1.97	-2.85	-8.00	-2.25	-2.54	-3.06	-2.9 6	-2.14	-1.26	-0.86	-2.11
2	-1.07				-3.25			-8.17					
8	-1.03	-1.67	-2.2 8	-3.27	-3.34	-2.84	-2.82	-3.25	-8. 19	-2.12	-1.20	-0.95	-2.82
4								-8.14					
5			-1.70			1	l	-2.72		l			1
6	1	-0.74	_					-2.21					ıl.
7	-0.22	-0.46	-0.64	-1.13	-1.55	-1.75	-1.44	-1.22	-0.82	-0.63	-0.11	-0.15	-0.84
8	-0.12	-0.20	-0.27	-0.84	-0.67	-0.57	-0.89	-0.30	-0.16	-0.30	0.05	-0.02	-0.27
9	0.06		1	0.40	0.13	0.81	0.38	0.84	0.36	-0.08	0.10		0.22
10	0.14		0.39	0.93			1.01	1.06	0.98		0.20	0.17	0.59
11	0.24	0.38	0.65	1.37	1.56	1.58	1.44	1.57	1.20	0.56	0.36	0.25	0.93
6, 6	0.17	0.82	0.40	0.82	-0.06	-0.81	-0.12	0.19	0.49	0.32	0.27	0.28	0.10
7, 7	0.27		0.49	0.44		-0.40	-0.13	0.30	0.60	0.26	0.27	0.24	0.22
8, 8	0.25	0.35	0.44	0.30	-0.08	-0.08	0.03	0.23	0.44	0.16	0.26	0.29	0.13
9, 9	0.24	0.26	0.80	0.12	0.21	-0.05	0.02	0.24	-0.28	-0.06	0.28	0.22	0.12
10, 10	0.17		ı	1	1		-0.07			-0.28			0.05
7, 1	-0.09		ı		-0.79	l.	-0.68	-0.61		-0.49		l .	-0.42
7, 2, 9	-0.09			-0.19		-0.49	-0.36	-0.17		-0.89			i
6, 2, 10	-0.07 	-0.04	0.04	0.21	-0.07	-0.01	0.06	0.15	0.18	-0.15	-0.08	-0.03	-0.07
Daily ext.	-0.16	-0.17	-0.16	-0.11	0.33	0.31	0.28	0.08	-0.13	0.11	-0.22	-0.13	0.00

LVIII.

GERMANY. - SALZUFLEN. Lat. 52° 5' N. Long. 8° 40' E. Greenw.

Corrections to be applied to the Means of the Hours.of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					248.00	s of Ba							
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.00	1.10	1.05	2.11	2.41	2.57	2.05	1.71	2.12	1.24	0.90	0.31	1.46
2	0.55	1.22	1.20	2.44	2.98	2.85	2.27	2.01	2.44	1.55	1.26	0.48	1.77
8	0.60	1.27	1.84	2.64	3.29	2.98	2.89	2.28	2.74	1.82	1.53	0.65	1.96
4	0.62	1.26	1.38	2.62	8.37	2.86	2.32	2.26	2.87	1.98	1.64	0.78	2.00
5	0.72	1.18	1.29	2.35	8.08	2.47	1.99	2.00	2.71	1.97	1.58	0.83	1.85
6	0.62	1.01	1.06	1.80	2.41	1.83	1.42		2.18	1.75	1.37	0.79	1.48
7	0.51	0.75	0.70	1.05	1.45	1.02	0.70		1.84	1.84	1.04	0.64	0.94
8	0.31	0.41	0.25	0.20	0.88		-0.06		0.30	0.75	0.62	0.38	0.31
9	0.08		-0.22	_0.69	A 80	A 67	_0 ~1	84	85	0.09	0.14	0.00	-0.31
10			-0.22 -0.68						1			ĺ	
	1			-									1
. 11	-0.74		-1.06										
Noon	-0.91	-1.42	-1 .8 9	-2.82	-2.81	-2.89	-1.90	-1.7Z	-2.41	-1.78	-1.18	-0.62	-1.70
1	-1.01	-1.68	-1.59	-2.54	-2.58	-2.72	-2 .18	-2.03	-2.75	-2.09	-1.48	-0.64	-1.93
2		1	1					L .					-2.03
8		ł	-1.56						1				
الأسا	4		-1.83						ı	1			
		l	,					ŀ	ļ	1			
5	-0.20		-0.98										
6			-0.56										
7			-0.15)		1	1	-0.47		i .	
8	0.08	0.11	0.19	-0.04	-0.6 5	-0.09	0.09	0.21	0.12	−0.11	-0.8 1	-0.27	-0.06
9	0.14	0.84	0.45	0.48	0.04	0.62	0.70	0.71	0.81	0.18	-0.20	-0.21	0.34
10	0.21	0.55	0.68	0.94	0.68	1.22	1.26		1.30				0.67
11	0.22	0.74	0.77		1.27		1.52		1.61	0.66	1	1	
Midn.	0.40		0.90		1.84		1.80	ſ	1.86				1.22
	0.10	3.50	3.55		1.01	2.10	2.00		2.00	5.51	0.00		
6. 6	0.26	0.25	0.25	0.29	0.04	0.11	0.05	0.13	0.32	0.43	0.36	0.24	0.24
11 1					0.24						1		0.22
7. 7	0.26	0.29	0.29	0.22	0.06	0.08	0.04				0.80 0.16	0.17 0.06	
8.8	it i	1	1	0.08	-0.14								
9. 9	0.11	0.16	-0.03	-0.08		-0.0 3 -0.08	-0.02 0.06		0.09 -0.09		-0.03 -0.21	-0.08	-0.11
10.10	-0.06	0.01	-0.08	-U.Z1	-v.87	-0.08	0.06	0.01	~v.09	-U.11	-V.ZI	-V.18	-0.11
7. 2. 9	-0.10	-0.22	-0.17	-0.36	-0.39	-0.42	-0.30	-0.27	-0.25	-0.22	-0.24	-0.05	-0.2 5
6. 2. 8	-0.08	-0.21	-0.13	-0.28	-0.8 0	-0.39	-0.26	-0.20	-0.20	-0.18	-0.17	-0.02	-0.20
6. 2.10	-0.04	-0.06	0.01	0.05	0.14	0.05	0.13	0.07	0.19	-0.00	-0.08	0.03	0.04
6. 2. 6	-0.14	-0.41	-0.38	-0.67	-0.78	-0.90	-0.73	-0.6 8	-0.76	-0.44	-0.2 8	-0.04	-0.51
7. 2	-0.22	_0.50	-0.48	-0.78	-0.61	_0.9K	-0.80	-0.78	-0.78	-0.42	-0.26	0.03	-0.54
8. 2													-0.86
8. 1	-0.85		-0.67										
7. 1			-0.45										
	1	ì					1					1	
9.12.8.9	1	I	-0.6 8		1								
7. 2.2(9)	-0.04	-0.08	-0.01	-0.15	-0.2 8	-0.16	-0.05	-0.02	0.02	-0.12	-0.23	-0.09	-0.10
Dail.ext.	-0.15	-0.24	-0.14	0.02	0.88	0.08	0.02	-0.08	-0.02	-0.10	0.04	0.10	-0.02
			_										

LIX.

PRUSSIA. — STETTIN. Lat. 53° 25' N. Long. 14° 34' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Resumur.

1 0. 2 0. 8 0. 6 0. 7 0. 8 0. 9 0. 10 -0.	.26 0.54 .38 0.59 .43 0.70 .49 0.88 .53 0.89 .57 0.97 .55 0.94 .46 0.98 .36 0.66 .22 0.36	1.17 1.80 1.41 1.51 1.63 1.62	1.66 1.91 2.15 2.39 2.60 2.67 2.40 1.70	2.21 2.66 3.03 3.39 3.58 3.45 2.78 1.63	2.21 2.46 2.84 3.10 3.03 2.78 2.12	1.83 2.25 2.62 2.95 8.07 2.85	1.93 2.24 2.54 2.83	1.53 1.61 1.87 2.11	0.88 1.01 1.13 1.24	0.50 0.44 0.47 0.51	0.39 0.46 0.50 0.56	1.24 1.43 1.63 1.99
1 0. 2 0. 3 0. 4 0. 5 0. 6 0. 7 0. 8 9 0. 10 -0. 11 -0.	.38 0.59 .43 0.70 .49 0.88 .53 0.89 .57 0.97 .55 0.94 .46 0.88 .36 0.66 .22 0.36 .04 -0.02	1.17 1.80 1.41 1.51 1.63 1.62	1.91 2.15 2.39 2.60 2.67 2.40	2.66 3.03 3.89 3.58 3.45 2.78	2.46 2.84 3.10 3.09 2.78 2.12	2.25 2.62 2.95	2.24 2.54 2.88 3.08	1.61 1.87 2.11	1.01 1.13 1.24	0.44 0.47 0.51	0.46 0.50	1.43 1 63
2 0. 3 0. 4 0. 5 0. 7 0. 8 0. 9 0. 10 -0.	.43 0.70 0.88 .53 0.89 0.97 .55 0.94 .46 0.88 .36 0.66 .22 0.36 .04 -0.02	1.80 1.41 1.51 1.63 1.62 1.87	2.15 2.39 2.60 2.67 2.40	3.03 3.89 3.58 3.45 2.78	2.84 8.10 8.09 2.78 2.12	2.62 2.95 8.07	2.54 2.88 3.08	1.87 2.11	1.13 1.24	0.47 0.51	0.50	1 63
8 0. 6 0. 7 0. 8 0. 9 0. 10 -0. 11 -0.	.49 0.88 .53 0.89 .57 0.97 .55 0.94 .46 0.88 .36 0.66 .22 0.86	1.41 1.51 1.63 1.62 1.37	2.60 2.67 2.40	8.89 8.58 8.45 2.78	3.10 3.09 2.78 2.12	2.95 8.07	2.88 3.08	2.11	1.24	0.51		1
4 0. 5 0. 6 0. 7 0. 8 0. 9 0. 10 -0.	.53 0.89 .57 0.97 .55 0.94 .46 0.88 .36 0.66 .22 0.86	1.51 1.63 1.62 1.37	2.60 2.67 2.40	8.58 8.45 2.78	8.09 2.78 2.12	8.07	3.0 8				0.56	1.99
5 0. 6 0. 7 0. 8 0. 9 0. 10 -0. 11 -0.	.57 0.97 0.94 .46 0.88 .36 0.66 .22 0.36	1.63 1.62 1.37	2.67 2.40	8.45 2.78	2.78 2.12	1		2.83	1:00			41
6 0. 7 0. 5 0. 9 0. 10 -0. 11 -0.	.36 0.66 .22 0.36	1.62	2.40	2.78	2.12	2.85			1.00	0.55	0.61	1.92
7 0. 8 0. 9 0. 10 -0. 11 -0.	.36 0.66 .22 0.36	1.87					3.10	2.46	1.40	0.58	0.64	1.92
8 0. 9 0. 10 -0. 11 -0.	.36 0.66 .22 0.36		1.70	1.63		2.21	2.78	2.45	1.42	0.60	0.56	1.70
9 0. 10 -0. 11 -0.	.22 0.86 .04 -0.02	0.90		1	1.17	1.31	2.02	1.98	1.25	0.52	0.46	1.23
10 -0. 11 -0.	.04 -0.02		0.66	0.83	0.20	0.85	0.96	1.11	0.79	0.43	0.38	0.59
11 -0.		0.23	-0.42	-0.88	-0.72	-0.53	-0.26	-0.05	0.16	0.13	0.23	-0.18
	36 LA 59		1					-1.11		-0.22	•	-0 83
Noon0.		-1.06	-2.07	-2.62	-2.18	-1. 96	-2.23	-1.96	-1.23	-0.60	-0.85	-1.48
11 00	.63 -0.93		1	1		-2.46	-2.93	-2.5 8	-1.6 8	-0.90	-0.64	-1.98
	.81 -1.26		-2.80		-2.90	-2.81				-1.06	-0.86	-2.17
	.90 -1.39				-2.99				-2.06		-0.94	
з —0.	.78 –1.84	-2.06	-2.84	-3.35	-2.90	-2.80	-8.3 8	-2.82	-1.88	-0.94	-0.86	-2.16
	.63 -1.15											
- 11	.41 -0.83		1 I									,
	.23 -0.46											
7 -0.	.11 -0.23	-0.40	-0.55	-0.89	-0.89	-0.98	-0.78	-0.52	-0.10	-0.00	-0.19	-0.46
g 0.	.01 -0.04	-0.02	0.10	-0.14	-0.14	-0.17	0.02	0.06	0.17	0.18	-0.06	-0.00
- h	.08 0.16	i		0.78	0.78	0.48	0.74	0.60	0.39	0.30	0.07	
	.20 0.30	0.61	. 1.10	1.80	1.30	1.03	1.20	1.00	0.58	0.43	0.22	0.77
11 0.	.25 0.42	0.79	1.42	1.76	1.76	1.47	1.60	1.31	0.74	0.50	0.32	1.03
	.15 0.24	0.36	0.54	0.52	0.19	0.29	0.55	0.65	0.48	0.21	0.18	0.86
-, -	.17 0.30	1	0.54	0.37	0.14	0.19	0.62	0.78	0.40	0.21	0.14	0.38
**	.19 0.31		0.38	0.10	0.03	0.09	0.49	0.75	0.48	0.20	0.14	0.30
-, - ,	.15 0.26	1 1	0.18	-0.08	1	-0.08	0.24	0.28	0.28	0.22	0.15	0.16
10, 10 0.	.08 0.14		-0.18	-0.29	-0.12	-0.15	-0.10	-0.06	0.02	0.11	0.10	-0.03
7, 1 -0.	.17 -0.21	-0.67	-0.55	-0.86			-0.68		t .	-0.27	-0.20	-0.50
7, 2, 9 -0.	.13 -0.13	1	-0.19	-0.38		-0.40		i	-0.14	1	-0.14	11
6, 2, 10 -0.	.05 -0.05	0.38	0.19	0.19	0.14	0.08	0.16	0.15	-0.02	-0.01	-0.05	0.09
Daily ext0.				1	1				I	ł		1

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LX.

SLESWICK. - APENBADE. Lat. 55° 3' N. Long. 9° 25' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

						s of Re	wear.						
Hours.	Jan.	Feb.	Marsh.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mesn.
Morn. 1	0.26	0.69	0.98	1.73		8.82		ł	2.16				1.65
2	0.81	0.78	1.14	1.83	8.17	8.90	2.38	2.66	2.29	1.19	0.59	0.35	1.72
8	0.88	0.79	1.26	1.98	3.02	8.82	2.13	2.66	2.54	1.30	0.64	0.87	1.74
4	0.42	0.75	1.34	2.10	2.71	3.50	1.78	2.64	2.62	1.87	0.66	0.38	1.69
5	0.44	0.69	1.31	2.02	2.22	2.89	1.85	2.18	2.43	1.86	0.69	0.40	1.50
6	0.50	0.62	1.18	1.63	1.54	1.94	0.86	1.56	2.02	1.25	0.69	0.40	1.18
7	0.47	0.54	0.90	1.15	0.70	0.83	0.30	0.77	1.18	0.97	0.61	0.37	0.73
8	0.89	0.38	0.50	0.41	-0.23	-0.34	-0.29	ľ	0.18	0.52	0.42	0.27	0.17
9	0.23	0.10		49	-1 14	_1 00	_0 07	-1.10	V 60	_0.70	0.10	0.10	-0.44
10	11	ı				1 1			ľ			-0.15	(
11		ı						1					
	11	i										-0.43	
Noon	-0.62	-1.19	-1.62	-2.42	-2.80	-2.95	-2.09	-2.74	-2.79	-1.94	-0.90	-0.66	-1.91
1	-0.78	-1.40	-1.90	-2.75	-8.08	-8.24	-2.23	-2.89	-3.03	-2.15	-1.10	-0.78	-2.11
2	-0.69	-1.34	-1.96	-2.39	-3.16	-8.49	-2.27	-2.90	-3. 08	-2.07	-1.02	-0.75	-2.14
8	-0.61	-1.06	-1.78	-2.79	-8.10	-3.6 8	-2 .21	-2.78	-2.93	-1.74	-0.82	-0.59	-2. 01
4	-0.3 8	-0.64	-1.41	-2.48	-2.86	-3.62	-2.02	-2.89	-2.54	-1.28	-0.59	-0.38	-1.71
5	-0.16	-0.23	-0 02	-1.80	-2.40	-2.21	-1.70	-2.02	_1. 9 8	-0.71	-0.29	-0.15	-1.30
6	-0.03					1		-1.23					-0.80
7	0.01	0.18	0.02				l .	-0.47	1				-0.27
8	0.03	0.18	0.02			-0.07		1	ł				,
٥	0.00	0.10	0.33	0.00	0.22	-0.01	0.10	0.40	0.00	0.03	0.00	0.14	0.20
9	0.01	0.17	0.54	1.25	1.22	1.25	0.97	1.21	1.21	0.51	0.09	0.15	0.71
10	0.02	0.22	0.66	1.57	2.05	2.33	1.63	1.72	1.61	0.65	0.18	0.18	1.07
11	0.07	0.33	0.76	1.69	2.66	8.10	2.14	2.25	1.83	0.85	0.30	0.21	1.35
Midn	0.15	0.52	0.86	1.70	3.02	8.57	2.48	1.68	1.97	0.92	0.42	0.26	1.46
6. 6	0.24	0.84	0.88	0.89	0 0e	-0.82	_0.18	0.17	0.45	0.50	0.29	0.21	0.19
7. 7	0.24	l .	0.46		1	-0.80					0.30		0.23
8. 8	0.21	0.28	0.42			-0.21	-0.06		- 0.87	0.48	0.23	0.21	0.21
9. 9	0.11	0.14	0.26	0.42		-0.07	0.05	0.06	0.19	0.21	0.10		0.14
10.10	-0.02	1	-0.00				0.12			-0.07			0.01
10:10	0.02	0.00	0.00	0.20	0.00	0.00	0.12	00	0.00	0.0.	0.00		0,01
7. 2. 9	-0.08	-0.21	-0.17	-0.16	-0.41	-0.47	-0.33	-0.31	-0.23	-0.20	-0.11	-0.08	-0.23
6. 2. 8	-0.05	-0.18	-0.15	-0.20	-0.47	-0.54	-0.41	-0.31	-0.17	-0.16	-0.10	-0.07	-0.23
6. 2.10	-0.06	-0.17	-0.04	0.10	0.14	0.26	0.07	0.18	0.18	0.0 6	-0.05	-0.06	0.04
6. 2. 6	-0.07	-0.22	-0.40	-0.75	-1.11	-1.37	-0.86	-0.86	-0.78	-0.36	-0.15	-0.11	-0.58
7. 2	-0.11	_0.40	_0 K9	_0.87	1.22	_7.82	0.gg	-1.07	0.9×	-0.55	-0.21	-0.19	-0.70
8. 2												-0.24	
8. 1												-0.26	
7. 1		1										-0.21	
''	3.10	V. 23	0.00	-0.00	1.10	-1.01	V.01	1.00	V.60	V.03			
9.12.3.9	-0.25	-0.50	-0.72	-1.10	-1.47	-1.70	-1.05	-1.85	-1.34	-0.82	-0.40	-0.25	-0.91
7. 2.2(9)	-0.06	-0.12	0.01	0.19	0.01	-0.04	-0.01	0.07	0.18	-0.02	-0.06	-0.02	0.01
Dail.ext.	-0.14	-0.81	-0.31	-0.40	0.01	0.11	0.12	-0.12	-0.23	-0.39	-0.21	-0.19	-0.20
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LXI.

Scotland. — Leith. Lat. 55° 59' N. Long. 3° 10' E. Greenw. orrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	of Fal	renhelt	·						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.	
Morn. 1	0.88	0.86	1.76	8.02	8.04	3.29	4.10	2.95	2.54	1.10	1.26	0.72	2.09	I
2	0.61	0.77	ı	3.92	8.47	8.62	4.28	8.20	2.77			0.65	2.83	I
8	0.68	0.77		4.57	3.96	8.74	4.66	8.49	8.29	1.81	1.40	1	2.57	I
4	0.95	0.95		5.81	4.41	3.98	5.11	8.71	8.65	1.33	1.46	0.70		l
				İ										I
. 5	1.06	1.17		ı	4.28	3.94	4.59	3.65	8.78	1.62	1.37			H
6	1.06	1.81				3.04	8.56	8.26	8.51	2.03	1.28		1	I
7	0.97	1.24		8.47	2.66	2.25	2.89	2.25	2.75		1.06		1.98	I
8	0.88	1.26	1.80	2.18	1.40	1.10	1.15	1.08	1.46	0.97	1.04	0.54	1.24	I
9	0.61	0.77	0.81	-0.27	0.11	-0.18	-0.28	-0.50	-0.14	0.32	0.56	0.32	0.18	H
10	0.16							-1.26	l	-0.83		-0.02	1	l
11	-0.84							-2.08		1		-0.86	l	1
Noon	-1.04	-1.69						-2.99						l
						İ	l		ł			l		ı
1			-2.97	-4.87	-8.35	-3.15	-8.67	-8.44	-3.92	-2.79	-2.30	-1.51		ı
2			-8.29	-4.78	-3.78	-8.88	-4.07	-3.65	-4.28	-2.84	-2.57	-1.55	-3.20	ı
8		-2.27						-3.65						I
4	-1.19	-1.78	-8.55	-4.79	-4.19	-8.94	-4.40	-8.87	-8.06	-1.96	-1.69	-0.83	-2.96	ı
. 5	-0.68	-0.95	-2.84	-4.25	-4.03	-8.71	-4.57	-3.76	-3.56	-1.31	-1.04	-0.50	-2.60	ı
6	-0.45		-2.14		-8.51			-3.47				-0.27	-2.12	ı
7	-0.09	-0.09	-1.17	-2.45	-2.61	-2.52	-3.58	-1.69	-0.97	0.05	-0.25	0.18	-1.27	l
. 8	0.14	0.82	-0.45	-0.81	-1.17	-0.79	-1.31	-0.41	-0.16	0.59	0.05	0.29	-0.31	i
	0.00			0.00	0.00		0.40	0.00						l
9	0.28		,		0.32	0.50		0.59	0.59	0.72	0.82		0.44	۱
10 11	0.18	1		1	0.86 1.69	1.89 2.16	1.71 2.52	1.58 2.23	1.24	1.15	0.79	0.41	1.04	ı
Midn	0.32	1.01	1.44		2.82	2.68	3.44	2.77	1.67 2.27	1.60 1.49	1.19 1.42	0.54	1.58 1.87	۱
midi	0.00			2.00	2.02	2.00	0.21	2	2.21	1.20	1.42	0.08	2.01	d
														ı
6. 6	0.82	0.48	0.84	0.77	0.00	-0.14	-0.48	-0.11	0.61	0.72	0.32	0.16	0.25	I
7. 7	0.45	0.59	0.65			-0.14		0.29	0.90	0.83	0.41	0.43	0.86	ı
8. 8	0.52		1		0.11		-0.09	0.84	0.65	0.79	0.54	0.48	0.47	۱
9. 9	0.48			1		0.16		0.05	0.23	0.52	0.45	0.84	0.32	ı
10.10	0.18	0.41	0.47	-0.47	-0.11	0.29	0.18	0.16	0.07	0.16	0.23	0.20	0.15	۱
7. 2. 9	-0.14	-0.14	-0.18	-0.29	-0.27	-0.36	-0.48	-0.27	-0.82	-0.16	-0.41	-0.18	-0.26	ı
6. 2. 8			-0.32				-0.61					-0.28		۱
6. 2.10	ll .	-0.02		•		0.86		0.41	0.16	1	-0.16		0.15	ı
6. 2. 6	ll .	-0.47				1	ı	-1.28					-0.90	ı
				1										ı
7. 2			-0.41											I
8. 2	II.		-0.74											۱
8. 1	-0.27	1	-0.59											ı
7. 1	-0.28	-0.52	-0.25	-0.4 5	- 0.86	-0.45	-0.65	-0.01	-v.09	-0.59	-0.63	-0.41	-0.47	ı
9.12.8.9	-0.45	-0.65	-1.24	-2.23	-1.55	-1.71	-1.94	-1.64	-1.71	-0.97	-0.92	-0.45	-1.29	۱
7. 2.2(9)	-0.05	ı	-0.09	1								-0.05		ı
' '			1				1		1		1			I

LXII.

Scotland. - Leith. Lat. 55° 59' N. Long. 3° 10' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Morn. 1							o or Re							
2	Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sopt.	Oes.	Nov.	Dec.	Moss.
2				2 = 2				- 00			0.40			
1.14		1										1	i .	1
1.26	- 1								1		i .		1	, ,
5											l			
6 0.47 0.58 1.24 2.38 1.56 1.85 1.58 1.45 1.56 0.90 0.57 0.26 1.16 7 0.43 0.55 1.10 1.84 1.18 1.00 1.06 1.00 1.22 0.72 0.47 0.30 0.98 8 0.39 0.56 0.80 0.97 0.62 0.49 0.51 0.48 0.55 0.42 0.45 0.24 0.55 0.14 0.07 0.08 0.08 0.08 0.08 0.08 0.08 0.08	4	0.42	0.42	1.15	2.36	1.96	1.77	2.27	1.65	1.62	0.59	0.65	0.31	1.26
6 0.47 0.58 1.24 2.38 1.56 1.85 1.58 1.45 1.56 0.90 0.57 0.26 1.16 7 0.43 0.55 1.10 1.84 1.18 1.00 1.06 1.00 1.22 0.72 0.47 0.30 0.98 8 0.39 0.56 0.80 0.97 0.62 0.49 0.51 0.48 0.55 0.42 0.45 0.24 0.55 0.14 0.07 0.08 0.08 0.08 0.08 0.08 0.08 0.08	5	0.47	0.52	1.22	2.44	1.90	1.75	2.04	1.62	1.68	0.72	0.61	0.34	1.28
8						1.56	1	1.58	1.45	1.56	0.90	0.57	0.26	1.16
8	7	0.43	0.55	1.10	1.54	1.18	1.00	1.06	1.00	1.22	0.72	0.47	0.30	0.88
10	8	0.39	0.56		0.97	0.62	0.49	0.51	0.48	0.65	0.48	0.46	0.34	0.55
10					0.00	0.05	0.00	A 10	A 00	0.00				0.00
11 Noon	1 - 1									1				
Noon	1													1 1
1	1 1							1			ľ			
2	Noon	-U.46	− 0.75	-1.16	-1.74	-1.Z2	-1.24	-1.59	-1.23	-1.39	-1.05	-0.87	-0.59	-1.12
2	1 1	-0.68	-1.00	-1.82	-1.94	-1.49	-1.40	-1.68	-1.58	-1.74	-1.24	-1.02	-0.67	-1-30
3	1 6					1								
4													•	
5	1 1												i	
6	- 1	0.20												
7	5	-0.30												
8	6	-0.20	-0.21	-0.95	-1.70	-1.56	-1.46	-1.96	-1.54	-1.02	-0.26	-0.30	-0.12	-0.94
9 0.10 0.27 0.11 0.17 0.14 0.22 0.19 0.26 0.26 0.32 0.14 0.16 0.20 10 0.08 0.39 0.34 0.48 0.88 0.84 0.76 0.70 0.55 0.51 0.35 0.18 0.46 11 0.14 0.44 0.58 0.97 0.75 0.96 1.12 0.99 0.74 0.71 0.53 0.24 0.68 Midn 0.17 0.45 0.64 1.19 1.03 1.19 1.58 1.28 1.01 0.66 0.63 0.26 0.88 0.84 0.76 0.70 0.55 0.51 0.35 0.18 0.46 0.88 0.84 0.76 0.70 0.55 0.51 0.35 0.24 0.68 0.68 0.10 0.17 0.45 0.64 1.19 1.03 1.19 1.58 1.28 1.01 0.66 0.63 0.26 0.88 0.26 0.29 0.28 0.01 0.06 0.07 0.05 0.27 0.32 0.14 0.07 0.11 0.20 0.26 0.29 0.23 0.01 0.06 0.07 0.04 0.15 0.29 0.35 0.24 0.19 0.21 0.9 0.9 0.19 0.31 0.24 0.03 0.10 0.07 0.05 0.02 0.10 0.23 0.20 0.15 0.14 10.10 0.08 0.18 0.21 0.21 0.05 0.13 0.08 0.07 0.03 0.07 0.10 0.09 0.06 0.28 0.00 0.18 0.21 0.21 0.02 0.16 0.18 0.07 0.05 0.02 0.10 0.23 0.20 0.15 0.14 0.06 0.28 0.06 0.09 0.14 0.03 0.01 0.07 0.05 0.02 0.10 0.23 0.20 0.15 0.14 0.08 0.21 0.05 0.09 0.16 0.18 0.18 0.07 0.05 0.07 0.08 0.07 0.10 0.09 0.06 0.28 0.09 0.14 0.03 0.07 0.05 0.07 0.05 0.00 0.07 0.05 0.00 0.00	7	-0.04	-0.04	-0.52	-1.09	-1.16	-1.12	-1.5 9	-0.75	-0.48	0.02	-0.11	0.08	-0.56
10	8	0.06	0.14	-0.20	-0.86	-0.52	-0.85	-0.58	-0.18	-0.07	0.26	0.02	0.13	-0.14
10														
11	1 1											1		
Midn. . 0.17 0.45 0.64 1.19 1.03 1.19 1.58 1.23 1.01 0.66 0.63 0.26 0.88 6. 6 0.14 0.19 0.15 0.84 0.00 -0.06 -0.19 -0.05 0.27 0.82 0.14 0.07 0.11 7. 7 0.20 0.26 0.29 0.23 0.01 -0.06 -0.27 0.13 0.40 0.37 0.18 0.19 0.16 8. 8 0.23 0.35 0.30 0.31 0.04 0.07 -0.04 0.15 0.29 0.35 0.24 0.01 0.05 0.07 -0.04 0.15 0.29 0.35 0.24 0.19 0.10 0.02 0.15 0.18 0.19 0.15 0.14 0.19 0.15 0.14 0.19 0.15 0.29 0.35 0.24 0.19 0.15 0.11 0.12 0.15 0.11 0.12 0.15 0.14 0.19 0.1	• 1		1											
6. 6	1 1	1 1						1	1					l i
7. 7	Midn	0.17	0.45	0.64	1.19	1.08	1.19	1.58	1.28	1.01	0.66	0.63	0.26	0.88
7. 7													1	
7. 7	8.6	0.14	0.19	0.15	0.84	0.00	-0.06	-0.19	-0.05	0.27	0.82	0.14	0.07	0.11
8. 8 0.23 0.35 0.30 0.31 0.05 0.07 -0.04 0.15 0.29 0.35 0.24 0.19 0.21 9. 9 0.19 0.31 0.24 0.03 0.10 0.07 0.05 0.02 0.10 0.23 0.20 0.15 0.14 10.10 0.08 0.18 0.21 -0.21 -0.05 0.13 0.08 0.07 0.03 0.07 0.10 0.09 0.06 7. 2. 9 -0.06 -0.06 -0.08 -0.13 -0.12 -0.16 -0.19 -0.12 -0.14 -0.07 -0.18 -0.08 -0.12 6. 2. 8 -0.06 -0.09 -0.14 -0.03 -0.21 -0.23 -0.27 -0.12 -0.14 -0.03 -0.11 -0.03 -0.21 -0.23 -0.27 -0.12 -0.14 -0.03 -0.11 -0.02 -0.27 -0.12 -0.14 -0.03 -0.11 -0.02 -0.09 -0.16 0.18 0.18 0.18 0.07 0.06 -0.07 -0.08 -0.07 -0.08 -0.0	1 1						l		ı			1	1	
9. 9			1								l .			1
10.10 0.08 0.18 0.21 -0.21 -0.05 0.18 0.08 0.07 0.03 0.07 0.10 0.09 0.06 7. 2. 9 -0.06 -0.06 -0.08 -0.13 -0.12 -0.16 -0.19 -0.12 -0.14 -0.07 -0.18 -0.06 -0.12 6. 2. 8 -0.06 -0.09 -0.14 -0.03 -0.21 -0.23 -0.27 -0.12 -0.14 -0.03 -0.18 -0.10 -0.18 -0.10 -0.18 -0.10 -0.18 -0.10 -0.18 -0.10 -0.12 -0.12 -0.12 -0.14 -0.03 -0.10 -0.03 -0.21 -0.23 -0.27 -0.12 -0.18 -0.10 -0.00 -0.16 -0.18	1								ı			1	i .	
7. 2. 9 $\begin{array}{cccccccccccccccccccccccccccccccccccc$				1			1						L .	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10/10	0.00	0.10	0.21	J.21	5.05	*****				5.01	3.10		5300
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	7. 2. 9	-0.06	-0.06	-0.08	-0.18	-0.12	-0.16	-0.19	-0.12	-0.14	-0.07	-0.18	-0.08	-0.12
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1 - 1													
6. 2. 6 -0.14 -0.21 -0.39 -0.47 -0.56 -0.60 -0.78 -0.57 -0.45 -0.21 -0.29 -0.18 -0.40 7. 2 -0.14 -0.22 -0.18 -0.25 -0.35 -0.38 -0.31 -0.34 -0.27 -0.34 -0.20 -0.27 8. 2 -0.16 -0.22 -0.33 -0.57 -0.58 -0.61 -0.55 -0.57 -0.63 -0.42 -0.34 -0.23 -0.44 8. 1 -0.12 -0.22 -0.26 -0.49 -0.44 -0.46 -0.56 -0.53 -0.55 -0.41 -0.28 -0.21 -0.28 -0.22 -0.38 7. 1 -0.10 -0.28 -0.11 -0.20 -0.16 -0.20 -0.29 -0.27 -0.26 -0.28 -0.18 -0.21 9.12.3.9 -0.20 -0.29 -0.55 -0.99 -0.69 -0.76 -0.86 -0.73 -0.76 -0.43 -0.41 -0.20 -0.57			ı					0.18	0.18	0.07	0.05	-0.07	-0.08	0.07
7. 2	1 (l .	ı	ı			-0.57	-0.45	-0.21	-0.29	-0.18	-0.40
8. 2		}	ĺ	1	1	ĺ			i	ł		1		
8. 1	1													
7. 1	l													
9.12.3.9	i I													
	7. 1	-0.10	-0.23	-0.11	-0.20	-0.16	 0. 2 0	-0.29	-0.27	-0.26	-0.26	-0.2 8	-0.18	-U.ZI
	9.12.8.9	-0.20	-0.29	-0.55	-0.99	-0.69	-0.76	-0.86	-0.73	-0.76	-0.48	-0.41	-0.20	-0.57
		ll				1				t .	l .	1	1	1
Dail. ext. -0.12 -0.22 -0.18 0.09 0.05 -0.09 0.12 -0.04 -0.11 -0.18 -0.25 -0.18 -0.05	Dail. ext.	-0.12	-0.22	-0.18	0.09	0.05	-0.09	0.12	-0.04	-0.11	_0.18	-0. 2 5	-0.18	-0.09

LXIII.

Scotland. - Makerstoun. Lat. 55° 36' N. Long. 2° 31' W. Gr.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Resumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.67	0.88	1.24	2.80	2.00	2.25	2.10	1.98	1.95	0.88	0.46	0.24	1.41
1	0.76	0.92	1.37	2.52	2.04	2.43	2.44	2.24	2.15	0.88	0.46	0.16	1.53
2	0.78	1.08	1.37	2.70	2.33	2.54	2.57	2.38	2.26	1.06	0.60	0.18	1.65
3	0.76	1.06	1.49	2.79	2.55	2.65	2.79	2.56	2.35	1.57	0.60	0.29	1.79
4	0.67	1.01	1.66	2.96	2.51	2.48	2.70	2.56	2.49	1.20	0.68	0.40	1.77
5	0.78	0.92	1.77	2.88	2.06	1.96	2.21	2.44	2.46	1.40	0.60	0.44	1.60
6	0.60	0.85	1.73	2.25	1.81	1.12	1.35	1.78	2.22	1.81	0.66	0.51	1.8
7	0.51	0.99	1.26	1.48	0.48	0.82	0.46	0.91	1.24	1.26	0.66	0.44	0.88
8	0.53	0.79	0.46	0.86	-0.25	-0.51	-0.39	-0.09	0.00	0.62	0.66	0.40	0.22
9	0.83	0.08	-0.38	-0.79	-0.94	-1.11	-0.96	-1.02	-1.00	-0.16	0.08	0.22	-0.47
10	-0.22	-0.72	-1.12	-1.86	-1.52	-1.68	-1.59	-1.78	-1.92	-0.96	-0.47	-0.20	-1.17
11	-0.84	-1.21	-1.67	-2.55	-2.09	-2.26	-2.14	-2.33	-2.45	-1.63	-0.94	-0.62	-1.7
Noon.	-1.86	-1.61	-2.09	-3.06	-2.84	-2.48	-2.45	-2.73	-2.67	-2.08	-1.84	-0.93	-2.0
1	-1.71	-2.03	-2.27	-3.44	-2.69	-2.75	-2.48	-2.87	-3.03	-2.25	-1.56	-1.13	-2.8
2	-1.67	-2.05	-2.36	-8.57	-2.65	-2.57	-2.52	-2.93	-8.12	-2.20	-1.47	-0.96	-2.8
3	-1.29	-1.68	-2.32	-3.52	-2.65	-2.28	-2.54	-2.73	-2.85	-1.83	-0.96	-0.60	-2.1
4	-0.71	-1.30	-1.80	-8.05	-2.27	-1.95	-2.28	-2.47	-2.29	-1.23	-0.45	-0.16	-1.6
5	-0.13	-0.50	-1.20	-2.30	-1.76	-1.64	-1.81	-1.78	-1.49	-0.49	-0.07	-0.11	-1.1
0	0.18	-0.08	-0.40	-1.89	-0.98	-0.95	-1.34	-1.07	-0.60	-0.09	0.13	0.18	-0.5
7	0.29	0.15	0.08	-0.19	-0.18	-0.40	-0.59	-0.18	0.06	0.17	0.17	0.18	-0.0
8	0.31	0.87	0.46	0.52	0.62	0.86	0.85	0.56	0.46	0.40	0.28	0.18	0.4
9	0.29	0.52	0.78	1.21	1.15	1.00	0.95	1.09	0.95	0.64	0.37	0.24	0.7
10	0.27	0.64	0.95	1.74	1.46	1.56	1.48	1.58	1.33	0.73	0.46	0.81	1.0
11	0.22	0.79	1.06	2.08	1.77	1.94	1.70	1.89	1.51	0.73	0.40	0.36	1.2
Mean.	1.53	0.35	2.06	5.96	6.86	10.25	10.12	10.00	8.51	6.64	4.60	1.16	1

LXIV.

IRBLAND. — DUBLIN. Lat. 53° 23' N. Long. 6° 20' W. Gr. — Dove.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
A.M.1	0.58	0.58	1.56	2.18	2.53	2.76	2.18	2.22	1.64	1.16	0.53	0.36	1.52
8	0.80	0.71	1.64	2.40	2.89	8.11	2.58	2.40	1.87	1.42	0.67	0.49	1.74
5	0.93	0.98	1.64	2.49	2.31	2.18	2.18	2.58	1.87	1.73	0.76	0.58	1.68
7	0.84	0.93	1.38	0.58	-0.22	-0.89	-0.36	0.40	1.07	1.56	0.80	0.53	0.56
9	0.36	0.18	-0.31	-1.11	-1.24	-1.38	-1.10	-1.16	-0.76	-0.09	0.27	0.36	-0.50
11	-0.98	-0.07	-1.82	-2.40	-2 .18	-2.09	-2.04	-2.27	-2.18	-1.91	-0.98	-0.71	-1.71
P.M.1	-1.60	-1.78	-2.67	-2.93	-2.62	-2.40	-2.27	-2.62	-2.67	-2.44	-1.5 6	-1.16	-2.28
8	-1.83	-1.47	-2.44	-2.84	-2.71	-2.81	-2.27	-2.49	-2.22	-2.04	-1.11	-0.67	-1.99
5	-0.44	0.44	-1.29	-1.82	-1.82	-1.87	-1.64	-1.78	-1.29	-0.84	-0.27	-0.18	-1.14
7	0.09	0.18	0.18	0.04	-0.27	-0.44	-0.27	-0.09	0.27	0.04	0.04	0.09	-0.01
9	0.22	0.31	0.76	1.20	1.29	1.24	1.20	1.16	0.98	0.58	0.36	0.18	0.79
11	0.86	0.40	1.07	1.73	1.96	2.04	1.87	1.64	1.42	0.84	0.44	0.22	1.17
Mean.	4.09	4.75	5.10	6.66	9.51	11.86	12.48	12.81	10.79	7.73	5.99	4.88	

LXV.

Russia. — Catharinenburg. Lat. 56° 50' N. Long. 60° 34' E. Greens.

Corrections to be applied to the Means of the Hours of Observation to obtain the true
Mean Temperatures of the respective Days, Months, and of the Year. — Dovs.

						s of Re							
Hours.	Jen.	Feb.	March	April.	May.	June.	July.	Aug.	Sept.	Oct	Nov.	Dec.	Meen.
Morn. 1	0.59	0.91	1.84	1.97	3.09	3.69	3.51	2.49	1.99	0.68	0.47	0.65	1.82
2	0.58	0.89	2.09	2.41	3.52	4.15	3.76	2.93	2.27	0.84	0.42	0.67	2.04
8	0.58	0.87	2.42	2.87	8.80	4.85	3.96	3.42	2.60	1.04	0.86	0.64	2.24
4	0.48	0.89	2.80	3.21	8.82	4.17	4.01	3.78	2.89	1.23	0.85	0.61	2.35
5	0.58	0.95	8.11	8.28	3.45	8.54	3.78	8.79	2.98		0.40	0.63	2.32
6	0.54	1.00		2.88	2.67	2.49	3.18	•	2.74	1.36	ı	0.63	
, ,	0.60	0.94						2.29					
8				1.99	1.57	1.18	2.21	ì	2.11	1.17	0.64	0.81	1.52
°	0.56	0.71	1.90	0.84	0.31	0.17	0.98	0.94	1.16	0.80	0.60	0.80	0.79
9	0.87	0.27	0.65	-0.41	-0.88	-1.85	-0.34	-0.48	0.05	0.28	0.87	0.61	-0.07
10	-0.01	-0.88	-0.75	-1.52	-1.85	-2.23	-1.61	-1.70	-1.08	-0.82	-0.02	0.21	-0.93
11	-0.60	-0.97	-2.08	-2.84	-2.58	-2.79	-2.72	-2.55	-1.98	-0.89	-0.49	-0.84	-1.68
Noon	-0.98	-1.47	-8.00	-2.88	-2.98	-8. 18	-8.64	-8.08	-2.58	-1.84	-0.89	-0.90	-2.23
_													
1			-8.52										
2	1		-3. 62										
8			-3.89								1		
4	−0.84	-1.19	-2.96	-2.6 0	-8.88	-8.46	-4.62	-3.27	-2.98	-1.31	-0.66	-1.10	-2.36
5	-0.84	-0.79	-2.40	-2.18	-2.95	-3.09	-8.90	-2.98	-2.57	-0.96	-0.87	-0.73	-1.94
6	1		-1.77									-0.89	1 7
7			-1.08									-0.14	
8	0.22				-0.42		1	-0.58					
						3.20	0.00	0.0	0.20	0.00	0.22	0.00	J
9	0.80	0.42	0.32	0.42	0.58	0.56	1.28	0.48	0.52	0.26	0.22	0.15	0.45
10	0.37	0.63	0.90	0.91	1.35	1.51	2.22	1.20	1.13	0.40	0.88	0.28	0.95
11	0.36	0.80	1.32	1.29	2.03	2.35	2.84	1.74	1.52	0.48	0.42	0.43	1.30
Midn	0.55	0.89	1.62	1.61	2.59	8.07	3.23	2.12	1.77	0.56	0.48	0.57	1.59
6. 6	0.21	0.27	0.69	0.61	0.19	0.08	0.20	0.45	0.40	0.39	0.21	0.17	0.82
7. 7	0.35	0.42	0.84	0.58		-0.17			0.49		0.33	0.33	0.37
8. 8	0.39	0.44	0.77	1 1	-0.05		0.51	0.20	0.45	0.48	0.36	0.41	0.32
9. 9	0.38	0.34	0.49	0.01				-0.08	0.29	0.45	0.29	0.28	0.19
10.10	0.18	0.15	0.08		-0.25		1		0.05	0.04	0.15	0.25	0.00
10.10	0.10	0.10	0.00	-0.00	-0.20	0.00	0.01	-0.20	0.00	0.04	0.13	0.20	0.00
7. 2. 9	-0.16	-0.14	-0.18	-0.21	-0.44	-0.59	-0.43	-0.21	-0.18	-0.09	-0.09	-0.18	-0.20
6. 2. 8			-0.28										
6. 2.10		-0.05	0.14	0.24					0.24			-0.17	1 11
6. 2. 6	1		-0.75										
1			1 1					1		l i			
7. 2			-0.48										
8.2		1	-0.86		1								1
8. 1	-0.37	-0.52	-0.81	-1.10	-1.47	-1.76	-1.68	-1.16	-0.91	-0.41	-0.26	-0.26	-0.89
7. 1	-0.35	-0.41	-0.8 8	-0.58	-0.84	-1.09	-1.06	-0.48	-0.44	−0.23	-0.24	-0 .2 6	-0.53
9.12.8.9		A 80	1 00		7 80	_, _~	_1 00		_1 00	0.00			ا ا
7. 2.2(9)			-1.36 -0.06								1	-0.39 -0.10	1 1
` '	1		i i					1			1	1	1
Dail.ext.	- v.59	-v.59	-U.Z4	U.10	0.18	0.40	-0.45	0.22	0.17	-0.17	-0.25	-0.85	-0.17

LXVI.

Russia. — Catharinenburg. Lat. 56° 50' N. Long. 60° 34' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Resumur.

Hour.	Jan.	Jeb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.42	1.07	1.70	2.12	2.64	8.06	2.98	2.16	1.96	0.89	0.47	0.47	1.66
1	0.52	1.19	2.00	2.40	8.11	3.51	3.41	2.49	2.31	1.08	0.51	0.50	1.92
2	0.52	1.25	2.23	2.82	3.49	3.90	3.86	2.76	2.58	0.99	0.54	0.52	2.12
8	0.55	1.41	2.53	3.05	8.73	4.15	4-11	8.03	2.83	1.47	0.58	0.54	2.83
4	0.63	1.52	2.75	3.26	8.74	8.92	4.28	3.22	8.06	1.61	0.68	0.58	2.4
5	0.68	1.67	2.85	8.24	3.27	8.85	8.66	8.14	8.22	1.67	0.71	0.61	2.8
6	0.73	1.76	3.06	2.24	2.27	1.99	2.47	2.45	8.04	1.69	0.82	0.64	1.98
7	0.81	1.76	2.59	1.61	0.89	0.61	1.02	1.37	2.27	1.53	0.85	0.65	1.38
8	0.88	1.51	1.46	0.84	-0.24	-0.53	-0.28	0.18	0.85	0.91	0.77	0.58	0.54
9	0.67	0.73	-0.06	-0.81	-1.09	-1.46	-1.45	-0.97	-0.57	-0.03	0.33	0.89	-0.86
10	0.13	-0.45	-1.45	-1.99	-1.94	-2.23	-2.35	-1.72	-1.68	-0.78	-0.22	-0.08	-1.23
11	-0.57	-1.44	-2.39	-2.62	-2.72	-2.93	-3.10	-2.54	-2.50	-1,46	-0.72	-0.71	-1.98
Noon.	-1.04	-2.13	-2.95	-3.09	-8. 19	-3.38	-3.58	-2.99	-8.09	-1.73	-1.03	-1.19	-2.45
1	-1.39	-2.5 8	-3.27	-8.22	-3.28	-3.48	-3.57	-3.04	-8.32	-1.99	-1.25	-1.45	-2.6
2	-1.50	-2.74	-3.38	-3.26	-3.41	-8.59	-3.55	-3.02	-3.36	-2.02	-1.23	-1.89	-2.70
8	-1.28	-2.37	-3.18	-2.86	-3.14	-3.37	-3.40	-3.03	-8.48	-2.23	-1.11	-1.00	-2.54
4	-0.85	-1.97	-2.82	-2.65	-2.99	-8.05	-8.15	-2.83	-3. 18	-1.61	-0.79	-0.61	-2.21
5	-0.50	-1.28	-2.20	-2.14	-2.60	-2.49	-2.67	-2.87	-2.48	-0.95	-0.47	-0.83	-1.71
6	-0.22	-0.74	-1.87	-1.46	-1.98	-1.98	-2.14	-1.66	-1.56	-0.56	-0.26	-0.11	-1.17
7	0.00	-0.25	-0.67	-0.59	-0.95	-1.17	-1.29	-0.79	-0.65	-0.22	-0.07	0.02	-0.5
8	0.10	0.08	-0.12	0.13	-0.04	-0.12	-0.16	0.11	0.07	0.06	0.06	0.11	0.02
9	0.17	0.40	0.44	0.65	0.85	0.96	0.83	0.84	0.67	0.36	0.16	0.26	0.5
10	0.24	0.65	0.94	1.13	1.58	1.88	1.67	1.89	1.25	0.53	0.27	0.39	0.99
11	0.84	0.86	1.84	1.58	2.13	2.51	2.36	1.81	1.65	0.74	0.40	0.56	1.8
Mean.	-10.76	-9.50	-5.83	0.47	6.31	12.08	14.58	10.61	6.32	1.41	-6.11	-11.68	

LXVII.

Russia. — St. Petersburg. Lat. 59° 56' N. Long. 30° 18' E. Gr. — Dove.

Hour.	Jan.	y eb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.14	0.88	0.73	1.44	2.08	1.99	1.77	1.68	1.17	0.52	0.15	0.17	1.02
1	0.21	0.44	0.99	1.68	2.43	2.29	2.05	2.02	1.38	0.60	0.17	0.21	1.21
2	0.25	0.46	1.22	1.91	2.70	2.56	2.24	2.24	1.58	0.65	0.15	0.27	1.85
3	0.30	0.52	1.38	2.11	2.91	2.73	2.48	2.48	1.75	0.73	0.25	0.84	1.49
4	0.88	0.63	1.56	2.24	2.86	2.44	2.82	2.59	1.87	0.78	0.80	0.36	1.58
5	0.43	0.72	1.71	2.28	2.88	1.97	1.92	2.40	1.96	0.84	0.34	0.34	1.44
6	0.45	0.76	1.75	1.95	1.72	1.33	1.83	1.96	1.90	0.90	0.87	0.80	1.23
7	0.41	0.78	1.57	1.32	0.93	0.68	0.64	1.19	1.47	0.82	0.37	0.29	0.87
8	0.42	0.60	1.07	0.65	0.14	-0.04	0.05	0.42	0.81	0.57	0.32	0.25	0.44
9	0.35	0.40	0.40	-0.05	-0.59	-0.69	-0.56	-0.40	0.00	0.20	0.17	0.17	-0.05
10	0.13	-0.05	-0.19	-0.78	-1.30	-1.21	-1.12	-1.07	-0.71	-0.22	0.00	0.04	-0.54
11	-0.20	-0.48	-0.86	-1.42	-1.92	-1.71	-1.58	-1.64	-1.27	-0.61	-0.20	-0.14	-1.00

LXVII.

RUSSIA. - ST. PETERSBURG, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Resumur.

Hour.	Jan.	Job.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Yes
Moon.	-0.38	-0.90	-1.81	-1.98	-2.30	-1.99	-1.89	-2.10	-1.72	-0.94	-0.87	-0.30	-1.4
1	-0.63	-0.97	-1.62	-2.10	-2.41	-2.17	-2.03	-2.47	-2.26	-1.75	-0.64	-0.48	-1.6
2	-0.66	-1.04	-1.88	-2.26	-2.65	-2.82	-2.15	-2.60	-2.84	-1.29	-0.63	-0.58	-1.7
8	-0.53	-0.99	-1.94	-2.49	-2.90	-2.45	-2.29	-2.64	-2.81	-1.06	-0.46	-0.40	-1.7
4	-0.83	-0.83	-1.92	-2.65	-2.92	-2.60	-2.41	-2.80	-2.27	-0.86	-0.20	-0.81	-1.6
5	-0.25	-0.45	-1.58	-2.81	-2.48	-2.28	-2.06	-2.45	-1.76	-0.50	-0.16	-0.22	-1.3
6	-0.19	-0.26	-1.02	-1.48	-1.65	-1.41	-1.80	-1.41	-0.95	-0.25	-0.11	-0.14	-0.8
7	-0.18	-0.16	-0.55	-0.61	-0.74	-0.71	-0.63	-0 62	-0.85	-0.09	-0.05	-0.10	-0.#
8	-0.14	-0.08	-0.25	-0.03	0.06	-0.08	0.02	0.09	0.07	0.07	0.01	0.06	-0.0
9	-0.11	0.08	0.08	0.47	0.79	0.67	0.64	0.65	0.40	0.18	0.08	0.03	0.3
10	-0.03	0.17	0.24	0.84	1.22	1.25	1.18	1.05	0.66	0.33	0.08	0.02	0.5
11	0.06	0.80	0.50	1.17	1.76	1.65	1.45	1.40	0.91	0.45	0.11	0.11	0.8
	-7.41	-6.73	-3.56	1.10	7.01	11.83	18.89	18.58	8.43	8.61	-0.60	-8.75	

LXVIII.

RUSSIA. - HELSINGFORS. Lat. 60° 10' N. Long. 24° 57' E. Gr. - Dove.

Degrees of Resumur. Jan. Feb. March. April. Aug. Nov. Year. Hour. May. June. July. Sept. Oct. Dec. Midn. 0.06 0.47 1.28 1.61 1.61 2.01 1.65 1.36 0.83 0.37 0.18 0.20 0.97 0.13 0.49 0.15 0.21 1.15 1.48 1.87 1.94 2.44 1.90 1.68 1.03 0.452 0.16 0.52 2.07 0.55 0.18 0.18 1.31 1.64 2.21 2.84 2.17 1.98 1.21 3 0.23 0.67 1.84 2.21 2.58 3.04 2.23 1.35 0.65 0.280.15 1.47 2.45 0.28 0.23 1.52 0.35 0.64 1.91 2.87 2.68 2.77 0.624 2.42 2.49 1.48 5 0.38 0.77 1.98 2.34 2.28 2.21 2.05 2.41 1.63 0.67 0.33 0.10 1.43 6 0.88 0.92 2.01 1.74 0.75 0.83 0.03 1.13 1.81 1.81 1.33 1.81 1.63 7 0.41 0.991.78 1.14 0.58 0.51 0.55 1.11 1.28 0.730.360.01 0.79 0.48 0.99 0.35 0.00 0.81 8 1.04 -0.10 0.260.57 0.17 -0.19-0.860.58 0.25 0.06 -0.18 9 0.38 0.55 0.04 -0.73 -0.86 -0.88-0.78 -0.56 -0.09 0.3310 0.08 -0.20-0.89-1.49 -1.39 -1.29-1.23-1.12 -0.65 -0.150.13 0.07 -0.69 11 -0.19 -0.93-1.19 -1.93 -1.76 -1.83 -1.59-1.05-0.47-0.19 -0.82-1.09-1.650.72 -0.59 -0.42-1.25 -2.36-2.26 -1.82 -1.76-1.80-2.02-1.67 -0.90 Noo -0.45 -1.82 -1.08 -0.70 -1.67 1 -1.50-2.62-2.46 -2.12 -2.06 -2.18-2.262 -0.74 -1.60 -2.62 -2.56 -2.19 -2.86 -2.26 -2.81-1.85 -1.10 -0.64-0.42 -1.72 8 -0.49 -1.88 -2.46 -2.87 -2.16 -2.49 -2.18-2.17-1.75-0.95-0.50 -0.22 -1.58 4 -0.90 -2.12 -0.29-0.02:-1.28-0.21 -1.89 -1.82 -2.16 -1.75-1.84-1.52-0.77 5 -1.56 -1.59 -1.49 -1.89 -1.48-1.20 -0.43 -0.170.03 - 1.00-0.12 -0.43 -1.646 -0.04 -1.15 -0.72 -0.09 -0.02 -0.69 -0.21 -0.79-1.09-1.09 -1.58-1.19-0.257 0.03 0.07 -0.29-0.49 -0.86 -0.96-0.68 -0.64-0.27 -0.13 -0.040.01 | -0.35 8 0.00 0.11 -0.020.08 0.20 0.01 -0.86-0.10 -0.140.05 -0.03 0.14-0.16 0.10 0.25 0.44 0.640.44 0.87 0.55 0.28 0.230.05 0.060.13 0.29 10 0.08 0.85 1.04 0.13 0.10 0.18 0.56 0.74 1.04 1.02 0.71 0.480.9411 0.78 0.01 0.42 1.01 1.87 1.34 1.54 1.87 1.06 0.63 0.27 0.180.15

9.23 4.55

1.13 -8.42

Mean. -5-02 -7-43 -8.89 -0.06

LXIX.

RUSSIA. - PETERSBURG. Lat. 59° 56' N. Long. 30° 18' E. Greenw.

corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

						es of Re							
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.20	0.88	0.92	1.52	2.59	2.40	1.98	2.08	1.89	0.72	0.14	0.17	1.21
2	0.23	0.87	1.10	1.75	2.84	2.69	2.26	2.43	1.67	0.77	0.13	0.27	1.88
8	0.22	0.89	1.80	2.01	8.08		2.49	2.79	1.97	1		ı	
4	0.21	0.48	1.49	2.19	8.05		2.57	8.01	2.20	0.88			1.62
												•	
5	0.26	0.50	1.59	2.17	2.79	ı	2.87	2.92	2.25	0.95	0.20	ı	1.58
6	0.87	0.57	1.56	1.88	2.20		1.88	2.46	2.06	0.98	0.23	0.84	1.88
7	0.51	0.56	1.36	1.35	1.27	1.18	1.15	1.70	1.62	0.92	0.23	0.83	1.01
8	0.59	0.46	0.99	0.68	0.41	0.24	0.84	0.79	1.01	0.72	0.16	0.81	0.56
9	0.53	0.23	0.47	-0.02	-0.47	-0.53	-0.40	-0.10	0.81	0.86	0.03	0.27	0.06
10			1 1					-0.86			1		-0.48
11	0.01	-0.48						-1.47			1		-0.86
Noon	-0.84	-0.78	<i>'</i>					-2.01	1				-1.25
1	1						ı	-2.53		1			
2	1							-3.01				1	
' 8	-0.61	-0.86	-1.92	-2.52	-3.25	-2.9 8	-2.5 8	-8.35	-2.81	-1.30	-0.35	-0.48	-1.92
4	-0.45	-0.67	-1.75	-2.50	-3.86	-8.12	-2.6 8	-8.89	-2.65	-1.12	-0.18	-0.44	-1.86
5	-0.27	-0.44	-1.44	-2.10	-3.11	-2.89	-2.46	-8.02	-2.19	-0.88	-0.02	-0.36	-1.61
6								-2.26				-0.26	
7	i i							-1.25				-0.19	1
11 1								-0.20				-0.14	
8	-0.18	0.18	-U.ZU	-0.10	-0.04	-0.51	-U.Z9	-0.20	-0.01	-U.12	0.19	-0.14	-0.18
9	-0.14	0.24	0.14	0.54	0.69	0.61	0.49	0.66	0.53	0.11	0.19	-0.12	0.88
10	-0.09	0.32	0.40	0.96	1.47	1.30	1.07	1.24	0.87			-0.09	0.66
11	0.02	0.37	0.59	1.20	2.00		1.45	1.58	1.05			-0.02	1
11													
Midn	0.12	0.88	0.75	1.35	2.88	2.11	1.78	1.81	1.20	0.63	0.16	0.07	1.05
ii l													
6. 6	0.11	0.18	0.26	0.74	19	-0.14	A A9	0.10	0.28	0.18	0.17	0.04	0.10
11 11													
7. 7	0.20	0.27	0.38	0.25		-0.10		0.23	0.45		0.20	0.07	0.18
8. 8	0.23	0.29	0.40	0.29		-0.04	0.03	0.29	0.50		0.18	0.09	0.22
9. 9	0.20	0.24	0.81	0.26	0.11	0.04	0.04	0.28	0.42	0.24	0.11	0.08	0.19
10.10	0.12	0.12	0.18	0.15	0.16	0.11	0.05	0.19	0.22	0.12	0.01	0.05	0.12
7. 2. 9	-0.10				_0 =0	-0.00	_0 00	-0.22	_0 17		_0 00	0 00	-0.16
11 11													
6. 2. 8			-0.18				-0.24			-0.17			
6. 2.10		-0.02		0.17	0.25	0.22	0.21	0.23		-0.02			
6. 2. 6	-0.15	-0.20	-∪.46	-0.69	-1.05	-U.97	-U.79	-0.94	− 0.70	-∪.5 3	-0.0 5	-0.12	-U.54
7. 2	-0.09	-0.20	-0.27	-0.49	-0.82	-0.75	-0.58	-0.66	-0.58	-0.22	-0.18	-0.06	-0.40
8. 2	-0.05	-0.2 5	-0.45	-0.83	-1.25	-1.19	-0. 9 9	-1.11	-0.83	-0.32	-0.17	-0.07	-0.63
8. 1	0.00	-0.2 8	-0.35	-0.67	-1.05	-0.98	-0.82	-0.87	-0.64	-0.28	-0.19	-0.01	-0.51
7. 1								-0.42					-0.2 8
9.12.3.9	-0.14	-0.28	-0.85	-0.91	-1.99	-1,12	-1.04	-1.20	-0-02	-0.46	_0.16	-0.12	-0.70
7. 2.2(9)	-0.11		-0.06			-0.07		1		-0.06		-0.09	
Dail.ext.	-0.05	-0.19	-0.17	-0.17	-0.16	-0.11	-0.06	-0.19	-0.2 8	-0.19	-0.16	-0.07	-0.15

LXX.

Russia. — Helsingfors. Lat. 60° 10' N. Long. 24° 57' E. Greeno.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Ocs.	Nov.	Dec.	Mon.
Morn. 1	0.47	0.85	1.40	2.10	2.49	3.87	3.16	2.58	1.60	1.06	0.64	0.34	1.67
2	0.79	1.25	1.86	3.18	2.82	3.78	8.48	2.96	2.09	1.45	0.99	0.68	2.11
8	0.99	1.55	2.28	2.79	2.89	8.74	8.45	8.11	2.48	1.70	1.22	0.91	2.26
4	1.18	1.71	2.52	2.77	2.62	8.22	3.02	2.92	2.61	1.74	1.26	0.97	2.21
5	1.06	1.66	2.49	2.41	2.06	2.32	2.25	2.89	2.40	1.51	1.09	0.84	1.87
6	0.86	1.48	2.16	1.76	1.80	1.24	1.23	1.59	1.84	1.10	0.76	0.59	1.32
7	0.58	1.07	1.57	0.92	0.49	0.20	0.17	0.64	1.06	0.59	0.38	0.31	0.67
8	0.28	0.60	0.79	0.05	−0.2 6	-0.65	-0.78	-0.28	0.21	0.08	0.02	0.07	0.01
9	0.01	0.10	-0.05	-0.74	-0.87	-1.26	-1.51	-1.07	-0.58	-0.38	-0.27	-0.10	-0.56
10	-0.25	-0.42	-0.87	-1.85	-1.84	-1.65	-2.02	-1.68	-1.23	-0.77	-0.48	−0.22	-1.02
11	-0.48	-0.91	-1.56	-1.80	-1.70	-1.93	-2.85	-2.12	-1.71	-1.07	-0.64	-0.32	-1.38
Noon	-0.70	-1.29	-2.06	-2.10	-1.98	-2.16	-2.54	-2.48	-2.04	-1.3 0	-0.76	-0.48	-1.65
1	-0.86	-1.54	-2.86	-2.80	-2.19	-2.36	-2.65	-2.61	-2.28	-1.42	-0.85	-0.54	-1.83
2	1				1		į:						-1.89
8	-0.84	-1.47	-2.82	-2.81	-2.81	-2.55	-2.55	-2.55	-2.20	-1.80	-0.82	-0.60	-1.82
4	-0.78	-1.20	-2.01	-2. 10	-2 .11	-2.42	-2.27	-2.26	-1.92	-1.05	-0. 6 8	-0.49	-1.60
5	-0.52	-0.87	-1.56	-1.78	-1.77	-2.13	-1.85	-1.80	-1.48	-0.74	-0.48	-0.33	-1.27
6	1	-0.57						-1.24					
7	-0.19	-0.38	-0.60					-0.62					11
8	-0.15	-0.25	-0.2 0	-0.21	-0.24	-0.61	-0.04	-0.08	-0.00	-0.10	-0.12	-0.12	-0.17
9	-0.16	-0.18	0.10	0.26	0.29	0.07	0.61	0.52	0.31	-0.03	-0.12	-0.20	0.12
10	-0.16	-0.08	0.36	0.69	0.82	0.87	1.27	1.03	0.54	0.08	-0.10	-0.25	0.42
11	-0.06	0.12	0.63	1.13	1.40	1.75	1.95	1.54	0.79	0.29	0.02	-0.19	0.78
Midn	0.16	0.44	0.96	1.60	1.97	2.63	2.61	2.08	1.14	0.63	0.28	0.02	1.21
6. 6	0.27	0.48	0.55	0.26	-0.00	-0.24	-0.04	0.18	0.45	0.83	0.24	0.21	0.22
7. 7	0.20	0.85	0.49	0.10	-0.15		-0.26		0.32	0.19	0.11	0.10	0.08
8. 8	0.07	0.18	0.80	-0.08	-0.25	-0.63	-0.41	-0.16	0.11	-0.01	-0.05	-0.08	-0.06
9. 9	-0.08	-0.04	0.03	-0.24	-0.29	-0.60	-0.45	-0.28	-0.14	-0.21	-0.20	-0.15	-0.22
10.10	-0.21	-0.25	-0.2 6	-0.33	-0.26	-0.39	-0.38	-0.88	-0.85	-0.85	-0.29	-0.24	-0.30
7. 2. 9	-0.17	-0.24	-0.26	-0.40	-0.51	-0.75	-0.68	-0.50	-0.31	-0.29	-0.21	-0.17	-0.87
6. 2. 8	-0.07	-0.14	-0.16	-0.27	-0.42	-0.63	-0.49	-0.37	-0.15	-0.14	-0.08	-0.05	-0.25
6. 2.10	-0.07	-0.08	0.02	0.08	-0.07	-0.18	-0.05	-0.01	0.03	-0.08	-0.07	-0.09	-0.05
6. 2. 6	-0.18	-0.25	-0.45	-0.62	-0.77	-0.99	-0.91	-0.77	-0.47	-0.26	-0.18	-0.07	-0.49
7. 2	-0.17	-0.27	-0.44	-0.78	-0.92	-1.16	-1.25	-1.01	-0.62	-0.42	-0.25	-0.15	-0.62
8. 2	-0.82	-0.50						-1.47					
8. 1	-0.29	-0.47	-0.79	-1.18	-1.23	-1.51	-1.72	-1.45	-1.01	-0.67	-0.42	-0.24	-0.91
7. 1	-0.14	-0.24	-0.40	-0.69				-0.99					
9.12.3.9	-0.42	-0.71	-1.08	-1.22	-1.22	-1.48	-1.KO	-1.38	-1.13	-0.75	-0.49	-0.83	-0.98
7. 2.2(9)	1	-0.22						-0.25					
Dail.ext.	0.11	0.06	0.04	0.41	0.29	0.62	0.41	0.23	0.16	0.16	0.19	0.18	0.19

LXXI.

Norway. — Christiania. Lat. 59° 55′ N. Long. 10° 43′ E. Greenw. orrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	s of Re	eumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.16	0.89	1.07	1.56	2.55	2.58	2.21	2.04	1.64	0.74	0.52	0.22	1.85
2	0.21	0.94	1.30	1.88	2.85	8.15	2.53	2.28	1.88	0.82	0.50	0.21	1.54
3	0.27	1.17	1.51	2.03	8.23	8.28	2.64	2.41	2.08	0.94	0.49	0.28	1.69
4	0.32	1.49	1.67	2.12	8.21	3.05	2.62	2.60	2.07	1.06	0.55	0.30	1.84
_													
5	0.38	1.60	1.82	2.23	2.55	2.39	2.09	2.44	2.14	1.16	0.51	0.22	1.68
6 7	0.47 0.51	1.54	1.69	1.81	1.63 0.71	0.48	1.87 0.58	1.98	2.10	1.16		0.11	1.81
8	0.51	1.67	1.71 1.29	0.56	0.71	-0.32	-0.22	1.00	1.50	1.18		0.19	0.93
•	0.04	1.42	1.29	0.50	0.07	-0.52	-0.22	0.10	0.62	0.75	0.38	0.15	0.44
9	0.48	1.11	0.36	-0.06	-0.52	-0.86	-0.78	-0.59	0.01	0.15	0.17	0.16	-0.03
10	0.24				1			-1.23	1				-0.59
11	-0.17				-1.66					-1.00			
Noon	-0.67	-1.82			-2.17			1 -	-2.02		-1.06		
1							•						
1	-0.87	-1.90	-1.74	-2.22	-2.46			-2.35	-2.4 1	-1.59	-1.15	-0.42	-1.82
2	-1.04		-1.95		1		-2.2 0			-1.67			-1.90
3	-0.91				-2.54					-1.58			
4	-0.62	-2.00	-1.99	-2.11	-2.53	-2.29	-2.00	-2.82	-2.35	-1.88	-0.55	-0.12	-1.68
_										0.00			
5	-0.85							-1.97					-1.86
6		i i			-1.82				-1.21			-0.03	1
7	-0.01	-0.60		-0.70	1		-0.89		-0.57	-0.24		-0.10	-0.58
8	0.12	-0.32	-0.20	-0.14	-0.44	-0.81	_0.30	-0.10	0.02	0.18	0.28	-0.13	-0.12
9	0.16	0.09	0.09	0.36	0.24	0.44	0.45	0.55	0.36	0.36	0.27	-0.05	0.28
10	0.27	0.84	0.36	0.70	0.93	1.20	1.06	1.08	0.81	0.58	0.33	-0.04	0.63
11	0.31	0.52	0.58	0.99	1.46	1.76	1.63	1.41	1.06	0.75	0.43	0.10	0.91
Midn	0.83	0.86	0.77	1.20	1.90	2.31	2.00	1.75	1.38	0.95	0.48	0.09	1.17
								1					
1													
6.6	0.18	0.22	0.80		-0.10				0.45	0.32	0.29	0.04	0.16
7.7	0.25	0.54	0.53	1	-0.82				0.47	0.45	0.29	0.05	0.18
8.8	0.33	0.55	0.55		-0.19			0.00	0.32	0.47	0.31	0.01	0.16
9. 9	0.82	0.60	0.28	0.15		-0.21	-0.17	-0.02	0.19	0.26	0.22	0.06	0.12
10.10	0.26	0.31	0.01	0.05	-0.13	-0.18	-0.10	-0.08	0.02	0.05	0.05	0.04	0.02
7. 2. 9	-0.12	-0.15	_0 0K	_0.98	-0.50	-0 K1	_0.80	_0 89	_∩ 38	-0.06	_0 14	_0 07	-0.23
6. 2. 8		-0.33	-0.15					-0.21		-0.11			-0.28
6. 2.10	-0.10		0.03	0.06	0.08	0.04	0.08	0.19	0.12		-0.07		0.02
6. 2. 6	-0.23	-0.59		-0.59		-0.67						-0.11	-0.49
	1.25	03									7.13		J. 20
7. 2	-0.27	-0.28	-0.12	-0.52	-0.8 8	-0.99	-0.81	-0.75	-0.52	-0.27	-0.35	-0.08	-0.49
8. 2	-0.25	-0.40	-0.88	-0.88	-1.20	-1.04	-0.99	-1.20	-0.96	-0.46	-0.39	-0.10	-0.68
8. 1	-0.17	-0.24	-0.23	-0.83	-1.20	-1.09	-1.00	-1.13	-0.90	-0.42	-0.39	-0.14	-0.64
7. 1	-0.18	-0.12	-0.02	-0.47	-0.88	-1.04	-0.82	-0.68	-0.46	-0.23	-0.85	-0.12	-0.50
			0.00		ا ـ ـ ـ ا					ا ا			
9.12.3.9	-0.56	1			1			-1.16					
7. 2.2(9)	-0.05	-0.09	U.U2	-v.08	-v.32	- ∪.27	-U.18	-0.10	-v.08	0.05	-0.04	-0.07	-0.11
Dail.ext.	-0.25	-0 27	_0.17	_0.05	0.85	0.20	0.22	0.06	_0 20	_0 96	0 9£	_0.04	_0.0x
Dail. ext.	70.20	V.01	0.17	0.00	0.00	U.45	V.66	0.00	0.20	V.20	V-20	0.00	V-00

LXXII.

NORWAY. - DRONTHEIM. Lat. 63° 26' N. Long. 10° 25' E. Greenie.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Deft.	205	œ	Kesum	ur.		

1												I	
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.29	0.41	0.77	1.94	2.63	2.64	2.58	2.51	1.37	0.89	0.27	0.33	1.38
2	0.25	0.50	0.95	2.09	2.97	2.76	2.75	2.68	1.48	0.91	0.31	0.31	1.50
8	0.22	0.64	1.11	2.19	8.13	2.82	2.77	2.91	1.59	0.97	0.23	0.42	1.58
4	0.20	0.71	1.27	2.32	3.08	2.82	2.65	2.77	1.55	1.07	0.28	0.34	1.58
5	0.18	0.75	1.87	2.05	2.76	2.52	2.85	2.58	1.59	0.86	0.30	0.42	1.47
6	0.11	0.82	1.42	1.67	2.80	1.96	1.86	2.13	1.49	0.71	0.14	0.43	1.25
7	0.04	0.58	1.85	1.86	1.68	1.39	1.17	1.58	1.07	0.42	0.00	ŀ	0.92
8	0.08	0.28	1.17	0.94	0.88	0.61	0.40	1.02	0.57	0.06		0.36	0.52
							30.20			.5155	0		
9	0.00	-0.08	0.41	-0.02	-0.2 8	-0.03	-0.14	0.22	-0.07	-0.29	-0.14	0.19	−0.02
10	-0.09	1	-0.18	-0.85				-1.22	-0.89	-0.59	-0.16	0.02	-0.65
11	-0.16	-0.78		-1.90		-2. 01		I				−0.12	
Noon	-0.5 9	-1.06	-1.85	-2.57	-2. 81	-2.43	-2.77	-8.21	-2.05	-1.20	-0.38	-0.42	-1.75
1	-0.80	-1.22	-1.70	-2.66	-8.28	-3.25	-8.20	-3.39	-2.12	-1.14	-0.44	-0.42	-1.97
2	1	ı	-1.70		1								
8			-1.54									1	
4			-1.87									-0.29	
ا ۽	-0.00			_1 00		_0 45				A 50	0.00		ا ـ ـ ـ ا
5			-1.07			-2.45 -1.84		1				-0.22	1
6 7	-0.17		-0.75 -0.54							-0.51		-0.23	-0.78
8	0.09		-0.27					-0.68 0.11		-0.28 -0.02		-0. 3 0 -0.19	
			"	0.20	0.0.		0.01	""	0.00	0.02	0.2.	0.15	0.02
9	0.45	0.87	0.00	0.16	0.50		0.66	0.51			0.05	-0.11	0.30
10	0.52	0.53	0.23	0.61	1.10		1.17	1.18	0.75			-0.06	1 12
11	0.47	0.50	0.43	0.90	1.61	1.63	1.48	1.67	1.02		0.11	1	I il
Midn	0.45	0.49	0.63	1.27	1.92	2.07	1.88	2.13	1.28	1.14	0.19	0.02	1.12
												1	
6.6	-0.03	0.86	0.84	0.89	0.80	0.06	0.86	0.48	0.35	0.10	0.11	0.10	0.24
7. 7	0.07	0.27	0.41	0.40	0.83	0.20	0.28	0.45	0.88			ı	0.24
8.8	0.18	0.20	0.45	0.87	0.23	0.33	0.21	0.57	0.80		0.08	í	0.25
9. 9	0.23	0.15	0.21	0.07	0.11	0.19	0.26	0.87	0.18	-0.04	-0.05	0.04	0.14
19.10	0.22	0.08	0.05	-0.12	−0.10	0.08	-0.07	-0.02	-0.07	-0.02	-0.02	-0.02	0.00
7. 2. 9	-0.06	-0.07	-0.12	-0.81	0.8e	-0.51	-0.41	_0.42	-0.98	-0.15	_0.19	_0.07	-0.24
6. 2. 8	-0.10		-0.18					1		1		1	
6. 2.10	-0.02	0.07	1	-0.06		-0.09		-0.02	ı	i .		-0.03	
6. 2. 6	-0.25	1	-0.39					l		ı	1	(
								1		ŀ		1	
7. 2	-0.32	1	-0.18			1			1		•	-0.06	
8. 2	-0.80		l .					1					-0.63
8. 1	-0.36					1		•	1			1	-0.78
7. 1	-0.3 8	-0.32	-0.18	-0.6 5	-0.80	-0.93	-1.02	-0.91	-0.58	-0.86	-0.22	-0.03	-0.53
9.12.3.9	-0.16	-0.40	-0.62	-1.16	-1.46	-1.28	-1.83	-1.42	-0.89	-0.59	-0.19	-0.18	-0.87
7. 2.2(9)	0.07	1							1		l		-0.11
Dail. ext.	-0.14	-0.20	-0.14	-0.17	-0.08	-0. 2 5	-0.22	-0.24	-0.3 5	-0.07	-0.07	-0.02	-0.16

LXXIII.

STEALT OF KARA. Lat. 70° 37' N. Long. 57° 47' E. Greenw.

Descriptions to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove. Degrees of Resumur.

Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct	Nov.	Dec.	Mean.
Morn. 1	0.27	0.38	1.66	2.58	2.26	1.86	1.87	0.62	0.83	0.00	0.08	0.55	0.99
2	0.24	0.88	1.78	2.67	2.22	1.68	1.24	0.58	0.40	t .	1		
					•		I			0.02	0.14	0.42	0.98
8	0.22	0.40	1.86	2.66	2.06	1.41	1.08	0.53	0.49	0.02	0.14	0.26	0.92
4	0.28	0.42	1.88	2.44	1.82	1.12	0.79	0.47	0.58	0.06	0.15	0.11	0.84
, 5	0.25	0.42	1.80	1.98	1.48	0.82	0.54	0.38	0.61	0.17	0.22	-0.00	0.72
6	0.27	0.33	1.55	1.80	1.01	0.49	0.25	0.26	0.58	0.29	0.36	-0.15	0.55
7	0.29	0.16	1.10	0.52	0.40	0.10	ı	0.10	0.42	0.35	0.52		0.30
8	0.20		l l				i					1	
	0.30	0.08	0.42	-0.27	-0.30	-0.83	-0.35	-0.07	0.27	0.82	0.64	-0.42	0.01
9	0.26	0.80	-0.48	-0.98	-1.01	-0.78	-0.66	-0.28	0.01	0.18	0.66	-0.54	-0.32
10	0.18	-0.50	-1.32	-1.58	-1.63	-1.19	-0.85	-0.36	-0.28	0.02	0.55	-0.61	-0.68
11	0.04	-0.64	-2.07	-2.18	-2.06	-1.48	-0.98	-0.46	-0.54	-0.25	0.88	-0.62	-0.91
Noon	-0.12	-0.70		-2.41	i 1	-1.62			-0.72	-0.37		-0.54	1 1
NOOL	0.22	0		2.42		2.02	2.01	0.00	02	0.5.	0.10	0.04	1.01
1	-0.81	-0.70	-2.70	-2.67	-2.26	-1.62	-1.08	-0.63	-0.81	-0.43	-0.18	-0.44	-1.14
2	-0.49	-0.64	-2.52	-2.81	-2.11	-1.54	-1.00	-0.71	-0.78	-0.36	-0.25	-0.31	-1.18
	-0.60	-0.58	-2. 10	-2.75	-1.88	-1.40	-0.95	-0.76	-0.66	-0.23	-0.30	-0.21	-1.08
4		-0.38						-0.69				-0.11	
5	-0.58	-0.21	-0.98	-1.91	-1.30	-1.05	-0.78	-0.59	-0.30	0.02	-0.35	-0.04	-0.67
6	-0.46	-0.02	-0.47	-1.18	-0.90	-0.76	-0.59	-0.88	-0.13	0.07	-0.41	0.06	-0.48
7	-0.26	0.14	-0.04	-0.37	-0.40	-0.85	-0.29	-0.09	0.06	0.08	-0.48	0.18	-0.15
8	-0.06	0.82	0.34	0.42	0.20	0.18	0.11	0.22	0.11	0.07	-0.52	0.38	0.14
	0.00	0.00	5351		3.23		0.20			0.00		0.00	
9	0.11	0.42	0.67	1.08	0.83	0.78	0.54	0.46	0.17	0.06	-0.49	0.48	0.48
10	0.22	0.46	0.98	1.59	1.42	1.81	0.94	0.62	0.20		-0.38	0.61	0.67
11	0.28	0.44	1.25	1.98	1.88	1.71	1.23	0.68	0.28		-0.20	0.66	0.85
14 1													1
Midn	0.29	0.40	1.48	2.29	2.16	1.90	1.38	0.66	0.27	0.01	-0.03	0.64	0.95
													i i
6.6	0.10	0.16	0.54	0.06	0.00	-0.14	-0.17	-0.06	0.28	0.18	_0.00	-0.05	0.06
11 1	1											1	
7. 7	0.02	0.15	0.58		-0.00			0.01	0.24	0.22		-0.06	0.08
8.8	0.12	0.12	0.38		-0.05			0.08	0.19	0.20		-0.05	0.08
9.9	0.19	0.06	0.12	0.05	-0.09	-0.00	i	0.12	0.09	0.12	0.09	-0.03	0.05
10.10	0.20	-0.02	-0.17	0.01	-0.11	0.06	0.05	0.18	-0.04	0.04	0.09	-0.00	0.02
7. 2. 9	-0.03	-0.02	-0.25	-0.40	-0.29	-0.22	-0.17	-0.05	-0.06	0.02	-0.07	-0.04	-0.18
6. 2. 8	-0.09	-0.00	-0.21	-0.36	-0.30	-0.29	-0.21	-0.08	-0.03	-0.00	-0.14	-0.04	-0.15
6. 2.10	-0.00	0.05	-0.00	0.03	0.11	0.09	0.06	0.06	-0.00	-0.00	-0.09	0.05	0.08
6. 2. 6	-0.23		-0.48					-0.28		-0.00		1	0.84
0. 2. 0	-0.23	-0.11	70.46	0.50	0.07	0.00	0.40	0.20	0.11	0.00	-0.10	-0.13	0.04
7. 2	-0.10	-0.24	-0.71	-1.15	-0.86	-0.72	-0.53	-0.81	-0.18	-0.01	0.14	-0.30	-0.41
8. 2	-0.10	-0.36	-1.05	-1.54	-1.21	-0.94	-0.68	-0.39	-0.26	-0.02	0.20	-0.87	-0.56
8. 1	-0.01	-0.39	-1.14	-1.47	-1.28	-0.98	-0.69	-0.35	-0.27	-0.06	0.26	-0.43	-0.57
7. 1	-0.01	-0.27	•	-1.08		-0.76			-0.20	-0.04	0.20	-0.87	-0.42
0.10.00	0.00	0.00			1.00	0.80		0~	_0 00	0.00	-0.01	00	
9.12.3.9	-0.09			-1.27		-0.76	l	-0.27	-0.80	-0.09	-0.01	-0.20	0.50
7. 2.2(9)	0.01	0.09	-0.02	-0.03	-0.01	0.08	0.01	0.08	-0. 01	0.08	-0.18	0.09	0.01
Dail. ext.	-0.17	-0.12	-0.41	-0.07	-0.01	0.14	0.17	-0.04	-0.10	-0.04	0.07	0.02	-0.08

LXXIV.

NOVAIA ZENLIA. - MATOSCHKIN SCHAR. Lat. 73° - N. Long. 57° 20' E. Gr.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

				_	Degree	s of Re	eamer.						
Hours.	Jan.	Peb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct	Nov.	Dec.	Moss.
													<u> </u>
Morn. 1	-0.22	0.16	0.46	1.68	2.42	1.70	1.18	0.78	1.08	-0.49	-0.14	-0.11	0.70
1 2	-0.80	0.09	0.70	1.34	2.28	1.54	1.20	0.79	0.88	-0.47	-0.14	0.05	0.66
3	-0.81	0.01	0.91	1.15	1.89	1.26	1.11	0.80	0.62	-0.22	-0.10	0.17	0.61
4	-0.26	-0.06	1.02	1.09	1.41	0.93	0.94	0.72	0.46	0.02	-0.00	0.26	0.54
1													
5	1	-0.09	0.99	0.81		0.61	0.78	0.55		0.20	0.10	0.34	0.45
6		-0.09	1	0.68		0.80	0.47	0.80		0.26	0.20	0.41	0.34
7		-0.07	0.62	0.09		-0.02	0.18	0.01	0.58	0.18	0.26	0.45	0.16
8	0.10	-0.05	0.34	-0.50	-1.08	-0.3 8	-0.13	-0.80	0.38	0.06	0.26	0.46	-0.07
						A ==0	0.40	A #0		0.00	0.04	0.40	
9		-0.05		-1.14							0.24		-0.33
10			-0.28										-0.61
11		1	-0.58								0.15		-0.79
Noon	0.05	-0.13	-0.78	-2.09	-2.67	-1.58	-1.08	-0.93	-1.46	-0.12	0.11	0.18	-0.8 8
1 1	0.06		-0.93	_,	_9 89	_1 59	_1 06	_0 85	-1.32	_0.10	0.08	0.10	-0.85 [!]
2			-0.96									-0.02	1.
2												-0.11	
11 - 1													
4	0.10	-0.07	-0.71	-0.50	-1.50	-V.70	-0.00	-0.8Z	70.07	-U.UZ	-0.10	-0.20	-0.41
5	0.10	-0.03	-0.50	-0.54	-0.72	-0.57	-0.54	-0.14	-0.02	0.10	-0.18	-0.26	-0.28
8	0.10		-0.30	-0.26		-0.38			-0.17			-0.36	
7	0.10		-0.16	0.30		-0.16			-0.35			-0.43	
8	0.12		-0.09	0.70			-0.11		-0.86			-0.48	0.13
°	V.12	0.20	0.05	0.70	1.04	0.10	0.11	0.21	0.00	0.40	V.24	0.10	0.10
9	0.12	0.15	0.06	1.24	1.59	0.56	0.14	0.80	-0.12	0.36	-0.10	-0.49	0.31
10	0.08	ı	-0.02	1.50		1.02	0.46	0.89			-0.08		0.47 :
11	-0.00	0.21	0.09	1.75	2.40	1.42	0.78	0.50			-0.08		0.61
Midn	-0.11	0.20		1.72	2.55	1.66	1.03	0.62			-0.11		0.69
	1												1
ll												ľ	li li
6.6	0.04	0.04	0.28	0.19	0.06	−0.04	0.02	0.15	0.20	0.26	0.00	0.03	0.10
7. 7	0.08	0.01	0.28	0.20	0.04	-0.09	-0.06	0.07	0.12	0.29	0.04	0.01	0.08
8.8	0.11	0.03	0.13	0.10	0.01	-0.12	-0.12	-0.05	0.01	0.26	0.06	-0.01	0.03
9. 9	0.11	0.05	-0.02	0.05	-0.03	-0.11	-0.16	-0.14	-0.06	0.15	0.07	-0.03	-0. 01 ,
10.10	0.08	0.07	-0.15	-0.14	-0.06	-0.07	-0.15	-0.20	-0.19	-0.01	0.05	-0.04	-0.07
1												ı	
7. 2. 9	0.09		-0.18								0.06		-0.09
6. 2. 8	0.06	ı	-0.06	-0.10						0.21	0.03		-0.09
6. 2.10	0.05	ı	-0.04	0.17				-0.00		0.12	0.05	-0.02	0.08
6. 2. 6	0.05	-0.07	-0.18	-0.42	-0.72	-0.47	-0.81	-0.13	-0.17	0.14	0.01	0.01	-0.18
1					١			امما			Ace.		
7. 2	ll .		-0.17							0.05	0.14	0.22	-0.29
8. 2		1	-0.31						1		0.14		-0.40
8. 1	0.08	1	-0.30					1 1		-0.02	0.17	0.28	-0.46
7. 1	0.06	-0.11	-0.16	-0.92	-1.48	-0.77	-0.44	-0.42	-0.37	0.04	0.17	0.28	-0.84
9.12.3.9	0.09		-0.43		_, ,,	_0 71	_0 55	امه مـا	-0.50	0.03	0.05	-0.00	-0.37
							l .						0.01
7. 2.2(9)	0.10	0.02	-0.12	0.24	0.18	-0.00	-0.18	-0.02	-0.14	0.20	0.02	-0.14	9.01
Dail.ext.	-0.10	0.04	0.03	-0.17	-0.0e	0.08	0.08	-0.07	-0.19	-0.02	0.08	-0.02	ا ممـ
L aut. CA.	J			J.17	0.00	0.00	5.00	0.07	-0.10	0.05	0.00	0.02	

LXXV.

NORWAY. - BOSSEKOP. Lat. 69° 58' N. Long. 22° E. Greenw.

corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

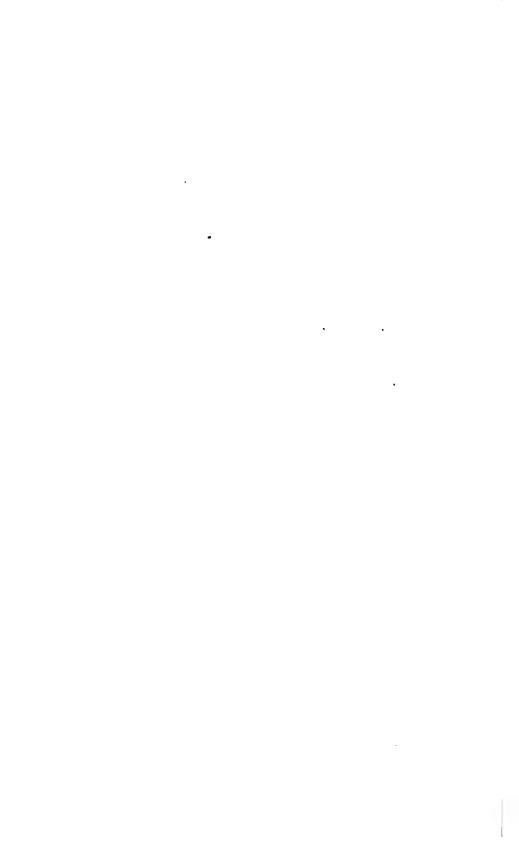
Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	Sept.	Oct.	Nov.	Dec.	80 Days without Sun.
A.M. 2	-0.26	0.86	1.87		1.20	0.66	0.04	0.85	0.04
4	-0.11	0.80	1.78		1.01	0.53	-0.03	0.42	0.10
6	0.00	0.50	1.90		1.22	0.73	0.04	0.28	0.08
8	0.09	0.26	1.18	0.36	0.62	0.41	0.07	0.10	0.02
10	-0.18	-0.19	-1.09	-0.85	-1.01	-0.29	-0.15	-0.14	-0.19
Noon.	0.18	-0.79	-2.89	-1.29	-1.66	-1.05	-0.18	-0.09	-0.08
2	0.20	-1.02	-2.85	-1.22	-1.69	-1.02	-0.09	-0.34	-0.10
4	0.80	-0.11	-2.38	-0.82	-1.54	-0.50	0.09	-0.38	0.06
6	0.18	0.06	-0.57	-0.10	-0.27	-0.17	0.18	-0.23	0.09
8	0.12	0.16	0.46	0.70	0.39	0.09	0.14	-0.26	0.02
10	-0.34	0.21	1.19	1.44	0.79	0.13	-0.03	0.14	-0.10
12	-0.27	0.22	1.39	1.88	0.89	0.49	-0.18	0.17	-0.10
Mean.	-7.67	-6.39	-7.55	-0.77	5.91	-1.62	-6.55	-5.66	-7.66

LXXV'.

NORWAY. — BOSSEKOF. Lat. 69° 58' N. Long. 22° E. Greenw. Contigrade Degrees.

Hour.	Jan.	Feb.	March.	April.	Sept.	Oct.	Nov.	Dec.	80 Days without Sun.
A.M. 2	-0.32	0.45	1.71		1.50	0.82	0.05	0.44	0.05
4	-0.14	0.37	2.22		1.26	0.66	-0.04	0.52	0.12
6	0.00	0.62	2.37		1.52	0.91	0.05	0.35	0.10
8	0.11	0.82	1.47	0.45	0.77	0.51	0.09	0.12	0.02
10	-0.16	-0.24	-1.36	-1.06	-1.26	0.86	-0.19	-0.17	-0.24
Noon.	0.22	-0.99	-2.98	-1.62	-2.07	-1.31	-0.16	-0.11	-0.04
2	0.25	-1.27	-3.56	-1.52	-2.11	-1.27	-0.11	-0.42	-0.12
4	0.87	-0.14	-2.97	-1.02	-1.92	-0.62	0.11	-0.47	0.07
6	0.22	0.07	-0.71	-0.12	-0.84	-0.21	0.22	-0.29	0.11
8	0.15	0.20	0.57	0.87	0.49	0.11	0.17	-0.32	0.02
10	-0.42	0.26	1.48	1.80	0.99	0.16	-0.04	0.17	-0.12
12	-0.84	0.27	1.78	2.29	1.11	0.61	-0.16	0.21	-0.12
						<u></u>	<u> </u>		
Mean.	-9.59	-7.99	-9.44	-0.96	7.89	-2.02	-8.19	-7.07	-9.57



HOURLY CORRECTIONS

FOR

PERIODIC VARIATIONS.

AFRICA. - AUSTRALIA.



LXXVI.

AFRICA. - St. Helena. Lat. 15° 55' S. Long. 5° 43' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.76	0.70	0.63	0.58	0.52	0.48	0.48	0.48	0.52	0.62	0.71	0.73	0.59
1	0.85	0.76	0.71	0.66	0.61	0.48	0.53	0.48	0.56	0.71	0.78	0.81	0.6
2	0.93	0.84	0.77	0.70	0.66	0.54	0.56	0.53	0.62	0.78	0.86	0.90	0.72
8	1.03	0.92	0.86	0.76	0.73	0.59	0.62	0.63	0.69	0.86	0.95	0.98	0.8
4	1.06	1.00	0.92	0.81	0.80	0.65	0.66	0.66	0.76	0.91	0.99	1.02	0.8
5	1.11	1.04	0.98	0.86	0.83	0.67	0.69	0.73	0.79	0.94	1.02	1.08	0.8
6	1.15	1.07	0.98	0.98	0.83	0.68	0.72	0.74	0.83	0.99	1.07	1.09	0.9
7	1.16	1.08	0.97	0.94	0.89	0.71	0.75	0.79	0.81	0.96	1.08	1.06	0.9
8	0.95	0.99	0.78	0.85	0.88	0.69	0.72	0.72	0.72	0.77	0.80	0.98	0.8
9	0.53	0.63	0.52	0.49	0.46	0.42	0.41	0.43	0.42	0.38	0.40	0.48	0.4
10	-0.05	0.06	-0.07	-0.04	-0.08	-0.04	-0.04	-0.02	-0. 05	-0.17	-0.16	-0.09	-0.0
11	-0.62	-0.55	-0.49	-0.51	-0.47	-0.4 0	-0.40	-0.40	-0.55	-0.66	-0.67	-0.56	-0.5
Noon.	-1.14	-1.06	-0.95	-1.00	-0.96	-0.73	-0.76	-0.80	-0.92	-1.11	-1.12	-1.08	-0.9
1	-1.64	-1.46	-1.28	-1.81	-1.20	-1.04	-1.06	-1.12	-1.25	-1.45	-1.60	-1.52	-1.8
2	-1.81	-1.67	-1.48	-1.46	-1.82	-1.20	-1.26	-1.25	-1.42	-1.67	-1.80	-1.80	-1.5
8	-1.76	-1.78	-1.62	-1.50	-1.35	-1.18	-1.24	-1.81	-1.88	-1.64	-1.84	-1.82	-1.5
4	-1.69	-1.66	-1.54	-1.35	-1.24	-1.03	-1 .12	-1.13	-1.20	-1.87	-1.64	-1.76	-1.8
5	-1.48	-1.88	-1.27	-1.06	-0.91	-0.78	-0.84	-0.86	-0.91	-0.99	-1.24	-1.38	-1.0
6	-0.92	-0.91	-0.83	-0.61	-0.47	-0.40	-0.44	-0.42	-0.48	-0.48	-0.66	-0.82	-0.6
7	-0.27	-0.33	-0.28	-0.11	-0.23	-0.03	-0.07	-0.03	0.01	0.02	-0.04	-0.18	-0.1
8	0.26	0.21	0.18	0.20	-0.12	0.17	0.18	0.15	0.28	0.29	0.32	0.30	0.1
9	0.47	0.44	0.34	0.84	0.14	0.26	0.23	0.25	0.82	0.26	0.48	0.48	0.8
10	0.60	0.55	0.48	0.44	0.41	0.82	0.83	0.82	0.88	0.49	0.56	0.58	0.4
11	0.69	0.64	0.55	0.51	0.45	0.39	0.38	0.38	0.46	0.55	0.64	0.67	0.5
Mean.	14.21	15.04	15.22	14.93	13.80	12.48	11.55	11.19	11.14	11.66	12.87	13.28	

LXXVII.

Africa. — Cape of Good Hope. Lat. 33° 56'S. Long. 19° 39'E. Gr. — Dove.

Degrees of Resumur.

Hour	Jan.	∦ eb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	1.69	1.50	1.51	1.37	1.00	0.88	1.04	0.85	1.07	1.45	1.62	1.85	1.82
1	2.80	1.64	1.64	1.49	1.07	1.01	1.20	1.08	1.25	1.62	1.79	2.01	1.55
2	1.89	1.74	1.81	1.61	1.14	1.09	1.33	1.14	1.39	1.72	1.98	2.16	1.58
3	2.01	1.92	1.92	1.70	1.24	1.16	1.48	1.23	1.54	1.82	2.12	2.30	1.70
4	2.10	2.00	2.05	1.88	1.34	1.80	1.53	1.37	1.63	1.92	2.21	2.42	1.81
5	1.96	2.13	2.18	1.93	1.46	1.42	1.59	1.53	1.59	1.93	1.92	2.01	1.80
6	1.06	1.53	1.97	1.98	1.59	1.48	1.73	1.55	1.62	1.26	0.85	0.86	1.46
7	0.15	0.70	1.21	1.89	1.41	1.47	1.57	1.22	0.81	0.39	-0.02	-0.20	0.84
8	-0.53	-0.01	0.16	0.36	0.53	0.86	0.77	0.64	-0.06	-0.46	-0.67	-0.81	0.06
9	-1.10	-0.80	-0.76	-0.68	-0.89	-0.12	-0.24	-0.42	-0.82	-1.24	-1.25	-1.86	-0.77
10	-1.72	-1.65	-1.66	-1.48	-1.10	-0.90	-1.09	-1.08	-1.41	-1.82	-1.80	-1.90	-1.47
11	-2.23	-2.31	-2.87	-2.10	-1.64	-1.46	-1.72	-1.63	-1.85	-2.25	-2.24	-2.25	-2.00

LXXVII.

AFRICA. - CAPE OF GOOD HOPE, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Resumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Noon.	-2.48	-2.72	-2.66	-2.56	-2.09	-1.92	-2.11	-1.88	-2.15	-2.45	-2.46	-2.52	-2.83
1	-2.54	-2.74	-2.9 5	-2. 81	-2.20	-2.07	-2.83	-2.04	-2.23	-2.55	-2.48	-2.61	-2.46
2	-2.42	-2.54	-2.86	-2.79	-2.14	-2.06	-2.33	-1.97	-2.18	-2.44	-2.80	-2.44	-2.37
8	-2.16	-2.20	-2.51	-2.42	-1.84	-1.86	-2.13	-1.77	-1.82	-2.08	-2.01	-2.16	-2.08
4	-1.73	-1.70	-1.78	-1.75	-1.28	-1.28	-1.49	-1.82	-1.28	-1.52	-1.66	-1.90	-1.56
5	-1.21	-1.09	-1.03	-0.71	-0.61	-0.64	-0.76	-0.57	-0.56	-0.71	-1.05	-1.28	-0.85
6	-0.16	-0.18	-0.10	-0.03	-0.21	-0.29	-0.88	-0.17	0.00	0.20	-0.01	-0.15	-0.12
7	0.63	0.54	0.85	0.22	0.09	-0.05	-0.08	0.12	0.80	0.57	0.60	0.63	0.33
8	0.95	0.79	0.61	0.48	0.86	0.19	0.26	0.82	0.51	0.86	0.92	0.96	0.60
9	1.14	1.00	0.92	0.73	0.54	0.40	0.48	0.46	0.69	1.09	1.10	1.20	0.81
10	1.80	1.14	1.14	1.00	0.78	0.61	0.69	0.65	0.97	1.26	1.31	1.46	1.03
11	1.55	1.82	1.29	1.22	0.95	0.81	0.91	0.76	1.02	1.44	1.48	1.67	1.20
Mean.	15.81	15.96	15.00	13.61	11.88	9.84	9.96	10.06	11.01	12.43	13.54	14.82	

LXXVIII.

Australia. — Hobarton. Lat. 42° 53' S. Long. 147° 21' E. Gr. — Dove.

					De	grees of	Keaum	ur.					
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	2.81	1.95	1.78	1.81	0.88	0.66	0.72	1.10	1.51	1.99	2.44	2.45	1.59
1	2.59	2.17	1.99	1.41	1.03	0.76	0.86	1.86	1.71	2.19	2.67	2.76	1.79
2	2.89	2.82	2.19	1.62	1.11	0.88	1.01	1.48	1.93	2.45	2.77	2.95	1.96
3	8.09	2.53	2.39	1.75	1.23	0.97	1.16	1.58	2.06	2.68	2.98	3.24	2.14
4	8.20	2.68	2.49	1.85	1.81	1.15	1.28	1.69	2.20	2.80	8.11	8.38	2.26
5	8.83	2.82	2.54	1.99	1.44	1.15	1.40	1.82	2.32	2.85	2.99	3.13	2.31
6	2.62	2.59	2.64	2.11	1.55	1.29	1.50	1.91	2.34	2.60	2.24	2.24	2.14
7	1.48	1.75	2.10	2.00	1.60	1.87	1.50	1.90	1.84	1.61	1.16	1.03	1.61
8	0.27	0.68	1.08	1.80	1.27	1.26	1.81	1.32	0.93	0.41	0.01	-0.24	0.80
9	-0.88	-0.56	-0.17	0.24	0.45	0.60	0.60	0.44	-0.21	-0.70	-1.18	-1.27	-0.22
10	-1.92	-1.61	-1.29	-0.85	-0.46	-0.18	-0.21	-0.52	-1.21	-1.68	-2. 10		-1.18
11	-2.75	-2.84	-2.24	-1.78	-1.29	-0.96	-1.01	-1.53	-2.09	-2.54	-2. 89	-2.85	-2.02
Noon.	-3.51	-3.22	-8.03	-2.58	-2.00	-1.67	-1.67	-2.28	-2.70	-8.10	-3.43	-3.36	-2.71
1	-3.82	-8.52	-3.48	-2.95	-2.42	-2.08	-2.17	-2.78					-8.10
2	-3.91	-3.54	-3.63	-8.11	-2.53	-2.22	-2.8 8	-2.91					-8.18
8	-3.60	-3.36	-3.48	-2.87	-2.82	-2.02	-2.28	-2.71	-8.10	-3.82	~3.3 3	-8.45	-2.9 8
4	-3.20	-2.94	-2.92	-2.23	-1.69	-1.48	-1.73						-2.51
5	-2.57	-2.22	-2.02	-1.85	-0.92	-0.73	-1.01	-1.87	-1.59	-2.02	-2.30	-2.56	-1.72
6	-1.88	-1.04	-0 84	-0.56	-0.86	-0.25	-0.48	-0.64	-0.65	-0.80	-1.01	-1.38	
7	-0.18	-0.20	-0.04	-0.05	0.01	0.00	0.12	-0.13	0.01	0.05	0.20	-0.09	-0.02
8	0.82	0.68	0.45	0.32	0.27	0.24	0.14	0.21	0.46	0.55	0.90	0.89	0.49
9	1.81	1.18	0.82	0.57	0.42	0.24	0.84	0.57	0.79	1.00	1.41	1.51	0.84
10	1.71	1.47	1.19	0.84	0.62	0.40	0.50	0.79	1.08	1.84	1.75	1.91	1.13
11	2.05	1.77	1.47	1.06	0.77	0.54	0.64	0.98	1.81	1.68	2.05	2.25	1.37
Mean.	13.38	13.96	11.96	9.41	7.69	5.93	5.21	6.24	7.97	9.39	11.38	12.95	!

CORRECTIONS FOR TEMPERATURE.

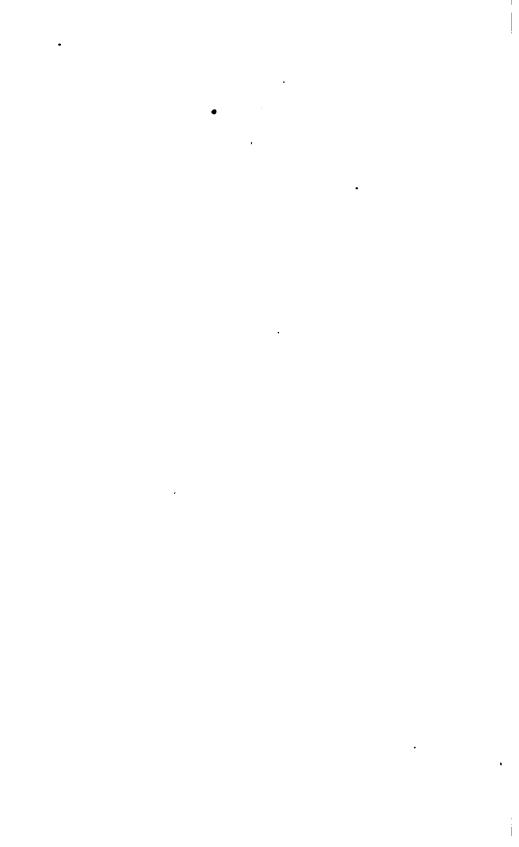
MONTHLY AND YEARLY

CORRECTIONS FOR NON-PERIODIC VARIATIONS,

OR

TABLES

FOR REDUCING THE MONTHLY AND YEARLY MEANS OF SINGLE YEARS
TO THE MEANS DERIVED FROM A SERIES OF YEARS.



TABLES

FOR REDUCING THE MONTHLY AND YEARLY MEANS OF SINGLE YEARS TO THE
MEANS DERIVED FROM A SERIES OF YEARS.

OBSERVATION shows that the monthly and annual mean temperature of a place somewhat varies from year to year. No law, however, has been as yet discovered as to the course of these oscillations. It follows that the means derived from observations carried on during a single year are but approximations to the true means. These last must be obtained from observations made for a series of years, during which these irregular variations become insensible by compensating each other; and it is obvious that their accuracy increases with the number of years which compose the series.

Professor Dove, having proved by his researches that these abnormal temperatures above and below the average of a whole month, or of a year, are apt to be felt simultaneously on extensive tracts of country, concluded that the means of a single year could be made available for obtaining the true means of the place, by being corrected for the non-periodic variations by means of normal stations in the same meteorological region, in which those elements had been more accurately determined by the observations of a long series of years. Comparing, namely, the means of a given year with the means derived from the whole series, we find a difference in + or -, which, applied, with reverse signs, to the means of the same year in the neighboring station to be corrected, will reduce, with a good degree of probability, the means of that particular year to the means which would have been obtained from a long series of years similar to that of the normal station.

The following tables, LXXIX. to XCVII., have been selected from those given by Dove in his five papers on the non-periodic variations of the atmospheric temperature, to be found in the *Memoirs of the Academy of Sciences of Berlin* for the years 1838, 1839, 1842, 1848, and 1853, to which we must refer for further details. They furnish normal stations for various latitudes; the columns contain the corrections for every month, viz. the differences, with *reverse* signs, between the monthly means in the year indicated in the first and last columns, and the means derived from the whole series, which are contained in the line at the bottom.

E

LXXIX.

Region of the Monsoons. - MADRAS.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year.	Jan.	Pob.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	•	•	0	•	0	•	•	0		•	•	0	
1796	0.00	0.24	0.00	0.36	-0.10				-0.81				1796
1797	::-		0.66	0.53	0.89	0.56	0.09	0.85		-0.83	0.16	-0.02	1797
1798	-0.13	1.12	0.40			0.39	0.58	-0.81	0.27	0.56	l .	0.20	1796
1799	-0.18	-0.08	0.62	0.86	0.26	-0.06	-1.20		-0.36	0.88		0.25	1799
1800	0.40	0.41	0.57	1.20	-0.23	-0.50	-1.02	-0.40	-0.58	0.20	0.47	-0.60	1900
1801	0.44	0.01	1.77	••	• •	-0.59	-0.67	0.63	1				1801
1802	0.44	0.86	1.77	1.02	-0.86	0.65	0.58	-0.04	1	0.48	4	1	1802
1808	0.22	0.24	0.80	0.58	-0.82	f .	0.18	0.80	1	0.88		0.65	1803
1804	1.64	1.48	0.75	1.88	0.70		1.24	0.00	1 -	0.88	0.91	0.29	1804
1805	0.27	0.41	0.66	-0.86	0.61	0.52	-0.76	-0.22	-0.27	-0.88	0.69	0.65	1805
1806	0.00	-0.89	-0.09	0.09	-0.41	-1.61	0.00	-0.13	1.07	0.47	0.96	0.12	1806
1807	0.22	-1.54	-8.20	-5.47	-1.79	0.48	1.20	-0.17	-0.09	-0.64	-0.20	0.78	1807
1813	0.80	0.87	0.13	0.96	1.12	-0.32	0.44		-0.18	0.25	-0.38		1813
1814	-0.86	-0.89	-0.58	0.04	-2.99	1.10	1.38	0.29	-0.22	0.07	-0.20	-0.37	1814
1815	-0.98	0.82	-0.67	2.00	1.55	-1.89	-0.98	0.27	0.31	-0.73	-0.91	-0.82	1815
1816	-1.09	-1.76	-1.56	-0.98	0.44	0.39	-0.44	-0.71	-0.67	-0.20	0.33	-0.51	1816
1817	-0.58	-0.70	-0.67	-0.62	0.12	-0.19	0.67	0.29	-0.71	-0.55	-0.96	0.52	1817
1818	0.22	0.32	-0.80	-0.04	1.41	0.65	-1.33	-2.00	-0.18	-0.55	-0.56	-0.87	1818
1819	-1.78	-1.28	-0.76	-0.18	0.48	0.88	0.44	0.98	-0.81	0.08	0.78	0.16	1819
1820	-0.67	-0.80	-0.85	0.59	-1.16	-0.82	0.18	0.23	-0.09	0.47	0.69	0.47	1820
1821	1.02	0.64	1.06	-1.51	0.26	0.08	0.58	0.94	-0.04	-0.02	0.20	0.20	1821
Means.	19.19	20.07	21.80	22.41	24.41	24.96	23.84	28.43	23.08	22.16	20.74	19.48	Means.
1822	-0.86	0.87	0.41	-0.28	0.07	-0.95	-0.76	0.72	-0.87	-0.70	-0.35	-0.19	1822
1823	0.31	0.37	-0.21	0.80	0.15	0.29	0.22	0.17	-0.60	0.72	0.27	0.97	1823
1824	0.71	0.59	0.27	0.52	-0.02	0.60	1.55	0.88	1.36	-0.98	0.14	0.26	1824
1825	-0.09	0.37	-0.21	0.12	0.24	-0.29	0.04	-0.86	0.08	0.32	0.59	-0.59	1825
1826	0.80	0.24	0.45	0.92	0.78	-1.17	0.04	-0.36	0.25	0.81	0.36	0.30	1826
1827	-0.09	-0.29	-0.17	0.17	-1.27	-0.46	-0.01	-0.09	-0.15	-0.18	0.54	0.08	1827
1828	1.07	0.51	-0.57		-0.42		-0.28	0.04	-0.60		0.81	0.21	1828
1829	0.09	-0.69	-0.35	0.08	-0.11	0.16	-0.89	-0.01	0.16	0.54	0.23	0.12	1829
1830	-0.27	-0.74	0.01	-0.32	-2.78	-0.15	-0.86	-0.23	0.25	1.12	0.68	0.53	1830
1831	0.31	1.49	1.66	0.48	1.89	1.36	0.04	0.67	0.70	0.41	0.41	0.58	1831
1832	-0.49	-0.29	1.26	1.73	2.51	2.65	1.64	2.40	0.84	-0.25	0.46		1832
1833	0.86	0.91	-0.19	0.97	0.83	0.83	1.33	0.40	0.16	0.41	0.19	1.06	1833
1834	0.18	0.60	0.55	-0.58	1.81	0.12	-0.98	-0.18	-0.15	-0.03	0.01	-0.01	1834
1885	-0.66	-0.73	-0.57	-1.07	-0.24	-0.86	-0.67	-0.45	-0.46	-0.74	-0.48	-0.94	1835
1886	-0.75	-0.73	-1.41	-0.72	0.60	0.12	-0.58	-1.29	-0.24	0.15	∸0.92	-1.03	1836
1837	-0.31	-0.02	0.06	-0.63	-1.17	-0.41	-0.40	-0.05	0.03	-0.34	-0.17	-0.85	1837
1838		-0.69		0.04						1	-0.57		1838
1839	1 .	-0.11			-0.15		-0.49	1			-0.83		1839
1840		-0.42		0.17	0.29	1	-0.45	0.27		0.19	1		1840
1841	1 1	-0.16		-0.58	-1.17		0.35	-0.71	0.74	-1.28			1841
1842	-0.09		-0.08	-0.49	0.47	0.07		0.09	-0.86	-0.30	-0.30	-0.23	1842
1848	0.23			0.22	-1.53		-C.22	0.44	1	l .	j	,	1843
Means.	20.53	21.81	22.92	24.27	25.62	25.35	24.31	23.73	23.70	22.92	21.32	20.67	Means

LXXX.

Sicily. — Palermo.

For Reducing the Monthly and Yearly Means of Single Years to the Mcans derived from Series of Years.

Year. Jan. Feb. March April May. June July Aug. Sept. Oct. Nov. Dec. Year.														
1791	Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1792	1791	0	0	0	0									1791
1798	N (1 18	0.51	0.00	0.12									
1794														
1795	II 1			1						1	1		1	
1796									1		-0.03			
1797	1795	-1.02	1.2	0.76	-0.10	0.12	0.08	-1.12	70.54	-0.72	•••	-0.23	0.18	1790
1798	1796	0.78	0.58	-0.84	-1.56	-0.19	-0.59	-0.39	-0.01	0.40	1.11	0.00	0.98	1796
1799	1797	-0.24	-0.29	-1.15	-0.19	-0.24	-0.70	-0.56	0.89	0.15	0.18	-0.12	0.16	1797
1800	1798	0.03	0.20	0.78	-0.90	-0.99	-0.45	0.72	-0.41	0.00	-1.00	1.97	0.31	1798
1801	1799	-1.75	1.38	0.52	0.64	-0.35	0.08	0.87	0.75	0.48	1.40	-0.32	0.40	1799
1801	1800	2.27	2.96	0.69	2.46	0.63	-0.14	0.26	-0.41	-0.58	0.02	-0.18	0.09	1800
1802														
1802	1801	-0.11	0.76	1.45	0.24	-0.10	-0.16	1.26	-0.56	-0.07	1.04	1.04	1.64	1801
1808	1	0.09	-0.16	ı		t								1802
1804	1803	1.67	-1.69	· .	2.08	-1.08	0.66	0.04	0.52		-0.65		0.42	1803
1805	11 /	1	l .			l							1	
1806	11 1	0.80	0.69	ı		i .				l .	0.06		l 1.	1805
1807			1	ł	İ	İ				1				
1807	1806	-1.15	0.64	-0.04	-0.50	0.41	0.10	-0.14	-0.85	-1.16	-0.43	-0.14	0.40	1806
1809	1807	-1.06	0.16	ı		1								1807
1809	1808	-0.24	-1.22	-0.86	-1.36	-0.48	-0.43	0.88	0.04	2.42	-1.92	-0.29	-2.31	1808
1810	12	1	1	l		1							1	1809
1811	н і	i .	1	I		l							l I	
1812			ł											
1813	1811	-0.15	0.69	-0.91	0.24	0.48	1.46	0.97	0.26	0.04	0.95	0.00	-0.76	1811
1813	1812	-1.51	0.40	0.00	-0.89	-0.61	0.15	-1.32	-0.21	-0.69	-0.16	0.35	-0.18	1812
1815	1813	-1.51	-1.02	-0.80	-0.52	0.79	0.82	-0.92	-1.25	-1.00	1.31	0.04	-1.18	1813
1816	1814	0.54	-8.04	-0.88	0.04	-1.46	-0.59	-0.96	-0.56	-2.03	-0.49	-0.52	-0.42	1814
1816	1815	-0.46	0.07	0.29	0.90	0.61	-0.63	-1.12	-2.01	-0.78	0.22	0.08	-0.78	1815
1817	1 1	1	ľ			l								
1818	1816	-0.40	-0.31	-0.71	-0.54	0.05	-1.94	-0.65	-0.48	-0.80	-1.09	-0.63	-1.24	1816
1819 -1.02 0.18 0.72 0.97 -0.12 -0.21 -0.28 -0.34 -0.32 0.82 1.11 0.82 1819 1820 1.89 -0.11 -0.97 0.87 2.03 0.68 0.48	1817	-0.11	-0.09	-0.15			0.82	-0.89	0.46	-0.34	0.11	-0.47	-0.02	1817
1819	1818	-0.66	0.87		1.21	0.19	-1.10	−0.2 5	-0.45	0.24	-0.78	0.33	0.62	1818
1821	1819	-1.02	0.18	0.72	0.97	-0.12	-0.21	-0.28	-0.84	-0.32	0.82	1.11	0.82	1819
1821 1.92 -0.76 0.49 0.50 0.85 -0.74 -0.30 -0.21 0.51 -0.74 -0.72 0.69 1821 1822 -1.28 -1.11 -0.53 0.68 2.97 1.48 1.46 1.88 1.51 0.06 0.18 1822 1823 0.52 1.78 -0.80 0.28 0.99 0.30 -0.36 0.35 -0.84 -0.76 -1.63 -0.53 1823 1824 -0.91 0.42 -1.04 -1.01 1.25 -0.25 -0.70 1.86 0.13 1.51 0.64 0.51 1824 1825 -1.04 -1.02 -0.17 0.12 0.30 -0.45 -0.10 0.46 0.55 -1.00 -0.05 1.67 1824 1826 -0.88 0.56 -0.29 -0.59 -1.08 -0.74 0.39 0.52 1.85 0.46 -0.87 -0.24 1826 1827 0.07 0.83 0.82 -0.51 0.18 -1.30 0.80 1.33 -0.7		1.89	l .	1	0.87	ı						ı	0.29	1820
1822			1	ł	l	1				}	l			
1823 0.52 1.78 -0.80 0.28 0.99 0.80 -0.36 0.35 -0.34 -0.76 -1.63 -0.53 1823 1824 -0.91 0.42 -1.04 -1.01 1.25 -0.25 -0.70 1.86 0.13 1.51 0.64 0.51 1824 1825 -1.04 -1.02 -0.17 0.12 0.30 -0.45 -0.10 0.46 0.55 -1.00 -0.05 1.67 1825 1826 -0.88 0.56 -0.29 -0.59 -1.08 -0.74 0.39 0.52 1.85 0.46 -0.87 -0.24 1826 1827 0.07 0.83 0.82 -0.51 0.18 -1.30 0.80 1.33 -0.73 0.50 -1.76 -0.04 1827 1828 -0.16 0.20 0.23 0.29 1.99 1.28 2.48 1.10 0.74 -0.34 0.06 -0.37 1828 1829 0.79 -1.90 1.12 2.49 -0.09 -0.47 0.16 -0.12 0.41	1821	1.92	-0.76	0.49	0.50	0.85	-0.74	-0.80	-0.21	0.51	-0.74	-0.72	0.69	1821
1823 0.52 1.78 -0.80 0.28 0.99 0.80 -0.36 0.35 -0.84 -0.76 -1.63 -0.53 1823 1824 -0.91 0.42 -1.04 -1.01 1.25 -0.25 -0.70 1.86 0.13 1.51 0.64 0.51 1824 1825 -1.04 -1.02 -0.17 0.12 0.30 -0.45 -0.10 0.46 0.55 -1.00 -0.05 1.67 1825 1826 -0.88 0.56 -0.29 -0.59 -1.08 -0.74 0.39 0.52 1.85 0.46 -0.87 -0.24 1826 1827 0.07 0.83 0.82 -0.51 0.18 -1.30 0.80 1.33 -0.73 0.50 -1.76 -0.04 1827 1828 -0.16 0.20 0.23 0.29 1.99 1.28 2.48 1.10 0.74 -0.34 0.06 -0.37 1828 1829 0.79 -1.90 1.12 2.49 -0.09 -0.47 0.16 -0.12 0.41	1822	-1.28	-1.11	-0.53		0.68	2.97	1.48	1.46	1.88	1.51	0.06	0.18	1822
1825 -1.04 -1.02 -0.17 0.12 0.30 -0.45 -0.10 0.46 0.55 -1.00 -0.05 1.67 1825 1826 -0.88 0.56 -0.29 -0.59 -1.08 -0.74 0.39 0.52 1.85 0.46 -0.87 -0.24 1826 1827 0.07 0.83 0.82 -0.51 0.18 -1.30 0.80 1.33 -0.73 0.50 -1.76 -0.04 1827 1828 -0.16 0.20 0.23 0.29 1.99 1.28 2.48 1.10 0.74 -0.34 0.06 -0.37 1828 1829 0.79 -1.90 1.12 2.49 -0.09 -0.47 0.16 -0.12 0.41 -0.38 -0.35 -0.16 1829	1823	0.52	1.78	-0.80	t e	0.99	0.80		i .	1	-0.76	-1.63	-0.58	1823
1825 -1.04 -1.02 -0.17 0.12 0.30 -0.45 -0.10 0.46 0.55 -1.00 -0.05 1.67 1825 1826 -0.88 0.56 -0.29 -0.59 -1.08 -0.74 0.39 0.52 1.85 0.46 -0.87 -0.24 1826 1827 0.07 0.83 0.82 -0.51 0.18 -1.30 0.80 1.33 -0.73 0.50 -1.76 -0.04 1827 1828 -0.16 0.20 0.23 0.29 1.99 1.28 2.48 1.10 0.74 -0.34 0.06 -0.37 1828 1829 0.79 -1.90 1.12 2.49 -0.09 -0.47 0.16 -0.12 0.41 -0.88 -0.35 -0.16 1829	1824	-0.91	0.42	-1.04	-1.01	1.25	-0.25	-0.70	1.86	0.13	1.51	0.64	0.51	1824
1826 -0.88 0.56 -0.29 -0.59 -1.08 -0.74 0.39 0.52 1.85 0.46 -0.87 -0.24 1826 1827 0.07 0.83 0.82 -0.51 0.18 -1.30 0.80 1.33 -0.73 0.50 -1.76 -0.04 1827 1828 -0.16 0.20 0.23 0.29 1.99 1.28 2.48 1.10 0.74 -0.34 0.06 -0.37 1828 1829 0.79 -1.90 1.12 2.49 -0.09 -0.47 0.16 -0.12 0.41 -0.88 -0.35 -0.16 1829	11 1	-1.04		Į.	1		4	i e	i .	4	ı	-0.05	1.67	1825
1827 0.07 0.88 0.82 -0.51 0.18 -1.30 0.80 1.33 -0.73 0.50 -1.76 -0.04 1827 1828 -0.16 0.20 0.23 0.29 1.99 1.28 2.48 1.10 0.74 -0.34 0.06 -0.37 1828 1829 0.79 -1.90 1.12 2.49 -0.09 -0.47 0.16 -0.12 0.41 -0.38 -0.35 -0.16 1829	 		1	1	1	1					1	1		
1828	1826	-0.88	0.56	-0.29	-0.59	-1.08	-0.74	0.89	0.52	1.85	0.46	-0.87	-0.24	1826
1829 0.79 -1.90 1.12 2.49 -0.09 -0.47 0.16 -0.12 0.41 -0.88 -0.35 -0.16 1829	1827	0.07	0.88	0.82	-0.51	0.18	-1.80	0.80	1.33	-0.73	0.50	-1.76	-0.04	1827
	1828	-0.16	0.20	0.23	0.29	1.99	1.28	2.48	1.10	0.74	-0.34	0.06	-0.37	1828
	1829	0.79	-1.90	1.12	2.49	-0.09	-0.47	0.16	-0.12	0.41	-0.38	-0.35	-0.16	1829
	Means.	8.35	8.27	9.40	11.52	14.85	17.12	19.25	19.48	17.60	14.78	11.69	9.44	Means.

LXXXI.

NORTH ITALY. - MILAN.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

	Jan.	Feb.	March.	A	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Year.	Jan.			April.									
1763	。 -1.82	1.58	-0.60	0.27	-2.28	-0.79	0.68	o 1.11	-î.11	-1. 6 9	-0.56	1.02	1763
1764	1.68	1.98	-0.70	-0.63	1.32	0.91	-0.12	-1.29	-1.21	1 .		1.52	1764
1765	3.88	-0.92	0.60	0.47	-1.08	0.11	-2.62	-1.69	-0.11	0.11	0.24	-0.98	1765
1766	-3.42	-1.52	-0.40	0.57	0.02	1.31	,	1	l .	-0.49	2.14	-0.68	1766
1767	-4.22	0.88	0.10		-1.08	-1.19	ŀ	1	I			-0.88	1767
1768	-0.82	-1. 2 2	-1.50	A 97	-0.58	-2 .19	0.68	0.51		١	0.64	-0.78	1768
,	1.88	-0.42		-1.68	1	I	-0.52	1.51		-2.19	1.24	0.62	1769
1769	-0.52	0.98	-0.60		-0.58	0.81	-0.72	0.01	1.99	0.51	1.04	1 1	1770
1770	1.78	-0.52	-0.60	-0.33 -1.43	1.02	-0.19	1	1.51	0.49	-0.69	-1.06	2.32	1771
1771						l	1	0.41	0.29	2.01	1.94	2.02	1772
1772	1.58	2.48	2.50	0.57	-0.50	1.61	1.38	0.41	0.25	2.01	1.54	2.02	1772
1773	1.58	-0.42	-0.80	-0.03	-0.48		-1.72	-1.29	0.69	1.61	0.34	1.82	1773
1774	0.48	0.08	0.70	0.77	-0.28	0.51	-0.12	1.31	-0.81	-1.09	-0.96	-2.68	1774
1775	0.38	2.08	1.60	0.47	-0.58	0.71	0.78	-0.09	−0.3 1	-1.79	-0.16	-0.88	1775
1776	-0.32	-0.02	1.30	0.97	-1.28	0.11	0.48	0.41	-0.71	0.11	-0.36	-1.18	1776
1777	-1.52	-1.42	1.30	-0.23	-1.08	-0.79	-1.22	0.51	0.19	0.41	1.24	-1.98	1777
1778	0.38	0.08	-1.90	1.47	0.62	-0.2 9	0.98	0.81	-0.81	-0.09	0.64	1.72	1778
1779	-3.52	1.98	0.00	1.07	1.72		0.18	-0.19	1.59	1.81	-0.16		1779
	1 . 1		2.70	-0.43	1.72	1.51	0.78	0.11		1.81		-1.08	1780
1780	-0.62 -0.12	-1.92 0.38	1.90		0.22	0.01	1.78	0.11	0.39	-0.89	0.04	1.42	1781
1781 1782	2.18	-2.42	-0.70	1.47 -1.03	-1.08	1.21	2.08	0.91		-1.79	-2.46		1782
1702	2.10	-2.42	-0.70	-1.03	-1.00	1.21	2.00	0.51	0.51	-1.75	2.40	0.30	1702
1783	0.98	1.18	-0.60	0.97	0.42	-0.99	1.06	-0.29	-0.31	1.51	0.24	-1.88	1783
1784	0.48	-2.02	0.50	-2.03	2.62	2.11	1.38	0.61	1.49	-1.49	-0.46		1784
1785	0.58	-1.12	-3.80	-1.23	0.72	1.21	0.68	0.61	2.69	0.41	0.74	2.02	1785
1786	0.18	0.68	-0.90	0.87	0.72	0.81	-0.52	-0.89	1.09	-1.89	−0.3 6	-0.48	1786
1787	-0.32	0.08	0.90	-0.03	-1.9 8	1.71	-0.02	1.61	0.09	0.81	0.84	1.72	1787
1798	2.78	1.08	2.30	1.37	-0.18	1.51	2.78	-0.39	0.99	0.21	-0.86	-2.88	1788
1789	-1.72	0.98	-1.70	1.37			0.28	0.11	0.29	0.31	1		1789
1790	-0.12	1.48	-0.20	-1.73	1.62	1	-0.72	1.21	0.19	2.21	1.24	0.02	1790
1791	2.48	1.08	1.20	1.87			I	1.51	0.09	-0.29	-0.46	1.92	1791
1792	0.98	-0.12	1.30	1.87		0.21	0.08	0.11	I .	0.71	0.54	-0.08	1792
1800	, ,	0.00	0.40	_,	-0.88	0.01	1.78	-0.29	2.49	,	٠, ,	2.22	1793
1798	-1.22 2.28	-0.02 3.08	2.00	1	-0.08	1	1	1	1	1.31 -0.49	1.44 1.84		1793
1794	1	1		ſ	ı		ı	1	0.49	1	-0.16	1 1	1795
1795	-3.72	-3.12	-0.20	1.37	1	-0.79 -0.29	l .	1		1.71	1.24	1.52 -1.38	1796
1796	2.48	1.18	-1.70	Į.	-0.28 1.22	1	1	2.51	1.09	0.41 -0.59	0.94	1.32	1797
1797	0.78	0.18	-1.40	0.67	1.23	-1.59	1.18	2.31	1.09	70.09	0.54	1.02	1101
1798	1.78	2.08	0.20	0.27	0.72	-0.09	0.48	0.51	0.29	-0.39	-0.86	-2.08	1798
1799	-3.22	0.88	0.60	-1.23	-0.98	-1.49	-0.62	0.41	1.39	0.31	-0.96	-1.18	1799
1800	1.78	4.58	-1.10	2.67	1.32	-1.59	0.39	-0.09	0.49	0.01	1.24	-0.08	1800
1901	1.38	1.08	1.50	0.77	0.32	-0.39	-0.62	-0.79	0.49	0.61	0.04	0.02	1801
1801	0.18	1.18	0.70	ı	4	•	1	1	1	I	1		1802
1802	ll .	-3.82		l .	-0.88	1	I .		1.09 -0.91	1	1.04 0.54	1 1	1803

LXXXI.

NORTH ITALY. - MILAN (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year.	Jan.	Peb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1804	3.98	-1. 32	-0.60	_0.03	1.82	o 2.11	•	° -0.89	0.49	0.71	-0. 8 6	-0.18	1804
1805	-0.12			-2.03			1	-0.29			-2.36	-1.58	1805
1806	0.18	1	I	-1.58	0.82			-1.19		-0.19	1.34	1.92	1806
1807	0.58	i .		-1.88	1.32		1.18		0.19	1.71	1.84		1807
1808	-1.02	-1.62		-1.23	1.62			-0.69	0.89	-2.89	0.24	-2.08	1808
H	ll l		İ	l		•							1
1809	0.48	1.98	-1.40	-2.68	1.02	0.51	-0.52	0.21	-0.51	-0.19	-0.96	0.22	1809
1810	0.08	-0.72	1.90	-0.23	0.22	-1.49	-2.12	-0.79	0.59	1.11	0.84	1.82	1810
1811	-0.72	1.48	1.70	1.47	1.82	-0.29	1.18	-0.49	0.89	2.21	2.24	-0.88	1811
1812	-3.32	-0.32	-0.40	-1.78	0.92	1.01		-0.59		0.11	-2.96	-2.38	1812
1813	-0.12	1.08			1.52		-2.12	1	ı	0.21	-0.56	1.82	1813
1	1												
1814	-0.12	-4.42	-1.40	0.77	-1.98	-1.09	-0.12	-1.09	-1.91	-0.69	1.04	1.82	1814
1815	-2.02		1		1.22	1	-1.22		0.29	0.81		-1.78	1815
1816	-0.52	-2.92	-1.20				-2.22		-0.51	0.41	-1.46	-1.88	1816
1817	-2.52	1	0.30	1				-0.59	1	-1.89	0.44	-0.18	1817
1818	0.48		0.70		-3.80			-0.79	1	0.48		-0.39	1818
1819	0.00	0.73	1.48	1.85	-0.02	-0.58	0.82	-0.50	0.48	0.46	0.98	0.80	1819
1820	-0.79	1		1		ł	-0.48	1.76		-0.30			1820
1821	0.80	1				-2.20		1		-0.29) 1	1821
1822	1.81	1.28	2.10	1	1.05		0.58	0.26		0.66	1.88	-0.48	1822
1823	11			-0.55			-0.60		1.18		-1.87	0.01	1828
1020	1.52	0.20	0.0.	0.00	0.00	0	0.00	0.00	2020			0.02	1020
1824	1.01	1.49	_0.40	-0.85	-0.16	-1.57	1.33	0.90	0.71	0.23	1.25	2.07	1824
1825	1.39	1			-0.17	l.			0.86	-0.81		8.92	1825
1826	-2.18		l .	-0.72		-0.09	0.18	1.55	0.71	1.48		1.16	1826
1827	0.86		1.12	0.73	0.46		1.20	-0.60			-1.46	0.25	1827
1828	1.38		1.49	0.64	0.45	l	1.38	0.19	0.47		-0.81	0.60	1828
1020	1.00	0.00	1.70	0.04	0.40	1.21	1.00	0.13	0	0,00	0.01	0.00	1020
1829	-0.04	-2.79	0.05	0.05	-0.03	0.28	0.22	-1.15	-0.89	-0.40	-1.68	-1.90	1829
1830	-8.72		1.66	2.66	1 1	-0.33			-0.79	-0.81	0.99	0.60	1830
1831	0.88		0.78	0.19		-0.56		-1.05		1.77		1.84	1831
1832	0.41	0.52			-2.07	1	0.03		-1.15	-0.47		l i	1832
1833	-0.47			-1.23	2.00				-8.20			1.87	1883
. 1000	0.47	1.10	0.08	1.40	2.00	0.07	2.20	2	5.20	1.00	J	1.07	1000
1884	0.17	_0.80	-0.19	-1.97	0.58	-0.81	-0.28	-1.16	0.41	-0.79	-0.28	-0.94	1834
1835	1.03					1	-2.59						1835
1836	-2.51								1			-0.02	1836
1837	-0.83						-1.29		-2.40			-0.36	1837
1838	-2.16						-0.78		1	-1.74		-0.80	1838
1000	_												
Means	0.52	2.82	6.40	10.08	14.08	17.09	18.92	18.89	15.31	10.79	5.76	2.08	Means.
	3.32		0.20										
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LXXXII.

SWITZERLAND. — GENEVA.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year.	Jan.	Pob.	March.	April.	May.	June.	July.	Ang.	Sept.	Oct	Nov.	Dec.	Year.
1768	-0.86	-0.01	° -3.86	-0.14	-0.61	-1.71	-0.92	-1.25	-1.42	0.99	°.77	0.08	1768
1769	0.92	0.16	1		-0.71	1	ł			1			1769
1770	-1.25	-1.80			-1.20	1		-1.24					1770
1771	0.58	-0.67		-2.68	1	-1.84	1		-0.57	1			1771
1772	0.61	2.57			-2.23	1	-0.72						1772
1778	1.47	-1.84	-1.18	-1.16	-1.64	-0.87	-2.03	-1.70	-0.12	-0.35	-0.12	1.01	1773
1774	1.22	0.91	2.38	0.73	-0.94	-0.47	-1.27	0.42	-1.08	-1.45	-1.18	-2.03	1774
1775	0.89	1.89	0.99	-1.60	-1.90	0.54	-0.84	-0.82	-0.02	-0.24	0.33	-0.68	1775
1776	-1.78	1.92	1.85	0.18	-1.96	0.09	0.20	0.28	-1.50	0.26	-0.26	-0.09	1776
1777	-0.41	-0.76	2.46	-1.23	-1.51	-0.8 8	-1.12	0.45	-0.41	1.27	0.21	-1.72	1777
1778		-0.98	0.86	0.78					-1.85				1778
1779	-3.43	-0.2 8	-0.14	1.70			-0.61		0.48	1.77		2.70	1779
1780	-1.48	-1.63	2.35	-0.86	0.97	1.14		1.16	0.14	0.51		-1.25	1780
1781	0.96	1.09	0.87	2.15	1.78	0.28		0.30	0.76	-0.47	1.69	2.97	1781
1782	2.22	-8.74	-0.58	-0 .95	-1.76	0.18	-1.10	-0.72	-0.97	-1.06	-1.83	-2.04	1782
1788	2.01	1.68	-0.27	-0.71	-0.06	-1.18	1.75	-0.94	0.17	0.98	0.81	1.03	1783
1784	-1.06	-2.03	-0.43	-2.5 1	1.73	1.69	0.84	-1.62	1.40	-1.87	-0.76	-3.38	1784
1785	0.58	-8.26	-6.75	-5.48	-0.19	0.80		-1.75		-0.40	0.11	0.42	1785
1786	0.41	0.08	-1.62	0.69	-0.25	1.92	-0.99	-1.22	-0.5 9	-1.71	-0.69	0.19	1786
1787	-1.99	-1.15	1.76	-0.80	-1.98	0.79	-0.70	0.21	-0.27	0.41	0.72	2.83	1787
1788	1.01	2.06	2.19	1.04	1.18	1.04	1.61	-0.45	0.71	-0.88	-2.15	-4.48	1788
1789	-1.17	1.12	-1.97	1.19	1.71	-1.25	-0.80	-0.19	-0.57	-0.59	-1.59	-0.17	1789
1790	0.36	0.75	0.99	-0.78	1.52	0.94	-1.10	0.63	-0.84	1.95	1.13	0.78	1790
1791	2.40	0.04	-0.02	2.86	0.61	1.04	0.98	2.30	0.98	0.72	-1.37	1.30	1791
1792	1.22	~0.28	2.11	1.81	-0.12	1.14	1.08	0.88	-0.0 9	1.87	0.86	0.45	1792
1798	-0.52	1.05	1.77	0.08	-0.05	0.20	8.12	2.49	-0.12	1.24	0.61	1.19	1793
1794	0.14	2.21	1.91	3.26	0.76	1.10	2.11	0.39	-0.74	-0.28			1794
1795	-4.85	0.87	0.26	1.76	1.32	1.84	-0.78	1.34	1.54	1.92	1	1.11	1795
1796	1.25		-2.15	-0.06	0.60		0.87	0.80	1.61	0.41		-1.92	1796
1797	0.11		-1.08	1.49	2.14		2.21	1.28	0.71	-0.08		1.61	1797
1798	0.58		-1.02	0.88	1.00	1.29	0.45	0.81	0.48	-0.29		-0.96	1798
1799 1800	-1.57 1.64	1.71 0.06	-0.16 -1.66	-1.75 2.48	-1.70 2.40	-1.16 -0.88	-0.18 1.48	0.67 0.82	0.21 0.96	-0.40 -1.55	-0.54 0.68	-2.59 -0.27	1799 1800
Means.	-0.48	0.75	3.08	7.19	11.21	14.03	15.44	14.85	11.49	7.82	3.34	0.57	Means.
1796	2.27	0.07	-2.14	-0.25	-0.91	-0.64	-1.10	0.16	0.70	0.08	-0.68	-1.70	1796
1797	0.45		-0.66	0.97		-2.08	1.27	0.71		-0.26		1 1	1797
1798	0.68	-0.25		0.96			-0.64	-0.14	0.12			-1.36	1798
1799	-1.44	1.98	-0.26	-1.60		-0.49	-0.46	0.33	0.19	-0.26			1799
1800	2.06	0.08		2.88	1.66		1.62	0.70	0.41			1 : * - 1	1800
1801	1.81	0.18	1.48	0.74	0.48	-0.26	0.42	0.15	0.90	0.84	0.67	0.95	1801
1802	-3.98	-0.38	0.94	1.18	0.58	1.66	-0.12	2.68	1.72	2.51	0.63	0.58	1802
1803	-0.26	-2.58	0.24	2.05	-1.42	0.89	2.20	2.25	-0.79	-0.57	1.04	1.88	1803
1904	4.58	-1.58	-0.19										1804

LXXXII.

SWITZERLAND. — GENEVA (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year.	Jan.	Peb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1805	° -0.41	-0.23	° -0.41	o -1.85	。 1.22	-0.49	-0.41	_0.78	o 0.18	-1.45	。 -2.19	-1.64	1805
1806	3.23	1.88		-1.80	1	1.66		-0.89	0.11	1.10			1806
1807	-1.10	0.24	-2.65		1.42	0.48	2.66	3.03	-0.58	1.42	0.89		1807
1808	-0.49	-8.14		-1.87	1.14	-1.83	0.70	0.59	-0.14	-2.40			1808
1809	2.28	1.95		-8.68	-0.06	0.12	1	-0.32	-1.00	-1.05		0.70	1809
	2.20	2100	0.13	••••	-0.00	0.12	0.40	0.02	-1.00	1.00	1.10	0.70	1000
1810	-8.14	-8.84	3.08	-0.28	0.29	-0.45	-1.01	-0.70	1.87	1.26	1.05	1.19	1810
1811	-2.22	1.98	1.46	1.84	1.28	1.82	1.58	-0.14	0.70	2.21	0.71	-0.85	1811
1812	-3.92	1.40	-0.02	-1.54	0.27	0.02	-0.87	-0.69	-0.48	0.13	-1.80	-2.74	1812
1813	-1.74	1.51	-0.69	0.58	0.54	-0.84	-2.10	-1.02	-1.14	0.78	-0.49	0.82	1818
1814	-1.82	-3.92	-1.44	0.96	-1.74	-0.26	0.87	-0.66	-1.74	-0.87	0.95	2.84	1814
													l
1815	-2.24	1.43	2.17	1.06	0.82	0.08	0.20	-0.59	0.54	1.48	-1.57	-0.89	1815
1816	-0.18	-1.83	2.54	-0.48	-0.54	-1.41		-2.14	-0.47	0.59	-1.05	-0.02	1816
1917	2.50	2.88	0.29	-2.11	-1.84	1.85	−0.2 5	-0.71	2.16	-1.58	0.85	-0.45	1817
1818	0.54	0.69	0.18	-0.08	-1.26	0.66	1.41	-0.41	0.89	-0.29	1.60	-0.26	1818
1819	1.86	0.98	0.82	1.00	-0.21	-0.19	0.07	-0.84	0.42	0.07	-0.40	0.95	1819
1820	0.10	0.54	-1.24	2.07	0.89	-0.59	-0.65	0.84	-1.93	-0.81	-2.16	0.02	1820
1821	1.98	-1.31	0.94	0.71		-1.54		0.62	0.26	0.27	2.34	1 1	1821
1822	0.20	1.27	8.06	0.47	1.82			-0.85		0.69	1.60	1 1	1822
1823	-1.17	1.46	-0.29	-0.42			1	-1.04		-2.10		1.04	1823
1824	-0.78	-0.80	-1.84	-2.05	-1.50			-1.49		-1.58	0.03	1.30	1824
1825		-0.55	-1.09	1.69	-0.63	0.26		-0.11	0.88	0.30	0.54	2.76	1825
	-0.07		1.03	1.05		0.20	70140	-0:11	0.00	0.00	0.54	2.70	1020
Means.	-0.42	1.87	4.70	8.79	18.45	15.81	17.67	17.66	14.70	9.78	5.28	1.27	Means.
1826	-3.23	1.12	1.47	0.34	-1.04	-0.06	0.90	2.57	1.22	0.95	-1.19	0.03	1826
1827	1.49	-2.15	1.02	1.29		-0.07	1.95	-	0.24	0.99			1827
1828	2.82	1.06	0.70	0.81	1.22	0.89		-0.80	0.86	0.96	0.62	0.94	1828
1829	-0.85	-0.68	0.10	0.25			0.15	-0.89	-0.71	-1.52	-1.28	-8.87	1829
1830	-4.14	-1.74	1.20	2.70		-0.49	0.58		-0.94	-0.86		1 1	1830
1831	-1.10	0.46	1.67	1.54	0.58		-0.02	i	-0.29	2.16		1 1	1831
1832	0.10	0.86	-0.25	0.45		-0.83	0.81		-0.89	0.07	1	1 1	1882
1833	-0.06	3.36	-0.50	-0.68	2.67	1.28	-1.29			0.59	0.89		1888
1884	5.06	1.47	0.85	-0.70	2.28	1.58	1.94	1.07	2.74	0.68	0.71	-1.18	1884
1885	1.15	1.40	-0.44	-0.06	0.56	0.15	1.69	0.40	0.22	-1.84	1	1 "	1885
1886	0.48	-0.04	1.82	-0.95	-2.14	0.17	0.57	0.28	-0.62	0.14	Ì		1836
1837	0.87	0.52	-2.94		-2.14 -2.18		-0.58	ı	-1.16		ı	-0.46	1837
1838	-8.64		0.25									-0.57	1838
1889	0.55	-0.07	-0.42		-0.11 -0.97	1.14	ı	-1.28 -1.78		1.11	1.43		1889
1840	2.60		-0.42 -8.22		-0.97 -0.10	1		-0.01		-1.74	1	-3.14	1840
1 1								}		l	ł	1	İ
1841	0.45		0.77	-0.69	1.82	-1.71	-1.98	1	0.09	0.90	0.26		1841
1842	-5. 18	-2.84	0.56	-0.58	0.02	1.00		0.78	-1.08	i	-1.08		1842
1843	1.50	2.22	-0.84	0.27	-1.60	-2. 56	-2.85	-0.78	0.60	-0.24	0.25	-0.88	1843
1844	• •	• •	• •	• •	• •	••	• •	• •	• •		• •		1844
1845	1.70	-3.38	-1.77	0.49	-1.98	0.47	0.06	-1.53	1.10	0.40	1.54	1.74	1845
Means.	-0.72	0.98	4.16	7.08	10.77	18.61	14.96	14.58	11.84	7.98	3.98	1.30	Means.

LXXXIII.

South Germany. - Vienna.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Ang.	Sept.	Oes.	Nov.	Dec.	Year.
1775	o -1.43	o 1.86	0	。 -2.8 5	-2.77	o 1.82	-0.41	o 1. 29	o 0.84	0.26	0.29	-1.09	1775
1776	-4.30	0.57	0.70		-2.80	-0.42	-0.24	0.25		-1.53	-1.82	-2.19	1776
1777	-1.79	-1.24	0.82		-0.22	-0.10	-1.17	0.57		-0.58	0.85	-1.00	
1778	1.92	-1.04	0.18	1.89	0.04	1	i i	0.95		-0.54	0.87	3.61	1777
1	1					-0.48	1.18						1778
1779	-1.75	8.15	2.27	3.05	1.24	-1.82	-1.85	-0.07	0.65	1.00	0.43	8.01	1779
1780	-1.68	8.04	2.73	-1.88	-0.18	-0.92	-0.70	-0.48	-1.08	0.51	0.19	-1.99	1790
1781	-0.87	0.05	0.77	0.86	0.25	1.44	-0.06	2.31	1.40	-0.45	1.84	0.84	1781
1782	2.72	-2.68	0.60	-0.06	0.54	1.82	2.74	0.85	0.86	-0.76	-1.50	0.62	1782
1783	3.59	4.12	-0.08	0.65	1.81	1.94	1.66	1.81	2.12	1.59	0.58	-2.56	1783
1784	-3.51	-1.87	-0.42	-1.86	1.69	0.86	0.47	0.49	1.98	-2.56	0.70	0.03	1784
												1 1	
1785	-0.73	-0.93	-5.63	-8.04	-0.67	-1.47	-0.83	-0.86	2.11		0.41	0.17	1785
1786	0.52	0.16		1.84	-1.12	0.25	-1.54	-1.85	1	1	-2.12	0.60	1786
1787	-0.89	1.47	0.65	-1.46		1.11	-0.40	0.35		1.10	0.98	2.82	1787
1788	2.22	0.17	0.81	0.05	-0.86	1.18	2.28	-1.72	1.00	-0.29	-1.89	-6.79	1788
1789	-0.49	2.00	-2.48	1.19	2.15	-0.49	0.40	-0.60	0.87	0.77	0.78	0.21	1789
1790	0.86	2.87	0.31	-1.11	1.20	1.56	-1.10	0.81	-0.83	-0.76	-0.48	2.09	1790
1791	4.29	1.01	1.68	1.33	-0.44	-0.38	-0.87	0.67			-0.46	0.89	1791
1792	0.56	-1.24	0.47	0.88	-0.96	0.62	0.88	0.26	1	-1.11	-0.24	0.56	1792
		1.27	-1.00	-2.40	-1.28	-1.08	1.81	1.86		1.18	0.64	1.99	1798
1798	-1.55								-1. 8 8	-0.19	0.88		
1794	2.24	2.99	1.95	8.74	1.35	1.55	2.92	-0.75	_1.00	-0.15	0.20	-0.95	1794
1795	-4.94	-1.29	0.23	1.81	-0.05	1.44	-1.95	0.81	-0.17	2.75	-1.00	2.28	1795
1796	5.23	1.82	-2.78	-1.52	0.48	-0.04	0.14	0.58	1.96	0.84	-0.14	-1.48	1796
1797	1.58	1.02	-0.71	2.10	2.94	0.68	1.95	2.17	2.01	1.23	0.54	1.11	1797
1798	1.96	2.83	1.40	0.65	0.26	0.84	0.14	1.29	1.62	-0.47	-0.68	-3.68	1798
1799	-5.84	-2.08	-0.88	-0.43	-0.45	-1.16	-0.58	1.00	-0.50	0.45	0.58	-2.94	1799
1800	0.74	-0.19	-8.81	5.57	1.90	-1.45	-0.44	1.49	0.27	-0.40	1.57	0.10	1900
1801	1.85	-0.21	2.47	0.80	1.88	-0.85	-1.18	-1.82	1.37	1.94	1.71	0.99	1801
1802	-0.43	-1.84	0.89	0.73	-1.14	1.83	1.02	1.65	0.88	2.10	1.84	1.40	1802
	-2.68	-3.46		2.49	1	-0.75	0.23	0.08		-0.45	1.24	0.27	1803
1803		-0.59		0.05	0.29	-0.10	0.25	-0.51	0.80	0.48	-2.47	-2.40	1804
1804	3.42	70.55	-2.44	0.00	0.25	-0.10	0.20	7.01	0.00	0.40	2.2.	_2.40	1004
1806	-0.48	-1.18	-1.28	-2.16	-1.85	-0.79	-1.26	-1.61	-0.04	-2.89	-2. 19	0.24	1805
1806	4.04	2.12	1.07	-2.07	1.84	-0.02	-0.16	-0.62	0.56	-0.80	1.60	2.48	1806
1807	1.08	1.96	-1.54	-1.18	1.28	-0.84	1.25	4.74	0.17	1.87	1.96	0.46	1807
1808	1.20	-0.51	-4.99	-1.20	1.42	0.15	1.80	1.80	1.18	-0.97	-0.82	-3.68	1808
1809	-0.08	1.54	-1.18	-2. 51	0.89	0.27	0.23	0.79	0.11	-1.81	-0.75	1.67	1809
1810	-0.71	-0.08	2.03	-0.74	0.50	-1.65	0.82	0.15	2.26	-0.18	-0.09	2.01	1810
1811	-8.58	-0.91	2.08		8.12	4.62	2.56	0.99		8.63	1.20	0.19	1811
	-2.13	0.58	0.67		0.65	0.85	l .	-0.52		2.04	-0.84	-3.96	1812
1812		2.07	-0.76	1.56	0.86	-1.82	-1.84	-1.80		-0.37	-0.24	0.68	1813
1813	-1.84		1		-2.19	-1.5Z -1.76		-0.21	-2.45		0.82	2.19	1814
1814	-0.84	-4.87	-0.55	1.54	l		0.66	1	ŀ				1
1815	-1.03	2.39	2.06			0.28		-1.29					1815
1816	1.84					-0.73		-1.89			-0.89		1816
1817	8.24	3.78	0.51		0.53	2.18		-0.25	0.56		1.09	0.16	1817
1818	2.77	0.78	1		-0.11	0.55	ı	-0.71	0.41	0.84	0.60		1818
1819	1.22	2.04	1.94	1.17	-0.75	1.01	0.66	-0.35	0.71	-0.12	0.51	-1.21	1819

LXXXIII.

South Germany. - VIENNA (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De		Keaum						
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1820	-2.47	0.86	-0.86	° 1.78	0	-1.18	-0.96	2.86	-0.71	0.16	-0. 36	-1.49	1820
1821	2.22	-1.56	-0.72	1.57	1	-3.08		-0.76		-0.12	1.93	2.90	1821
1822	2.85	1.63	8.44	1.05	1.21	1.50	1.16	1	0.06	2.12	0.44	-0.27	1822
1823	-4.55	0.68	0.80	-0.29		-0.68	-1.35	0.15		1	0.29	1.35	1823
1824		ł	ì							1.18			
1024	1.77	2.81	0.09	-0.72	-0.74	-0.60	-0.22	-0.58	1.36	0.60	1.56	4.00	1824
1825	3.15	0.50	-1.59	1.02	-0.14	-0.81	-0.72	-0.47	-0.62	-1.71	1.74	3.11	1825
1826	-3.65	-2.12	0.91	-0.12	-2.42	-0.38	1.34	2.06	0.69	0.89	-0.82	1.78	1826
1827	0.69	-2.92	1.61	1.65	1.38	1.19	1.67	-1.06	-0.57	0.82	-3.48	0.88	1827
1828	0.19	-2.22	0.88	1.80	-0.16	0.21	0.63	-1.49	-0.70	-0.82	0.48	1.57	1828
1829	-1.66	-8.79	-1.87	-0.28	-2.26	-2.69	-0.32	-2.62	-0.31	-2.12	-3.62	-6.11	1829
											l	1 1	
1830	-5.81	-3.23	-0.44	ł .	-0.39	0.88	0.02		1	-1.68	0.76		1830
1831	-1.42	0.26	0.48	2.23		-1.86	0.33		-1.96	2.02	1		1831
1832	0.55	0.61	0.04		-1.90	-1.46	-1.29	0.32		0.04		1 1	1832
1833	-3.8 5	2.33	0.24		2.57	1.20	-2.26	-2. 80	-1.22	-0.55	0.23	4.03	1833
1834	4.67	0.32	-0.29	-1.17	2.24	1.65	2.61	1.26	2.85	-0.08	-0.89	1.25	1884
1835	1.71	1.46	0.46	-1.10	0.27	-0.07	0.92	0.19	0.09	-0.76	-8.77	-1.89	1835
1836	-0.08	0.29	8.84		-2.95		-0.48	ł .	1	0.91	ı	1 1	1836
1837	0.20	-2.39	-1.96		-2.57			1			-0.74	1 1	1837
1838	-5.10	-4.14	-0.50		-0.76		-1.89		ŀ	-1.75		-0.84	1838
1839	1.12	0.73	-0.30 -2.31		-0.76 -2.04		1 1	i .	0.23	1.05	ł	0.70	1839
1840		-0.88		-3.85		1.06	0.36			ı	1.55	1 1	l .
	1.08		-3.76				-1.56		1	-2.08	ı	-7.72	1840
1841	0.83	-8.24	0.65	0.93	2.19	-1.02	0.55	-1.10	0.24	2.04	0.28	2.27	1841
Means.	-1.22	0.63	3.85	8.66	13.31	15.72	17.14	16.77	18.25	8.51	8.67	0.39	Means.
							<u>' </u>	<u> </u>		<u>'</u>			'
			LXX	XIV.	Sou	rn G	BRMAI	NY. —	- Rati	SBON.	•		
1773	3.00	-0.28	-0.04	-0.28	0.25	0.84	-1.23	-0.60	0.47	1.20	1.06	2.35	1778
1774	1.63	0.85	2.17	1.97		-0.17			-1.29			-2.82	1774
1775	0.67	2.87	1.18		-8.42	-0.51	-1.91	0.10	-0.73	-2.19		1 1	1775
1776	-3.04	1.19	1.10					::		2.10	0.14	0.04	1776
11110	-9.04	1.15	• •	• •	••	• •	• • •	١	•••	•••	١	١ ١	1
1777	-1.47	-0.68	2.87	-1.29	-0.16	0.28	-1.02	1.24	0.01	1.07	1.81	-1.17	1777
1778	1.88	0.21	0.89	1.98	1.76	0.81	8.20	2.38	-1.33	-0.36	1.36	3.06	1778
1779	-2.51	1.43	2.27	2.89	1.88	-0.84	-0.38	0.95	1.40	2.18	1.47	3.74	1779
1780	-0.83	-1.52	2.87	-0.92	0.87	1.30	0.64	1.65	1.82	1.25	0.25	-0.75	1780
1781			1.52	1.88	0.82	1.52	0.48	2.86	2.45	-1.08	0.58	0.56	1781
1782	0 40	_0.00		0.15		* 00	2.02	-0.28	0.80	-1.67	-2.72	-0.32	1782
11	2.46	-2.98	8.82	8.15	8.74	1.92							
1783	3.48	2.22	-0.95	0.26	0.98	0.92	1.78	0.45	0.18	1.00		-2.88	1788
1784	-4.07	-8.45	-1.69	-2.76	1.67	0.60	0.28	0.34	2.21	-2.46	0.86	-1.21	1784
1785	-1.20	-2.85	-6.49	-4.87	-1.08	-0.83	-1.42	-1.91	2.05	-0.77	0.28	0.10	1785
1786	0.66	0.04	-2.05	1.32	-1.54	1.28	-2.81	-1.85	-1.30	-1.93	-2.68	-0.18	1786
1787	-1.03	4.29	0.75		-2. 51	0.92	-1.31	0.36	0.07	1.78	0.89	2.06	1787
1788	1.86	-0.61	-0.80	-0.59	-0.35	0.88	1.66	i .	1.44	-0.20			1788
1789	-1.93	1.41	-2.90		1.62	-1.30	-0.29	-0.28		0.27	0.25	0.64	1789
1790	1.99	1.73	0.91		1.20		-1.49	-0.08	-0.87	1	-0.26	0.89	1790
1791	3.24	0.14	1.00	1.81	-0.76	-0.35	-0.35	1.14	-0.15	0.50	-2.48	0.84	1791

LXXXIV.

South Gernany. - Ratisbon (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

7					De	grees or							
Year.	Jen.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1792	-0.57	_0.21	0	1.17	-1.12	0.87	0.66	0.88	-1.01	0.05	° 0.17	0.89	1792
1793	-1.17	1.26	0.58	-1.81	-1.23	-0.76	1.56	1.09	1	1.87	0.95	1.26	1793
1794	2.80	3.01	3.05	3.04	1.19	1.69	2.85	-0.80	l	1.24	0.67	-0.78	1794
1795	-5.05	-0.89	-0.10	1.96	-0.82	1.39	-2.22	0.29	1.08	8.11	-0.98	2.26	1795
1796	4.26	1.59	-1.63	1	-0.25	0.03	0.47	0.98	2.24	0.28	ı	-2.04	1796
1797	1.46	1.52	-0.17	2.09	2.60	-0.72	2.14	1.73	0.75	0.06	1.00	1.59	1797
1798	1.88	1.94	0.18	1.02	0.66	1.65	0.50	1.26	1.08	-0.73		-2.69	1798
1799	-5.61	0.14	-0.29	-1.87	-1.87	-0.83	-0.91	-2.86	1	i .	•	-3.81	1799
1800	1.15	-0.63	-2.62	4.66	1.80	-1.42	0.32	1.53	0.43	-0.69	1.30	0.63	1800
1801	2.72	0.10	1.82	0.76	2.45			0.13	1.15	1.60	1.45	0.81	1801
1802	-3.20	-0.90	0.29	0.62	0.16	1.66	-0.04	2.80	0.73	2.40	0.63	0.71	1802
1803	-1.24	-2.05	-0.06	2.70	-1.78	-0.31	1.70	1.81	-0.96	-0.83	0.29	0.93	1803
1804	3.84	-0.86	-1.18	-0.49	1.17	0.88	0.29	-0.14	1.27	1.09	-0.71	-1.68	1804
1805	-1.41	-1.00	-0.34	-1.27	-1.76	-0.88	-0.88	-1.60		-2.03	-1.81	-0.21	1805
1806	4.22	2.45	0.40	-2.24	2.47	0.16	-0.49	0.15	0.86	0.04	1.94	3.5 8	1806
1807	1.19	1.18	-1.17	-1.82	1.24	0.46	2.87	4.63	-0.94	1.58	1.08	1.54	1807
1906	1.08	-0.73	-2.79	-1.98	2.02	-0.45	1.61	1.19	0.83	-1.97	-0.23	-5.46	1808
1809	0.88	2.19	-0.40	-2.92	0.71	-0.25	0.02	0.23	-0.81	-0.76	-0.86	0.93	1809
1810	-1.72	-2.39	0.86	-0.63	-0.05	-1.00	-0.41	0.17	2.72	0.52	0.04	1.89	1810
1811	-2.93	-0.16	2.09	1.48	2.28	2.85	1.75	0.24	0.43	2.24	1.43	-0.25	1811
1812	-1.88	1.05	0.28	-2.87	0.18	-1.15	-2. 18	-1.44	-1.89	0.60	-1.99	-4.72	1812
1813	-3.03	0.99	-1.15	0.46	-0.60	-1.86	-1.78	-2. 10	-1.47	0.50	-0.75	-0.33	1813
1814	-1.37	-4.71	-2.93	0.49	-2.79	-2.39	-0.12	-1.12	-2.45	-1.50	.0.65	1.77	1814
1815	-1.30	1.05	1.18	-0.37	-0.46	-0.74	-2.23	-2.07	-1.85	-0.70	-1.87	-2.26	1815
1816	1.86	-1.83	-1.23	-0.93	-2.69	-2.21	-2.42	-2.56	-2.04	-0.93	-1.49	-0.75	1816
1817	2.51	2.42	-1.14	-5.01	-1.93	0.61	-1.79	-1.89	0.56	-3.22	0.68	-0.70	1817
1818	2.08	0.29	-0.16		-1.72			1		-0.71	0.41	1 1	1818
1819	1.49	0.60	0.64		-0.76		-0.05	1		-0.78	-0.99	-1.34	1819
1820	-2.43	-0.35	-2.26	0.38	-0.47			0.93		-1.22	-1.63	-1.66	1820
1821	1.17	-3.06	-1.51	0.99		-8 .01			1	-0.99	1.51	2.53	1821
1822	2.21	0.63	1.92	0.26	0.58	2.48	0.49	-0.87	-0.56	0.73	0.48	-2.29	1822
1828	-4.17	0.86	0.11	-1.72	0.20	-0.97		0.48	0.38	0.02	-0.61	1.05	1823
1824	0.92	0.38	-1.02	-2.10	-1.74	-1.07	-0.14	-0.51	0.97	-0.26	1.44	8.93	1824
1825	2.80	0.89	-1.05	2.12	0.98	0.56	0.51	0.32	1.81	0.21	8.09	4.15	1825
1826	-8.57	-0.34	1.89	0.17	-1.04	1.05	1.99	8.61	1.61	1.88	-0.28	0.92	1826
1827	0.09	-4.95	1.00	1.81	1.20	1.05	2.06	-0.57	0.98	1.35	-1.80	2.93	1827
1828	2.12	0.27	0.51	0.81	-0.77	0.89	0.85	-2.47	-1.95	−0.20	0.61	2.28	1828
1829	-0.85	-3.13	-1.38	0.20	-1.14	-1.11	-0.20	-2.37	-1.85	-1.41	-3.79	-5.79	1829
1830	-5.9 8	-3.61	1.17	0.77	-0.12	-0.94	0.50	-1.28	-1.05	-0.88	1.14	-0.58	1830
1831	-2.09	-0.82	0.70	3.60	-0.48	-1.86	-0.09	-0.12	-1.57	2.40	2.27	0.26	1831
1832	0.77	1.28	0.09	0.21	-2.45	-0.87		0.59		0.16	-0.71	0.25	1832
1833	-3.05	8.32	0.21	-1.45	2.29	1.06	-1.70	-3.06	-2.01	-0.90	2.78	3.95	1833
1884	5.52	-0.48	-0.25	-1.69	0.99	0.44	4.89	2.48	1.21	0.50	0.74	1.86	1834
Means.	-2.42	-0.09	3.09	7.55	11.94	13.72	14.88	14.62	11.69	7.11	2.22	-0.71	Means.

LXXXV.

South Germany. - Stuttgard.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Resumur.

Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1792	0.64	。 -1.28	° 1.78	0	0	-0.30	1.04	0	_0.70	0	-0.73	0.44	1792
1793	-1.41	1.64	0.37				2.52		-0.84				
1794	2.02	3.72	2.76	8.26	0.41	1.80	2.75	0.12	!	1.71 0.32	0.66 0.85	2.10	1798 1794
1795	-4.88	0.86	0.65	2.81	0.64	1.48	-1.01	1.33	1.93	8.69	1	-1.72 8.76	1795
1796	6.17	1.90		3	t .	ı	-0.86	0.23	2.84				
1790	0.17	1.90	-2.51	-0.67	-0.52	0.10	~0.80	0.28	Z.84	0.18	-0.87	-2.18	1796
1797	2.46	0.08		1.88		-1.80	2.86	1.01	1.04	0.86	1.82	8.02	1797
1798	0.65	1.44	ŀ	1.16	0.66	1.21	0.14	0.66	1.36	0.58	0.88	-2.05	1798
1799	-8.46	1.77	ı	-1.80	-0.89	-0.75	l	0.82	1	-0.15	0.42	-4.70	1799
1800	3.03	-0.92	-2.04	4.56	2.03	-1.81	0.00	0.79	0.84	-0.87	1.61	-0.18	1800
1801	8.95	0.97	1.98	0.24	0.94	-0.54	0.91	1.42	2.32	2.89	1.80	1.46	1801
1802	-2.5 5	-0.02	0.80	2.13	0.28	1.58	-0.24	2.22	0.62	2.08	0.81	1.41	1802
1803	-0.81	-1.90	-1.31	1.49	-2.28	0.05	1.21	1.28	-1.78	-0.90	0.46	1.86	1803
1804	4.61	-0.98	-1.05	-0.22	0.78	0.92	-0.85	-0.66	2.88	0.74	0.56	-1.56	1804
1805	-1.03	-0.28	-0.60	-1.38	-2.16	-1.85	-1.28	-1.44	0.88	-2.73	-2.47	0.06	1805
1806	-2.78	2.77	1.10	-1.99	1.87	-0.27	-0.62	-0.59	-0.27	0.03	1.67	4.85	1806
1807	0.76	1.58	-2.48	-1.14	-1.02	-0.21	2.15	8.28	-0.74	1.71	1.87	-0.94	1807
1808	1.95	-1.28	l	I	l .	-0.98	0.54				-0.17		1808
1809	1.56	8.64	0.69		l .	-0.65				-1.05			1809
1810	-1.56	-2.45	2.11		1	1	1)	2.08	0.09	1.44	0.97	1810
1811	-3.01	0.49	2.81	0.97	1.41	1	0.75			3.02		-0.04	1811
1812	-2.36	1 96	-0.23	-3.17	0.64	0.87	-1.85	-1.17	_0.40	0.01	-2.28	_4.81	1812
1813	-2.25	0.28	1	0.53		-1.45	ı		-1.63	ı	1	-0.70	1813
1814	-1.96		1		t .	-1.52	1		-1.56				1814
1815	-1.92	1.26	1	1	1	-0.42	1	ì	l	1	1	-1.44	1815
1816	0.69		-0.60			-2.68	1				-2.45		1816
	0.01					0.00						0.40	1015
1817	8.31	1.47					i	-0.97		-8.25	1.62	-0.49 2.04	1817 1818
1818	2.67	0.40	0.41	1.38	1	4	0.15	ı	-0.70 -0.92	1			1818
1819	-0.61	1.54	0.89	1.21	0.29		1.02			i	1	_	1
1820 1821	-1.64 2.13	-0.06 -2.72	-2.16 0.19	•	-0.05	-1.91 -2.26	-1.37	1.10 0.15		-1.11 -0.62	-2.81 2.42	-0.66 3.25	1820 1821
1021	2.13	-2.12	0.15	1.02	-1.50	-2.20	-1.57	0.15	0.77	-U.UA	2.42	8.25	1021
1822	2.11	1.58	2.61	0.51	1.48		0.08	1	-0.48	1.88	1.82		1822
1828	-2.76		-0.05		1		-1.19		ı	ì	i	1.70	1828
1824	0.79	0.79)	0.80	ł	0.68	0.44	l		1324
1825	1.92	-0.87		1.85	0.27		0.19	0.02		-0.64		2.74	1825
1826	-4.81	1.06	1.16	0.19	-0.98	0.54	1.70	1.78	1.51	1.48	-1.07	0.54	1826
1827	-0.49	-5.36	1.47	1		4	_	-0.45			-2.41	2.98	1827
1828	3.10	-0.35	0.61	0.54	0.43	0.97		-1.10			-0.17	1.19	1828
1829	-2.45	-8.10	-0.58	0.46	-0.86	-0.61	0.45	-1.13	-1.50	-1.66	-2.88	-5.91	1829

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LXXXV.

South Germany. - Stuttgard (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Resumur.

Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Your.
1830	° 40	0 47	0	2.06	0 00	0	1.05	0 00	0	-0.89	0 00	-0.74	1830
		-8.47				-0.88						1	
1831	-0.78				1	-0.09		-0.10	1	l			1831
1832			-0.64		l .	-0.59	1	1			-1.41		1832
1833	-2.56		-0.99				I	-2. 81			1		1833
1884	5.05	0.14	−0.60	-1.87	2.16	1.83	2.74	0.90	1.73	-0.06	0.12	-0.27	1834
	1				l	i	ł	l	l	l	l I		
1885	1.58	1.20	-0.15	-0.90	-0.58	0.28	1.62	-0.21	0.60	-1.20	-3.22	-2.85	1835
1836	0.45	-1.27	3.18	-0.90	-2.14	0.64	0.22	0.46	-1.21	0,47	-0.01	1.04	1836
1837	0.90	0.24	-2.68	-2.84	-2.28	1.16	-1.19	1.17	-1.94	-0.60	-0.40	0.04	1837
1838	-4.48	-2.08	0.21	-2.32	-0.45	-0.03	-0.36	-0.90	0.64	-0.36	1.03	-1.84	1838
1889	0.78	-0.03	-1.81	-2.71	-1.07	2.80	0.58	-1.55	0.64	0.84	1.07	1.95	1839
1000							0.00	-:	0.01	5.55			
	[1						[]			1	
1940	1.82	0.15	-2.90	1.36	0.29	0.16	-1.42	-0.23	-0.26	-2.89	1.10	-5. 61	1840
1841	0.89	-1.98	2.09	0.58	3.42	-1.55	-1.83	-0.69	1.65	1.24	1.22	2.85	1841
1842	-1.50	-1.05	1.36	-0.47	1.35	1.74	0.35	2.64	0.07	-2.47	-1.82	-0.20	1842
1848	2.07	1.54	0.15	0.60	-1.06	-1.48	-0.68	0.20	-0.15	0.02	0.67	0.23	1843
1844	0.31	-0.91	-0.30	1.42	-1.01	1.39	-1.99	-2.17	0.56	0.39	0.91	-8.18	1844
!													
Means.	-0.80	1.64	3.97	7.80	11.87	14.03	15.48	15.02	12.05	8.05	4.11	1.25	Means.

LXXXVI. South Germany - Carlsruhe.

1780 -2.23 -2.20 8.27 -1.17 0.52 0.41 0.27 1.39 0.18 0.83 0.00 -1.32 177 1781 0.45 1.82 0.99 2.26 0.87 1.63 0.63 1.20 1.11 -0.94 -0.38 1.09 178 1782 8.13 -3.95 -0.67 -1.10 -1.44 0.93 1.00 -1.62 -1.69 -2.08 -3.90 -1.07 178 1783 -3.33 1.35 -1.60 0.05 -0.14 0.47 1.69 -0.88 -0.71 -0.85 -1.04 -3.26 178 1784 -4.85 -8.17 -1.67 -2.72 0.42 -0.13 -0.48 -1.97 -0.63 -8.71 -0.71 -2.14 178 1785 -0.27 -8.06 -5.49 -3.26 -1.28 -0.44 -0.46 -0.63 -0.60 178 1786														
1781 0.45 1.82 0.99 2.26 0.87 1.63 0.63 1.20 1.11 -0.94 -0.38 1.09 178 1782 3.13 -3.95 -0.67 -1.10 -1.44 0.93 1.00 -1.62 -1.69 -2.08 -3.90 -1.07 178 1783 3.33 1.35 -1.60 0.05 -0.14 0.47 1.69 -0.38 -0.71 -0.35 -1.04 -3.26 176 1784 -4.85 -8.17 -1.67 -2.72 0.42 -0.13 -0.48 -1.97 -0.63 -8.71 -0.71 -2.14 178 1785 -0.27 -3.06 -5.49 -3.26 -1.28 -0.44 -0.46 . . . -0.63 -0.60 178 1786 . . . 0.76 -1.35 1.20 -1.77 . . -1.97 -3.18 -0.18 178 1798 	1779	-3.98	1.18	1.26	2.19	1.14	-0.64	0.80	1.72	2.40	2.75	1.71	2.94	1779
1782 8.13 -8.95 -0.67 -1.10 -1.44 0.98 1.00 -1.62 -1.69 -2.08 -8.90 -1.07 178 1783 1.35 -1.60 0.05 -0.14 0.47 1.69 -0.38 -0.71 -0.35 -1.04 -3.26 178 1784 -4.85 -8.17 -1.67 -2.72 0.42 -0.13 -0.48 -1.97 -0.63 -8.71 -0.71 -2.14 178 1785 -0.27 -3.06 -5.49 -3.26 -1.28 -0.44 -0.46 . . . -0.63 -0.60 178 1786 . . . 0.76 -1.35 1.20 -1.77 . . -0.63 -0.60 128 1789 -0.91 1.74 -3.16 . 2.19 -1.49 0.34 -0.14 -1.17 . . . -8.65 178 1799 -3.09 0.92 -0.59 -1.15 -1.43 -0.70 -0.60 0.20 0.01 0.12 -0.12	1780	-2.23	-2.20	8.27	-1.17	0.52	0.41	0.27	1.89	0.18	0.88	0.00	-1.32	1780
1783 3.33 1.35 -1.60 0.05 -0.14 0.47 1.69 -0.38 -0.71 -0.35 -1.04 -3.26 176 1784 -4.85 -8.17 -1.67 -2.72 0.42 -0.13 -0.48 -1.97 -0.63 -8.71 -0.71 -2.14 177 1785 -0.27 -3.06 -5.49 -3.26 -1.28 -0.44 -0.46 . . . -0.63 -0.60 178 1786 . . . 0.76 -1.35 1.20 -1.77 . . -1.97 -3.18 -0.18 178 1789 .	1781	0.45	1.82	0.99	2.26	0.87	1.63	0.63	1.20	1.11	-0.94	-0.38	1.09	1781
1784 -4.85 -8.17 -1.67 -2.72 0.42 -0.13 -0.48 -1.97 -0.63 -8.71 -0.71 -2.14 178 1785 -0.27 -3.06 -5.49 -3.26 -1.28 -0.44 -0.46 . . . -0.63 -0.60 178 1786 .	1782	8.13	-3.9 5	-0.67	-1.10	-1.44	0.98	1.00	-1.62	-1.69	-2.08	-3.90	-1.07	1782
1785 -0.27 -8.06 -5.49 -3.26 -1.28 -0.44 -0.46 -0.63 -0.60 177 1786 -1.97 -3.18 -0.18 178 1788	1788	8.33	1.85	-1.60	0.05	-0.14	0.47	1.69	-0.88	-0.71	-0.85	-1.04	-3.26	1783
1785 -0.27 -8.06 -5.49 -3.26 -1.28 -0.44 -0.46	1004		- 0 16	_1 60		Λ 40	10	_ 40	_1 07	A 60	_ ~.		-0.74	1004
1786		11		l				ı			ł .			
1738		ll .)		l .		I 1		1			
1789 -0.91 1.74 -3.15 . 2.19 -1.49 0.34 -0.14 -1.17 . . 0.91 178 1798 .		'		1										ľ
1798		11						-	l .					
1799 -3.09 0.92 -0.59 -1.15 -1.43 -0.70 -0.60 0.20 0.01 0.12 -0.12 -4.22 179 1800 2.53 -1.60 -2.25 3.40 1.46 -2.10 -0.26 1.20 0.89 -0.43 1.15 0.21 180 1801 3.13 0.68 1.95 0.32 0.98 -0.15 -0.49 0.76 0.98 1.17 2.21 180 1802 -2.69 0.64 0.83 1.08 -0.60 1.37 -0.97 2.33 0.23 1.38 -0.38 0.53 180 1803 -1.27 -2.92 -1.30 1.11 -2.75 -0.71 0.63 0.54 -2.87 -0.90 0.52 1.99 180 1804 4.53 -1.30 -1.12 -0.47 0.94 0.96 -0.56 -0.70 0.10 0.90 0.08 -2.05 180 1805 -1.49 -0.61 -0.70 -0.89 -1.66 -0.76 -1.21 -1.17 0.16 -2.18 -2.92 -0.39 180	1759	70.91	1.74	-3.15	''	2.19	-1.49	0.54	-0.14	-1.17	' '	٠.	0.91	1109
1800 2.53 -1.60 -2.25 8.40 1.46 -2.10 -0.26 1.20 0.89 -0.43 1.15 0.21 180 1801 3.13 0.68 1.95 0.32 0.98 -0.98 -0.15 -0.49 0.76 0.98 1.17 2.21 180 1802 -2.69 0.64 0.83 1.08 -0.60 1.37 -0.97 2.33 0.23 1.38 -0.38 0.53 180 1803 -1.27 -2.92 -1.30 1.11 -2.75 -0.71 0.63 0.54 -2.87 -0.90 0.52 1.99 180 1804 4.53 -1.30 -1.12 -0.47 0.94 0.96 -0.56 -0.70 0.10 0.90 0.08 -2.05 180 1805 -1.49 -0.61 -0.70 -0.89 -1.66 -0.76 -1.21 -1.17 0.16 -2.18 -2.92 -0.39 180	1798					••		0.20	0.39	0.59	0.55	0.14	-1.90	1798
1801 3.13 0.68 1.95 0.32 0.98 -0.15 -0.49 0.76 0.98 1.17 2.21 180 1802 -2.69 0.64 0.83 1.08 -0.60 1.37 -0.97 2.33 0.23 1.38 -0.38 0.53 180 1803 -1.27 -2.92 -1.30 1.11 -2.75 -0.71 0.63 0.54 -2.87 -0.90 0.52 1.99 180 1804 4.53 -1.30 -1.12 -0.47 0.94 0.96 -0.56 -0.70 0.10 0.90 0.08 -2.05 180 1805 -1.49 -0.61 -0.70 -0.89 -1.66 -0.76 -1.21 -1.17 0.16 -2.18 -2.92 -0.39 180	1799	-3.09	0.92	-0.59	-1.15	-1.48	-0.70	-0.60	0.20	0.01	0.12	-0.12	-4.22	1799
1802 -2.69 0.64 0.88 1.08 -0.60 1.37 -0.97 2.33 0.23 1.38 -0.38 0.53 180 1803 -1.27 -2.92 -1.30 1.11 -2.75 -0.71 0.63 0.54 -2.87 -0.90 0.52 1.99 180 1804 4.53 -1.30 -1.12 -0.47 0.94 0.96 -0.56 -0.70 0.10 0.90 0.08 -2.05 180 1805 -1.49 -0.61 -0.70 -0.89 -1.66 -0.76 -1.21 -1.17 0.16 -2.18 -2.92 -0.39 180	1800	2.58	-1.60	-2.25	8.40	1.46	-2.10	-0.26	1.20	0.89	-0.48	-1.15	0.21	1800
1803 -1.27 -2.92 -1.80 1.11 -2.75 -0.71 0.63 0.54 -2.87 -0.90 0.52 1.99 1804 4.53 -1.30 -1.12 -0.47 0.94 0.96 -0.56 -0.70 0.10 0.90 0.08 -2.05 1805 -1.49 -0.61 -0.70 -0.89 -1.66 -0.76 -1.21 -1.17 0.16 -2.18 -2.92 -0.89 1806 -2.18 -2.92 -0.89 1806 -2.18 -2.92 -0.89 1806 -2.18 -2.92 -0.89 -2.18 -2.92 -0.89 -2.18 -2.92 -0.89 1806 -2.18 -2.18 -2.92 -0.89 1806 -2.18 -2	1801	3.18	0.68	1.95	0.32	0.98	-0.98	-0.15	-0.49	0.76	0.98	1.17	2.21	1801
1804 4.58 -1.30 -1.12 -0.47 0.94 0.96 -0.56 -0.70 0.10 0.90 0.08 -2.05 180 1805 -1.49 -0.61 -0.70 -0.89 -1.66 -0.76 -1.21 -1.17 0.16 -2.18 -2.92 -0.39 180 -2.05 180 -2.05 -2.05 180 -2.05	1802	-2.69	0.64	0.88	1.08	-0.6 0	1.87	-0.97	2.33	0.28	1.38	-0.3 8	0.53	1802
1804 4.58 -1.30 -1.12 -0.47 0.94 0.96 -0.56 -0.70 0.10 0.90 0.08 -2.05 180 1805 -1.49 -0.61 -0.70 -0.89 -1.66 -0.76 -1.21 -1.17 0.16 -2.18 -2.92 -0.39 180 -2.05 180 -2.05 -2.05 180 -2.05	1909	_1 97	_2 09	_1 90	, ,,	_9 75	_0.71	0.69	0.64	_9 97	00	0.52	1 90	1803
1805 -1.49 -0.61 -0.70 -0.89 -1.66 -0.76 -1.21 -1.17 0.16 -2.18 -2.92 -0.89 180		11					ı	1		l .	i e			1804
		11									ı		1 1	
	1806	4.11	1.89			1		l						1806

LXXXVI.

South Gernany. — Carlsruhe (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year
	0 00	0	0	•	•	0 00	0	0	•	0	0	0	
1807	0.02		-2.88		i i	-0.28	2.84	1	-1.57	. 1.80	1.21		180
1808	1.88	-1.25		-1.63	1	-0.41	1.94	l	-0.54				180
1809	1.24	3.25		-3 .16		-1. 2 2		I	0.80	-1.86	1		180
1810	-3.19	-2.7 8	1	-0.17		-0.62	l	-0.46	ı	-0.05	0.84		181
1811	-2.40	1.17	2.79	1.65	2.82	1.55	0.78	-0.29	0.53	2.92	1.21	0.48	181
1812	-2.09	1.47	-0.16	-2.96	0.83	-0.50	-1.58	-0.27	-0.24	1.38	-1.42	-3.80	181
1813	-0.84	2.15	0.57	1.50	0.12	-1.01	-1.75	-1.78	-1.15	0.27	-0.11	-0.89	181
1814	-1.51	-3.24	-1.56	1.82	-1.68	-1.66	0.07	-1.12	-1.07	-0.68	0.82	2.67	181
1815	-2.35	2.31	2.67	0.75	1.10	-0.57	-1.75	-1.03	0.09	0.62	-1.99	-1.02	181
1816	1.38	-2.00	-0.27	0.27	-2.23	-2.48	-2.61	-2.16	-0.89	-0.88	-2.14	0.17	181
1817	8.56	2.16	-0.36	-8.14	-1.63	0.87	-1.47	-1.40	1.60	-2.82	1.78	0.13	181
1818	2.91	1.12	0.59		-1.44	1.00		1	-0.50	-0.63	1.49	-2.11	181
1819	1.85	1.30	0.75	1.42	0.49	0.15	0.42	0.64	0.49	-0.15	-0.75	0.31	181
1820	-1.09	0.55	-1.35	2.19	0.22	-2.16	-0.96	0.66	-1.20	-0.61	-1.80	0.00	182
1821	2.31	-1.59	0.78	1.78	-1.87	-2.01	-2.03	0.14	0.17	-0.68	2.72	3.52	182
1822	2.52	2.96	4.04	1.75	2.11	3.77	0.56	-0.14	0.46	1.19	2.66	-1.31	182
1823	-2.23	2.20		-0.09		-1.02	-1.14		0.24		-0.11	2.95	182
1824	1.39	1.98		-0.89			0.82		1.04	0.66	2.68	4.09	182
1825	1.92	0.28	-0.76		-0.15	1	0.85		1.15	0.15	1.51	8.05	182
1826	-8.48	1.85		0.20		1.06	2.12		1.75		-0.21	0.93	182
1827	-0.55	-5.10	1.19	1.50	1.25	1.01	2.06	0.00	1.15	1.84	-2 .01	2.85	182
1828	3.18	0.41	1.17	0.82	0.74			-1.22		0.28	-0.33		182
1829	-2.12	-2.83	-0.05		-0.04			-1.17		-0.60		• •	182
1830	-5.88	-2.98	2.14	2.21	1 1	-0.22		-0.18	1	-0.17	1.31		188
1831	-0.98	0.96	1.68		-0.50		0.88		-0.81	3.26	0.80	1.64	183
1832	0.10	-0.27	0.23	0.96	0.88	_0.49	-0.01	1.02	-0.59	0.18	-0.6 8	0.95	183
1883	-2.63	8.41		-0.78	2.94	1.45		-2.23		-0.17	0.51	4.43	183
1834	5.74	0.29		-1.12	1.87	1.12	2.76		1	0.58	0.79	0.29	188
1835	1.77	1.74		-0.90	-0.68	0.18			-0.03	-0.83	-2.92	-2.28	188
1836	0.43	-0.85	_	-0.66	-1.99	0.47	0.21	0.47	1.67	0.82	0.66	1.56	1836
1837	1.30	0.80	_1.86	-2.83	-2 .05	1.98	-0.86	1.94	-1.66	0.28	0.46	0.72	183
1838	-4.35	-2.13	0.21	-2.86		,	-0.36	-1.20	0.44	-0.02		-0.52	188
1839	0.88	0.67	-0.78	-2.24		2.28	0.16	-0.47	0.09	1.20	1.10		183
1840	1.37	-0.69	-2.82	1.28	-0.51	0.23	-1.39	0.84		-2.04	1.45		184
Means.	-0.17	1.95	4.89	8.31	12.40	14.43	15.80	15.41	12.60	8.80	4.16	1.85	Mean
													•

LXXXVII.

NORTH GERMANY. - BERLIN.

Yor Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year.	Jen.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1719	2.44	0.21	1.50	0.69	0	2.38	3.18	1.86	0.08	0.66	2.09	° -1.02	1719
1720	2.27	0.40		0.70	1.84	0.94			0.10		-0.08	1.47	1720
1721	2.38	-1.80		2.28	-0.91	1.21	1		0.54	0.40	1		1721
1728	1.50	-2.28	2.89	0.65	1.24	0.26		-1.36	l .	0.66	l .		1728
1729	-8.18		-8.57	-2.11	•••	• •							1729
							' '	••	' '		• •	'	
1780	1.64	0.20	0.29	0.70	0.00	0.12	-0.62	-0.08	-0.69	-2.55	1.99	-0.48	1730
1781	-2.00	-1.78	-0.67	-1.67			ł	1	-0.25	1.85			1781
1782	-1.50	1.84	1.05	1.84			-1.95	1	1	1.14			1732
1783	2.69	2.54	0.86			1	1		-2.02	-0.58	•		1788
1784	0.40	2.51	1.86		-0.54		ı	ı	ı		-2.85		1784
1785	1.79	0.80	1.81	1.49	-0.87	-0.83	-1.88	-0.84	0.91	-1.01	-1.07	-0.17	1785
1786	-0.08	-0.92			-0.88		•	l .	-0.98	1	-0.09		1736
1787	1.88	0.55		-1.86			(l .	-0.10	ľ			1737
1738	-0.55	0.55	1.11		-0.08			I .		ŀ	-2.21		1738
1789	-0.17	2.06		-1.65	1	-0.96	1	l	I		-5.85		1739
								1					
1740	-6.61	-6.54	-8.28	-8.45	-8.49	-1.70	-0.96	-0.62	1.62	-8.12	-2.35	-0.18	1740
1741	-0.93		-0.71					1	-0.20	1.22		-0.16	1741
1742	-1.23		-0.99		-1.88		ľ	L	l	0.19	ı	-3.22	1
1748	1.82		-0.58			1.05		1		-1.44			
1744		l	-0.09	2.88		-1.47		-0.60	ı	2.10	ì	-0.39	1644
			0.00		3123		1	""	""		1.20	0.00	
1745	-1.92	-1.26	-0.10	0.20	0.78	1.01	0.01	0.17	0.10	1.15	2.17	-2.86	1745
1746	0.12		-1.88	-0.89	0.48	-0.72	i .	1			I		1746
1747	-0.17		-2.09	0.70	-0.67	2.34	-0.33	0.18	1.48	0.48	l		1747
1748	-1.17		-2.29	0.22	1.58	2.11	0.56	2.85	-0.14	0.00	l	1	1748
1749	2.28		-1.52		1.58	0.21	0.89	1.64	0.83	0.05		1.28	1749
1750	1.19	8.22	8.87	1.26	0.80	1.06	1.97	1.56	0.26	-0.55		-0.06	1750
1751	-0.45	-1.70		-0.86	3.59	2.89	1.78	8.12	0.42	-0.04			1751
Means.	-0.19	0.69	2.65	6.51	10.68	12.82	14.02	18.14	11.06	6.53	8.15	1.24	Means.
ļ													
1755	-4.56	-6.47		0.54			 	-0.25			١	2.14	1755
1756	4.18	2.68	1	1.77	0.87	2.55	1.50	-0.85	1.61	1.62	-0.88		1756
1757	1.17	2.87	1.71		-0.39	1.47	8.25	i .	-1.70	-2.88	1.21		1757
1758	-2.57	-0.17	0.18	-0.21	1.08	0.18		0.55	i				1758
1759	8.26	1.79	1.18	-0.01	-1.45	0.87	1.15	0.60	-0.45	1.09	-2.21	-8.85	1759
									l				
1760	-0.56	-1.48	-0.81	0.84	0.88	0.57	-0.29	0.08	0.87	0.98	0.12	2.05	1760
1761	0.97	1.65		-0.01	1.55	1.95	-0.62	1.88	2.80	-1.02	-0.12		1761
1762	2.11	-0.01		1.88	0.42	0.27		-1.45	i	-1.84	1		1762
1768	-2.25	8.02	1 - 1	-0.55	-0.84	0.17	}	1.32			-0.25		1763
1764	2.91	2.89		-0.80		-1.94	•		-1.70				1764
											/-		
1765	1.64	-2.90	1.70	0.78	-2.50	-0.88	-1.92	1.12	-1.16	1.20	0.15	0.08	1765
1766	-0.10	-0.12	1.01	2.07	1.17	0.30	-0.86		0.78	-0.43		-0.26	1766
1767	-5.54	1.74	0.01	-1.58	-1.03		1	•		0.95		-1.75	1767

LXXXVII.

NORTH GERMANY. - BERLIN (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1768	-8.52	-0.98	。 -1.28	_0°.11	-0.68	-0.06	o 0.28	_0.0s	-1.08	-0.48	o 0.54	0.47	1768
1769	1.22	-0.74	0.75	0.14		-1.01	1	-1.07		-2.26	0.26	0.84	1769
1770	-0.20	1	-8.16			-1.20		-0.08	0.62	0.81	0.16	1.92	1770
1771	-1.24	-3.28	-3.40			-0.21	1	-2.12		0.76	ı	0.95	1771
1772	0.66	1.20	0.86				-1.40		0.60	1.62	ı	1.88	1772
1773		l .		0.49		-1.22	1	0.06			-0.92	2.21	1778
	2.00			0.40				0.00	0.01	1.00	0.52	2.21	1110
Means.	-0.13	1.64	8.87	7.71	11.94	15.23	16.18	15.84	12.12	7.73	4.38	1.85	Means.
1774	1.50	2.26	2.29	1.56	-0.05	0.69	-1.56	-1.92	-1.61	0.71	-3.7 0	-0.75	1774
1775	0.95	8.20	2.53	-0.65	-0.72	3.26	1.88	1.61	2.00	1.23	-0.84	2.16	1775
1776	-5.55	2.42	2.10	-0.13	-2.11	1.19	1.21	0.82	0.12	-0.47	0.70	0.54	1776
1777	0.04	-1.67	0.67	-1.12	0.52	0.04	-0.60	-0.01	-1.71	0.23	2.23	0.75	1777
1778	-0.58	-1.72	1.09	1.98	0.67	0.30	1.02	0.66	-0.67	−1.6 9	1.44	3.84	1778
1779	0.83	3.82	2.99	2.89	0.61	-0.80	0.74	1.71	1.59	1.95	0.90	2.26	1779
1780	-1.06	-2.02	3.37	-1.27	0.72	0.24	0.45	0.99	-0.03	1.46		-0.70	1780
1781	-0.44	0.53	2.05	1.85	1.19	1.97	2.02	2.56	1.60	-0.89	0.80	0.01	1781
1782	3.15	-2.86	-0.39	-0.87	0.38	1.78	1.52	0.21	1.75	-0.80		0.78	1782
1788	3.19	3.67	-0.58	0.86	1.88	2.71	1.45	0.71	0.86	0.84			1788
	5.25	5.51		0.00	2.00		2.10	0.,1	5.55		0.00	1.02	1100
1784	-3.97	-8.54	-1.68	-2.80	0.58	0.20	-0.75	-1.85	0.02	-2.21	1.29	-0.94	1784
1785	0.47	-3.28	-5.74	-2.54	-1.48	-0.84	-0.70	-1.12	0.61		1.09	-1.42	1785
1786	1.81	-0.93	-2.82	1.60	-1.25	1	-1.71			-1.97		-0.16	1786
1787	-0.29	1.88	2.05	-1.81		0.99	-0.65	-0.59	-0.17	1.32	0.69	2.07	1787
1788	2.46	-1.26	-1.47	0.10	0.45	1.64	1.64	-1.21	1.20				1788
		1.20		0.20	0.10		1.01		2.20	0.00		0.01	1100
1789	-1.93	1.46	-4.45	0.01	1.85	0.14	0.11	0.36	1.85	0.64	0.89	3.55	1789
1790	8.05	2.82	2.19	-1.67	1.70	0.58	-1.18	-0.54	-0.48	-0.44	-0.80	1.92	1790
1791	8.91	1.52	1.47	1.74	-1.16	0.19	0.78	1.08	-0.78	0.22	-0.89	1.33	1791
1792	0.53	-1.89	0.80	1.45	-0.81	0.83	1.59	0.46	-0.98	-0.80	-0.01	1.14	1792
1798	-0.70	2.14	0.61	-0.68	-0.58	-1.84	1.68	0.22	-0.83	1.99	0.99	2.05	1798
1794	1.18	2.56	8.66	8.12	0.18	1.77	2.79	-0.59	-1.62	0.87	1.58	-2.14	1794
1795	-5.23	-0.86	-0.84		-1.78	2.10		-0.87	1.27	8.86	0.10	3.14	1795
1796	6.51	0.68	-1.70	-0.84	-0.46	0.88	0.48	1.33	1.74	0.07		-1.82	1796
1797	1.60	1.89	0.66	1.09	1.41	-0.28	1.55	1.26	2.02		-0.80	1.81	1797
1798	1.79	1.57	-0.07	1.29	0.76	1.20	0.88	0.92	1.24	-0.17		-3.54	1798
												l (
1799	-2.97	-4.47					-1.05			-0.70	0.48	-4.41	1799
1800	-1.12	-8.61	-4.09	4.48	2.83			0.22	0.67	-0.41	1.47	0.00	1800
1801	1.88	-1.02	1.84	0.05		-1.87		-0.68	1.01	1.40	0.93	0.84	1801
1802	-1.00	0.50	1.65	0.45			-1.54	1.54	-0.08	8.04	0.78	1.81	1802
1803	-5.33	2.02	-0.16	2.84	-1.8 6	-1.46	2.03	1.80	-1.82	-0.45	0.68	-0.89	1808
1804	1.51	-1.48	-8.11	-1.06	1.04	-0.54	0.10	-0.73	1.17	-0.02	-2.40	-3.92	1804
1806	-8.90	-1.94	-0.48	-1.58	1.86	-1.53	-1.18	-1.83	0.55	-8.53	-2.58	1.24	1805
1806	8.02	0.94	0.19	-2.82	0.99	-2.26	-1.85	-0.98	0.41	-0.12	1.47	4.14	1806
1807	1.62	0.18	-1.97	-1.43	-0.42	-1.50	0.42	8.72	-2.15	0.08	1.11	1.53	1807
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LXXXVII.

NORTH GERMANY. - BERLIN (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year. 1808 1809 1810 1811 1812 1813	0.83 -8.81 -0.99 -2.93 -1.14 -1.20 -2.12 -2.81	1.64 -1.66 -0.72 -0.27	-1.09	-2.80 -8.84 -1.41 -0.15		June. -0.42 -0.89 -1.98		Aug. 0.69	Sept. -0.54	Oct.	Nov. -0 -1.10	Dec.	Year.
1809 1810 1811 1812	-8.81 -0.99 -2.98 -1.14 -1.20 -2.12	1.64 -1.66 -0.72 -0.27	-3.89 -1.09 0.40 2.01	-2.80 -8.84 -1.41 -0.15	0.80 0.99 -1.88	-0.42 -0.89	1.19			o -1.56			1900
1809 1810 1811 1812	-8.81 -0.99 -2.98 -1.14 -1.20 -2.12	1.64 -1.66 -0.72 -0.27	-1.09 0.40 2.01	-8.84 -1.41 -0.15	0.99 -1.88	-0.89							1000
1810 1811 1812 1818	-0.99 -2.98 -1.14 -1.20 -2.12	-1.66 -0.72 -0.27 2.88	0.40 2.01	-1.41 -0.15	-1.88			0.86	t	-0.99	0.02	2.28	1809
1811 1812 1818	-2.98 -1.14 -1.20 -2.12	-0.72 -0.27 2.88	2.01	-0.15			4					1.22	
1812 1818	-1.14 -1.20 -2.12	-0.27 2.88	1			ŀ	t .			-1.88			1810
1818	-1. 2 0 -2.12	2.88	-1.05	-A 04		2.67		-0.59		2.21	0.85	1.50	1811
11 11	-2.12			9.90	-1.20	-0.08	-2.87	-0.78	-1.51	1.14	-1.57	-5.52	1812
11 11	-2.12		0.24	1.00	-0.73	-1.28	-1.27	-2.07	-0.82	-1.80	0.05	1.02	1813
		-5.52	-2.78			-1.99	l .	1	-2.23			1.26	1814
1815	-2.01	1.14	1.56		-0.15	0.61	1	-1.57		0.42		1 1	1815
1816	0.95	-2.27			l				1				
rı 11		1	-0.68		-2.68		-1.82		í		i i		1816
1817	2.58	1.79	-0.19	-8.86	-0.49	1.04	-1.57	-0.00	1.43	-2.57	2.37	-0.14	1817
1818	2.54	0.19	1.56	0.58	0.22	0.95	0.72	-1.41	0.14	-0.58	-0.60	-0.89	1818
1819	2.51	1.57	1.59	0.85	1.00	2.28	1.42	1.60	0.81	-0.41	-0.66	-2.61	1819
1820	-8.08	0.84	-0.02	1.52	0.91	-2.88	-2.08	1.23	-0.75	0.99	-1.57	-1.88	1820
1821	1.52	-1.05	0.14			1	-1.51	ì		1.88		8.44	1821
Means.	-1.59	0.80	2.28	6.89	11.86	18.78	15.16	15.00	11.88	7.16	2.61	-0.82	Means.
					0.50								7000
1822	8.89	8.67	8.22	1			1	-0.19		1.86	1.58	1 1	1822
1828	-7.56	-0.25	0.41				-1.76		-0.84	0.66	1.01	1.12	1823
1824	8.67	2.45	0.29			1	-0.56			0.56	1.96	2.69	1824
1825	8.92	0.92	-2.26	0.86	-0.15	-1.10	-0.47	0.05	0.54	-0.12	1.30	2.03	1825
1826	-3.44	1.98	1.15	-0.19	-0.24	1.20	8.03	8.00	0.35	0.71	-0.33	0.49	1826
1827	0.25	-4.90	1.25	2.29	1.98	1.33	0.80	-0.04	1.09	0.83	-2.24	1.16	1827
1828	-0.26	-0.55	0.67	1.22	0.38	0.30	1.17	-0.71	-0.15	-0.28	0.17	0.47	1828
1829	-2.87	-2.67	-1.28	0.41	-0.29	0.12	0.41			-1.62	-2.54	-8.25	1829
1880	-4.21	-2.70	1.09	1.58	0.80	0.07	0.35		1	-0.69	1.47	1 1	1830
1881	-1.81	0.75	0.40				1		-1.22			1	1831
1001	-4.01	0.10	0.40	2.21	V.54	-1.84	0.00	0.20	-1.22	1.77	-0.54	0.11	1001
1832	0.76	1.12	0.42	0.82	-1.48	-0.88	-2.40	0.22	-1.22	-0.35	-0.63	-0.24	1832
1888	-0.86	3.16	-0.18	-1.82	8.46	1.33	-0.45		-0.48	-0.98	0.14	2.48	1833
1834	4.73	1.81		-0.68	1.82	1.23	8.65	2.84	0.74	-0.28	0.56	0.36	1834
1885	2.81	2.87	0.57		-0.86	0.18		-0.59	1.22	-0.97		-1.77	1835
1886	1.87	1.11	8.42		-2.55		-1.08				-1.10	0.26	1836
1000	1.07	1.11	0.44	0.07	2.00	0.20	-1.00	-1.40	-1.00	2.00	-1.10	0.20	1000
1837	1.91	0.38	-1.98	-1.68	-1.42	-0.69	-1.11	1.20	-0.92	0.37	0.72	-0.87	1837
1838	-6.3 0	-8.63		-1.42	-0.24			-1.78	1.27		-1.14		1838
1889	0.79	1.50		-2.54	0.58	0.95			1.10	0.15		-1.49	1839
1840	-0.09	0.65		-0.07	-0.03	0.16				0.09		-0.83	1840
1841	-0.01	-4.08	0.91	1.01	2.51		-1.10		0.58	1.29	0.75	1.62	1841
1041	-0.01	4.03	0.51	1.01	0.01	~~.00	-1.10	V-V1	0.08	1.28	0.75	1.02	1041
1842	-1.84	0.89	0.93	-1.52	0.75	-0.54	-0.84	8.18	0.42	-1.55	-2.82	0.71	1842
1848	2.40	2.45	-1.09	0.44	-2.01	-1.00	-0.41	1.17	-0.64	-0.66	1.42	1.96	1843
1844	1.00	-0.96	-1.50	0.48	0.56	-1.00	-2.35	-1.60	0.86	-0.24	0.56	2.41	1844
1845	1.65	-4.55	-6.24	0.28	-1.48	0.49	0.90	-0.94	-0.98		1.26	0.88	1845
Means.	-1.90	-0.15	2.74	6.88	10.92	18.94	15.04	14.43	11.75	7.97	8.25	1.82	Means.

LXXXVIII.

DENMARK. — COPENHAGEN.

for Reducing the Monthly and Yearly Means of Single Years to the Means derives from Series of Years.

Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1767	-3.89	0.84	0.52	° -1.49	o -1.88	-1.99	。 -1.40	-0.47	0.22	-0.75	1.58	-0.29	1767
1768	-0.67	-0.14	-1.01		-0.82	l			-1.87		ı	1	1768
1769	1.74	0.79	1.44		-0.70	1				1	0.03		1769
1770	0.19	1.64	-2.57	-0.77	-0.82	-0.88	0.21	0.86		1.38		0.69	1770
1771	-1.20		-8.96				-0.83					1.10	1771
1771	1.20	-2.10	-0.50	0.14	0.27	1.00	V.65	2.04	-0.50	0.05		1.10	1777
	i						İ		ŀ	l	l		ł
1772	-0.88	-1.71	-2.53	-1.72	-1.94	-0.51	-0.56	-0.59	0.83	1.49	2.89	1.33	1772
1773	1.78	-0.46	0.35	0.33			0.50	1	0.45	1.73	i	0.94	1778
1774	-2.87	0.84	0.87		-0.09	0.87	0.04	I .	1		-5.39		1774
1775	-0.51	1.79	1.72		-0.09	2.18	1.89			0.78		0.71	1775
						1.61	2.80	1.85	0.59	0.67	0.77	0.69	1776
1776	-5.22	1.18	1.49	0.78	70.07	1.01	2.50	1.00	0.55	0.07	0.77	0.09	17770
1	1						l		l	ł	ł	1	
1782	2.88		-0.99	_0 69	_0 63	3.43	0.12	0.82	0.00	-1.09	_1 42	0.07	1782
1				2.01	1.97	2.36		ı	1	I		-0.87	1788
1783	0.81		-0.38			1		1					
1784	-2.02			-1.51	0.24	0.07			l	-0.78		-0.76	1784
1785	0.53		-2.96	-1.04		0.78	1			-0.05		-0.20	1785
1786	0.13	0.06	-2.69	0.83	-1.08	1.48	-0.35	-0.41	-0.74	-1.21	-2.91	-0.04	1786
							Ì	i	1	l	l	}	
						0.01			0.50	١.,,		0.00	7000
1787	0.94	2.21	2.09	-0.2 0	0.07	0.01		1	0.58			0.26	1787
1788	2.02	0.68		0.95	1.00	1.28	ı	1	1.71	1	-0.19		1788
1798	1.15	2.27	1.31	2.48	2.71	2.06	2.00		1.09	1.01		-2.29	1798
1799	-0.71	-4.50	-1.94	-1.59	-2.12		1	-0.48	0.21	0.56	1	-2.55	1799
1800	-0.96	-2.07	-8.57	2.60	1.77	-1.69	-0.89	0.42	0.21	1.19	1.78	1.20	1800
	ł l								1			!	
										۰			
1801	1.28	0.75	2.82	1.44		-0.10		1	0.69	ı			1801
1802	−0.56	1.04	1.90	• •				-0.56	1	0.98			1802
1803	-3.02		-0.39		-1.69		1		l		-0.31	1 1	1808
1804	2.01	-1.47	-1.82	-0.58		-0.57			1	0.77	1	-2.85	1804
1805	-1.79	-2. 02	0.26	-1.03	-2.14	-3.46	-1.48	-1.03	0.77	-2.53	-0.56	0.77	1805
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1806	1.90	1.64	-0.49	-1.59	0.08	-2.28	-1.79	-0.08	1.32	0.35	1.27	2.54	1806
1807	1.75	1.46	-0.55	-0.56	-0.87	-1.60	-0.17	2.54	-2.22	0.02	0.19	0.77	1807
1808	1.04	-0.77	-1.30	-1.40	0.19	0.02	1.26	1.84	1.10	0.14	−0. 85	-2.42	1808
1809	-2.64	0.80	-0.42	-2.52	0.60	-0.91	-0.89	0.47	0.30	-0.44	-0.23	1.65	1809
1810	0.60	-0.28	0.05	-1.19	-2.69	-1.01	-0.07	-0.29	0.51	-0.79	-0.22	0.10	1810
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()						1	l				•		
1811	-0.65	0.28	2.46	-0.71	1.75	0.96	2.07	-0.82	-0.26	1.28	1.12	1.07	1811
1812	0.40	1.21	-1.55		-1.63	l .		-0.61			-1.14		1812
1818	0.23	2.66	1.50		-1.01	-1.00		-0.89	l	-2.01	0.20		1818
1814	-3.81	-4.01	-2.15		-2.99		i .	-0.87	l	-0.58	1.22		1814
11 1	1		1.82			1		-0.81	1	0.59	1	-0.66	1815
1815	-0.67	1.47	1.02	0.50	U.20	-1.E0	1.50	7.01		0.08	0.20	7.00	1010
R I	1						1	1		1	İ		
		,	0.00	-0.40		_1 0=	_0 40	_1 00		_0 70	0=		1816
1816	0.72	-1.56	-0.05	-U.49	-z.69	-1.87	-U.49	1-1.56	-U.59	-U.72	ספים-	,-V.51	1910

LXXXVIII.

DENNARE. - COPENHAGEN (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

						Reses of	A-0-0111	ш.					
Year.	Jen.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1817	2.79	2.98	0	-1.10	-0.01	-1.04	0	0	0 69	-9 94	0	-0 -1.71	1817
1818	1.99	1.78			-0.05	t .		-0.24		0.87		0.20	1818
1819	8.46	2.80	2.39		1.25		1.58				-1.03		1819
1820	-1.67	0.51	0.52					-0.88					1820
1821	0.36	0.16	0.34	ı				-0.86			1.68		1821
1021	0.30	0.10	0.24	3.54	0.45		7.01	- Va00	0.07	1.02	1.00		1021
1822	2.56		8.64					-0.17					1 11
1823	-2.60			-0.04				0.41			1.88		1823
1824	3.65	i	0.97					-0.48				• 1	1824
1826	• •	• •	• •	••	4.80	5.91					• •	2.04	1826
1827	0.16	-2.20	0.59	2.14	1.44	1.98	0.09	-0.29	1.48	1.16	-1.20	2.30	1827
1828	-0.07	0.43	1.87	0.58	1.81	1.84	1.36	0.26	0.41	0.46	0.61	0.50	1828
1829	-1.14	-8.06	-0.95	-1.00	1.84	1.50	-0.28	-1.01	0.08	-1.43	-2.91	-3.60	1829
1830	H .	-2.85	1.89					-0.81			1.75		1830
1881	-1.60	0.61	-0.16	1.87	0.81	0.85	2.52	1.55	-0.59	2.71	-0.65	1.91	1831
1882	1.52	1.78	1.55	1.84	-0.28	1.29	-0.94	-0.06	-0.98	0.60	-0.47	0.58	1832
							0.00		0.00	0.00			
1888	0.05		-0.45					-2.27				1.32	1833
1884	2.26	1.71			1.98		8.60				0.22		
1885	1.87	2.16		1	-0.92	l .		-0.57				-0.88	
1836 1837	0.29	0.63	2.71		-0.17 -1.10		-0.89 -0.21	-1.86			-0.91		1836 1837
1837	0.17	0.54	-1.08	-1.50	-1.10	0.00	-U.ZI	0.00	-0.80	-0.00	-0.91	-0.75	1837
1838	-2.83	-4.85	-0.56	-2.63	-0.97	-0.70	-0.09	-2.25	-0.44	-1.82	-2. 01	-0.25	1888
1839	-0.17	-0.88	-2.06									-2.12	1839
1840	-0.63	-0.89	-0.64	0.85								-2.65	1840
1841	-1.14	-2.52	0.97	0.62	2.21	-1.37	-2.56	-0.97	-0.71	-0.38	-0.36	2.87	1841
1842	-0.26	1.48	2.05	0.61	1.78	-0.11	-0.99	2.78	0.81	-0.88	-1.57	2.36	1842
					,	ŀ				•			1
1015				0 :-	0.00		A 000	1.00			0.00	0.00	1040
1843			-0.88									2.99	: 1
1844 1845	11		-1.50 -4.45					-1.42 -0.86				-1.48 0.59	1844 1845
1043	1.24	-4.10	7.40	U.04	-1.01	0.20	U.33		-1.20	-1.04	1.20	0.08	1043
Means.	-1.16	-0.80	0.55	4.45	8.98	12.45	18.81	18.50	10.86	7.05	8.12	0.68	Means.
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LXXXIX.

France. - Paris.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year.	Jan.	Feb.	March	April.	May.	June.	July.	Aug.	Sept.	Oct	Nov.	Dec.	Year.
	-	0	0	•		0	-	0	•	-	-	-	
1806	8.85	1.38	0.28	-1.54	2.07	0.77	0.64	-0.88	0.58	-0.26	1.69	4.00	1806
1807	0.84	1.89		-0.63	1.28	-0.52	1.94	2.84	-2.08	1.15	-0.74	-1.75	1807
1808	0.42	-1.42		-2.28	2.55				1		0.58		1808
1809	2.95	2.91	0.42	-2.72	0.54	-1.38			-0.81	-1.09	-1.54		1809
1810	-2.90	-1.11	1.16	-0.42	-0.62	-0.06	-0.74	-0.70	1.75	0.25	0.80	1.30	1810
1811	-1.88	2.81	1.90	1.58	2.14	0.25		-0.66	• .	2.55	1.38	0.72	1811
1812	-0.32		-0.82	-1.92	0.88		ı	-0.46		0.51			1812
1818	-1.18	1.83		0.71	0.48		l .	-1.42			-0.68		1818
1814	-1.70	-3.87		1.30		-1.17	ı	-0.91			-0.51		1814
1815	-1.98	2.39	2.29	0.36	0.18	-0.89	-0.93	-0.54	-0.11	0.77	-2.70	-1.84	1815
1816	0.54	-1.69	-0.71	0.10	-1.40	-1.88	-2.58	-2.87	-1.26	0.29	-2.24	0.07	1816
1817	2.48		-0.20	-2.02		0.61		-1.66		-8.16	1.80		1817
1818	1.94	-0.21	-0.15	1.20	-0.65	1.75	1.14	-0.18	0.05	0.38	1.98	-1.28	1818
1819	2.48	0.95	0.16	1.81	0.02	-0.85	0.30	0.78	0.58	-0.12	-1.66	-0.30	1819
1820	-2.02	-0.99	-1.42	1.20	-0.80	-1.87	-0.85	0.11	-1.19	-0.98	-1.30	-0.22	1820
1													
1821	1.02	-2.58	0.54	1.84	-1.95	-2.05	-1.39	1.20	0.85	-0.14	2.70	8.10	1821
1822	1.96	1.52	2.62	1.01	1.72	8.26	0.09	0.42	0.18	1.72	1.82	-3.42	1822
1828	-1.79	0.88	-0.14	-0.62	0.50	-1.69	-1.28	0.46	0.00	-0.58	-0.54	1.58	1828
1624	0.61	0.68	-1.00	-0.54	-1.52	-0.61	-0.02	−0.17	0.89	0.54	2.30	2.74	1824
1825	1.28	0.06	-0.94	1.54	-0.22	-0.05	1.24	0.70	1.77	0.75	0.40	2.18	1825
1826	-2.77	1.78	0.56	0.27	-1.48	1.85	1.59	2.10	1.11	1.70	-1.08	1.72	1826
1827	-1.63	-4.14	1.14	1.14	0.18	-0.0 9	0.85	-0.48	0.46	1.52	-0.77	2.58	1827
1828	8.28	0.80	0.29	0.50	0.46	0.84	0.84	-0.74	0.74	-0.30	0.51	0.89	1828
1829	-3.16	-0.97	-0.75	-0.0 8	0.32	0.05	-0.10	-1.30	-1.53	-1.01	-1.64	-5.70	1829
1830	-3.42	-2.59	2.54	1.68	0.11	-0.82	0.16	-1.28	-1.50	-0.44	0.88	-0.82	1830
1831	0.13	1.53	1.85	1.80	-0.20	-0.12	0.86	0.12	-0.85	2.88	-0.10	1.50	1831
1832	-0.86	-0.59	1	0.65	-1.05	0.22	0.68		-0.10		-0.10	0.58	1832
1833	-1.78	2.84		-0.38	2.54	1.06	-0.24		-1.58		-0.61	8.46	1888
1834	4.84	-0.42		-0.70	1.59	0.70	1.25	0.69	1 1		-0.05		1884
1885	1.35		-0.14				. 1.92	1.42			-1.10		1885
1886	0.55	-1.03	1.62	-1.02	-1.67	1.06	0.56	0.80	-1.24	-0.04	0.66	0.86	1836
1837	0.89	0.97	-8.26	-8.34	-2.79	1.14	-0.82	1.26	-0.84	0.04	-0.62	0.60	1887
1838	-5.21	-5.03	0.26	-2.52	-0.28	-0.68	-0.32	-0.42	-0.12	-0.04	0.74	-1.48	1888
1839	0.75	0.78	-0.62	-1.70	-0.71	1.62	-0.04	-0.86	0.00	-0.56	1.10	1.60	1839
1840	1.28	-0.47	-2.58	2.26	0.49	1.02	-1.08	0.98	-0.64	-1.40	0.99	-4.76	1840
}		•											
1841	0.47	-1.85	1.94	0.42	2.25	-1.26	-1.68	-0.50	2.28	0.12	0.02	1.48	1841
1842	-2.65	0.83	1.80	0.26	0.05	2.66	0.52	8.18	-0.12	-2.2 8	-1.10	0.86	1842
1848	2.07	-0.89	1.06	0.50	-0.81	-0.86		0.70		0.12	0.54	0.60	1843
1844	0.88	-1.81	0.18	2.22	-1.85	0.54	-1.12	-2.84	0.24	-0.36	0.26	-8.40	1844
Moans.	1.53	8.85	5.33	7.90	11.59	18.66	14.96	14.82	12-52	9.00	5.41	2.92	Means.

Holland. — Zwanenburg.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

	1	_											
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1748	0.60	1.40	_0.15	-2.69	-0.40	0.59	o -1.15	0.05	-0.22	。 2.27	1.83	-0.23	1743
1744	-0.91		-0.74		1 1	í	!		1	1	0.66		1744
1745	0.15		-0.70		1	ı	ı		1				1745
1746	-0.82		-2.19		1	-0.62	0.04	-1.28	1	-2.09	-2.80		1746
1747	-0.47		-2.29			0.92		-0.21	0.84				1747
	***	2.20		0.20	0.02	0.02	0.00		0.00	0.10		1.00	
1	1												
1748	-0.24	-2.68	-4.14	-2.12	-0.31	1.45	0.08	0.89	-0.08	0.28	1.68	3.46	1748
1749	2.68	0.11	-1.09	-0.52	1.11	-2.30	-0.10	0.28	-0.11	-0.85	-0.45	1.65	1749
1750	-0.84	2.60	2.88	-0.06	0.14	-0.10	0.97	-0.45	0.75	-1.25	-1.63	-0.31	1750
1751	1.09	-2.29	1.88	-0.60	-1.21	-0.10	-0.78	-0.52	-1.19	-0.48	-1.81	0.83	1751
1752	1.71	-0.56	0.72	-0.68	-1.10	0.95	-0.48	-0.09	0.89	0.07	0.90	1.87	1752
	l					1				}		1	
1758		-0.11	1.84		0.80	1	-0.84						1753
1754	0.64	-1.14		-1.40		-0.49		-0.16		0.61	0.05	l i	1754
1755	-1.98		-1.24		-1.37	1.89		-1.83	1			1.22	1755
1756	8.20	1.32	0.88		-1.58	0.97	0.80					-2.60	1756
1757	-2.22	-0.59	0.00	1.00	-1.01	-0.11	2.87	0.36	-0.21	-1.09	1.43	-0.09	1757
	1												
1758	-1.28	0.87	0.41	-0.89	1.95	0.29	-1.41	0.99	-0.17	0.21	0.05	0.36	1758
1759	2.86	2.13	1.49	0.86		0.99	1.66		-0.07	1.05		-2.68	1759
1760	-1.64	-0.69	0.15		-0.22		-0.15		1				1
11 1	1.78	1.90		0.77		1.81	1	-0.40	1.14	0.28	1.08	1 (1760
1761			2.87	0.47	0.92	0.86	i .	1.16	0.67	-1.75	1	-1.59	1761
1762	2.10	0.09	-1.25	2.87	0.98	0.67	0.80	-1.81	-0.04	-1.98	-1.87	-2.02	1762
1768	-4.88	0.79	-0.84	-0.24	-1.04	0.28	-0.08	0.22	-0.56	-0.99	0.56	1.52	1763
1764	3.87	2.52	0.17	0.52	1.71	0.02	1.43	-0.82	-1.14	-0.74	-0.45	-1.01	1764
1765	2.24	-2.13	2.30	1.62	0.27	1.22	-0.84	0.85	-0.05	1.24	0.08	-0.82	1765
1766	-0.22	-0.78	0.72	1.67	0.87	0.85	0.20	0.45	0.49	0.32	0.46	-0.68	1766
1767	-8.84	2.84	1.08	-0.63	-1.86	-0.94	-0.80	0.86	0.98	0.71	2.15	-1.33	1767
						,							
1768	-1.94	0.98			-0.02	1	0.65	0.88		-0.87	0.70		1768
1769	1.19	0.09	0.85	0.99	1	-0.58	0.58	-0.06	0.48		0.58	1.43	1769
1770	1.45	0.92			-0.15	-0.84	0.02	1.20	1.59	0.19	0.06	2.01	1770
1771	-0.50	-1.44		-2.59		0.26	-0.29	-1.01	0.04	0.89	0.69	1.68	1771
1772	0.11	0.21	0.68	-0.50	-1.11	1.19	0.57	0.36	0.88	2.68	2.36	1.16	1772
1778	3.38	-0.57	1.86	0.81	0.85	0.81	-0.16	1.17	0.66	1.79	1.51	1.76	1773
1774	0.58	1.62	2.18	1.80		0.96	1.12	0.51	ı	1.79			1774
1775	1.81	8.40	2.12	1.04		2.19	0.78	0.88	1.84	1.25	1		1775
1776	-4.40	1.20	1.99	1.45	-0.12	1.11	1.56	0.88		1.25	-1.58 0.46	1.65 0.05	1775
			1 1						-0.01				
1777	-0.28	-1.57	1.14	-0.56	0.15	-0.19	-0.07	0.88	0.60	0.78	1.97	-0.60	1777
1													
1778	-1.26	-1.70	-0.55	0.36	0.71	0.43	1.43	0.54	-1.58	-2.02	1.08	2.90	1778
1779	-0.28	2.55	1.79	1.21	0.61		0.60	1.51	1.27	1.61	0.19	0.53	1779
1780	-1.54	-0.56		-0.78		-0.51		2.04			-0.07		1780
								1				,00	

XC.

Holland. — Zwanenburg (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year.	Jan.	Feb.	March	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1781	-0.97	1.18	° 1.18	0	0.87	2.47	1.04	1.56	0.91	°.75	0	-0.39	1781
	1			1			ı		i				
1782	2.88		-0.56		-1.09	0.77	0.84	l .	0.50			-0.89	1782
1788	2.39		-1.81		-0.05	0.92			0.44	0.78		-2.74	1788
1784	-8.26	1	-2.04			0.15	l .	1	0.94	-2.80		-1.60	1784
1785	-0.06	-2.54	-8. 82	-1.54	-0.96	-0.46	-0.01	-0.59	1.14	0.40	0.41	-1.70	1785
													1
1786	0.85	-0.08	-8.19	0.44	-0.59	0.72	1.80	-0.75	-1.55	-1.49	-8.59	-0.28	1786
1787	-0.23	1.24		-0.90				-0.56					1787
1788	2.20	-0.42	1	0.24	0.58	1.05		-0.66	0.30	0.88	-0.73	-6.22	1788
1789	-2.66	0.98		-1.64	1			-0.07		-1.18			1789
1790	2.20	2.51		-2.00				-1.25					1790
					0.00	3112				0.00	2002	0.00	-:
1791	2.74	1.29	1.28	1.84	-1.21	-1.25	-1.20	-0.14	-0.74	-0.60	-0.79	-0.53	1791
1792	1.06	-0.88	0.08	1.70	-1.11	-0.93	-0.07	0.27	-1.53	-1.18	-0.14	1.05	1792
1798	0.52	1.59	0.03	-1.40	-1.61	-1.70	0.67	-0.65	-1.6 8	0.98	-0.17	1.60	1798
1794	-0.21	2.09	2.58	2.59	-0.76	-0.48	1.52	-0.87	-1.14	-0.54	0.41	-2.08	1794
1795	-4.52	-1.53	-0.92	0.85	-1.88	-0.18	-2.29	-0.08	1.51	2.39	0.37	2.87	1795
													l i
								0.00				امما	1000
1796	4.72		-0.99		-0.63			0.02		-0.80			1796
1797	0.84		-0.18	0.81		-1.18	1.88		-0.78	-0.60	0.82		1797
1798	1.45	1.78		1.22	0.11		-0.05	0.86	0.19	0.68		-8.49	1798
1799	-2.11		-1.77	-2.19		-1.88			-0.72	-0.68		-8.54	1799
1800	-0.65	-1.76	-1.97	2.08	1.85	-2.10	-1.82	0.04	0.50	0.02	1.12	-0.46	1800
i i													1
1801	1.97	-0.59	1.61	0.26	0.68	-1.48	-0.76	0.82	0.45	1.16	0.58	0.47	1801
1802	-0.75	0.24	0.56		-1.10			1.08	0.08	1.15		1.19	1802
1803	-3.04	-2.29	0.00		-1.55		1.48	0.75		0.06		0.48	1803
1804	8.80	0.18	-0.92	-0.84	1.85		0.03	-0.20	1.57		-1.79	-2.84	1804
1805		-0.86	1	1	-2.16			0.05		-2.00			1805
2000			0.00	0.00			2.20						
		İ											
1806	8.14	1.58		-1.95	1.79	-0.52	0.18	0.67	1.41	0.28	2.52	4.12	1806
1807	2.36	1.74	-1.32	-0.37	1.09	-0.17	1.64	2.58	-1.40		-0.15		1807
1808	1.19	0.07	-1.71			-0.46	2.62	1.64		-1.35			1808
1809	• • •	• •		-2.53	1.80	-1.03	-0.47	0.09	-0.27	-1.82	-0.99	0.68	1809
1810	-1.94	-1.39	-0.36	-0.41	-1.76	-0.96	0.05	-0.07	0.99	-0.63	-0.03	1.06	1810
1													
1811	-2.75	0.55	1.41	1.16	9 75	1.58	0.47	-0.80	40	2.40	1.80	1.05	1811
1812	0.81	1.20		-2.48		-0.68		-0.56				-4.00	1812
1813	-0.84	1.53	0.16	0.04		-0.82		-0.91				-1.31	1812
1814	-3.33	-4.20								_			1814
1815	-2.69	0.96		1.27		-1.86		-0.66	ı			-1.90	1815
1910	2.09	0.80	Z.25	0.59	0.09	-0.05	71.08	-0.77	-U.D4	0.07	-0.97	71.50	1919
1816	0.52	-1.64	-0.78	-0.28	-1.48	-2.28	-1.31	-1.85	-1.14	-0.12	-2.06	-0.45	1816
1817	2.86	2.31	0.19	-2.12	-1.38	0.84	-0.88	-1.80	0.69	-8.16	1.88	-0.67	1817
1818	1.96	-0.40	0.40	-0.21	-0.56	1.69	0.99	-0.64	-0.86	-0.84	0.74	-1.22	1818

XC.

HOLLAND. - ZWANENBURG (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Resumur.

Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1819	° 1.47	1.04	0.68	0.84	0.91	0.50	0.56	°	0 85	0 70	0 19	° -2.18	1819
1820			-1.21	0.72			-1.06						1820
1821		-1.22				ı	-1.81	1		1		(I	1821
1822	2.64	1.93			1.58	1		-0.19				-2.95	1822
1622	-6.29	-0.94		-1.19			-0.89			-0.66			1823
1080	-0.20	70.54	0.11	-1.15	0.44	-1.00	-0.59	0.12	-0.57	~0.00	0.90	1.65	1023
	ŀ						l '						ľ
1824	2.80	0.20	-0.22	-0.78	-0.47	-0.40	-0.19	0.00	1.08	0.86	1.52	2.59	1824
1825	2.68	0.60	-1.42	0.48	0.12	0.00	-0.04	-0.36	1.20	1.04	1.03	1.70	1825
1826	-2.57	0.97	0.87	0.17	-0.59	1.52	2.12	2.01	0.80	1.95	0.16	1.99	1826
1627	-0.65	-8.83	0.58	0.98	0.40	-0.24	0.14	-0.55	-0.14	0.88	-0.91	2.79	1827
1828	0.75	-0.75	1.05	0.43	0.49	0.70	0.79	-0.64	0.48	0.24	-0.18	1.96	1828
	1					l	i	ł					
1829			-1.48				-0.42						1829
1880	-2.70		0.50			-1.45		-1.17	-1.45	0.84	1.00	-1.80	1830
1881	-1.07	0.04	1.24	1.61	-0.10	-0.09	0.90	0.66	-0.14	3.16	0.66	1.72	1831
1832	-0.77	-1.34	-0.48	0.55	-1.49	-0.07	-1.74	-0.12	-0.64	0.48	-1.37	0.72	1832
1883	-2.12	1.58	-1.62	-0.68	2.22	0.92	-0.48	-2.08	-0.99	0.11	0.44	8.07	1883
						i i					l l	l l	i
1884	4.21	0.40	1712	. A 0=	1.01	A 0=	1.00	1 00	0.00	A 40	A 83	1 40	1007
				-0.87				1.00			-0.31		1834
1885	1.21	1.81	U.47	-0.76	-1.09	0.92	0.47	0.07	-U.ZZ	-0.77	-1.44	-0.44	1835
Means.	0.99	8.14	3.86	6.80	10.12	12.45	18.97	14.18	12.80	8.61	4.84	2.16	Means.

XCI. England. - London.

1794	-0.96	2.72	1.23	1.64	-0.99	-0.48	1.83	-0.3 8	-1.36	-0.61	0.36	-1.10	1794
1795	-5.04	-2.08	-1.26	-0.23	-0.46	-1.98	-0.04	0.11	1.76	1.61	-0.88	2.46	1795
1796	4.42	0.50	-1.00	1.10	-1.26	-1.00	-1.28	-0.51	1.23	-1.45	-0.97	-3.76	1796
1797	-0.01	-1.44	-1.51	-0.45	-0.70	-1.56	0.62	-0.82	-0.97	-1.34	-0.44	0.98	1797
1798	-3.44	-0.28	-0.12	1.41	0.44	1.31	-0.10	0.88	-0.11	0.09	-1.24	-2.39	1798
	1					Ì	i		l	İ		1 1	ł
1799	_1 00	_1 05	-1 74	-1.04	1 90	_3 94	-0.79	_1 40	_1 10	_1 00	0.10	-2.79	1799
1860	11	-2.04				_							
	11					-1.87					-0.15		1800
1801	11	-0.08		1	l		-0.48					-1.37	1801
1802	-1.21	0.11	-0.04	1.14	-1.50	-0.66	-2.2 0	1.74	0.49	0.28	-0.89	-0.56	1802
18 03	−0.92	-1.03	0.51	0.88	-1.12	-0.89	0.97	0.41	-1.77	-0.40	-0.81	0.98	1803
	H	1					l		}	l		l i	ĺ
1804	8.39	-0.73	0.00	-0.95	1.80	1.07	-0.57	-0.20	1.16	0.66	0.68	-1.52	1804
1805	-0.52	•		-0.20			-0.89				-1.17		1805
1866	2.27	1.27		-1.21			-0.06				2.11		1806
1807	0.64			-0.14		-0.84			-1.61			-1.19	1807
1808	1	-1.01							-0.55			-1.82	1808
1809	-0.11	l		-2.05					•			0.72	
2000	J		0.00	2.00	1.20	V.30	0.78	-1.09	-U.Z4	-0.00	-1.33	U.72	1809

XCI.
England. — London (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

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Year.	Jen.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1810	-0.47	0.01	0.38	0.12	o −1.44	o 0.20	-0.44	-0.16	o 1.32	0.95	0.32	-0.03	1810
1811	-1.09	0.85	1.54	1.64		I		-0.51		2.50	ı	-0.16	
1812	0.42	1.48	-0.68				-1.24	1		1	1		1612
- 11	-0.51	1.84	0.87	-0.81			-0.97				-0.84		1818
1814	-8. 80	-2.21	-2.55	1.06	1		-0.04				-0.75		1814
										2.50			
1014	-1.49	1.04		0.44				^~~	0.40				
1815		1.84	1.94	0.44			-0.53		2.48			-0.83	1815
1816	0.64		-0.64	-0.50			-2.35					-0.48	
1817	1.84	2.05	0.25	-0.63			-1.46		-0.81		1	-0.70	
1818	1.67	-1.82	0.08		-0.06		2.40		2.30	2.06	ı	-0.08	1818
1819	2.29	0.85	1.36	1.87	0.88	-0.69	0.36	1.58	0.70	8.08	-0.75	-C.74	1819
1000		0.00	0.05		0.01					0.00			
1820	-1.44				1		-0.71	1	t .	1	1	0.59	
1821		-0.97	0.87		1		-1.55	t	1				1821
1822 1823	2.16 -1.40	2.19 0.19	2.78	0.48 -0.10	1.45 2.16		0.36 0.14		-0.24 0.39	1.04 0.56	2.36 0.54	-1.14 0.55	1822 1828
11			1							1			
1824	0.78	2.41	-0.78	-0.94	-1.48	-1.40	0.00	-0.29	0.48	-0.03	1.38	1.08	1824
1825	1 01	יפ ח		1 00	0.00	0.00	7 47	0.38	1 60	V 60	-0.84	0.59	100#
11			-1.17	1.28		-0.03	1	l .		l			1825
1826 1827	-1.49 -0.96	1.61 -3. 19	0.74	1.46 0.89	1.16 -0.08		1.69	1.67 -0.73	0.30 0.21	1	-1.11 -0.28	1.19 1.99	1826
- 11							[1	1		1	1 1	1827
1828 1829	1.73	0.54 -0.24	1.00 -1.08	0.28	0.70		-0.48	-0.62 -1.22	1	-0.16	0.65 -1.60		1828
1029	-1.70	70.24	-1.08	-0. 85	0.50	0.85	-0.40	-1.22	-1.41	-1.10	-1.60	-8.14	1829
1830	-2.31	-2.17	1.98	1 16	_1 90	-1.09	0.65	-1 00	-1.37	0.32	0.68	-2.12	1830
1831	-0.78	1.01	1.16	1.21			1.49	1	-0.04	2.39	ı		1831
1832	0.13		-0.42		-0.70			ı	-0.06	0.52			1832
1833	-0.64	1.45		-0.10			-0.13	-1.81	1	0.24			1833
1834	8.73	0.48		-0.48	1.59		1.29	0.76		0.10		0.35	1884
1001		0.10	1.70	0.20	1.00	1.20	1.20			0.20	0.40	0.00	1004
1835	0.82	0.81	-0.22	0.80	-0.12	0.71	0.87	1.09	0.21	-0.90	0.05	-1.76	1885
1836	0.80	-0.99			-1.28				-1.50	1	1		1836
1837	0.73	0.74		-2.79	•	0.04			-0.75		-0.57		1887
1838	-2.93	-2.57		-1.50	1	0.02		i	-0.92		-0.68		1888
1889	0.78				1		-0.85	ı	1		1	-0.21	1889
1840	1.27	-0.50	-1.97	-0.01	0.14	1.02	-0.77	0.73	-1.10	-1.32	0.60	-2.41	1840
1841	-0.38	-1.41	2.58	0.61	2.08		l .	-0.02	1	-0.01	I		1841
1842	-1.02	0.81	1.47	-0.43	0.59				1	-1.70	1	1	1842
Means.	2.38	3.81	5.00	7.80	10.46	12.92	14.26	14.07	12.06	8.88	5.51	3.81	Means.
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l l								١.	l	1			
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XCII.

SCOTLAND. - KINFAUNS CASTLE.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

						Alees o	Resum	ш.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Yest.
1814	-4.71	-1.63	-1.78	0.56	-2.46	-9.86	-0.60	0 12	-0.84	-1.16	-1.61	-1.46	1814
1815	-1.69	1.18	0.16		0.95	0.24				1	-1.68	1 1	1815
1816	-0.24	-1.60			-0.74		-0.96		-0.99		I	, ,	1816
1817		l		0.33	-1.12	0.80	l	l .	0.18		1.78	1 1	1817
11 1	1.60	1.29	-0.44			1		1			l .		
1818	0.51	-1.08	-1.41	-1.59	1.03	1.48	0.85	-0.22	-0.15	2.84	2.54	0.25	1818
1819	0.85	-0.88	0.67	-0.20	-0.86	-0.85	0.07	2.00	0.90	-0.82	-2.85	-2.60	1819
1820	-2.48	0.95	0.88	1.10	0.20	-0.12	0.89	-0.26	-0.86	-1.20	0.15	0.86	1820
1821	0.55	0.97	0.26	1.12	-1.09	-0.45	-0.01	0.84	1.44	0.83	0.88	0.78	1821
1822	1.85	1.28	1.08	0.79	0.97	2.04	0.50	0.26	-0.81	0.48	1.38	-0.61	1822
1828	-0.91	-1.69	-0.16	-0.60	0.68	-1.01	-0.92	-0.85	-0.15	-0.56	2.02	-0.04	1823
						l					۱		
1824	2.64	1.20	-0.56	0.39	0.18	0.26	0.43		0.24		-0.16		1824
1825	1.94	0.84	0.45	0.82	-0.09	0.81	1.59	1.53	1.85		-0.82	0.80	1825
1827	0.68	-0.77	0.02	0.78	0.51	0.38	0.16	0.87	1.48		-0.99	2.23	1827
1828	2.50	1.44	1.63	0.69	1.20	1.23	0.98	1.03	1.23	1.10		2.78	1828
1829	-0.38	0.96	0.42	-0.48	0.87	1.00	-0.12	-0.44	-1.02	0.34	-0.19	0.02	1829
1830	0.40	-0.22	2.07	0.87	0.60	-0.63	0.50	-1.18	0.11	1.33	0.92	-0.89	1830
1832	1.91	1.27	0.92		-0.19	0.50	0.24	0.93	1.85	1.53	-0.56	0.40	1832
1833	-1.40	0.51	-0.41	0.82	2.79	0.59	0.67		-0.24	0.58	0.12	0.57	1833
1834	2.28	0.97	1.05	0.51	1.01	0.58	0.98	0.84	0.28	0.49	0.14	0.57	1834
1885	-0.27	0.72	-0.08	0.23	-0.58	0.20		1.09	-0.10		-0.31	-0.84	1835
1000	J-0.21	0.72	0.00	0.23	7.00	0.20	70.17	1.03	0.10	-1.10	0.51	0.04	1000
1836	0.59	-0.67	-0.70	-0.81	0.10	-0.54	-1.16	-1.09	-1.67	-0.86	-0.94	-0.05	1836
1837	-0.07	0.20	-2.26	-2.35	-1.70	-0.05	0.52	-1.13	-1.32	0.23	-1.18	1.74	1837
1888	-2.58	-4.61	-0.88	-1.44	-1.75	-1.08	-0.04	-0.24	-0.58	-0.55	2.73	0.48	1838
1839	-0.90	-0.79	-1.56	-1.24	-1.18	-0.45	-0.84	-0.79	-0.64	-0.17	0.11	-0.85	1839
1840	0.65	-0.26	-0.07	1.00	-0.72	-0.40	-1.30	0.21	-1.29	-0.63	-0.17	-0.58	1840
1841	-2.19	-0.09	2.25	-0.28	0.51	-1.07	-0.88	-0.20	0.51	-1.52	-1.94	-0.49	1841
1842	-1.17	0.49	0.35	-0.07	0.48	0.02	-0.88	1.24	0.82	-1.52	-0.81	1.81	1842
i													
Means.	1.77	2.74	3.87	5.71	8.13	10.58	11.76	11.28	9.52	6.72	4.35	2.96	Means.
3				XCII	I. F	INLAR	īD. —	Torn	TBÅ.				
1801										• •	-0.01	-1.67	1801
1802	-0.57	-0.17	-0.15	0.10	-2.88	-0.66	-2.08	-1.60	-1.60	1.80	-2.10	-4.06	1802
1803	-8.50	-0.90	-0.18	1.57	1.69	-0.44	-0.58	0.98	-0.90	1.18	0.71	-8.67	1803
1804	-2.50	-4.82	-2.34	1.99	1.50	-0.97	0.78	-0.70	-0.21	1.19	1.46	-4.01	1804
1805	8.86	-2.94	-1.15	-0.79	-1.56	-2.90	-1.03	0.62	-1.84	-4.62	-2.83	-2.98	1805
1000	0.0-			0.00	1.00	.,	1 00	0.00	1.00		0.00		3000
1806	2.91	1.91	-0.08	2.02		-1.18		2.00	1.20	0.13	-0.97	0.74	1806
1807	-8.40	1.94	-1.25		-1.98		0.84	0.89	-1.41	-2.3 0	-0.20	ì	1807
1808	1.80		0.19	1	1.14	2.65	0.58	-0.11	-0.51	8.53	2.24	-3.74	1808
1809	-7.19		-2.74			0.62			-0.84	-0.25	-1.67	8.07	1809
1810	-2.18	-2.36	-2.41	-2.45	−6.4 5	-0.68	-2.13	-0.68	-1.84	-1.23	-4.13	-2.20	1810
1811	2.98	-2.74	3.64	-2.04	-0.69	0.42	-0.91	-2.66	-1.05	-1.90	-0.10	-2.06	1811
1812	1.18	1.85	-3.37	-1.89	0.55		-2.58						1612
1813	1.32				-0.71	-1.58	1.87	0.08		-2.89		-1.48	1813
	1						2101	2.00	1 2.00		2.00		

XCIII.

FINLAND. - TORNEA (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Resumur.

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Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	-	•	0	•		-	•	-	-	-	-	-	
1814	-7.01	2.71	-1.85	0.92	-0.59	2.44		4.46	2.60	0.44	-0.15	-4.50	1814
1815	1.22	3.16	0.66	5.27	8.22	5.58	4.70	5.03	4.02	8.88	4.80	4.82	1815
1816	2.27	-8.28	-4.25	0.50	-8.05	-0.12	0.18	-0.41	1.97	0.16	1.17	2.29	1816
1817	3.54	-2.18	-2.78	0.19	2.42	-1.14	0.65	-1.84	-0.36	-1.14	-0.07	-2.85	1817
1818	3.46	-8.84	-1.07	-2.61	-8.48	-0.92	2.98	-2.55	0.09	1.08	2.89	5.83	1818
1819	4.47	-0.15	-0.50	-2.07	0.23	1.46	2.90	2.22	1.04	-4.58	-8.62	-2.15	1819
1820	-5.74	-0.22	-0.63	-1.82	-0.78	1.62	0.13	-0.17	0.18	-2.17	-1.94	-2.67	1820
1821	-2.18	1.12	0.50	0.83	1.24	-3.70	-2.44	-1.82	-0.58	8.58	-1.52	-4.18	1821
1822	0.13	6.44	5.68	4.22	1.67	-1.89	-0.89	1.75	-0.14	0.47	-2.05	4.46	1822
1823	-4.01	-1.08	4.15	0.66	0.87	-0.43	-0.09	-0.78	-0.86	2.06	-1.38	1.26	1828
1824	0.71	4.20	1.75	-0.22	-0.40	0.29	-0.89	-0.73	1.25	-2.18	-1.01	-0.96	1824
1825	8.99	1.42	1.83	1.78	-0.29	-0.48	-1.53	-0.17	6.84	2.14	2.85	8.20	1825
1826	1.99	4.70	4.99	0.50	2.65	1.56	2.28	1.70	-0.70	2.67	3.23	8.74	1826
1827	0.03	0.00	0.59	-2.13	2.39	1.79	-2.00	-1.64	1.21	-1.53	-0.56	5.68	1827
1828	-0.50	- 0.84	-1.77	-0.66	2.84	0.18	-1.78	-0.73	-2.86	1.18	0.50	1.69	1828
1829	1.26	-4.27	-2.69	-2.58	1.26	-0.81	0.80	-1.82	0.88	-1.78	-0.58	2.86	1829
1830	0.99	0.80	2.08	-0.54	-1.10	-0.66	-0.89	-1.78	-0.88	-0.08	8.44	-1.22	1830
1831	-3.98	-0.07	-2.81	2.01	0.98	1.98	0.81	0.79	-0.54	0.01	2.99	1.69	1881
1832	5.26	8.25	3.64	2.92	0.10	0.51	-1.11	-1.22	-8.67	2.86			1832
Means.	-12.55	-10.76	-7.19	-1.62	4.01	10.59	13.05	10.81	6.22	0.26	-6.27	-10.82	Means.
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XCIV. NORTH AMERICA. — ALBANY, N. Y.

1826	1.92	2.44	1.65	-1.02	3.28	1.07	0.72	1.09	1.57	1.46	0.81	0.85	1826
1827	-2.91	1.07	1.15	1.62	-0.02	0.05	0.55	0.08	0.43	1.14	-1.72	0.77	1827
1828	2.80	4.52	2.10	-0.88	0.76	2.66	-0.41	1.33	0.35	-0.81	0.76	8.17	1828
1829	-0.21	-2.27	-0.87	0.12	2.09	0.03	-1.54	-0.42	-1.98	0.92	0.50	3.63	1829
1830	0.28	-0.11	1.41	3.64	-0.21	-0.92	0.81	0.27	0.19	1.42	3.88	4.71	1830
1831	-1.80	-1.03	2.77	1.89	1.07	2.11	0.82	1.01	1.00	1.52	0.68	-4.94	1831
1832		-0.87		-1.29				-0.81		1			1832
1888		-1.84			1			-1.47					1833
1834	-1.18							-0.03		_		-1.18	l l
1885								-0.90	1	1		-3.06	
1000	1.00	1.00	0.00	-1.05	70.07	7.54	0.40	0.50	-2.14	1.20	0.51	3.00	1000
1886	-0.85	-3.89	-8.48	-2.27	-0.95	-1.80	0.20	-2.89	-0.39	-8.06	-0.62	-0.92	1886
1837	-3.40	-0.72	-1.94	-2.02	-1.23	0.07	-0.95	-0.98	-0.60	-0.89	0.38	-0.49	1887
1888	8.84	-4.01	0.97	-3.07	-1.26	1.78	0.81	0.27	0.36	-0.6 8	-1.47	-2.11	1888
1839	-0.25	1.62	0.14	0.79	-0.79	-1.79	0.15	-0.14	0.41	0.99	-0.94	-0.19	1839
1840	-3.32	8.14	0.60	1.32	0.96	-0.14	0.94	0.81	-0.91	0.28	0.28	-1.26	1840
1841	1.95	-0.72	-1.19	-2.58	-1.18	1.90	0.	1.23	0.88	-1.72	-0.49	0.86	1841
1842	2.08	_				-0.98						-1.69	
1843		-3.06				•		ı			-1.11	1 1	
1844	-	-0.15		ł	1	l .	i	-0.19	ı		-0.20	1 1	1 1
											- 0.20		1044
Means.	-3.58	-8.08	1.28	7.04	12.38	16.02	17.80	16.86	13.06	7.64	2.70	-1.65	Means.

XCV.

NORTH AMERICA. - SALEM, MASS.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

						4 1000 0.	Kesum						
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.	Year.
1787	0.40	° -1.87	0.24	 _0.24	-0.61	-0.84	-1.53	-0.28	° -1.13	° -1.00	o 0.58	0.07	1787
1788		-2.15		-0.47	1	-1.89		1			2.03	-1.60	1788
1789		-2.81	-0.65		-1.94	0.61	1	l .	-0.47		0.47	1.18	1789
1790		-1.04			-0.50		l		-1.02	· ·	-0.97	-2.82	1790
1791		-1.48	0.90				-0.08		-0.69		-0.42	0.07	1791
													1 1
1792	-2 .94	-0.87	1.79	0.87	1.61	-0.84	-0.64	-0.28	-1.80	0.77	0.92	-1.15	1792
1793	1.08	0.70	1.42	1.51	2.55	2.07	0.59	0.75	0.87	-0.09	0.07	-0.10	1793
1794	0.95	-0.25	1.91	1.19	1.16	0.11	0.52	0.58	0.75	-1.26	-0.16	4.35	1794
1795	0.20	-0.50	0.54	0.21	0.39	0.12	-0.31	1.85	1.04	1.24	0.86	1.51	1795
1796	1.18	0.12	-0.87	1.17	-0.11	0.40	0.89	0.80	-0.06	-0.55	-1.26	-8.02	1796
						٠							
1797	-1.15	2.24	0.55		l	0.41	1.40	l i		-0.83			1797
1798	0.68	-0.89	0.54	0.76		0.60	0.46	1	0.83		-1.57		1798
1799	0.28	0.08	0.81	0.51	0.63	0.58	0.45		1		-0.58	1 1	1799
1800	0.31	0.24	-0.81	1.92	-0.12	1.22	1.15	0.11	0.04	0.43	-0.93	1.63	1800
1501	0.40	0.46	1.51	0.21	1.69	0.08	0.35	0.49	1.41	0.96	0.17	0.30	1801
1802	8.79	-0.16	0.76	0.81	-1.34	0.13	0.13	0.88	1.19	1.87	1.23	1.19	1802
1803	1.12	2.15	0.67	0.38	1	0.13	-0.08	1.09			-0.71	1.99	1803
1804	-0.48	0.08	-0.48		1.55	0.20	-0.25	1	0.28		0.16		1804
											0.18		1805
1805	-1.46	1			0.91	0.11	1.40			-0.82			
1806	0.48	1.60	-1.03	-2.28	-0.44	-0.19	-1.12	-0.77	-U.0Z	-0.04	0.15	-0.06	1806
1807	-1.05	-1.13	-1.80	-0.81	-0.80	-0.62	0.05	0.00	-1.08	0.22	-0.65	2.45	1807
1808	0.13	1.41	1.55	0.87	-0.74	0.04	-0.15	-0.86	0.54	-0.72	0.69	0.72	1808
1809	-1.15	-1.73	-1.36		1	-0.42	i	I	l .	3.00	-2.19	2.04	1809
1810	0.11	0.95	-0.68		1	0.04	-0.93	i .	0.46	-0.12	-0.24	-0.34	1810
1811	0.80	0.14	1.69		0.65	0.43	0.16			1.74	0.67	-0.84	1811
		! '			l								
1812	-1.51		-2.6 8				i		-2.07				1812
1813	-1.09		-2.55		1	l l	-1.17			-0.62		-0.70	1813
1814	-0.73	0.80	-0.51	1.08	0.76	-1.58	-0.80	-0.94	-0.57	-0.07	0.39	-1.78	1814
1815	-0.93	-1.98	0.28		1		1.12	-1.82	-0.50	-0.69		−0.45	1815
1816	-0.16	0.07	-2.14	-0.44	-1.86	-2.3 6	-2.49	-1.81	-1.77	0.17	1.79	0.81	1816
1817	-0.71	_8 49	-1.43	_0.70	-0 44	_1 &K	_0 K0	-0.76	0.19	-0.70	0.78	0.68	1817
1818	-0.51	-3.56	. 1	-0.75 -2.31	i	1.17	0.85		-0.84	0.61	1.92		1818
1819	2.45	4.91	1	-2.31 -1.06		1.88	0.64	0.59	1.68	0.64		-0.48	1819
1820	-1.51	1.00		-0.07		0.51	1.95					-2.49	1820
1821	-1.51 -2.75	1.50	1	-0.07 -0.97		0.86	-1.08	•		-0.05	0.42		1821
1021	_2.75	1.50	-0.00	70.87	-v.57	U-30	-1.08	0.53	-0.11	~0.00	U.4Z	_1.91	1021
1822	-1.60	-0.50	1.64	-0.87	1.77	0.09	0.44	0.06	1.84	0.75	0.96	0.12	1822
1823	0.37	-1.99	-0.99	0.20	-1.19	-0.42	-0.19	0.85	-1.63	-0.58	-1.72	0.52	1823
1824	2.28	0.47	-0.11		l .	-0.59	-0.14	-1.08	0.12	0.21	-0.61	1.48	1824
1825	1.80	1.27	2.16	1.49	0.69	1.74	2.86	-0.12	-1.05	0.70	-0.14	0.62	1825
1826	0.96	1.11	0.10	-1.05	2.95	0.04	1.56		0.78	0.23	0.19	0.55	1826
1827	-1.49	0.52	0.64		-0.03	-0.60	-0.8 5	i	1	1.18	-2.74		1827
1828	2.42	4.05	1.10	-U.97	-0.68	1.06	0.86	0.96	0.87	-0.19	1.17	2.04	1828
Means.	-2.84	-1.85	1.54	6.96	11.05	15.61	17 07	17 17	13.80	8.56	2 50	-0.63	Means.
		,	1.04	0.00	11.05	10.01	11.97	17.17	12.00	6.00	5.03	-0.03	

XCVI.

ICELAND. — REIKIAVIK.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Resumur.

Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	_			-	-	-	-	-	-	-	-	_	
1823	1.80	-0.56			-0.60					-1.50		-0.86	1823
1824	-0.82	0.61	-0.05	2.16	2.95	4.68	8.12	1.58	-0.78	-2.37	-3.64	-8.99	1824
1825	-1.07	-0.40	8.04	0.98	0.50	0.88	1.70	0.66	2.84	1.68	-0.81	-0.92	1825
1826	-0.19	2.84	2.15	-0.79	1.58	-1.10	-0.75	-0.18	1.24	1.12	0.36	1.17	1826
1827	-0.72	1.98	-8.80	-0.86	0.67	0.86	0.14	1.78	0.64	2.29	2.26	0.88	1827
ŀ					1				٠ .	l	1	1 1	
1828	1.98	2.48	1.54	1.29	2.37	0.53	8.15	3.98	8.07	8.26	0.94	2.77	1828
1829		-0.09					i		-0.20	1			1829
1830	1.89		-1.22				-0.80					-2.60	1830
1831		-0.95			-1.76		1	-1.85			-0.76		1831
1832	1		-1.77	1	-2.20		l					-0.29	2002
1001	0.1.2	0.20										5.25	
												ا ـ ـ ا	1832
1838	1	-0.18		ľ	-0.57		l		1	l	l	-1.64	1888
1834	-0.43				-1.85			ŀ		i			1834
1835	11 1				-2.35		ı		1	1	1.58		1835
1836	H			1		1		ı	-1.80	-1.67	-1.52	-1.95	1886
1837	-0.42	0.48	-2.28	-1.91	-2.07	-0.32	0.40		•••	••	• • •	••	1837
Means.	-1.00	-1.60	-1.07	1.84	5.54	8.67	10.78	9.27	6.42	2.19	-0.60	-1.15	Means.

XCVII. GREENLAND. -- GODTHAAB.

1796			• •	• •		• •	• •	•••		-2.52	1.51	2.19	1796
1797	0.91	-2.08	-0.78	-1.96	1.14	0.27	1.40	1.31	0.77	1.02	2.22	0.87	1797
1798	-1.30	0.58	3.98	0.08	0.37	-0.39	0.39	0.07	-0.87	-0.67	0.88	-0.08	1798
1799	-0.40	3.09	-1.87	0.47	0.37	-0.71	-0.47	-0.72	0.62	-0.43	-0.91	4.72	1799
1800	2.75	0.22	2.32	-0.68	1.52	1.05	0.35	0.88	-0.42	0.48	0.05	0.07	1800
i l									1				
1801	-0.86	2.63	0.00	-1.00	-2.86	-1.61	0.89	0.92	-0.89	0.19	0.22	1.94	1801
1802	1.85	-2.99			-0.44		•••						1802
1816									-0.12		-0.01	1 1	1816
1817			-4.17									-1.78	1817
1818			-4.00		-0.90				_			-0.42	1818
2020	0.00	0.10	1.00	2.00	0.00	0.02	0.02	0.10	0		1.02	0.22	1010

1819	-2.74		-0.85		-0.91								1
1820	4.16	0.14		-2.15			-0.96	-1.57	-0.72	-0.06	1.60	1.19	1
1821	0.04	0.42	1.80	1.00	-0.07	0.68	••	• • •		• •	••	• • •	1821
1841	••	• •	• •	• •		• •		• •	0.45	0.14	-0.27	0.23	1841
1842	1.13	-1.15	-1.12	1.56	2.03	0.37	0.89	0.84	1.39	1.95	-0.87	-1.87	1842
						1	l	1		l			
1843	0.11	4.74	4.65	2.18	1.18	1.16	1.52	0.72	1.57	1.66	-2.89	-8.98	1843
1844	-0.13	0.40		ľ	-1.29		1	1.39	1	1	-1.08	0.01	1844
1845	1.54	0.76	8.98	2.84		0.82							1845
Means.	-8.72	-8.64	-7.29	-4.44	0.07	3.15	4.41	3.98	1.62	-0.96	-4.47	-6.45	Means.



CORRECTIONS

FOR

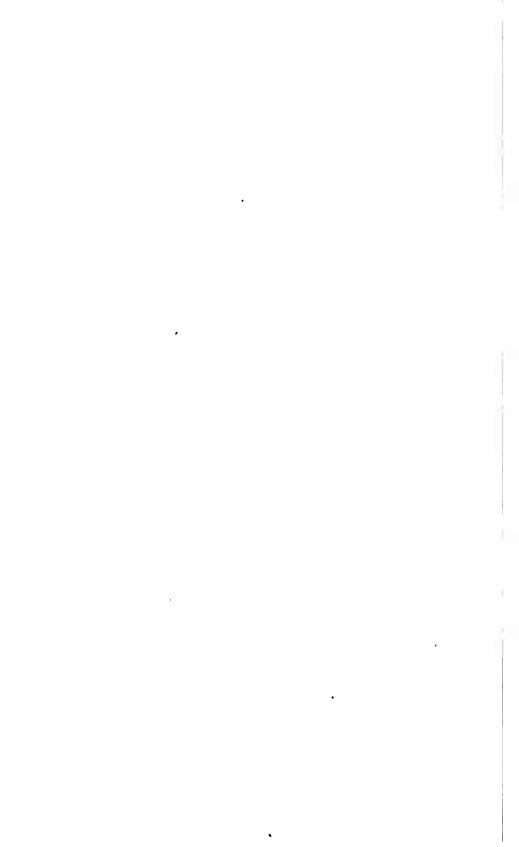
FORCE OF VAPOR AND RELATIVE HUMIDITY.

HOURLY CORRECTIONS FOR PERIODIC VARIATIONS,

OR

TABLES

FOR REDUCING THE MEANS OF THE OBSERVATIONS TAKEN AT ANY HOUR OF THE DAY TO THE TRUE MEAN FORCE OF VAPOR AND RELATIVE HUMIDITY OF THE DAY, OF THE MONTH, AND OF THE YEAR.



XCVIII.

England. — Greenwich. Lat. 51° 29' N.; Long. 0° 0'.

Corrections to be applied to the Means of the Hours of Observation, or Sets of Hours, to obtain the true Mean Force of Vapor for the respective Months. (GLAISHEE.)

English Inches.

									1				
Hours.	Jan.	Feb.	March.	Apçil.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
Midn	.006	.006	.008	017	.026	.081	.028	.025	.024	.018	.010	.009	.017
1	.011	.008	.010	.021	.028	.087	.081	.081	.080	.020	.012	.010	.021
2	.015	.010	.011	.024	.031	.043	.086	.035	.035	.021	.015	.010	.024
8	.015	.011	.018	.027	.082	.048	.088	.039	.087	.028	.017	.011	.026
i			ļ	1			i	l				l	i
4	.015	.018	.015	.029	.081	.047	.087	.040	.040	.025	.019	.011	.027
5	.015	.014	.016	.029	.027	.037	.081	.038	.040	.023	.021	.011	.025
6	.014	.015	.016	.025	.019	.022	.019	.029	.083	.021	.021	.010	.020
7	.013	.014	.014	.016	.007	.008	.007	.014	.022	.018	.018	.009	.013
							ļ				ĺ		l
8	.010	.010	.010	.005	005	004	004	.000	.010	.011	.012	.007	.005
9	.007	.006	.005	.005	016	015	1	012	005	.005	.005	.005	002
10	.002	.000	003	013	024	027	019	021	019	005	004	.001	010
11	004	005	007	ſ	028			027		009	010	004	017
								1	İ	i			ļ
Noon	007	009	612	026	030	042	029	080	080	015	017	007	021
. 1	008	013	018	027	080	045	083	082	030	018	019	008	028
2	007	015	018	027	028	048	084	084	029	017	020	008	023
8	007		012	1	026			081	027	014	016	008	021
1			'								İ	1	
4	007	010	01 0	020	021	035	028	027	021	009	010	007	017
5	004	006	006	014	015	ı	021		017	006	005	005	012
6	002	004	002	006	010	017	016	l	ı		.000	003	007
7	001	001	.002	.001	004		1	1	ı	.003	.004		
								1	ŀ	1			
8	.000	.001	.004	.005	.005	.005	.004	.004	.004	.005	.006	.001	.004
9	.000	.003	.005	.007	.018	.015	.010	.010	.008	.008	.008	.004	.007
10	.001	.004	.007	.010	.017	.023	.017	.015	.018	.011	.009	.005	.011
11	.002	.005	.008	.014	.022	.029	.024	.020	.018	.014	.010	.006	.014
					ĺ		1				ļ		1
									ł				
6.6	.006	.005	.007	.009	.005	.003	.001	-007	.012	.008	.010		.006
7. 7	.006	.006	.008	.009	.001	.000	.000	.004	.009	.011	.011	.004	.005
8.8	.005	.005	.007	.005	.000	.000	.000	.002	.007	.008	.009	.004	.005
9. 9	.003	.004	.005	.006	002	.090	1	001	.002	.006	•	.004	.008
10.10	.001	.002	.002	002	003	002	001	008	003	.003	.002	.008	.000
7. 2. 9	.002	.001	.002	001	003	007	006	003	.000	.003	.002	.002	001
												00-	
6. 2. 8	.002	.000	.002	.001	001	005	004	000	.008	.003	.002	.001	.000
6. 2.10	.003	.001	.003	.003	.002	.001	.001	.003	.006	.005	.003		
6. 2. 6	.002	001	.000	003	006	013	010	007	002	.000	.000	000	003
										000		000	00-
7. 2	.003	000	.000		011		014		003	.000	ł	.000	1
8. 2	.001	002	001		017	l	019		009	003	l .		•
8. 1	.001	001	001	011	017	•	018		1	1	1	000	1
7. 1	.002	.000	.000	005	012	018	013	009	004	000	000	.000	005
0.10.00		000	000	020	^1-		010	_ ^ ~	_ ^10	_ ^^	_ ^~	_ 607	009
9.12.3.9	002	003	008	010	015	020	016	016	013	004	005	001	009

XCIX.

England. — Greenwich. Lat. 51° 29' N.; Long. 0° 0'.

Corrections to be applied to the Means of the Hours of Observation, or Sets of Hours to obtain the true Mean *Humidity* for the respective Months. (GLAISHER.)

Thousandths.

						housend							
Hours.	Jen.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Midn	013	021	068	095	087	105	091	096	060	053	018	011	061
1	.002	021	065	106	100					059	009	012	064
2	.004	026	066	116	108	125	107	118		066	011	017	069
3	008	033	067	128	113	182	116	117	091	070	020	019	075
	•	1											
4	013	086		•				128			030		
5	019	035	066				120	•	•	•	030	024	060
6	021	084			1	107				071	033	026	
7	02 0	030	055	080	009	065	055	061	080	058	031	025	062
8	020		085	065	024	015	005	020	047	087	021	018	027
9	020 017	020 007	008	084	.018	.035	.041	.030	.000		008	007	: I
10	004	.009	.081	015	.051	.078	.080	.070	.042	.025	.008	.008	
11	.011	.028	.060	1	.083	.100		.102	.082	.060	.027	.022	
**		""				-100	-104	1.102		.500			
Noon	.081	.045	.084	.070	.110	.128	.114	.127	.M5	.088	.040	.033	.082
1	.054	.058	.100	.132	.126	.137	l	.142	.181	.109	.050	.046	.100
2	.059	.065	.106		.125	.185	.128	.145	.182	.118	.054	.048	.106
8	.048	.065	.104	.147	.118	.123	.121	.188	.126	.108	.047	.036	.096
					l		1	İ		'			1 1
4	.036	.058	.087	.128	.108	.118	.111	.120	.103	.089	.032	.024	.084
5	.021	.082	.063	.110	.091	.099	.095	.100	.071	.055	.018	.013	
6	.007	.009	.088	.068	-074	.078	.062	.071	.044	.080	.005	.004	
7	005	010	.010	.059	.052	.049	.025	.086	.009	.007	005	003	.019
_													
8	014		010	ł	.022			1	•			005	, ,
9		029	032				•	038		025	017		1 . 1
10		080	048		050	ı		1				008	1
11	018	086	060	080	075	065	080	085	071	048	02 0	009	000
		ŀ											1
6. 6	007	012	012	012	005	015	017	018	027	020	014	011	015
7. 7	012	ı	1					012					
8. 8	1	021		022			t .	010		i i	016		
]		1											
9. 9	016	018	018		.000	.005	.000		0 2 0		012	007	1 1
10.10	011	010	009	087	.000	.009	.006	-001	1	007	006	.000	1 1
7. 2. 9	.008	.002	-006	.014	.016	.015	.009	.015	.004	.010	.002	.005	.009
									010	010	000	000	010
6. 2. 8	.008	.008	.011	.019	.021	.013	.004	.013	.016	.010	.003	.006	1 1
6. 2.10	006	.000	002	006	003	010	014	009	008 026	.001 .024	.000	.005	009 .025
6. 2. 6	.015	.018	.027	.042	.038	.035	.029	.086	.020	.UZ4	.009	*009	.020
7. 2	.019	.017	.026	.086	.088	.035	.084	.042	.026	.027	.012	.011	.026
8. 2	.019	.022	.036	.048	.050	.060	.059	.062	.042	.088	.016	.015	
8. 1	.015	.019	.032	.034	.051	.061	.057	.061	.042	.036	.014	.014	1 1
7. 1	.017	.014	.023	.026	.083	.036	.032	.041	.025	.026	.009	.010	
' -													
9.12.8.9	.011	018	.038	.088	.082	.064	.059	.064	.050	.040	.016	.014	.087
لــــــــــــــــــــــــــــــــــــــ		<u> </u>				<u> </u>							

METEOROLOGICAL TABLES.

VI.

MISCELLANEOUS TABLES,

useful in

TERRESTRIAL PHYSICS AND METEOROLOGY.

1

F



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1.

POSITIONS OF THE PRINCIPAL OBSERVATORIES.

[From the American Nautical Almenac.]

(North Latitudes and West Longitudes are considered as positive.)

Place.	Latitude.	Longitude from Washington in Time.	Longitude from Washington in Arc.	Longitude from Greenwich in Arc.
Åbo,	+60 26 56.8	h. m. s. - 6 37 20.0	260 40 0.6	887 42 48.6
Altona,	58 32 45.3	5 47 57.4	278 0 89.8	350 3 27.8
Athens,	3 7 58 20	6 48 6.4	259 18 24.2	836 16 12.2
Berlin,	52 30 16.7	6 1 46.1	269 83 28.1	346 86 16.1
Bilk,	51 12 25	5 85 16.1	276 10 58.1	858 18 46.1
Bonn,	50 48 45.0	5 86 85.7	275 51 5.1	852 58 53.1
Breslau,	51 6 56.0	6 16 21.2	265 54 42.0	842 57 30.0
Brussels,	50 51 10.7	5 25 88.8	278 35 18.0	355 38 6.0
Cambridge (Eng.),	52 12 51.8	5 8 84.7	282 51 18.9	859 54 6.9
Cambridge (Mass.),	+42 22 48.6	0 23 41.5	854 4 86.9	71 7 24.9
Cape of Good Hope,	-83 56 8	6 22 7.2	264 28 12.3	341 81 0.3
Christiania,	+59 54 48.7	- 5 51 6.0	272 13 30.6	849 16 18.6
Cincinnati,	89 5 54	+ 0 29 46.9	7 26 42.8	84 29 80.8
Copenhagen,	55 40 53.0	- 5 58 30.5	270 22 22.5	847 25 10.5
Cracow,	50 8 50.0	6 28 2.4	262 59 28.4	840 2 11.4
Dorpat,	58 22 47.1	6 55 5.8	256 13 83.6	333 16 21.6
Dublin,	53 23 13	4 42 49.2	289 17 42.0	6 20 30.0
Durham,	54 46 6.4	5 1 58.2	284 31 42.0	1 34 30.0
Edinburgh,	55 57 28.2	4 55 28.2	286 7 57.0	8 10 45 .0
Florence,	43 46 40.8	5 53 12.9	271 41 47.1	848 44 85.1
Geneva,	46 11 58.8	- 5 82 48.9	276 47 46.8	858 50 84.8
Georgetown,	88 54 26.1	+ 0 0 6.2	0 1 83.0	77 4 21.0
Göttingen,	51 81 47.9	- 5 47 57.8	273 0 40.5	850 8 28.5
Gotha,	50 56 5.2	5 51 6.9	272 18 17.1	849 16 5.1
Greenwich,	51 28 8 8.2	5 8 11.2	282 57 12.0	0 0 0
Hamburg,	58 83 7	- 5 48 4.8	272 58 48.6	850 1 36.6
Hudson,	41 14 42.6	+ 0 17 82.1	4 23 0.9	81 25 48.9
Kasan,	55 47 28.1	- 8 24 48.1	233 49 13.1	310 52 1.1
Königsberg,	54 42 50.4	6 30 11.6	262 27 6.6	839 29 54.6
Kremsmünster,	48 3 23.8	6 4 41.6	268 48 50.7	845 51 88.7
Leipsic,	51 20 20.7	5 57 89.7	270 85 4.5	847 37 52.5
Leyden,	52 9 28.2	5 26 8.6	278 27 50.6	355 30 38.6
Liverpool,	58 24 47.7	4 56 11.1	285 57 13.7	8 0 1.7
London,	51 81 29.8	5 7 84.1	288 6 28.5	0 9 16.5
Madras,	+18 4 9.2	-10 29 8.2	202 42 57.0	279 45 45.0

Place.	I.a	titu	de.	from V	ngita Vash Tim	ington	from V	ngita Vash a Arc	ington	from G	ngiti reen Arc.	wich
Mannheim,	+49	29	12.9	h -5	_	2.7	274		19.5	351		7.1
Markree,	54	10	31.7	4	34	22.8	291	24	18.0	8	27	6.
Marseilles,	48	17	49	5	29	40.2	277	84	57.2	354	87	45.
Milan,	45	28	0.7	5	44	57.8	278	45	82.4	350	48	20.
Modena,	44	38	52.8	5	51	55.2	272	1	12.5	349	4	0.
Moscow,	55	45	19.8	7	38	28.5	245	22	52.7	222	25	40.
Munich,	48	8	45	5	54	87.6	271	20	35.4	348	23	23.
Naples,	40	51	46.6	6	5	12.1	268	41	58.1	345	44	46.
Olmütz,	49	35	40.0	6	17	11.3	265	42	10.5	342	44	58.
Oxford,	51	45	86.0	5	8	8.6	284	12	51.0	1	15	39 .
Padua,	45	24	2.5	5	55	40.2	271	4	56.6	348	7	44.0
Palermo,	+38	6	44	-6	1	36.7	269	85	50.1	846	88	38.
Paramatta,	-83	48	49.8	+8	47	42.6	131	55	88.8	208	58	26.
Paris,	+48	50	13.2	-5	17	82.7	280	36	50.1	857	39	38.
St. Petersburg,	59	56	29.7	7	9	24.7	252	88	49.8	329	41	37.
Philadelphia,	89	57	7.5	0	7	83.6	358	6	85.4	75	9	23.
Prague,	50	5	18.5	6	5	58.2	268	31	42.6	345	34	80.0
Pulkowa,	59	46	18.7	7	9	29.9	252	37	81.9	329	40	19.
Rome,	41	53	54	5	58	5.9	270	28	31.5	347	81	19.
San Fernando,	+36	27	45	4	43	22.1	289	9	29.1	6	12	17.
Santiago,	-33	26	24.8	0	25	52.3	353	31	55.5	70	34	48.
Senftenberg,	+50	5	10.1	6	14	1.1	266	29	43.1	343	32	31.
Vienna,	48	12	35.5	6	13	43.7	266	84	4.1	343	3 6	52.
Washington,	88	53	89.8	0	0	0	0	0	0	77	2	48.0
Wilna,	+54	40	59.1	-6	49	28.0	257	89	15.5	834	42	8.8

11. TO CONVERT PARTS OF THE EQUATOR IN ARC INTO SIDIREAL TIME, OR TO CONVERT TERRESTRIAL LONGITUDE IN ARC INTO TIME.

				<u></u>	D	39 R 3 R 5.					
	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.
Arc.	1100			Arc.		- Arc		Art.	I ma	AIC.	
٩	h.m.	41	h. m. 2 44	81	h. m. 5 24	121	h. m. 8 4	0 161	h. m. 10 44	201	h. m. 13 24
1 2	0 8	42	2 48	82	5 28	122	8 8	162	10 48	202	13 28
8	0 12	48	2 52	83	5 82	123	8 12	163	10 52	203	13 32
4	0 16	44	2 56	84	5 86	124	8 16	164	10 56	204	13 36
5	0 20	45	3 0	85	5 40	125	8 20	165	11 0	205	13 40
6	0 24	46	8 4	86	5 44	126	8 24	166	11 4	206	18 44
7	0 28	47	8 8	87	5 48	127	8 28	167	11 8	207	13 48
8	0 32	48	8 12	88	5 52	128	8 32	168	11 12	208	18 52
9	0 86	49	8 16	89	5 56	129	8 36	169	11 16	209	18 56
10	0 40	50	8 20	90	6 0	130	8 40	170	11 20	210	14 0
11	0 44	51	8 24	91	6 4	131	8 44	171	11 24	211	14 4
12	0 48	52	8 28	92	6 8	182	8 48	172	11 28	212	14 8
18	0 52	58	8 32	98	6 12	188	8 52	178	11 32	213	14 12
14	0 56	54	8 36	94	6 16	184	8 56	174	11 86	214	14 16
15	1 0	55	8 40	95	6 20	135	90	175	11 40	215	14 20
	!	56		96		136	9 4	176	11 44	216	14 24
16 17	1 4	57	8 44 8 48	97	6 24	137	9 4 9 8	177	11 44 11 48	217	14 24
18	1 12	58	8 52	98	6 82	188	9 12	178	11 52	218	14 82
19	1 16	59	8 56	99	6 36	139	9 16	179	11 56	219	14 36
20	1 20	60	4 0	100	6 40	140	9 20	180	12 0	220	14 40
						}					
21	1 24	61	4 4	101	6 44	141	9 24	181	12 4	221	14 44
22	1 28	62	4 8	102	6 48 6 52	142	9 28 9 32	182 183	12 8 12 12	222 223	14 48
23	1 32 1 36	68 64	4 12 4 16	104	6 56	144	9 36	184	12 12 12 16	224	14 52 14 56
25	1 40	65	4 20	105	7 0	145	9 40	185	12 20	225	15 0
26	1 44	66	4 24	106	7 4	146	9 44	186	12 24	226	15 4
27	1 48	67	4 28	107	7 8	147	9 48	187	12 28	227	15 8
28	1 52	68	4 32	108	7 12	148	9 52	188	12 82	228	15 42
29	1 56	69	4 86	109	7 16	149	9 56	189	12 36	229 230	15 16
80	2 0	70	4 40	110	7 20	150	10 0	190	12 40	230	15 20
31	2 4	71	4 44	111	7 24	151	10 4	191	12 44	231	15 24
82	2 8	72	4 48	112	7 28	152	10 8	192	12 48	232	15 28
83	2 12	73	4 52	118	7 82	153	10 12	193	12 52	233	15 82
84	2 16	74	4 56	114	7 86	154	10 16	194	12 56	234	15 36
35	2 20	75	5 0	115	7 40	155	10 20	195	13 0	235	15 40
				110		350	10.04	100	10 4	000	ا ا
86 87	2 24 2 28	76 77	5 4 5 8	116 117	7 44 7 48	156 157	10 24 10 28	196 197	13 4 13 8	236 237	15 44 15 48
38 38	2 32	78	5 12	118	7 52	158	10 28	198	13 12	238	15 45 15 52
89	2 36	79	5 16	119	7 56	159	10 86	199	13 16	239	15 56
40	2 40	80	5 20	120	8 0	160	10 40	200	18 20	240	16 0
773		-			<u> </u>	<u> </u>		L	<u> </u>	9	

TO CONVERT PARTS OF THE EQUATOR IN ARC INTO SIDEREAL TIME, OR 2 TO CONVERT TERBESTRIAL LONGITUDE IN ARC INTO TIME.

					Dags	LECES.					
Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.
•	h. m.	0	h. m.	0	h. m.	0	h. m.	•	h. m.	•	h. m.
241	16 4	261	17 24	281	18 44	301	20 4	321	21 24	841	22 44
242	16 8	262	17 28	282	18 48	802	20 8	822	21 28	842	22 48
243	16 12	263	17 32	283	18 52	808	20 12	828	21 32	848	22 52
244	16 16	264	17 86	284	18 56	804	20 16	824	21 36	344	22 56
245	16 20	265	17 40	285	19 0	805	20 20	325	21 40	845	23 0
246	16 24	266	17 44	286	19 4	806	20 24	826	21 44	846	23 4
247	16 28	267	17 48	287	19 8	807	20 28	827	21 48	847	23 8
248	16 82	268	17 52	288	19 12	808	20 82	828	21 52	848	23 12
249	16 86	269	17 56	289	19 16	809	20 86	829	21 56	849	23 16
250	16 40	270	18 0	290	19 20	810	20 40	830	22 0	850	28 20
251	16 44	271	18 4	291	19 24	811	20 44	331	22 4	851	23 24
252	16 48	272	18 8	292	19 28	312	20 48	832	22 8	352	28 28
253	16 52	273	18 12	293	19 82	313	20 52	333	22 12	858	28 32
254	16 56	274	18 16	294	19 36	814	20 56	334	22 16	854	23 36
255	17 0	275	18 20	295	19 40	815	21 0	835	22 20	355	23 40
256	17 4	276	18 24	296	19 44	816	21 4	836	22 24	856	28 44
257	17 8	277	18 28	297	19 48	817	21 8	337	22 28	857	23 48
258	17 12	278	18 82	298	19 52	318	21 12	838	22 32	858	23 52
259	17 16	279	18 86	299	19 56	819	21 16	889	22 36	359	23 56
260	17 20	280	18 40	800	20 0	820	21 20	840	22 40	360	24 0
					Мін	UTRS.					
í	m. s. 0 4	ú	m. s. 0 44	21	m. s. 1 24	31	m. a.	41	m. s. 2 44	51	m. s. 3 24
2	0 8	12	0 48	22	1 28	32	2 8	42	2 48	52	8 28
8	0 12	13	0 52	28	1 82	83	2 12	48	2 52	58	8 32
4	0 16	14	0 56	24	1 36	84	2 16	44	2 56	54	3 36
5	0 20	15	1 0	25	1 40	85	2 20	45	8 0	55	8 40
6	0 24	16	1 4	26	1 44	36	2 24	46	8 4	56	8 44
7	0 28	17	18	27	1 48	87	2 28	47	8 8	57	3 48
8	0 82	18	1 12	28	1 52	38	2 82	48	8 12	58	3 52
9	0 86	19	1 16	29	1 56	39	2 86	49	8 16	59	8 56
10	0 40	20	1 20	80	20	40	2 40	50	8 20	60	4 0
 		n	т	n —	 .	ONDS.					
ĩ	0.067	ű	0.783	21	1.400	81	2.067	41	s. 2.788	51	8.400
2	0.133	12	0.800	22	1.467	32	2.133	42	2.800	52	8.467
8	0.200	18	0.867	28	1.538	88	2.200	48	2.867	53	3.538
4	0.267	14	0.983	24	1.600	84	2.267	44	2.933	54	3.600
5	0.838	15	1.000	25	1.667	85	2.838	45	8.000	55	8.667
6	0.400	16	1.067	26	1.733	36	2.400	46	8.067	56	3.738
7	0.467	17	1.133	27	1.800	37	2.467	47	3.138	57	8.800
8	0.583	18	1.200	28	1.867	88	2.538	48	8.200	58	3.867
9	0.600	19	1.267	29	1.938	89	2.600	49	3.267	59	8.983
10	0.667	20	1.888	80	2.000	40	2.667	50	3.888	60	4.000

III. TO CONVERT SIDEREAL TIME INTO PARTS OF THE EQUATOR IN ARC, OR TO CONVERT TIME INTO TERRESTRIAL LONGITUDE IN ARC.

[-				Hot	TRG.					
Time.	Arc.	Time.	Arc	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.
h.	.0	h.	0_	h.	0	h.	0	h.	0	Ь.	0
1 2	15 80	5 6	75 90	9 10	185 150	13 14	195 210	17 18	255 270	21 22	815 830
8	45	7	105	11	165	15	225	19	285	23	345
4	60	8	120	12	180	16	240	20	300	24	360
- 		<u>'</u>		·	Мія	UTBS.		•		-	
m. 1	0 / 0 15	m. 11	2 45	m. 21	5 15	m. 81	7 45	m. 41	° ′ 10 15	m. 51	0 , 12 45
2	0 80	12	8 0	22	5 30	32	8 0	42	10 10	52	13 0
8	0 45	13	8 15	28	5 45	88	8 15	48	10 45	58	13 15
4	1 0	14	8 80	24	6 0	84	8 30	44	11 0	54	18 30
5	1 15	15	8 45	25	6 15	85	8 45	45	11 15	55	13 45
6	1 80	16	4 0	26	6 30	36	9 0	46	11 30	56	14 0
7	1 45	17	4 15	27	6 45	37	9 15	47	11 45	57	14 15
8	2 0	18	4 80	28	7 0	88	9 80	48	12 0	58	14 30
9	2 15 2 30	19 20	4 45 5 0	29 30	7 15	89	9 45	49	12 15	59	14 45
10	2 30	20	8 0	30	7 80	40	10 0	50	12 30	60	15 0
ļ						ONDS.					
1	0 15	11	2 45	21	5 15	81	7 45	41	10 15	51	12 45
2	0 80	12	8 0	22	5 30	32	8 0	42	10 80	52	13 0
8	0 45	18	8 15	28	5 45	88	8 15	43	10 45	58	18 15
4	1 0	14	8 30	24	6 0	84	8 30	44	11 0	54	13 30
5	1 15	15	8 45	25	6 15	35	8 45	45	11 15	55	13 45
6	1 80	16	4 0	26	6 80	86	9 0	46	11 30	56	14 0
7	1 45	17	4 15	27	6 45	87	9 15	47	11 45	57	14 15
8	2 0	18	4 80	28	7 0	38	9 80	48	12 0	58	14 80
9 10	2 15 2 30	19 20	4 45 5 0	29 80	7 15 7 80	89	9 45	49 50	12 15 12 30	60	14 45 15 0
				11 00	Тантиз о	<u></u>			12.00	,1 00	
8.	1 "			8.	1 "	E.		8.		6 .	
0.01	0.15	0.18	2.70	0.85	5.25	0.52	7.80	0.69	10.35	0.86	12.90
0.02	0.30	0.19	2.85	0.86	5.40	0.58	7.95	0.70	10.50	0.87	18.05
0.08	0.45	0.20	3.00 3.15	0.37	5.55 5.70	0.54	8.10 8.25	0.71	10.65 10.80	0.88	13.20 13.35
0.04	0.75	0.21	3.15	0.89	5.85	0.56	8.40	0.72	10.95	0.90	18.50
0.06	0.90	0.28	8.45	0.40	6.00	0.57	8.55	0.74	11.10	0.91	13.65
0.07	1.05	0.24	3.60	0.41	6.15	0.58	8.70	0.75	11.25	0.92	13.80
0.08	1.20	0.25	8.75	0.42	6.30	0.59	8.85	0.76	11.40	0.93	13.95
0.09	1.85	0.26	3.90	0.43	6.45	0.60	9.00	0.77	11.55	0.94	14.10
0.10	1.50	0.27	4.05	0.44	6.60	0.61	9.15	0.78	11.70 11.85	0.95	14.25
0.11	1.65 1.80	0.28	4.20	0.45	6.75 6.90	0.62	9.80 9.45	0.79	12.00	0.96	14.40 14.55
0.12	1.95	0.29	4.50	0.47	7.05	0.64	9.60	0.81	12.15	0.98	14.70
0.14	2.10	0.31	4.65	0.48	7.20	0.65	9.75	0.82	12.30	0.99	14.85
0.15	2.25	0.32	4.80	0.49	7.85	0.66	9.90	0.83	12.45	1.00	15.00
0.16	2.40	0.38	4.95	0.50	7.50	0.67	10.05	0.84	12.60	1	1
0.17	2.55	0.34	5.10	0.51	7.65	0.68	10.20	0.85	12.75	<u> </u>	

F

IV. FOR CONVERTING SIDEREAL TIME INTO MEAN SOLAR TIME, AND MEAN TIME INTO SIDEREAL TIME.

	Hours	3.			MIN	TES.				SECO)NDS.	
Hours	Mean Time.	Sidereal Time.	Min- utes.	Mean Time.	Sidereal Time.	Min- utes.	Mean Time.	Sidereal Time.	Sec- onds.	Mean or Sidereal Time.	Sec- onds.	Mean or Sidereal Time.
	m s.	m. s.		15.	5.		8.			B .	<u> </u>	E
1	0 9.83	0 9.86	1	0.16	0.16	81	5.08	5.09	1	0.00	81	0.09
2	0 19.66	0 19.71	2	0.83	0.33	32	5.24	5.26	2	0.01	32	0.09
8	0 29.49	0 29.57	8	0.49	0.49	38	5.41	5.42	8	0.01	33	0.09
4	0 39.32	0 39.43	4	0.66	0.66	84	5.57	5.59	4	0.01	34	0.09
5	0 49.15	0 49.28	5	0.82	0.82	35	5.75	5.75	5	0.01	85	0.10
6	0 59.98	0 59.14	6	0.98	0.99	36	5.90	5.91	6	0.02	36	0.10
7	1 8.81	1 9.00	7	1.15	1.15	87	6.06	6.08	7	0.02	37	0.10
8	1 18.64	1 18.85	8	1.31	1.31	38	6.23	6.24	8	0.02	38	0.10
9	1 28.47	1 28.71	9	1.47	1.48	39	6.39	6.41	9	0.03	39	0.11
10	1 88.30	1 38.57	10	1.64	1.64	40	6.55	6.57	10	0.03	40	0.11
							_				1	
11	1 48.18	1 48.42	11	1.80	1.81	41	6.72	6.74	11	0.08	41	0.11
12	1 57.96	1 58.28	12	1.97	1.97	42	6.88	6.90	12	0.03	42	0.12
13	2 7.78	2 8.13	13	2 13	2.14	43	7.05	7.06	13	0.04	48	0.12
14	2 17.61	2 17.99	14	2.29	2.80	44	7.21	7.28	14	0.04	44	0.12
15	2 27.44	2 27.85	15	2.46	2.46	45	7.37	7.39	15	0.04	45	0.12
16	2 37.27	2 87.70	16	2.62	2.63	46	7.54	7.56	16	0.04	46	0.13
17	2 47.10	2 47.56	17	2.79	2.79	47	7.70	7.72	17	0.05	47	0.13
18	2 56.93	2 57.42	18	2.95	2.96	48	7.86	7.89	18	0.05	48	0.13
19	3 6.76	8 7.27	19	8.11	8.12	49	8.03	8.05	19	0.05	49	0.13
20	3 16.59	8 17.13	20	3.28	8.29	50	8.19	8.21	20	0.06	50	0.14
												l
21	8 26.42	3 26.99	21	3.44	8.45	51	8.86	8.38	21	0.06	51	0.14
22	3 36.25	3 86.84	22	8.60	8.61	52	8.52	8.54	22	0.06	52	0.14
23	3 46.08 3 55.91	8 46.70 3 56.56	23 24	3.77	3.79 3.94	53 54	8.68 8.85	8.71 8.87	28 24	0.06	53 54	0.15
25	4 5.74	4 6.41	25	4.10	4.11	55	9.01	9.04	25	0.07	55	0.15
-				2		"		0.02		""	"	"
26	4 15.57	4 16.27	26	4.26	4.27	56	9.17	9.20	26	0.07	56	0.15
27	4 25.40	4 26.13	27	4.42	4.43	57	9.34	9.36	27	0.07	57	0.16
28	4 35.23	4 85.98	28	4.59	4.60	58	9.50	9.53	28	0.08	58	0.16
29	4 45.06	4 45.84	29	4.75	4.76	59	9.67	9.69	29	0.08	59	0.16
30	4 54.89	4 55.69	30	4.92	4.98	60	9.83	9.86	80	0.08	60	0.16
	l	<u> </u>		l 	<u> </u>	l		<u> </u>	<u> </u>	l	t	

v.

CORRECTION OF THE TIME OBTAINED BY OBSERVATION OF THE SUN, IN ORDER TO HAVE THE TRUE TIME OF THE CLOCK.

							,			;	, —		,		_	
Day of	Jan.	Feb.	Mar.	≜ pr.	Apr.	May.	June.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Dec.	Day of
Month.	Add.	Add.	Add.	Add.	Subt.	Subt.	Subt.	Add.	Add.	Add.	Subt.	Subt.	Subt.	Subt.	Add.	Month.
1	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	
1 1	4	14	13	4		8	3		3	6	0	10	16	11		1
2	4	14	12	4		8	2	• • .	4	6	0	11	16	10	 . .	2
8	5	14	12	8		8	2		4	6	1	11	16	10	ا ا	3
4	5	14	12	3		8	2		4	6	1	11	16	10		4
5	6	14	12	3		4	2		4	6	1	12	16	9		5
6	6	14	12	2		4	2		4	6	2	12	16	9		6
7	7	14	11	2		4	2		4	5	2	12	16	8		7
8	7	15	11	2		4	1		5	5	2	12	16	8		8
9	8	15	11	2		4	1		5	5	3	13	16	7		9
10	8	15	11	1		4	1		5	5	8	13	16	7		10
11	9	15	10	1		4	1		5	5	8	13	16	6		11
12	9	15	10	1		4	1		5	5	4	13	16	6		12
18	9	15	10	1		4	0		5	5	4	14	16	5		13
14	10	14	9	0		4	0		5	4	5	14	15	5		14
15	10	14	9	0		4	0		6	4	5	14	15	4		15
16	10	14	9	0		4	0		6	4	5	14	15	4		16
17	11	14	9	0		4	0		6	4	6	15	15	8		17
18	11	14	8		1	4		1	6	4	6	15	15	8		18
19	11	14	8]	1	4]	1	6	8	6	15	14	2		19
20	11	14	8		1	4		1	6	3	7	15	14	2		20
21	12	14	7		1	4		1	6	8	7	15	14	1		21
22	12	14	7		2	4]	2	6	8	7	15	14	1		22
23	12	14	7		2	4		2	6	2	8	16	13	0		23
24	12	18	6		2	8		2	6	2	8	16	13	0		24
25	13	13	6		2	8		2	6	2	8	16	13	0		25
26	13	13	6		2	8		2	6	2	9	16	12	• •	1	26
27	18	13	5		2	3		8	6	1	9	16	12		1	27
28	18	13	5		8	3		3	6	1	9	16	12		2	23
29	14	18	5		8	8		8	6	1	10	16	11		2	29
30	14		4		8	3	• •	3	6	0	10	16	11-		3	30
81	14	• •	4	• •	• •	8	••	••	6	0	• •	16	• •	••	8	31
"	!				!									1		

TABLE FOR COMPUTING TERRESTRIAL SURFACES.

The tables under No. VI. were published by Delcros in the Annuaire Météorologique de la France pour 1850, p. 65 et seq.

The formula from which they have been computed reads as follows: -

$$S = \frac{a \, b \, \pi}{90} \begin{cases} \sin \frac{1}{2} \phi \cos \left(L + \frac{1}{2} \phi\right) \\ -\frac{1}{3} \left[2 \cdot \left(\frac{a - b}{a + b}\right) + \left(\frac{a - b}{a + b}\right)^{2}\right] \sin \left(\phi + \frac{1}{2} \phi\right) \cos \left[3 L + \left(\phi + \frac{1}{2} \phi\right)\right] \\ +\frac{1}{5} \left[3 \cdot \left(\frac{a - b}{a + b}\right)^{2} + \left(\frac{a - b}{a + b}\right)^{2}\right] \sin \left(2 \phi + \frac{1}{2} \phi\right) \cos \left[5 L + \left(2 \phi + \frac{1}{2} \phi\right)\right] \\ - \text{etc.}; \end{cases}$$

in which $a=\frac{1}{2}$ great axis of the globe; $b=\frac{1}{2}$ small axis; L= the latitude of the lower limit of a quadrilateral surface; L'= the latitude of the upper limit of the same; $\phi=L'-L$; S= the area of a quadrilateral surface of one degree in longitude; $\pi=$ the ratio of the circumference to the diameter.

Substituting the numerical values, the quarter of the meridian being = 10,000,724 legal metres; the $\frac{1}{2}$ great axis, or $a_1 = 6,376,989$ metres; the $\frac{1}{2}$ small axis, or $b_1 = 6,356,323$ metres; the ratio of the axis $\frac{1}{3000,84}$; and making $\phi = 1^\circ$ nonagesimal, the formula becomes,

$$\mathbf{S} \doteq \left\{ \begin{array}{l} 224.996360 \; \cos \; (\;\; \mathbf{L} + 0^{\circ} \; 30') \\ -0.730851 \; \cos \; (3 \; \mathbf{L} + 1^{\circ} \; 30') \\ +0.001784 \; \cos \; (5 \; \mathbf{L} + 2^{\circ} \; 30') \\ -0.000004 \; \cos \; (7 \; \mathbf{L} + 3^{\circ} \; 30') \\ + \; \mathrm{etc.} \end{array} \right.$$

The first three terms of the formula give the results with sufficient accuracy.

In order to avoid too large a number of figures, the results are given in square miles, the linear base of which is a mile equal to $\frac{1}{15}$ of the mean degree of the meridian. That mile is thus $=\left(\frac{10000724}{90\times15}\right)=7407.942$ metres. In order to convert the results into new geographical miles, of which $60=1^\circ$, multiply by 16, $\log=1.2041200$; into common French leagues, $25=1^\circ$, multiply by 2.777778, $\log=0.4436975$; into nautical leagues, $20=1^\circ$, multiply by 1.777778, $\log=0.2498775$; into English statute miles, $69.163=1^\circ$, by 21.711034, $\log=1.3366868$.

USE OF THE TABLES.

Table I., which gives the number of square miles contained in the quadrilateral surfaces of one degree in latitude and longitude, successively from the equator to the pole, will be more frequently used. Table II. has been computed for maps on a smaller scale; and Tables III. and IV. for maps of very small scale, covering large areas, in which surfaces of one degree could not be estimated with sufficient accuracy. If the scale is large enough to have the minutes traced on, then Table V. is to be used.

For computing a surface by Table I., which may serve as an example for all the others, find first the lowest parallel circle which crosses, on the map, the surface to be estimated; suppose it is 40° lat. N., and the zone within 40° and 41° lat. N. contains four integral degrees of longitude, that is, four surfaces of one degree each way; then in the first column of the table, on the line beginning with latitude 40°, and in the vertical column headed 4, take the value of these four surfaces, viz. 685.88. Then take likewise the value of the number of surfaces between 41° and 42° lat. N., and so on. The fractional parts left outside of the integral degrees are best estimated, with the compass, in decimals, the values of which can be found in the columns of the multiples, by properly moving the decimal point to the left. Having taken them in that way, and summing them up with all the integral surfaces, we obtain the total surface required.

F

TABLE I. QUADRILATERAL SURFACES OF 1 DEGREE IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

Limi	ting UDES.			Multiples	of these Qu	adrilateral f	Surfaces fro	m 1 to 9.		
Inf.	Sup.	1.	9.	8.	4.	5.	6.	7.	8.	9.
0	1	224.259	448.52	672.78	897.04	1121.29	1345.55	1569.81	1794.07	2018.33
1	2	224.192	448.38	672.58	896.77	1120.96	1345.15	1569.35	1793.54	2017.73
2	8	224.059	448.12	672.18	896.24	1120.30	1344.86	1568.42	1792.47	2016.53
8	4	223.860	447.72	671.58	895.44	1119.30	1343.16	1567.02	1790.88	2014.74
4	5	228.594	447.19	670.78	894.37	1117.97	1841.56	1565.16	1788.75	2012.34
5	6	223.261	446.52	669.78	893.05	1116.31	1339.57	1562.88	1786.09	2009.35
6	7	222.863	445.78	668.59	891.45	1114.31	1387.18	1560.04	1782.90	2005.76
7	8	222.398	444.80	667.19	889.59	1111.99	1834.89	1556.78	1779.18	2001.58
8	9	221.867	443.78	665.60	887.47	1109.33	1831.20	1553.07	1774.93	1996.80
9	10	221-270	442.54	663.81	885.08	1106.35	1327.62	1548.89	1770.16	1991.43
10	11	220.607	441.21	661.82	882.48	1103.03	1323.64	1544.25	1764.85	1985.46
11	12	219.878	439.76	659.63	879.51	1099.89	1319.27	1589.15	1759.02	1978.90
12	13	219.064	438.17	657.25	876.84	1095.42	1314.50	1583.59	1752.67	1971.76
13	14	218.225	486-45	654.67	872.90	1091.12	1309.35	1527.57	1745.80	1964.02
14	15	217.800	434.60	651.90	869.20	1086.50	1303.80	1521.10	1738.40	1 955.7 0
15	16	216.311	432.62	648.98	865.24	1081.55	1297.86	1514.17	1730.48	
16	17	215.257	480.51	645.77	861.03	1076.28	1291.54	1506.80	1722.05	1937.31
17	18	214.138	428.28	642.41	856.55	1070.69	1284.83	1498.97	1713.10	1927.24
18	19	212.955	425.91	638.87	851.82	1064.78	1277.78	1490.69	1703.64	1916.60
19	20	211.709	423.42	686.13	846.84	1058.54	1270.25	1481.96	1693.67	1905.38
20	21	210.399	420.80	631-20	841.59	1051.99	1262.39	1472.79	1683.19	1893.59
21	22	209.025	418.05	627.08	886.10	1045.13	1254.15	1468.18	1672.20	1881.23
22	23	207.589	415.18	622.77	830.36	1087.95	1245.54	1453.12	1660.71	1868.30
28	24	206.090	412.18	618.27	824.86	1030.45	1236.54	1442.63	1648.72	1854.81
24	25	204.529	409.06	613.59	818.12	1022.63	1227.18	1431.71	1636.24	1840.76
25	26	202.907	405.81	608.72	811.68	1014.58	1217.44	1420.35	1623.25	1826.16
26	27	201.228	402.45	603.67	804.89	1006.11	1207.34	1408.56	1609.78	1811.00
27	28	199.477	898.95	598.48	797.91	997.39	1196.86	1396.84	1595.82	1795.30
28	29 80	197.672	895.84	593.02	790.69	988.36	1186.08	1383.70	1581.38	1779.05
29 30	80	195.806	891.61	587.42	788.28	979.08	1174.84	1370.64	1566.45	1762.26
81	82	198.881 191.897	887.76	581.64	775.52	969.40	1163.29	1357.17	1551.05	1744.93
32	83		883.79	575.69	767.59	959.48	1151.38	1343.28	1585.17	1727.07
82	34	189.854	879.71	569.56	759.41	949.27	1139.12	1328.98	1518.83	1708.68
84	85	187.758 185.594	875.51 871.19	563.26 556.78	750.01 742.38	938.76 927.97	1126.52 1113.57	1314.27 1299.16	1502.02 1484.75	1689.77 1670.35
35	86	183.379	366.76	550.14	738.52	916.89	1100.27	1283.65	1467.03	1650.41
36	37	181.107	362.21	543.82	724.43	905.53	1086.64	1267.75	1448.86	1629.96
37	88	178.780	357.56	536.34	715.12	893.90	1072.68	1251.46	1430.24	1609.02
88	89	176.897	352.79	529.19	705.59	881.98	1058.38	1234.78	1411.18	1587.57
89	40	173.960	347.92	521.88	695.84	869.80	1043.76	1217.72	1391.68	1565.64
40	41	171.469	842.94	514.41	685.88	857.84	1028.81	1200.28	1371.75	1543.22
41	42	168.925	337.85	506.77	675.70	844.62	1013.55	1182.47	1351.40	1520.22
42	48	166.328	832.66	498.98	665.31	881.64	997.97	1164.30	1330.62	1496.95
48	44	163.680	827.36	491.04	654.72	818.40	982.08	1145.76	1309.44	1473.12
44	45	160.980	821.96	482.94	643.92	804.90	965.88	1126.86	1287.84	1448.82

TABLE L (Continued.) QUADRILATERAL SURFACES OF 1 DEGREE IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

Limi LATIT	iting UDES.			Multiples	of these Qu	adrilateral :	Surfaces fro	m 1 to 9.		
Inf.	Sup.	1.	2.	8.	4.	5.	6.	7.	8.	9.
45	46	158.231	316.46	474.69	632.92	791.15	949.39	1107.62	1265.85	1424.08
46	47	155.432	310.86	466.30	621.73	777.16	932.59	1088.02	1243.46	1898.89
47	48	152.584	305.17	457.75	610.84	762.92	915.51	1068.09	1220.67	1373.26
48	49	149.689	299.38	449.07	598.75	748.44	899.13	1047.82	1197.51	1347.20
49	50	146.746	298.49	440.24	586.98	733.73	880.48	1027.22	1173.97	1320.71
50	51	148.757	287.51	431.27	575.08	718.78	862.54	1006.30	1150.06	1293.81
51	52	140.723	281.45	422.17	562.89	703.61	844.84	985.06	1125.78	1266.51
52	53	137.644	275.29	412.93	550.58	688.22	825.86	963.51	1101.15	1288.80
53	54	184.522	269.04	403.57	538.09	6 72.61	807.13	941.65	1076.17	1210.70
54	55	131-857	262.71	894.07	525.43	656.78	788.14	919.50	1050.86	1182.21
55	56	128.150	256.30	384.45	512.60	640.75	768.90	897.05	1025.20	1153.85
56	57	124.903	249.81	374.71	499.61	624.51	749.42	874.32	999.22	1124.18
57	58	121.616	243.28	864.85	486.46	608.08	729.69	851.31	972.92	1094.54
58	59	118.289	286.58	354.87	473.16	591.45	709.74	828.03	946.32	1064.61
59	60	114.926	229.85	344.78	459.70	574.63	689.55	804.48	919.41	1084.38
60	61	111.525	223.05	334.58	446.10	557.68	669.15	780.68	892.20	1003.73
61	62	108.089	216.18	824.27	432.85	540.44	648.53	756.62	864.71	972.80
62	63	104.618	209.24	813.85	418.47	523.09	627.71	732.32	836.94	941.56
63	64	101.118	202.23	808.34	404.45	505.56	606.68	707.79	808.90	910.02
64	65	97.575	195.15	292.73	890.80	487.88	585.45	683.03	780.60	878.18
65	66	94.007	188.01	282.02	876.08	470.03	564.04	658.05	752.05	846.06
66	67	90.408	180.82	271.22	361.63	452.04	542.45	632.85	723.26	813.67
67	68	86.779	173.56	260.84	347.12	433.90	520.68	607.46	694.23	781.01
68	69	83.123	166.25	249.37	832.49	415.61	498.74	581.86	664.98	748.11
69	70	79.439	158.88	238.32	817.76	397.20	476.64	556.08	685.52	714.95
70	71	75.780	151.46	227.19	802.92	378.65	454.88	530.11	605.84	681.57
71	72	71.996	143.99	215.99	287.99	859.98	481.98	503.98	575.97	647.97
72	73	68.239	136.48	204.72	272.96	341.20	409.44	477.68	545.91	614.15
78	74	64.460	128.92	193.38	257.84	322.30	386.76	451.22	515.68	580.14
74	75	60.659	121.82	184.98	242.64	303.30	863.96	424.62	485.28	545.94
75	76	56.839	113.68	170.52	227.36	284.20	841.04	397.88	454.72	511.55
76	77	58.001	106.00	159.00	212.00	265.00	318.00	871.00	424.00	477.01
77	78	49.145	98.29	147.48	196.58	245.72	294.87	344.01	398.16	442.80
78	79	45.272	90.54	135.82	181.09	226.36	271.63	316.91	862.18	407.45
79	80	41.386	82.77	124.16	165.54	206.93	248.81	289.70	331.08	872.47
80	81	37.485	74.97	112.46	149.94	187.43	224.91	262.40	299.88	337.87
81	82	83.572	67.14	100.72	134.29	167.86	201.43	235.01	268.58	302.15
82	83	29.649	59.30	88.95	118.59	148.24	177.89	207.54	237.19	266.84
83	84 85	25.715 21.773	51.43 43.55	77.15 65.32	102.86 87.09	128.58 108.87	154.29 130.64	180.01 152.41	205.72 174.19	231.44 195.96
85	86	17.824	35.65	58.47	71.30	89.12	106.95	124.77	142.59	160.42
86	87	18.869	27.74	41.61	55.48	69.85	83.22	97.09	110.96	124.82
87	88	9.910	19.82	29.78	89.64	49.55	59.46	69.37	79.28	89.19
88	89	5.947	11.89	17.84	23.79	29.74	35.68	41.63	79.28 47.58	53.53
89	90									17.84
89	90	1.983	8.97	5.95	7.93	9.91	11.90	13.88	15.86	17.51

TABLE II. QUADRILATERAL SURFACES OF 2 DEGREES IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

THE IERRESTRIAL ELLIPSOID.										
LATIT	Limiting Multiples of these Quadrilateral Surfaces from 1 to 9.									
Inf.	Sap.	1.	9.	8.	4.	5.	6.	7.	8.	9.
0	2	896.908	1798.81	2690.71	3587.61	4484.51	5881.42	6278.32	7175.22	8072.13
2	4	895.838	1791.68	2697.51	8588.85	4479.19	5375.08	6270.87	7166.71	8062.54
4	6	893.710	1787.42	2681.13	3574.84	4468.55	5362.26	6255.97	7149.68	8043.39
6	8	890.520	1781.04	2671.56	3562.0 8	4452.60	5343.12	6233.64	7124.16	8014.68
8	10	886.272	1772.54	2658.82	3545.09	4431.86	5317.68	6203.91	7090.18	7976.45
10	12	880.969	1761.94	2642.91	35 23. 88	4404.85	5285.82	6166.79	7047.76	7928.72
12	14	874.617	1749.28	2628.85	8498.47		5247.70	6122.32	6996.94	7871.55
14	16	867.221	1784.44		3468.88		5203.83		6937.77	
16	18	858.789	1717.58	2576.87	8436.16		5152.74	6011.52	6870.31	7729.10
18	20	849.828	1698.66	2547.98	3397.31	4246.64	5095.97	5945.30	6794.68	7643.95
20	22	888.848	1677.70	2516.54	8355.89	4194.24	5033.09	5871.94	6710.78	7549.63
22	24	827.859	1654.72	2482.08	8309.44	4136.80	4964.16	5791.51	6618.87	7446.23
24	26	814.872	1629.74	2444.62	3259.49	4074.86	4889.23	5704.11	6518.98	7333.85
26	28	811.400	1602.80	2404.20	3205.60	4007.00	4808.40	5609.80	6411.20	7212.60
28	80	786.956	1578.91	2860.87	8147.88	8934.78	4721.74	5508.69	6295.65	7082.61
30	82	771.555	1548.11	2314.67	8086.22		4629.33		6172.44	1
82	84	755.213	1510.48	2265.64	8020.85		4531.28	5286.49		6796.92
84	36	787.946	1475.89	2213.84	2951.78		4427.68	5165.62	5903.57	6641.51
86	88 .	719.778	1489.55	2159.82	2879.09		4818.64	5038.41	5758.19	6477.96
38	40	700.713	1401.43	2102.14	2802.85	8508.57	4204.28	4904.99	5605.71	6306.42
40	42	680.787	1861.57	2042.86	2723.15	3403.93	4084.72	4765.51	5446.29	6127.08
42	44	660.016	1320.03	1980.05	2640.06	3300.0 8	3960.09	4620.11	5280.13	5940.14
44	46	638.423	1276.85	1915.27	2553.69	3192.11	8830.54	4468.96	5107.38	5745-81
46	48	616.032	1232.06	1848.10	2464.13	3080.16	3696.19	4312.23	4928.26	5544.29
48	50	592.869	1185.74	1778.61	2871.48	2964.34	8557.21	4150.08	4742.95	5335.82
50	.52	568.960	1137.92	1706.88	2275.84	2844.80	3418.76	8982.72	4551.68	5120.64
52	54	544.832	1088.66	1632.99	2177.83	2721.66	8265.99	3810.32	4354.65	4898.99
54	56	519.014	1038.03	1557.04	2076.06	2595.07	3114.09	8633.10	4152:11	4671.13
56	58	493.037	986.07	1479.11	1972.15	2465.18	2958.22	8451.26	3944.29	4487.33
58	60	466.480	932.86	1899.29	1865.72	2332.15	2798.58	8265.01	3731.44	4197.87
60	62	439.228	878-46	1317.68	1756.91	2196.14	2685.87	3074.59	3513.82	3953.06
62	64	411.461	822.92	1284.38	1645.84	2057.30	2468.76	2880.28	8291.69	3703.15
64	66	883.164	766.33	1149.49	1532.66	1915.82	2298.99	2682.15	3065.32	3448.48
66	68	354.374	708.75	1063.12	1417.50		2126.24	2480.62	2834.99	3189.30
68	70	325.124	650.25	975.87	1800.50	1625.62	1950.75	2275.87	2601.00	2926.12
70	72	295.458	590.91	886.86	1181.81		1772.72	2068.17	2363.63	2659.09
72	74	265.398	530.80	796.20	1061.59	1326.99	1592.39	1857.79	2123.19	2388.59
74	76	284.998	469.99	704.99	939.99	1174.99	1409.99	1644.98	1879.98	2114.96
76	78	204.290	408.58	612.87	817.16		1225.74	1430.03	1634.32	1838.6
78	80	178.316	346.63	519.95	693.26	866.58	1039.90	1213.21	1886.53	1559.8
80	82	142.115	284.23	426.84	568.46	710.57	852.69	994.80	1136.92	1279.03
82	84	110.728	221.46	832.18	442.91	558.64	664.37	775.09	885.82	996.5
84	86	79.195	168.39	237.59	816.78	395.98	475.17	554.37	633.56	712.76
86	88	47.559	95.12	142.68	190.24	237.79	285.35	832.91	380.47	428.03
88	90	15.860	31.72	47.58	63.44	79.30	95.16	111.02	126.88	142.7

ABLE III. QUADRILATERAL SURFACES OF 5 DEGREES IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

Limiting ATITUDES.		Multiples of these Quadrilateral Surfaces from 1 to 9.											
Inf.	Sup.	1.	2.	8.	.4.	5.	6.	7.	8.	9.			
0		5599.821	11199.64	16799.46	22399-29	27999.11	33598.93	39198.75	44798.57	50398.39			
5	10	5558.288	11116.58	16674.87	22233.15	27791.44	83849.73	88908.02	44466.31	50024.60			
10	15	5475.466	10950.93	16426.40	21901.87	27877.38	32852.80	38328.27	43803.73	49279.20			
15	20	5351.846	10703.69	16055.54	21407.39	26759.28	82111.08	87462.93	42814.77	48166.62			
20	25	5188.165	10376.33	15564.49	20752-66	25940-82	31128.99	36317.15	41505.32	46693.48			
25	80	4985.425	9970.85	14956.27	19941.70	24927.12	29912.55	84897-97	39883.40	44868.82			
30	35	4744.891	9485.78	14234.67	18979.57	23724.46	28469.35	33214.24	87959.13	42704.02			
85	40	4468.110	8936.22	13404.83	17872.44	22340.55	26808.66	31276.77	85744.88	40212.99			
40	45	4156.909	8313.82	12470.73	16627.64	20784.54	24941.45	29098-36	33255.27	37412.18			
45	50	8813.408	7626-82	11440.22	15253.63	19067.04	22880.45	26693-86	30507.26	34320.67			
50	55	3440.01 3	6880.03	10320.04	13760.05	17200.06	20640.08	24080.09	27520.10	30960.12			
55	60	3039.419	6078.84	9118.26	12157.68	15197.09	18236.51	21275.93	24315.35	27354.77			
60	65	2614.598	5229.20	7843.80	10458.39	13072-99	15687.59	18302.19	20916.79	23531.39			
65	70	2168.779	4337.56	6506.34	8675.12	10848-89	13012.67	15181.45	17350.23	19519-01			
70	75	1705.427	3410.85	5116.28	6821.71	8527-13	10232.56	11937.99	13643.42	15348-84			
75	80	1228.213	2456.43	3684.64	4912.85	6141.07	7869.28	8597.49	9825.71	11053.92			
80	85	740.973	1481.95	2222.92	2963.89	8704-86	4445-84	5186-81	5927.78	6668-76			
85	90	247.668	495.34	743.00	990.67	1238-34	1486-01	1783.68	1981.34	2229.01			

TABLE IV. QUADRILATERAL SURFACES OF 10 DEGREES IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

Limiting LATITUDES.			Multiples of these Quadrilateral Surfaces from 1 to 9.												
Inf.	Sup.	1.	2.	8.	4.	5.	6.	7.	8.	9.					
0	10	22316.220	44632.44	66948.66	89264.88	111581.10	133897.32	156213.54	178529.76	200845.98					
10	20	21654.626	43309.25	64963.88	86618.50	108273.13	129927.76	151582.88	178237.01	194891.68					
20	80	20347.180	40694.36	61041.54	81388.72	101785.90	122083.08	142430.26	162777.44	183124.62					
30	40	18426.004	36852.01	55278.01	78704.02	92180.02	110556-02	128982.03	147408.03	165884.04					
40	50	15940.634	31881.27	47821.90	63762.54	79703.17	95648-80	111584.44	127525.07	143465.71					
50	60	12958.864	25917.73	38876.59	51835.46	64794.32	77758-18	90712.05	103670.91	116629.78					
60	70	9566.755	19133.51	28 7 00. 2 6	38267.02	47833.77	57400-58	66967.28	76534-04	86100.79					
70	80	5867-281	11784-56	17601.84	23469-12	29336.40	35203-69	41070.97	46938.25	52805.58					
80	90	1977.282	3954-56	5931-85	7909.18	9886.41	11863-69	13940-97	15818-26	17795.54					

TABLE V. MEAN QUADRILATERAL SURFACES OF 1, 10, 20, AND 30 MINUTES IN LATITUDA AND IN LONGITUDE DEDUCED FROM BACK QUADRILATERAL OF 1 DEGREE IN TABLE I.

Limiting LATITUDES.		Mean Surfaces measuring in Latitude and in Longitude.					iting TUDES.	Mean Surfaces measuring in Latitude and in Longitude.			
Inf.	Sup.	1'.	10′.	204.	80'.	Inf.	Sup.	1/.	10'.	20'.	30'.
0	1	0.0623	6.229	24.918	56.065	45	46	0.0440	4.395	17.581	39.558
1	2	0.0623	6.228	24.910	56.048	46	47	0.0432	4.318	17.270	38.858
2	3	0.0622	6.224	24.895	56.015	47	48	0.0424	4.238	16.954	38.146
8	4	0.0622	6.218	24.878	55.965	48	49	0.0416	4.158	16.632	37.422
4	5	0.0621	6.211	24.844	55.898	49	50	0.0408	4.076	16.305	36.686
5	6	0.0620	6.202	24.807	55.815	50	51	0.0399	8.993	15.973	35.939
6	7	0.0619	6.191	24.763	55.716	51	52	0.0391	3.909	15.636	85.181
7	8	0.0618	6.178	24.711	55.599	52	53	0.0382	3.823	15.294	34.411
8	9	6.0616	6.163	24.652	55.467	53	54	0.0374	3.737	14.947	33.630
9	10	0.0615	6.146	24.586	55.317	54	55	0.0365	3.649	14.595	32.839
10	11	0.0613	6.128	24.512	55.152	55	56	0.0356	3.560	14.239	82.038
11	12	0.0611	6.108	24.431	54.970	56	57	0.0347	8.470	13.878	31.226
12	13	0.0609	6.086	24.348	54.771	57	58	0.0338	3.378	13.513	30.404
13	14	0.0606	6.062	24.247	54.556	58	59	0.0329	3.286	13.143	29.572
14	15	0.0604	6.036	24.144	54.325	59	60	0.0319	8.192	12.770	28.731
15	16	0.0601	6.009	24.035	54.078	60	61	0.0310	8.098	12.392	27.881
16	17	0.0398	5.979	23.917	53.814	61	62	0.0300	3.002	12.010	27.022
17	18	0.0595	5.948	23.793	53.534	62	63	0.0291	2.906	11.624	26.154
18	19	0.0592	5.915	23.662	53.239	63	64	0.0281	2.809	11.235	25.278
19	20	0.0588	5.881	23.523	52.927	64	65	0.0271	2.710	10.842	24.394
20	21	0.0584	5.844	23.378	52.600	65	66	0.0261	2.611	10.445	23.502
21	22	0.0581	5.806	23.225	52.256	66	67	0.0251	2.511	10.045	22.602
22	23	0.0577	5.766	23.065	51.897	67	68	0.0241	2.411	9.642	21.695
23	24	0.0572	5.725	22.899	51.523	68	69	0.0231	2.309	9.236	20.781
24	25	0.0568	5.681	22.725	51.132	69	70	0.0221	2.207	8.827	19.860
25	26	0.0564	5.636	22.545	50.727	70	71	0.0210	2.104	8.414	18.933
26	27	0.0559	5.590	22.358	50.306	71	72	0.0200	2.000	8.000	17.999
27	28	0.0554	5.541	22.164	49.869	72	73	0.0190	1.896	7.582	17.060
28	29	0.0549	5.491	21.964	49.418	73	74	0.0179	1.791	7.162	16.115
29	30	0.0544	5.439	21.756	48.952	74	75	0.0168	1.685	6.740	15.165
80	31	0.0539	5.386	21.542	48.470	75	76	0.0158	1.579	6.315	14.210
31	32	0.0538	5.330	21.322	47.974	76	77	0.0147	1.472	5.889	13.250
32	33	0.0527	5.274	21.095	47.463	77	78	0.0137	1.365	5.461	12.286
88	84	0.0522	5.215	20.861	46.938	78	79	0.0126	1.258	5.030	11.318
84	85	0.0516	5.155	20.622	46.399	79	80	0.0115	1.150	4.598	10.346
35	36	0.0509	5.094	20.375	45.845	80	81	0.0104	1.041	4.165	9.371
36	87	0.0508	5.031	20.123	45.277	81	82	0.0098	0.933	8.730	8.393
37	88	0.0497	4.966	19.864	44.695	82	83	0.0082	0.824	3.294	7.412
38	39	0.0490	4.900	19.600	44.099	83	84	0.0071	0.714	2.857	6.429
89	40	0.0488	4.832	19.329	43.490	84	85	0.0060	0.605	2.419	5.443
40	41	0.0476	4.763	19.052	42.867	85	86	0.0049	0.495	1.980	4.456
41	42	0.0469	4.692	18.769	42.231	86	87	0.0039	0.385	1.541	3.467
42	43	0.0462	4.620	18.481	41.582	87	88	0.0028	0.275	1.101	2.477
43	44	0.0455	4.547	18.187	40.920	88	89	0.0017	0.165	0.661	1.497
44	45	0.0447	4.472	17.887	40.245	89	90	0.0006	0.055	0.220	0.496

ERRATA IN THE FIRST EDITION.

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A, page 7, line below the title, instead of (32 + \frac{4}{3}x^0) read (32 + \frac{4}{3}x^0).
         21, on the line beginning with 30, in the last four columns,
                instead of
                              100.75
                                         100.97
                              100 85
                read
                                         101.07
                                                     101.30
                                                                101.52.
В,
          7, on the line beginning with 23°, second column, instead of 20.410, read 20.888.
В.
         23, on the line beginning with 12°, third column, instead of 5.87, read 5.37.
         30 - 32, at the head of each first column, Temperature of the Air, add "in Centigrade degrees."
В,
         40. Table II., first part, on the line beginning with 60, column headed 7, instead of 24.11.01.
B.
                read 24.9,01.
B,
             Table II., first part, on the line beginning with 70, column headed 5, instead of 27.4,47,
                read 27.8,47; and column headed 8, instead of 28.11,77, read 28.9,77.
             Table II., second part, on the line beginning with 70, column headed 5, instead of 328.47,
В,
                read 332.47.
В,
         41, Table III., line beginning with 20, the five last columns,
                              63.54
                                        66.08
                                                  68.62
                                                                      73.70,
                instead of
                                                            71.16
               read
                              63.50
                                        66.04
                                                  68.58
                                                            71.12
                                                                      73.66.
B,
          " Table III, line beginning with 200, column headed 3, instead of 515.11, read 515.61.
         42, Table V., line beginning with 180, column headed 7, instead of 516.21, read 506.21.
В,
B,
         43, Table VI., first part, on line beginning with 70, column headed 2, instead of 76.635, read
                76.735.
             Table VI., second part, on line beginning with 7, the last eight columns,
B,
                instead of 0.6483
                                      0.6572
                                               0 6661
                                                         0.6750
                                                                   0.6839
                                                                                      0.7016
                                                                                                0.7105.
                                                         0 6661
                            0.6395
                                      0.6483
                                               0.6572
                                                                   0.6750
                                                                             0.6839
                                                                                       0.6927
                                                                                                0.7016.
B,
         43, Table VI., second part, on line beginning with 12, column headed 5, instead of 1.1018,
C,
         11, on line beginning with 26.5 inches, column headed 6, instead of 674.41, read 674.61.
C,
          " on line of 27.1 inches, column headed 1, instead of 688.38, read 688.58.
C,
         12, on line of 30.5 inches, column headed 2, instead of 778.20, read 775.19.
C,
         39 and 41, at the head of table, instead of "Tenths of Degrees," read "English Inches."
     "
D,
         28, 29, and 30, head of page, instead of "Tenths of a Degree," read "Hundredths of a Degree."
         35, note at the bottom, instead of "Geology," read "Geodesy."
D.
         36, on line beginning with 160, columns headed 8 and 9, instead of 550.19 and 553.47,
D,
                                                                      read
                                                                                 551.19 and 554.47.
D,
         36, on line beginning with 260, columns headed 2, 3, 5, and 6,
                  instead of
                                  860.59
                                               863.87
                                                             879.43
                                                                           882.72,
                  read
                                  859.60
                                               862.88
                                                             869.44
                                                                           872.72.
     "
D,
         37, on line beginning with 620, column headed 4, instead of 2048.28, read 2047.28.
     "
          "
                        "
D,
                                                 "
                                                                       2526.39,
                                                                                     2526.29.
                                     770,
                                                          0,
     "
                        "
                               "
D,
         38,
                 "
                                                 "
                                                                   "
                                                                       2903.69,
                                                                                  "
                                                                                     2903.60.
                                     880.
                                                          5,
D,
     "
          "
                 "
                        "
                                     890,
                                                 "
                                                                       2939.79,
                                                                                     2939.69.
                                                          6,
     "
          "
                               "
                                                 "
D,
                                     930,
                                                          5.
                                                                       3069.64,
                                                                                     3067.64.
     "
D,
          "
                 "
                        æ
                               "
                                                 "
                                                                       3261.71.
                                     990.
                                                                                     3261.21.
                                                          4,
     "
                                                 "
D,
                                     990,
                                                          5,
                                                                       3264.59,
                                                                                     3264.49.
         39, on line beginning with 1380, columns headed 3, 4, 5, 6, 7, 8,
D,
               instead of 4537.28
                                       4540.56
                                                                            4550.41
                                                                                        4553.69,
                                                   4543.85
                                                                4547.13
                          4537.48
                                       4540.76
                                                   4544.05
                                                               4547.33
                                                                            4550 61
D,
```

40, on line beginning with 1610, column headed 5, instead of 5292.65, read 5298.65.
 44, Table X., on line beginning with 3, column headed 6, instead of 21.0205, read 23.0205.

45, Table XII., on line beginning with column 0, column headed 5, instead of 0.83333, read

D,

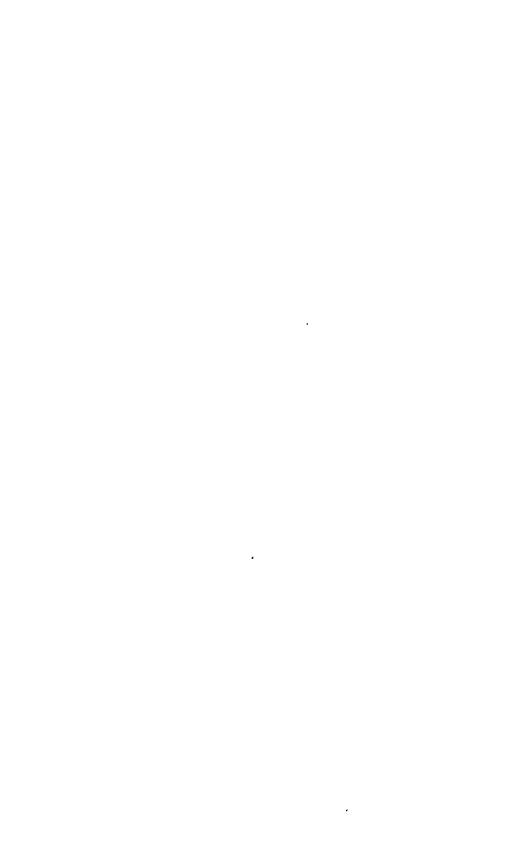
0.08333.

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